INTERNATIONAL STANDARD

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Building construction machinery and equipment — Concrete mixers —

Part 2:

Procedure for examination of mixing efficiency

Machines et matériels pour la construction des bâtiments — Malaxeurs de béton —

Partie 2: Mode opératoire pour la détermination de l'efficacité de malaxage



Reference number ISO 18650-2:2006(E)

ISO 18650-2:2006(E)

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Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

International Standards are drafted in accordance with the rules given in the ISO/IEC Directives, Part 2.

The main task of technical committees is to prepare International Standards. Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75 % of the member bodies casting a vote.

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights.

ISO 18650-2 was prepared by Technical Committee ISO/TC 195, Building construction machinery and equipment, Subcommittee SC 1, Machinery and equipment for concrete work.

ISO 18650 consists of the following parts, under the general title *Building construction machinery and equipment* — *Concrete mixers*:

- Part 1: Vocabulary and general specifications
- Part 2: Procedure for examination of mixing efficiency

Introduction

This part of ISO 18650 deals with the testing of the mixing capabilities of concrete mixers, characterized as the recommended mixing time.

The test consists of the determination of the variance of the mortar, coarse aggregate and air content, and the consistency of concrete mix samples, drawn after an assumed mixing time.

Compressive strength is also tested.

The measure of a concrete mixer's efficiency is the value of the variance of the above parameters, after the assumed mixing time.

This part of ISO 18650 provides for the preparation of concrete mix, sampling, execution of particular tests, criteria of test result evaluation and the test report.

Building construction machinery and equipment — Concrete mixers —

Part 2:

Procedure for examination of mixing efficiency

1 Scope

This part of ISO 18650 specifies the procedure and requirements for examination of the mixing efficiency of batch-type and continuous-type concrete mixers as defined in ISO 18650-1. It is applicable to concrete mixers having a rated capacity greater than or equal to 70/50.

2 Normative references

The following referenced documents are indispensable for the application of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 1920-3, Testing of concrete — Part 3: Making and curing test specimens

ISO 2736-1, Concrete tests — Test specimens — Part 1: Sampling of fresh concrete

ISO 2736-2, Concrete tests — Test specimens — Part 2: Making and curing of test specimens for strength tests

ISO 3310-1, Test sieves — Technical requirements and testing — Part 1: Test sieves of metal wire cloth

ISO 4012, Concrete — Determination of compressive strength of test specimens

ISO 4109, Fresh concrete — Determination of the consistency — Slump test

ISO 4848, Concrete — Determination of air content of freshly mixed concrete — Pressure method

ISO 6783, Coarse aggregates for concrete — Determination of particle density and water absorption — Hydrostatic balance method

ISO 7033, Fine and coarse aggregates for concrete — Determination of the particle mass-per-volume and water absorption — Pycnometer method

ISO 11375, Building construction machinery and equipment — Terms and definitions

ISO 18650-1, Building construction machinery and equipment — Concrete mixers — Part 1: Vocabulary and general specifications

Terms and definitions

For the purposes of this document, the terms and definitions given in ISO 18650-1 and ISO 11375 apply.

Requirements for mixer verified

The design and execution of the whole structure of the mixer and its components, such as the mixing chamber (drum, pan, or trough), rotor with blades or paddle agitator(s), their directions of rotation, charging and discharging devices (if any), should be verified according to the manufacturer's instructions.

It shall be determined that the number of revolutions per minute of a drum or mixing tools conforms to the manufacturer's specification.

The drive system should be able to restart 5 min after being stopped when the mixer has completed the mixing of the test batch as specified in 5.2.1.

The mixer shall be discharged according to its design or as specified by the manufacturer. The closure of the mixing chamber shall be so designed that the loss of the mix before discharge, i.e. during charging and mixing, remains below 0,5 %.

Mixing performance test 5

General 5.1

The mixing efficiency is determined by the uniformity of the concrete mix and the compressive strength of the concrete cubes or cylinders, sampled after mixing time. The determination of the uniformity of the concrete mix includes the following variance tests on the sampled specimens:

- air content; a)
- content of mortar per unit volume;
- content of coarse aggregate per unit volume; C)
- d) consistency (slump).

The values of the concrete-mix component content (air, mortar, coarse aggregate), determined as the test results, as well as the consistency and compressive strength, are subsequently used for calculation of their variances.

For calculating the variance, ΔX , of the considered components' content and other features, expressed as a percentage, the following formula is applied:

$$\Delta X = \frac{X_1 - X_2}{X_1 + X_2} \times 100$$

where

- is the value of component content, slump and compressive strength received from portion 1 or 2 larger value of X_1 and X_2 ;
- X_2 is the value of component content, slump and compressive strength received from portion 1 or 2 smaller value of X_1 and X_2 .

To explain the physical sense of this formula, it can be transformed as follows:

$$\Delta X = \frac{X_1 - X_2}{X_1 + X_2} = \frac{X_1 + \frac{X_2}{2} - X_2}{X_1 + \frac{X_2}{2}}$$

In this form it represents the variance of a subject parameter in two portions against its average value.

For evaluation of the test results, the particular variance values are compared with the acceptable results according to Clause 6.

5.2 Concrete mix preparation

The test concrete to be used for the mixing performance test should be specified by the concrete manufacturer or testing laboratory with the following conditions: coarse aggregates up to 20 mm, slump (80 ± 30) mm, air content $(4,5\pm1,5)$ % and nominal compressive strength 25 ± 5 N/mm². In case of difficulty in obtaining of the assumed air content, an appropriate admixture may be used.

The quantity of materials usually corresponds to the rating capacity declared by the mixer's manufacturer.

The constituent materials shall be weighed within measuring accuracy limits of \pm 3 %.

The sequence of a mixer charging with particular components should be as specified in the manufacturer's instruction. If there is no such instruction, the method of charging should be noted in the test report.

The charging of a mixer with constituent materials shall be carried out with a minimum loss of materials.

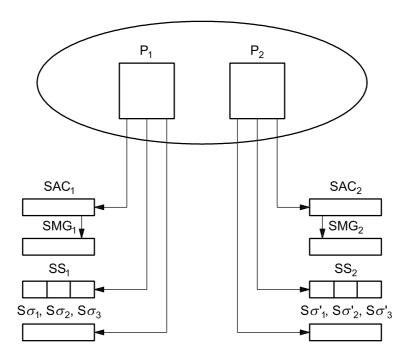
The mixing time shall be as specified by the manufacturer. If no such specification is available, the following approximate values — depending on the mixer type and its capacity — are recommended:

- a) For batch-type gravity mixers:
- rated capacity 1,0 m³ and less, 60 s;
- rated capacity above 1,0 m³, 5 s added to 60 s for every 0,5 m³ increase.
- b) For batch-type compulsory mixers:
- rated capacity 3,0 m³ and less, 30 s;
- rated capacity above 3,0 m³, 15 s added to 30 s for every 1,5 m³ increase.
- c) For continuous mixers: a mixing time corresponding to the duration of the concrete mix in the mixing chamber, which shall be at least 10 s.

5.3 Sampling

5.3.1 General

Two portions of the concrete mix are sampled directly from the mixing chamber immediately after assured mixing time (see Figures 2, 3, 4 and 5). Where the direct sampling from inside the mixing chamber is difficult, the sampling may be done from the concrete mix discharged to the hopper (see Figures 6 and 7). The volume of the sample (portion) should be a minimum of 20 I for batch mixers and 100 I for continuous mixers (see 5.3.4). Afterwards, the specimens for particular variance tests are prepared.



Key

 P_1, P_2 concrete mix portion sampled from the mixer

 SAC_1 , SAC_2 specimens for air content test

 SMG_1 , SMG_2 specimens for air content test used for coarse aggregate and mortar content testing in further

sequence

 $S\sigma_{1}$, $S\sigma_{2}$, $S\sigma_{3}$, specimens for compressive strength test (three cubes or cylinders from each portion)

 $S\sigma'_{1,}S\sigma'_{2,}S\sigma'_{3,}$ SS_1 , SS_2

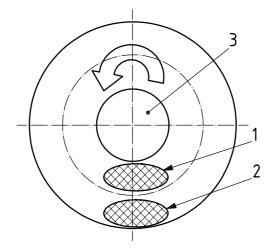
specimens for consistency (slump) test

Figure 1 — General scheme of sampling

Batch-type compulsory mixers

5.3.2.1 Pan-type mixers

In pan-type mixers the samples (portions) are taken from concentric circles. Figure 2 shows an example of sampling in a turbo mixer.



Key

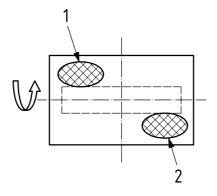
- 1 centre portion
- 2 edge portion
- 3 centre cylinder covering dead mixing area

Figure 2 — Sampling in turbo mixer

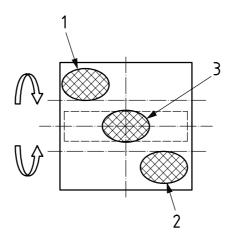
In other types of pan-type mixers, those not having a centre cylinder covering the dead mixing area, the radius separating two concentric circles is equal to a quarter of the inner pan diameter.

5.3.2.2 Paddle mixers

Examples of sampling in paddles mixers with one or two paddle agitators are shown in the Figure 3.



a) One-agitator mixer



b) Two-agitator mixer

Key

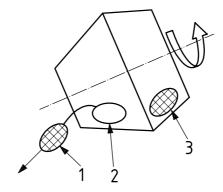
- front portion
- 2 rear portion
- centre portion

Figure 3 — Sampling in paddle-type mixer

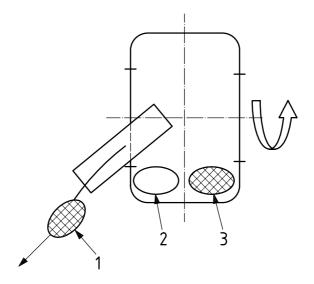
5.3.3 **Gravity mixers**

The concrete mix portions are taken to the receiving containers from the beginning and end of the concrete discharge stream, as shown in Figure 4.

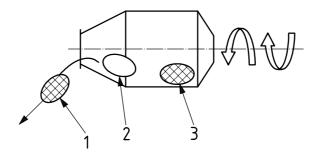
A batch during discharging is divided for convenience into three parts (beginning, middle and end), from which the corresponding portions are taken.



a) Tipping drum mixer



b) Discharging chute drum mixer



c) Reversing drum mixer

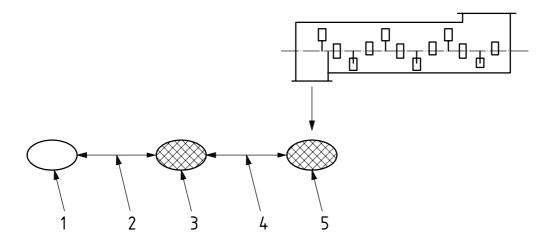
Key

- 1 beginning portion
- 2 middle portion
- 3 end portion

Figure 4 — Sampling in gravity mixers

5.3.4 Continuous mixers

The first-sampled portion should be from a stable flow, just at the moment when the discharged concrete reaches output capacity, with another sample being taken 4 min after the first. The volume of each portion should be at least 100 l.



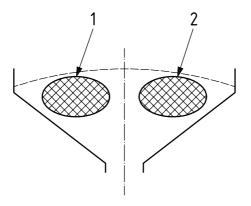
Key

- missed, initial quantity concrete mix until stable delivery achieved
- break minimum 0,5 min 2
- first portion 3
- break minimum 4 min
- second portion

Figure 5 — Sampling in continuous mixer

Sampling from concrete mix hopper

If there is no method of sampling directly from a mixing chamber, the portions may be taken from the concrete mix hopper. The scheme of sampling is shown in Figure 6.



Key

- left portion
- right portion

Figure 6 — Sampling from concrete mix hopper

5.4 Variance tests

5.4.1 Variance of air, mortar and coarse aggregate content in concrete mix

5.4.1.1 Test procedure

Perform the following procedure (see Figures 1 and 7).

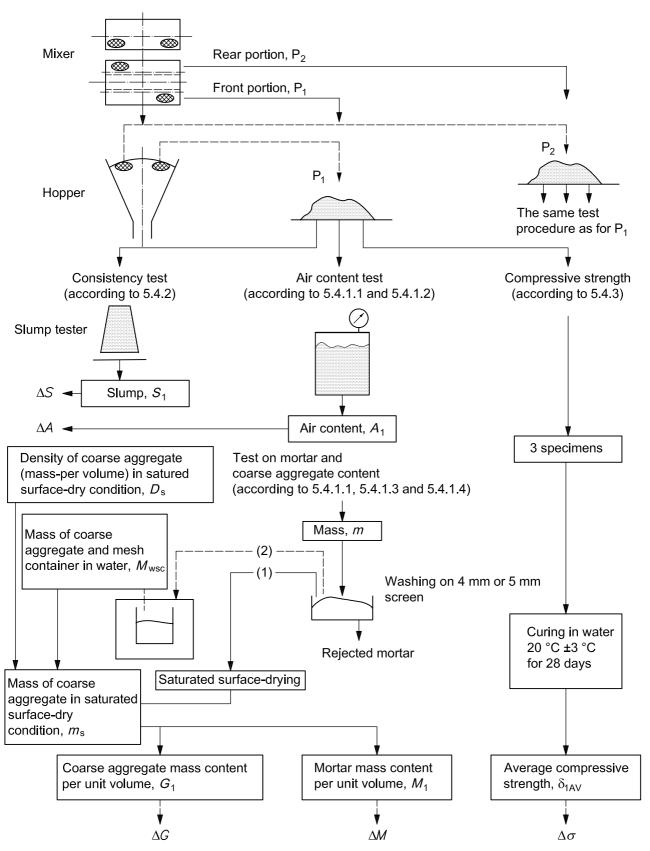
- a) Take one concrete mix specimen from each portion.
- b) Determine the air content, A_1 and A_2 , of the specimens, using the pressure method in accordance with ISO 4848 (see 5.4.1.2).

With the same test specimens — following the air content determination — determine the mortar and coarse aggregate content as follows.

- c) Measure the masses, m, of the specimens.
- d) Remove all particles in the specimens by washing on either a 4 mm or 5 mm screen in accordance with ISO 3310-1.
- e) Determine the mass of coarse aggregate.

Calculate the aggregate masses as follows:

- the mass of coarse aggregate remaining on the screen in the saturated surface-dry condition (m_s) ;
- the density of coarse aggregate in the saturated surface-dry condition (D_s), in accordance with the test methods for particle mass-per-volume and water absorption given in ISO 6783 and ISO 7033;
- the virtual mass of coarse aggregate remaining on the screen in water (m_w) .



NOTE There are two alternative methods of coarse aggregate volume measurement:

- saturated surface-dry method (m_S) , (1) in the figure, or
- calculation from mass of coarse aggregates in water (m_W) , (2) in the figure.

Figure 7 — Example of testing procedure for two-agitator paddle mixer and hopper use

5.4.1.2 Calculation of air content variance

For the air content test of the concrete mix, take two test specimens according to 5.3.1 and test according to ISO 4848; their variance, ΔA , from the average value, is calculated as a percentage using the formula:

$$\Delta A = \frac{A_1 - A_2}{A_1 + A_2} \times 100$$

where

 A_1 is the air content value of specimen SAC₁ (see Figure 1);

 A_2 is the air content value of specimen SAC₂ (see Figure 1).

In the case where $A_2 > A_1$, the absolute value of ΔA should be taken.

5.4.1.3 Calculation of mortar content variance

The mass of mortar per unit volume without air, M, per unit volume of concrete mix, is calculated in kilograms per cubic metre (kg/m³) using the formula:

$$M = \frac{m - m_s}{V - \left(V_A + \frac{m_s}{D_s}\right)} \times 1000$$

where

m is the mass of the concrete mix, in kilograms (kg) [see 5.4.1.1, c)];

 m_s is the mass of coarse aggregate remaining on the 4 mm or 5 mm mesh screen in saturated surfacedry condition (kg) [see 5.4.1.1, c)];

V is the volume of the container, in litres (I), used in the air content test according to ISO 4848 [see 5.4.1.1, b)];

*V*_A is the volume of air in litres (I) calculated from the volume (*V*) of the container, multiplied by the air content ratio (%) divided by 100;

 D_s is the density of coarse aggregate (particle mass-per-volume) in saturated surface-dry condition, in kilograms per litre (kg/l).

The mass of coarse aggregate, m_s , remaining on the 4 mm or 5 mm mesh screen after the virtual mass of coarse aggregate in the water has been measured is calculated using

$$m_{\rm S} = m_{\rm W} \times \frac{D_{\rm S}}{D_{\rm S} - 1}$$

where

 $m_{\rm w}$ is the mass of coarse aggregate in the water (kg);

 $D_{\rm S}$ is the density of the coarse aggregate (particle mass-per-volume) in saturated surface-dry condition (kg/l).



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The unit mass variance, ΔM , of mortar in concrete mix is then calculated, as a percentage, using

$$\Delta M = \frac{M_1 - M_2}{M_1 + M_2} \times 100$$

where

 M_1 is the mortar content of specimen SMG₁ (see Figure 1);

 M_2 is the mortar content of specimen SMG₂ (see Figure 1).

In the case where $M_2 > M_1$, the absolute value of ΔM should be taken.

5.4.1.4 Calculation of coarse aggregate mass variance

Coarse aggregate mass, G, in saturated surface-dry condition per unit volume is calculated in kilograms per cubic metre (kg/m³) using the formula:

$$G = \frac{m_{\rm S}}{V} \times 1000$$

where m_s and V are as given in 5.4.1.3.

Coarse aggregate mass variance, ΔG , in the concrete mix, expressed as a percentage, is then calculated using

$$\Delta G = \frac{G_1 - G_2}{G_1 + G_2} \times 100$$

where

 G_1 is the coarse aggregate content of specimen SMG₁ (see Figure 1);

 G_2 is the coarse aggregate content of specimen SMG₂ (see Figure 1).

In the case where $G_2 > G_1$, the absolute value of ΔG should be taken.

5.4.2 Consistency test

Verify the consistency of two specimens taken according to 5.3.1 by the slump test, using the method specified in ISO 4109; their variance, ΔS , from the average value is then calculated as a percentage using the formula:

$$\Delta S = \frac{S_1 - S_2}{S_1 + S_2} \times 100$$

where

 S_1 is the slump value of specimen SS_1 (see Figure 1);

 S_2 is the slump value of specimen SS_2 (see Figure 1).

In the case where $S_2 > S_1$, the absolute value of ΔS should be taken.

5.4.3 Compressive strength test

For the compressive strength test, take three specimens from each portion (see Figures 1 and 7) and prepare in accordance with ISO 1920-3 and ISO 2736-1. Perform the test in accordance with ISO 4012. The curing method of these specimens shall be in accordance with ISO 2736-2, with a curing period of 28 days.

The average compressive strengths, σ_{1AV} and σ_{2AV} , for particular portions are then calculated for portion 1 and portion 2, respectively using the formulae:

$$\sigma_{1AV} = \frac{\sigma_1 + \sigma_2 + \sigma_3}{3}$$

$$\sigma_{2AV} = \frac{\sigma_1' + \sigma_2' + \sigma_3'}{3}$$

where

 σ_1 , σ_2 , σ_3 is the compressive strength of specimens $S\sigma_1$, $S\sigma_2$, $S\sigma_3$, taken from portion 1;

 σ'_1 , σ'_2 , σ'_3 is the compressive strength of specimens $S\sigma'_1$, $S\sigma'_2$, $S\sigma'_3$ taken from portion 2.

Compressive strength variance $\Delta \sigma$ is calculated using

$$\Delta \sigma = \frac{\sigma_{1AV} - \sigma_{2AV}}{\sigma_{1AV} + \sigma_{2AV}} \times 100$$

In the case where $\sigma_{2AV} > \sigma_{1AV}$, the absolute value of $\Delta \sigma$ should be taken.

6 Evaluation of test results

With the aim of mixing time acceptance, the variance of the concrete mix component content proportions, the consistency and the compressive strength of the concrete cubes or cylinders shall be in accordance with Table 1.

Table 1 — Uniformity requirement

No.	Type of test	Acceptable variance value %			
1	Air content variance $\Delta 4$ in concrete mix (see 5.4.1.2)	≤ 10			
2	Mortar (≤ 5 mm) content variance ΔM in concrete mix (see 5.4.1.3)	≤ 0,8			
3	Coarse aggregate ($>$ 5 mm) content variance ΔG in concrete mix (see 5.4.1.4)	≤ 5			
4	Consistency (slump) variance ΔS (see 5.4.2)	≤ 15			
5	Compressive strength variance $\Delta\sigma$ (see 5.4.3)	≤ 7,5			

7 Test report

After the tests are concluded, a test report should be prepared. The format of the report should be according to Tables 2, 3 and 4. Tables 2 and 3 present data on the tested concrete mixer and the concrete mix preparation, while Table 4 presents the numerical values of the particular tests.

Table 2 — Batch type concrete mixer — Data on mixer and concrete mix preparation

Requested by:								
Type of mixer:								
Product plate information:								
Manufacturer:								
Dry components/ready concrete capacities (dm³)	Type Serial number		Year of manufacture	Power source output (kW)				
Remarks for mixing conditions (see 5.2)								
Mixing procedure								
Mixing conditions Test concrete								
The state of the s	Sample mix	cture 1	Sample mixture 2					
Mixed volume — ready concrete (dm³)								
Filling ratio(Mixed volume								
by nominal capacity) (%)								
Drum, number of revolution (min ⁻¹)								
Shaft, number of revolution (min ⁻¹)								
Charging time t_1 (s)								
Mixing time t_2 (s)								
Discharging time $t_3(s)$								
Resetting time $t_4(s)$								
Cycle time $t_8 = t_1 + t_2 + t_3 + t_4$ (s)								
Remarks								
Test place:	Test date:		Test report:					
Name and address of test facility:								
Test report date:								
Tested by (signature):								

Table 3 — Continuous concrete mixer — Data on mixer and concrete mix preparation

Requested by:							
Type of mixer:							
Product plate information:							
Manufacturer:							
Output capacity m ³ /h	Туре	Serial number	Year of manufa	cture	Power source output (kW)		
Remarks for mixing condit	tions		1				
Mixing procedure							
Mixing conditions		Test concrete					
		Sample mixture 1		Sample mixture 2			
Mixing capacity – ready concrete (m³/h)							
Sampling time (s)							
Drum, number of revolution (min ⁻¹)							
Shaft, number of revolutio	on (min ⁻¹)						
Inclination of the axis of th	ne mixing chamber (°)						
Remarks							
Test place:		Test date:		Test report:			
Name and address of test	t facility:			<u> </u>			
Test report date:							
Tested by (signature)							

Test date											
Mixer type											S
Rating capacity r				³ Mixing volume/ready concrete							m ³
Test concre	te				T	T	_				
Nominal strength	Slump Aggregate max. size		Air conten	t Water/ Cement ratio	Fine aggregate ratio		Content (kg/m ³)				
(N/mm ²)	(cm) (mm) (%)		(%)	(%)	W	С	S	G	Ad		
Test procedure								Sam	ple 1	Sam	ple2
1	Test spec	imen			S		(cm)		-		
2	·		air content		A		(%)				
3	-		ecimen with its	container	$M_{ m SC}$		(kg)				
4	Mass of s	aid c	ontainer		$M_{\rm c}$		(kg)				
5	Mass of tl	he sp	ecimen		$m = M_{sc} - M_{c}$		(kg)				
6	Container	r volu	me		V		(I)				
7	Air volum	е			$V_{A} = A \times V / 100$)	(I)				
8	Specimer	ı volu	ıme without air o	content	$V_{ss} = V - V_{A}$		(I)				
9	Mass of comesh con		e aggregate with r in water	n 4 or 5 mm	$M_{ m wsc}$		(kg)				
10	Mass of n	nesh	container in wa	ter	$M_{ m WC}$ (kg)						
11	Mass of c	oarse	e aggregate in v	vater	$m_{\rm W} = M_{\rm WSC} - M_{\rm WC}$ (kg)						
12			rse aggregates ırface-dry condi	tion	D_{s}		(kg/l)				
13	Mass of c surface-d		e aggregate in s	aturated	$m_s = m_w \times D_s /$	(D _s -1)	(kg)				
14	Absolute volume of a specimen sieved by 4 or 5 mm mesh $V_{as} = m_w / (D_s - 1) = m_s / D_s$						(I)				
15	Content of	of moi	rtar mass of the	specimen	$M_{\rm m} = m - m_{\rm s} \tag{kg}$						
16	Mortar vo	lume	of the specime	า	$V_{m} = V_{ss} - V_{as} \tag{I}$						
17	Mortar ma	ass c	ontent per unit v	olume	$M = 1000 \times M_{\rm m} / V_{\rm m} $ (kg/l)						
18	Coarse aggregates mass content per unit volume				$G = 1\ 000 \times m_{\rm s}/V_{\rm m}$ (kg/l)						
19	Capacity in concret		variance of mo	rtar	ΔΜ (%)						
20	Coarse aggregates variance in concrete mix				ΔG		(%)				
21	Slump variance from average				ΔS (%)						
22	Air conter	nt var	iance from aver	age	ΔA (%)					ı	
23	Compressive strength of specimens:			$\sigma_{1}, \sigma_{2}, \sigma_{3}$ $\sigma_{1}, \sigma_{2}, \sigma_{3}$	•	nm²) nm²)					
24	Average compressive strength			$\sigma_{1AV}, \sigma_{2AV}$							
25	Variance	from	average strengt	th	$\Delta\sigma_{n}$					1	
Test locatio	n:			Test date:							
Test report:			Name and address of test facility:								
Tested by (signature):				Test report of	date:						

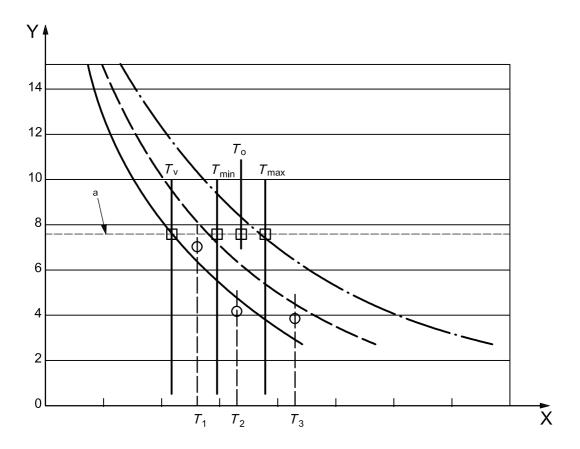
8 Final remarks

8.1 Filling ratio of tested mixer

The quantity of components used for the test usually corresponds to the rated capacity of the mixer for batchtype mixers and the rating output for continuous mixers declared by the manufacturer. The procedure presented in this part of ISO 18650 makes it possible also to examine the mixing efficiency for smaller filling mixers' ratios and rating outputs.

8.2 Optimization of mixing time

For the manufacturers and users of the mixers, of most importance is to obtain the shortest (optimum) mixing time providing required concrete quality and maximum output from the equipment. To obtain this, it is necessary to execute the same test for different mixing times chosen on the results of the variance of resistance to compression ($\Delta\sigma$) obtained in the previous tests. The results of tests are marked on a graph as a function of the mixing time and the curve drawn by interpolation. An example of optimum mixing time determination based on compressive strength testing is presented in Figure 8.



Key

X mixing time (s)

Y variance of resistance to compression, $\Delta \sigma$ (%)

 T_1 test time 1 for finding optimum mixing time and data point (O)

 T_2 test time 2 for finding optimum mixing time and data point (O)

 T_3 test time 3 for finding optimum mixing time and data point (O)

Regression curves:

where s is the standard deviation of $\Delta\sigma$

 $T_{\rm v}$ time at virtual intersection (\Box) between regression curve ($\Delta \sigma$ + 1s) and limiting quality line: value of variation over acceptable value, with 68,26 % probability at this time and thus unacceptable

 T_{\min} minimum allowable mixing time at data point (\square) corresponding to intersection between regression curve ($\Delta\sigma$ + 2s) and limiting quality line: value of variation acceptable with 95,44 % probability

 T_{max} maximum mixing time and data point (\square) corresponding to intersection betweem regression curve ($\Delta\sigma$ + 3s) and limiting quality line: value of variation adequate with 99,74 % probability

^a Acceptable limit, $\Delta \sigma$ = 7,5 %.

NOTE The optimum mixing time, $T_{\rm o}$ (\square) is such that $T_{\rm min} \leqslant T_{\rm o} < T_{\rm max}$.

Figure 8 — Determination of the optimum mixing time

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