

***MANUAL ON THE USE OF***  
**THERMOCOUPLES IN**  
**TEMPERATURE MEASUREMENT**

 **STP 470B**  
**AMERICAN SOCIETY FOR  
TESTING AND MATERIALS**

# MANUAL ON THE USE OF THERMOCOUPLES IN TEMPERATURE MEASUREMENT

Sponsored by ASTM  
Committee E-20 on  
Temperature Measurement  
and Subcommittee E20.04 on  
Thermocouples  
AMERICAN SOCIETY FOR  
TESTING AND MATERIALS

ASTM SPECIAL TECHNICAL PUBLICATION 470B

ASTM Publication Code Number (PCN)  
04-470020-40



1916 Race Street, Philadelphia, Pa. 19103

**Copyright © by AMERICAN SOCIETY FOR TESTING AND MATERIALS 1981**  
**Library of Congress Catalog Card Number: 80-69066**  
**ISBN 0-8031-0502-9**

**NOTE**

**The Society is not responsible, as a body,  
for the statements and opinions  
advanced in this publication.**

Printed in Baltimore, Md.  
July 1981

Second Printing, Baltimore, Md. (b)  
July 1982

Third Printing, Baltimore, Md. (b)  
February 1983

Fourth Printing, Baltimore, Md.  
April 1987

Fifth Printing, Baltimore, Md.  
January 1990

# Foreword

The Manual on the Use of Thermocouples in Temperature Measurement was sponsored and compiled by Committee E-20 on Temperature Measurement and Subcommittee E20.04 on Thermocouples of the American Society for Testing and Materials. The editorial work was co-ordinated by R. P. Benedict, Westinghouse Electric Corp. Helen Hoersch was the ASTM editor.

## **Related ASTM Publications**

**Evolution of the International Practical Temperature Scale of 1968, STP 565  
(1974), 04-565000-40**

# Contents

|  |    |
|--|----|
| Chapter 1—Introduction                                 | 1  |
| Chapter 2—Principles of Thermoelectric Thermometry     | 3  |
| 2.1 Historical Development of Basic Relations          | 3  |
| 2.1.1 Seebeck  | 3  |
| 2.1.2 Peltier  | 4  |
| 2.1.3 Thomson  | 5  |
| 2.1.4 Interim Summary                                  | 6  |
| 2.1.5 Kelvin Relations                                 | 7  |
| 2.1.6 Onsager Relations                                | 8  |
| 2.2 Laws of Thermoelectric Circuits                    | 13 |
| 2.2.1 Law of Homogeneous Metal                         | 13 |
| 2.2.2 Law of Intermediate Metals                       | 14 |
| 2.2.3 Law of Successive or Intermediate<br>Temperature | 14 |
| 2.3 Elementary Thermoelectric Circuits                 | 14 |
| 2.4 Bibliography                                       | 17 |
| 2.4.1 Early Historical References                      | 17 |
| 2.4.2 Recent References                                | 18 |
| 2.5 Nomenclature                                       | 19 |
| Chapter 3—Thermocouple Materials                       | 20 |
| 3.1 Common Thermocouple Types                          | 20 |
| 3.1.1 General Application Data                         | 20 |
| 3.1.2 Properties of Thermoelement Materials            | 25 |
| 3.2 Extension Wires                                    | 27 |
| 3.2.1 General Information                              | 27 |
| 3.2.2 Sources of Error                                 | 30 |
| 3.3 Nonstandardized Thermocouple Types                 | 35 |
| 3.3.1 Platinum Types                                   | 39 |
| 3.3.2 Iridium-Rhodium Types                            | 43 |
| 3.3.3 PlatineI Types                                   | 46 |
| 3.3.4 Nickel-Chromium Types                            | 49 |
| 3.3.5 Nickel-Molybdenum Types                          | 54 |
| 3.3.6 Tungsten-Rhenium Types                           | 54 |
| 3.4 Compatibility Problems at High Temperature         | 58 |
| 3.5 References   | 61 |

|            |  |     |
|------------|--|-----|
| Chapter 4— | Typical Thermocouple Designs and Applications        | 62  |
|            | 4.1 Sensing Element Assemblies                       | 63  |
|            | 4.2 Nonceramic Insulation                            | 63  |
|            | 4.3 Hard-Fired Ceramic Insulators                    | 66  |
|            | 4.4 Protecting Tubes, Thermowells, and Ceramic Tubes | 66  |
|            | 4.5 Circuit Connections                              | 73  |
|            | 4.6 Complete Assemblies                              | 80  |
|            | 4.7 Selection Guide for Protecting Tubes             | 80  |
|            | 4.8 Bibliography                                     | 80  |
| <br>       |  |     |
| Chapter 5— | Sheathed, Ceramic-Insulated Thermocouples            | 81  |
|            | 5.1 General Considerations                           | 81  |
|            | 5.2 Construction                                     | 81  |
|            | 5.3 Insulation                                       | 82  |
|            | 5.4 Wire   | 85  |
|            | 5.5 Sheath   | 85  |
|            | 5.6 Combinations of Sheath, Insulation, and Wire     | 85  |
|            | 5.7 Characteristics of the Basic Material            | 85  |
|            | 5.8 Testing  | 89  |
|            | 5.9 Measuring Junction                               | 89  |
|            | 5.10 Terminations                                    | 94  |
|            | 5.11 Installation of the Finished Thermocouple       | 94  |
|            | 5.12 Sheathed Thermocouple Applications              | 94  |
|            | 5.13 References                                      | 95  |
| <br>       |  |     |
| Chapter 6— | Emf Measurements                                     | 97  |
|            | 6.1 General Considerations                           | 97  |
|            | 6.2 Deflection Millivoltmeters                       | 97  |
|            | 6.3 Digital Voltmeters                               | 98  |
|            | 6.4 Potentiometers                                   | 98  |
|            | 6.4.1 Potentiometer Theory                           | 98  |
|            | 6.4.2 Potentiometer Circuits                         | 99  |
|            | 6.4.3 Types of Potentiometer Instruments             | 100 |
|            | 6.5 Voltage References                               | 101 |
|            | 6.6 Reference Junction Compensation                  | 102 |
| <br>       |  |     |
| Chapter 7— | Reference Junctions                                  | 103 |
|            | 7.1 General Considerations                           | 103 |
|            | 7.2 Reference Junction Techniques                    | 103 |
|            | 7.2.1 Fixed Reference Temperature                    | 104 |
|            | 7.2.2 Electrical Compensation                        | 107 |
|            | 7.2.3 Mechanical Reference Compensation              | 108 |

|           |                                      |     |
|-----------|--------------------------------------|-----|
| 7.3       | Sources of Error                     | 109 |
| 7.3.1     | Immersion Error                      | 109 |
| 7.3.2     | Galvanic Error                       | 109 |
| 7.3.3     | Wire Matching Error                  | 109 |
| 7.4       | References                           | 110 |
| Chapter 8 | — Calibration of Thermocouples       | 112 |
| 8.1       | General Considerations               | 112 |
| 8.1.1     | Temperature Scale                    | 112 |
| 8.1.2     | Reference Thermometers               | 116 |
| 8.1.3     | Annealing                            | 117 |
| 8.1.4     | Measurement of Emf                   | 118 |
| 8.1.5     | Homogeneity                          | 119 |
| 8.1.6     | General Calibration Methods          | 120 |
| 8.1.7     | Calibration Uncertainties            | 121 |
| 8.2       | Calibration Using Fixed Points       | 124 |
| 8.2.1     | Freezing Points                      | 125 |
| 8.2.2     | Melting Points                       | 125 |
| 8.3       | Calibration Using Comparison Methods | 126 |
| 8.3.1     | Laboratory Furnaces                  | 126 |
| 8.3.2     | Stirred Liquid Baths                 | 129 |
| 8.3.3     | Fixed Installations                  | 130 |
| 8.4       | Interpolation Methods                | 131 |
| 8.5       | Single Thermoelement Materials       | 136 |
| 8.5.1     | Test Specimen                        | 137 |
| 8.5.2     | Reference Thermoelement              | 137 |
| 8.5.3     | Reference Junction                   | 138 |
| 8.5.4     | Measuring Junction                   | 138 |
| 8.5.5     | Test Temperature Medium              | 139 |
| 8.5.6     | Emf Indication                       | 139 |
| 8.5.7     | Procedure                            | 139 |
| 8.6       | References                           | 140 |
| 8.7       | Bibliography                         | 142 |
| Chapter 9 | — Installation Effects               | 143 |
| 9.1       | Temperature Measurement in Fluids    | 143 |
| 9.1.1     | Response                             | 143 |
| 9.1.2     | Recovery                             | 145 |
| 9.1.3     | Thermowells                          | 146 |
| 9.1.4     | Thermal Analysis of an Installation  | 147 |
| 9.2       | Surface Temperature Measurement      | 148 |
| 9.2.1     | General Remarks                      | 148 |
| 9.2.2     | Installation Methods                 | 149 |
| 9.2.3     | Sources of Error                     | 153 |



|   |         |
|---|---------|
| 9.2.4 Error Determination                               | 154     |
| 9.2.5 Procedures for Minimizing Errors                  | 156     |
| 9.2.6 Commercial Surface Thermocouples                  | 156     |
| 9.3 References  | 158     |
| <br>Chapter 10— Reference Tables for Thermocouples      | <br>162 |
| 10.1 Thermocouple Types and Limits of Error             | 162     |
| 10.1.1 Thermocouple Types                               | 162     |
| 10.1.2 Limits of Error                                  | 163     |
| 10.2 Thermocouple Reference Tables                      | 163     |
| 10.3 Generation of Smooth Temperature-Emf Relationships | 163     |
| 10.3.1 Need for Smooth Temperature-Emf Relationship     | 163     |
| 10.3.2 Methods of Generation                            | 220     |
| 10.4 References   | 221     |
| <br>Chapter 11— Cryogenics                              | <br>222 |
| 11.1 General Remarks                                    | 222     |
| 11.2 Materials  | 222     |
| 11.3 Reference Tables                                   | 223     |
| 11.4 References   | 236     |
| <br>Chapter 12— Temperature Measurement Uncertainty     | <br>237 |
| 12.1 The General Problem                                | 237     |
| 12.2 Tools of the Trade                                 | 238     |
| 12.2.1 Average and Mean                                 | 238     |
| 12.2.2 Normal or Gaussian Distribution                  | 238     |
| 12.2.3 Standard Deviation and Variance                  | 239     |
| 12.2.4 Bias, Precision, and Uncertainty                 | 239     |
| 12.2.5 Precision of the Mean                            | 240     |
| 12.2.6 Regression Line or Least-Square Line             | 240     |
| 12.3 Typical Applications                               | 240     |
| 12.3.1 General Consideration                            | 240     |
| 12.3.2 Wire Calibration                                 | 241     |
| 12.3.3 Means and Profiles                               | 242     |
| 12.3.4 Probability Paper                                | 244     |
| 12.3.5 Regression Analysis                              | 245     |
| 12.4 References   | 247     |
| <br>Chapter 13— Terminology                             | <br>248 |
| <br>Index   | <br>251 |

# Acknowledgments

## **Editors for this Edition of the Manual**

R. P. Benedict (chairman), Westinghouse Electric Corp.  
E. L. Lewis (secretary), Consultant  
J. A. Bard, Johnson Matthey, Inc.  
P. Bliss, Pratt and Whitney Aircraft  
G. W. Burns, National Bureau of Standards  
G. J. Champagne, The Foxboro Co.  
R. S. Flemons, Canadian General Electric Co., Ltd.  
H. L. Kurtz, Driver-Harris Co.  
R. M. Park, Marlin Mfg. Corp.  
L. J. Pickering, Claud S. Gordon Co.  
F. S. Sibley, Hoskins Manufacturing Co.

## **Officers of Committee E-20**

E. D. Zysk (chairman), Engelhard Minerals and Chemical Corp.  
R. P. Benedict (1st vice chairman), Westinghouse Electric Corp.  
N. R. Corallo (2nd vice chairman), Becton Dickinson  
R. L. Shepard (recording secretary), Oak Ridge National Lab.  
A. E. Gealt (membership secretary), Honeywell, Inc.

## **Officers of Subcommittee E-20.04**

G. J. Champagne (chairman), The Foxboro Corp.  
F. S. Sibley (secretary), Hoskins Mfg. Co.

## **Those Primarily Responsible for Individual Sections of this Edition**

Principles—R. P. Benedict, Westinghouse Electric Corp.  
Common Thermocouples—G. J. Champagne, The Foxboro Co.  
Extension Wires—F. S. Sibley, Hoskins Manufacturing Co.  
Nonstandard Thermocouples—J. A. Bard, Johnson Matthey, Inc.  
Typical Thermocouples Designs—L. J. Pickering, Claud S. Gordon Co.  
Sheathed Thermocouples—P. Bliss, Pratt and Whitney Aircraft  
EMF Measurements—A. S. Tenney, Leeds and Northrup Co.  
Reference Junctions—R. S. Flemons, Canadian General Electric Co., Ltd.  
Calibration—G. W. Burns, National Bureau of Standards  
Single Element Calibration—H. L. Kurtz, Driver-Harris Co.

**Installations—R. P. Benedict, Westinghouse Electric Corp.**  
**Cryogenics—G. W. Burns, National Bureau of Standards**  
**Uncertainty—P. Bliss, Pratt and Whitney Aircraft**  
**Terminology—E. L. Lewis, Consultant**  
**Index—R. M. Park, Marlin Mfg. Corp.**

In addition to those listed, many other members of Committee E-20 have made substantial contributions to this manual as authors and reviewers. Their help is gratefully acknowledged.

# List of Figures

|   |    |
|---|----|
| FIG. 2.1— $E$ unaffected by third material $C$  | 15 |
| FIG. 2.2—Emfs are additive for materials  | 15 |
| FIG. 2.3—Emfs are additive for temperature intervals  | 16 |
| FIG. 2.4—Several methods for introducing copper extension wires in elementary thermocouple circuits | 16 |
| FIG. 2.5—Basic thermocouple circuit   | 17 |
| FIG. 2.6—Typical industrial thermocouple circuits   | 17 |
| FIG. 3.1—Recommended upper temperature limits—Types K, E, J, T thermocouples                        | 22 |
| FIG. 3.2—Thermal emf of thermoelements relative to platinum   | 34 |
| FIG. 3.3—Error due to $\Delta T$ between thermocouple-extension wire junctions                      | 38 |
| FIG. 3.4—Thermal emf of platinum-rhodium versus platinum-rhodium thermocouples                      | 40 |
| FIG. 3.5—Thermal emf of platinum-iridium versus palladium thermocouples                             | 42 |
| FIG. 3.6—Thermal emf of platinum-molybdenum versus platinum-molybdenum thermocouples                | 44 |
| FIG. 3.7—Thermal emf of iridium-rhodium versus iridium thermocouples                                | 46 |
| FIG. 3.8—Thermal emf of platinel thermocouples  | 48 |
| FIG. 3.9—Thermal emf of nickel-chromium alloy thermocouples   | 50 |
| FIG. 3.10—Thermal emf of nickel versus nickel-molybdenum thermocouples                              | 55 |

|  |     |
|--|-----|
| FIG. 3.11—Thermal emf of tungsten-rhenium versus tungsten-rhenium thermocouples          | 58  |
| FIG. 4.1—Typical thermocouple element assemblies   | 64  |
| FIG. 4.2—Cross-section examples of oval and circular hard-fired ceramic insulators       | 69  |
| FIG. 4.3—Examples of drilled thermowells   | 72  |
| FIG. 4.4—Typical examples of thermocouple assemblies with protecting tubes               | 74  |
| FIG. 4.5—Typical examples of thermocouple assemblies using quick disconnect connectors   | 74  |
| FIG. 5.1—Compacted ceramic insulated thermocouple showing its three parts                | 82  |
| FIG. 5.2—Nominal thermocouple sheath outside diameter versus internal dimensions         | 83  |
| FIG. 5.3—Exposed or bare wire junction   | 93  |
| FIG. 5.4—Grounded junction   | 93  |
| FIG. 5.5—Ungrounded or isolated junction   | 93  |
| FIG. 5.6—Reduced diameter junction   | 93  |
| FIG. 5.7—Termination with flexible connecting wires                                      | 94  |
| FIG. 5.8—Quick disconnect and screw terminals  | 94  |
| FIG. 5.9—Fittings to adapt into process line [up to $3.48 \times 10^4$ kPa (5000 psi)]   | 95  |
| FIG. 5.10—Braze for high pressure operation [up to $6.89 \times 10^5$ kPa (100 000 psi)] | 95  |
| FIG. 5.11—Thermocouple in thermowell   | 95  |
| FIG. 6.1—A simple potentiometer circuit  | 100 |

|   |     |
|---|-----|
| FIG. 7.1—Recommended ice bath for reference junction  | 105 |
| FIG. 8.1—Temperature emf plot of raw calibration data for an iron/<br>constantan thermocouple   | 132 |
| FIG. 8.2—Difference plot of raw calibration data for an iron/con-<br>stantan thermocouple   | 133 |
| FIG. 8.3—Typical determination of uncertainty envelope (from data<br>of Fig. 8.2)   | 134 |
| FIG. 8.4—Various possible empirical representations of the thermo-<br>couple characteristic (based on a single calibration run)                 | 135 |
| FIG. 8.5—Uncertainty envelope method for determining degree of<br>least squares interpolating equation for a single calibration<br>run (linear) | 136 |
| FIG. 8.6—Uncertainty envelope method for determining degree of<br>least squares interpolating equation for a single calibration<br>run (cubic)  | 137 |
| FIG. 8.7—Circuit diagram for thermal emf test   | 138 |
| FIG. 9.1—Graphical presentation of ramp and step changes  | 144 |
| FIG. 9.2—Common attachment methods  | 150 |
| FIG. 9.3—“Single wire” thermocouple   | 151 |
| FIG. 9.4—Types of junction using metal sheathed thermocouples   | 152 |
| FIG. 9.5—Thermocouple probe with auxiliary heater, diagramatic<br>arrangement   | 153 |
| FIG. 9.6—Three wire Type K thermocouple to compensate for<br>voltage drop induced by surface current (other materials may<br>be used)           | 154 |
| FIG. 9.7—Commercially available types of surface thermocouples  | 157 |
| FIG. 9.8—Commercial probe thermocouple junctions  | 158 |

|  |     |
|--|-----|
| FIG. 11.1—Seebeck coefficients for Types E, T, and EP versus Au-0.07Fe | 236 |
| FIG. 12.1—Bias of typical Type K wire                                  | 241 |
| FIG. 12.2—Typical probability plot                                     | 245 |
| FIG. 12.3—Typical probability plot—truncated data                      | 246 |

# List of Tables

|   |    |
|---|----|
| TABLE 2.1—Determination of various thermoelectric quantities applied to thermocouples                               | 9  |
| TABLE 3.1—Recommended upper temperature limits for protected thermocouples  | 21 |
| TABLE 3.2—Nominal Seebeck coefficients (thermoelectric power)   | 23 |
| TABLE 3.3—Nominal chemical composition of thermoelements  | 26 |
| TABLE 3.4—Environmental limitations of thermoelements   | 26 |
| TABLE 3.5—Recommended upper temperature limits for protected thermoelements   | 28 |
| TABLE 3.6—Seebeck coefficient (thermoelectric power) of thermoelements with respect to Platinum 67 (typical values) | 29 |
| TABLE 3.7—Typical physical properties of thermoelement materials  | 30 |
| TABLE 3.8—Thermoelements—resistance change with increasing temperature  | 32 |
| TABLE 3.9—Nominal resistance of thermoelements  | 33 |
| TABLE 3.10—Extension wires for thermocouples  | 36 |
| TABLE 3.11—Platinum-rhodium versus platinum-rhodium thermocouples   | 41 |
| TABLE 3.12—Platinum-iridium versus palladium thermocouple   | 43 |
| TABLE 3.13—Platinum-molybdenum versus platinum-molybdenum thermocouple  | 45 |
| TABLE 3.14—Iridium-rhodium versus iridium thermocouples   | 47 |
| TABLE 3.15—Platinel thermocouples   | 49 |



|   |     |
|---|-----|
| TABLE 3.16—Nickel-chromium alloy thermocouples  | 51  |
| TABLE 3.17—Physical data and recommended applications of the<br>20 Alloy/19 Alloy thermocouple  | 56  |
| TABLE 3.18—Tungsten-rhenium thermocouples   | 59  |
| TABLE 3.19—Minimum melting temperatures of binary systems   | 60  |
| TABLE 4.1—Insulation characteristics  | 67  |
| TABLE 4.2—Color code of thermocouple and extension wire<br>insulations  | 68  |
| TABLE 4.3—Properties of refractory oxides   | 70  |
| TABLE 4.4—Selection guide for protecting tubes  | 75  |
| TABLE 5.1—Characteristics of insulating materials used in ceramic-<br>packed thermocouple stock   | 84  |
| TABLE 5.2—Thermal expansion coefficient of refractory insulating<br>materials and three common metals                                       | 84  |
| TABLE 5.3—Sheathed materials of ceramic-packed thermocouple<br>stock and some of their properties   | 86  |
| TABLE 5.4—Compatibility of wire and sheath material   | 87  |
| TABLE 5.5—Dimensions and wire sizes of typical ceramic-packed<br>material   | 88  |
| TABLE 5.6—Various characteristics tests, and the source of test-<br>ing procedure applicable to sheathed ceramic-insulated<br>thermocouples | 90  |
| TABLE 8.1—Defining fixed points of The International Practical<br>Temperature Scale of 1968   | 114 |
| TABLE 8.2—Secondary reference points  | 116 |
| TABLE 8.3—Calibration uncertainties using fixed point techniques  | 122 |

|   |     |
|---|-----|
| TABLE 8.4—Calibration uncertainties using comparison techniques<br>in laboratory furnaces (Types R or S standards)  | 123 |
| TABLE 8.5—Calibration uncertainties using comparison techniques<br>in stirred liquid baths                          | 123 |
| TABLE 8.6—Calibration uncertainties: tungsten-rhenium type<br>thermocouples   | 123 |
| TABLE 8.7—Calibration uncertainties using comparison techniques<br>in special furnaces (optical pyrometer standard) | 124 |
| TABLE 10.1—Limits of error for thermocouples  | 164 |
| TABLE 10.2—Type B thermocouples (deg F—millivolts)  | 165 |
| TABLE 10.3—Type B thermocouples (deg C—millivolts)  | 171 |
| TABLE 10.4—Type E thermocouples (deg F—millivolts)  | 174 |
| TABLE 10.5—Type E thermocouples (deg C—millivolts)  | 178 |
| TABLE 10.6—Type J thermocouples (deg F—millivolts)  | 180 |
| TABLE 10.7—Type J thermocouples (deg C—millivolts)  | 185 |
| TABLE 10.8—Type K thermocouples (deg F—millivolts)  | 188 |
| TABLE 10.9—Type K thermocouples (deg C—millivolts)  | 193 |
| TABLE 10.10—Type R thermocouples (deg F—millivolts)   | 196 |
| TABLE 10.11—Type R thermocouples (deg C—millivolts)   | 202 |
| TABLE 10.12—Type S thermocouples (deg F—millivolts)   | 205 |
| TABLE 10.13—Type S thermocouples (deg C—millivolts)   | 211 |
| TABLE 10.14—Type T thermocouples (deg F—millivolts)   | 214 |
| TABLE 10.15—Type T thermocouples (deg C—millivolts)   | 216 |
| TABLE 10.16—Power series coefficients for Type T thermocouples  | 217 |

|   |     |
|---|-----|
| TABLE 10.17—Power series coefficients for Type J thermocouples                              | 218 |
| TABLE 10.18—Power series coefficients for Type E thermocouples                              | 218 |
| TABLE 10.19—Power series coefficients for Type K thermocouples                              | 219 |
| TABLE 10.20—Power series coefficients for Type R thermocouples                              | 219 |
| TABLE 10.21—Power series coefficients for Type S thermocouples                              | 220 |
| TABLE 10.22—Power series coefficients for Type B thermocouples                              | 220 |
| TABLE 11.1—Type E-thermocouples (kelvins-microvolts)  | 223 |
| TABLE 11.2—Type T-thermocouples (kelvins-microvolts)  | 226 |
| TABLE 11.3—Type K-thermocouples (kelvins-microvolts)  | 230 |
| TABLE 11.4—Thermocouple, KP or EP versus gold-0.07 atomic percent iron (kelvins-microvolts) | 233 |
| TABLE 12.1—Accuracy of unsheathed thermocouples   | 242 |
| TABLE 12.2—Accuracy of sheathed thermocouples   | 243 |

# Chapter 1—Introduction

---

## First Edition, 1970

This manual was prepared by Subcommittee IV of ASTM Committee E-20 on Temperature Measurement. The responsibilities of ASTM Committee E-20 include “Assembling a consolidated source book covering all aspects relating to accuracy, application, and usefulness of thermometric methods.” This manual was addressed to the thermocouple portion of this responsibility.

The contents include principles, circuits, standard electromotive force (emf) tables, stability and compatibility data, installation techniques, and other information required to aid both the beginner and the experienced user of thermocouples. While the manual is intended to be comprehensive, the material, however, will not be adequate to solve all the individual problems associated with many applications. To further aid the user in such instances, there are numerous references and an extensive bibliography. In addition to presenting technical information, an attempt is made to properly *orient* a potential user of thermocouples. Thus, it is hoped that the reader of this manual will make fewer mistakes than the nonreader.

Regardless of how many facts are presented herein and regardless of the percentage retained, all will be for naught unless one simple important fact is kept firmly in mind. The thermocouple reports only what it “feels.” This may or may not be the temperature of interest. The thermocouple is influenced by its entire environment, and it will tend to attain thermal equilibrium with this environment, not merely part of it. Thus, the environment of each thermocouple installation should be considered unique until proven otherwise. Unless this is done, the designer will likely overlook some unusual, unexpected, influence.

Of all the available temperature transducers, why use a thermocouple in a particular application? There are numerous advantages to consider. Physically, the thermocouple is inherently simple, being only two wires joined together at the measuring end. The thermocouple can be made large or small depending on the life expectancy, drift, and response-time requirements. It may be flexible, rugged, and generally is easy to handle and install. A thermocouple normally covers a wide range of temperatures, and its output is reasonably linear over portions of that range. Unlike many temperature transducers, the thermocouple is not subject to selfheating problems. In

practice, thermocouples of the same type are interchangeable within specified limits of error. Also, thermocouple materials are readily available at reasonable cost, the expense in most cases being nominal.

The bulk of the manual is devoted to identifying material characteristics and discussing application techniques. Every section of the manual is essential to an understanding of thermocouple applications. Each section should be studied carefully. Information should not be used out of context. The general philosophy should be—let the user beware.

### **Second Edition, 1974**

In preparing this edition of the manual, the committee endeavored to include four major changes which greatly affect temperature measurement by means of thermocouples. In 1968, at the same time the First Edition was being prepared, the International Practical Temperature Scale was changed. This new scale (IPTS-68) is now the law of the land, and Chapter 8 has been completely rewritten to so reflect this. In 1972-1973, new Thermocouple Reference Tables were issued by the National Bureau of Standards. Accordingly, Chapter 10 has been revised to include the latest tables of temperature versus electromotive force for the thermocouple types most commonly used in industry. Also, along these same lines, the National Bureau of Standards has issued new methods for generating the new Reference Table values for computer applications. These power series relationships, giving emf as a function of a temperature, are now included in Chapter 10.3. Finally, there have been several important changes in thermocouple material compositions, and such changes have been noted in the appropriate places throughout the text. The committee has further attempted to correct any gross errors in the First Edition and has provided a more complete bibliography in Chapter 12.

### **Third Edition, 1980**

This edition of the manual has been prepared by ASTM E-20.10, the publications subcommittee. The main impetus for this edition was the need for a reprinting. Taking advantage of this opportunity, the editors have carefully reviewed each chapter as to additions and corrections called for by developments in the field of temperature measurement by thermocouples since 1974. Chapters 3, 4, 5, 6, 7, and 8 have been completely revised and strengthened by the appropriate experts. An important addition is Chapter 12 on Measurement Uncertainty. This reflects the trend toward a more statistical approach to all measurements. A selected bibliography is still included at the end of each chapter. A final innovation of this edition is the index to help the users of this manual.

# Chapter 2—Principles of Thermoelectric Thermometry

---

The principles, or theory, underlying thermoelectric effects were not established by one man at one time, but by several scientists working over a span of many years beginning with Alessandro Volta, who concluded in 1800 that the electricity which caused Galvani's frog to twitch was due to a contact of two dissimilar metals. This conclusion was the forerunner of the principle of the thermocouple. Others built on this base; for example, Thomas Johann Seebeck (1821), Jean Charles Althanase Peltier (1834), and William Thomson—later Lord Kelvin—(1848–1854). During this same period, Jean Baptiste Joseph Fourier published his basic heat-conduction equation (1821), Georg Simon Ohm discovered his celebrated equation for electrical conduction (1826), James Prescott Joule found the principle of the first law of thermodynamics and the important  $I^2R$  heating effect (1840–1848), and Rudolf Julius Emanuel Clausius announced the principle of the second law of thermodynamics and introduced the concept of entropy (1850).

## 2.1 Historical Development of Basic Relations

### 2.1.1 Seebeck

Seebeck discovered the existence of thermoelectric currents while observing electromagnetic effects associated with bismuth-copper and bismuth-antimony circuits. His experiments showed that, when the junctions of two dissimilar metals forming a closed circuit are exposed to different temperatures, a net thermal electromotive force is generated which induces a continuous electric current.

The Seebeck effect concerns the net conversion of thermal energy into electrical energy with the appearance of an electric current. The Seebeck voltage refers to the net thermal electromotive force set up in a thermocouple under zero-current conditions. The direction and magnitude of the Seebeck voltage,  $E_S$ , depend upon the temperature of the junctions and upon the materials making up the thermocouple. For a particular combination of materials,  $A$  and  $B$ , for a small temperature difference

$$dE_S = \alpha_{A,B}dT \quad (1)^1$$

<sup>1</sup>Nomenclature not defined in the text is given at the end of this chapter.

## 4 THE USE OF THERMOCOUPLES IN TEMPERATURE MEASUREMENT

where  $\alpha_{A,B}$  is a coefficient of proportionality called the Seebeck coefficient. (This commonly is called the thermoelectric power.) The Seebeck coefficient is obtained usually in one of two ways: (1) as an algebraic sum,  $\alpha_{A,B}$ , of relative Seebeck coefficients,  $\alpha_{AR}$  and  $\alpha_{BR}$ , where, for a given temperature difference and at given temperature levels, emf's of each of the substances,  $A$  and  $B$ , making up the thermocouple are obtained with respect to an arbitrary reference material,  $R$ ; and (2) by numerically differentiating tabulated values of  $E_S$  versus  $T$  for a given reference temperature,  $T_R$ , according to the relation

$$E_S = \int_{T_R}^T \alpha_{A,B} dT \quad (2)$$

In either case, the Seebeck coefficient represents, for a given material combination, the net change in thermal emf caused by a unit temperature difference; that is

$$\alpha_{A,B} = \lim_{\Delta T \rightarrow 0} \frac{\Delta E_S}{\Delta T} = \frac{dE_S}{dT} \quad (3)$$

Thus, if  $E = aT + 0.5bT^2$  is determined by calibration, then  $\alpha = a + bT$ . Note that, based on the validity of the experimental relation

$$E_S = \int_{T_2}^T \alpha dT = \int_{T_1}^T \alpha dT - \int_{T_1}^{T_2} \alpha dT \quad (4)$$

where  $T_1 < T_2 < T$ , it follows that  $\alpha$  is entirely independent of the reference temperature employed. In other words, for a given combination of materials, the Seebeck coefficient is a function of temperature level only.

### 2.1.2 Peltier

Peltier discovered peculiar thermal effects when he introduced small, external electric currents in Seebeck's bismuth-antimony thermocouple. His experiments show that, when a small electric current is passed across the junction of two dissimilar metals in one direction, the junction is cooled (that is, it acts as a heat sink) and thus absorbs heat from its surroundings. When the direction of the current is reversed, the junction is heated (that is, it acts as a heat source) and thus releases heat to its surroundings.

The Peltier effect concerns the reversible evolution, or absorption, of heat which usually takes place when an electric current crosses a junction between two dissimilar metals. (In certain combinations of metals, at certain temperatures, there are thermoelectric neutral points where no Peltier effect is apparent.) This Peltier effect takes place whether the current is introduced

externally or is induced by the thermocouple itself. The Peltier heat was found early to be proportional to the current, and may be written

$$dQ_p = \pi Idt \quad (5)$$

where  $\pi$  is a coefficient of proportionality known as the Peltier coefficient or the Peltier voltage. Note that  $\pi$  represents the reversible heat which is absorbed, or evolved, at the junction when unit current passes across the junction in unit time, and that it has the dimensions of voltage. The direction and magnitude of the Peltier voltage depend upon the temperature of the junction and upon the materials making up the junction; however,  $\pi$  at one junction is independent of the temperature of the other junction.

External heating, or cooling, of the junctions results in the converse of the Peltier effect. Even in the absence of all other thermoelectric effects, when the temperature of one junction (the reference junction) is held constant and when the temperature of the other junction is increased by external heating, a net electric current will be induced in one direction. If the temperature of the latter junction is reduced below the reference-junction temperature by external cooling, the direction of the electric current will be reversed. Thus, the Peltier effect is seen to be related closely to the Seebeck effect. Peltier himself observed that, for a given electric current, the rate of absorption, or liberation, of heat at a thermoelectric junction depends upon the Seebeck coefficient,  $\alpha$ , of the two materials.

### 2.1.3 Thomson

It remained for Thomson (see the Kelvin relations discussed next) to show that  $\alpha$  and  $\pi$  are related by the absolute temperature. (We might appropriately mention at this time that the Peltier thermal effects build up a potential difference opposing the thermoelectric current, thus negating the perpetual-motion question.) Thomson came to the remarkable conclusion that an electric current produces different thermal effects, depending upon the direction of its passage from hot to cold or from cold to hot, in the same metal. By applying the (then) new principles of thermodynamics to the thermocouple, and by disregarding (with tongue in cheek) the irreversible  $I^2R$  and conduction-heating processes, Thomson reasoned that, if an electric current produces only the reversible Peltier heating effects, then the net Peltier voltage will equal the Seebeck voltage and will be linearly proportional to the temperature difference at the junctions of the thermocouple.

This reasoning led to requirements at variance with observed characteristics (that is,  $dE_S/dT \neq \text{constant}$ ). Therefore, Thomson concluded that the net Peltier voltage is not the only source of emf in a thermocouple circuit, but that the single conductor itself, whenever it is exposed to a longitudinal temperature gradient, must be also a seat of emf. (Bequerel had at that time already discovered a thermoelectric neutral point,



that is,  $E_S = 0$ , for an iron-copper couple at about  $280^\circ\text{C}$ . Thomson agreed with Becquerel's conclusion and started his thermodynamic reasoning from there.)

The Thomson effect concerns the reversible evolution, or absorption, of heat occurring whenever an electric current traverses a single homogeneous conductor, across which a temperature gradient is maintained, regardless of external introduction of the current or its induction by the thermocouple itself. The Thomson heat absorbed, or generated, in a unit volume of a conductor is proportional to the temperature difference and to the current, that is

$$dQ_T = \left[ \int \sigma dT \right] Idt \quad (6)$$

where  $\sigma$  is a coefficient of proportionality called the Thomson coefficient. Thomson refers to this as the specific heat of electricity because of an apparent analogy between  $\sigma$  and the usual specific heat,  $c$ , of thermodynamics. Note that  $\sigma$  represents the rate at which heat is absorbed, or evolved, per unit temperature difference per unit current, whereas  $c$  represents the heat transfer per unit temperature difference per unit mass. The Thomson coefficient is seen also to represent an emf-per-unit difference in temperature. Thus, the total Thomson voltage set up in a single conductor may be expressed as

$$E_T = \int_{T_1}^{T_2} \sigma dT \quad (7)$$

where its direction and magnitude depend upon temperature level, temperature difference, and material considered. Note that the Thomson voltage alone cannot sustain a current in a single homogeneous conductor forming a closed circuit, since equal and opposite emf's will be set up in the two paths from heated to cooled parts.

Soon after his heuristic reasoning, Thomson succeeded in demonstrating indirectly the existence of the predicted Thomson emf's. He sent an external electric current through a closed circuit, formed of a single homogeneous conductor which was subjected to a temperature gradient, and found the  $I^2R$  heat to be augmented slightly, or diminished, by the reversible Thomson heat in the paths from cold to hot or from hot to cold, depending upon the direction of the current and the material under test.

#### 2.1.4 Interim Summary

In summary, thermoelectric currents may exist whenever the junctions of a circuit formed of at least two dissimilar metals are exposed to different temperatures. This temperature difference always is accompanied by irreversible Fourier heat conduction, while the passage of electric currents always is

accompanied by irreversible Joule heating effects. At the same time, the passage of electric currents always is accompanied by reversible Peltier heating or cooling effects at the junctions of the dissimilar metals, while the combined temperature difference and passage of electric current always is accompanied by reversible Thomson heating or cooling effects along the conductors. The two reversible heating-cooling effects are manifestations of four distinct emf's which make up the net Seebeck emf

$$E_S = \pi_{A,B}|_{T_2} - \pi_{A,B}|_{T_1} + \int_{T_1}^{T_2} \sigma_A dT - \int_{T_1}^{T_2} \sigma_B dT = \int_{T_1}^{T_2} \alpha_{A,B} dT \quad (8)$$

where the three coefficients,  $\alpha$ ,  $\pi$ ,  $\sigma$ , are related by the Kelvin relations.

### 2.1.5 Kelvin Relations

Assuming that the irreversible  $I^2R$  and heat-conduction effects can be disregarded completely (actually, they can be only minimized since, if thermal conductivity is decreased, electrical resistivity usually is increased, and vice versa), then the net rate of absorption of heat required by the thermocouple to maintain equilibrium in the presence of an electric current is

$$q = \frac{Q_{\text{net}}}{\Delta t} = \left[ \pi_2 - \pi_1 + \int_1^2 (\sigma_A - \sigma_B) dT \right] I = E_S I \quad (9)$$

This is in accord with the first law of thermodynamics, according to which heat and work are mutually convertible. Thus, the net heat absorbed must equal the electric work accomplished or, in terms of a unit charge of electricity, the Seebeck emf,  $E_S$ , which may be expressed in the differential form

$$dE_S = d\pi + (\sigma_A - \sigma_B) dT \quad (10)$$

The second law of thermodynamics may be applied also to the thermocouple cycle, the unit charge of electricity again being considered, as

$$\Delta S_{\text{rev}} = \sum \frac{\Delta Q}{T_{\text{abs}}} = 0 \quad (11)$$

where  $\Delta Q$  implies the various components of the net heat absorbed (that is, the components of  $E_S$ ), and  $T_{\text{abs}}$  implies the temperature at which the heat is transferred across the system boundaries. Equation 11 can be expressed in the differential form

$$dS_{\text{rev}} = d\left(\frac{\pi}{T}\right) + \frac{(\sigma_A - \sigma_B)}{T} dT = 0 \quad (12)$$

Combining the differential expressions for the first and second laws of thermodynamics, we obtain the Kelvin relations

$$\pi_{A,B} = T_{\text{abs}} \left( \frac{dE_S}{dT} \right) = T_{\text{abs}} \alpha_{A,B} \quad (13)$$

$$(\sigma_A - \sigma_B) = -T_{\text{abs}} \left( \frac{d^2 E_S}{dT^2} \right) \quad (14)$$

from which we can determine  $\alpha$ ,  $\pi$ , and  $\Delta\sigma$ , when  $E_S$  is obtained as a function of  $T$ . Thus, if

$$E_S = aT + \frac{1}{2}bT^2 + \dots \quad (15)$$

is taken to represent the thermoelectric characteristics of a thermocouple whose reference junction is maintained at  $0^\circ\text{C}$ , and where the coefficients,  $a$  and  $b$ , are obtained (for example) by the curve fitting of calibration data, then

$$\alpha = (a + bT + \dots) \quad (16)$$

$$\pi = T_{\text{abs}}(a + bT + \dots) \quad (17)$$

$$\Delta\sigma = -T_{\text{abs}}(b + \dots) \quad (18)$$

Examples of the use of these coefficients are given in Table 2.1.

### 2.1.6 Onsager Relations

The historical viewpoint presented thus far has avoided the very real irreversible  $I^2R$  and heat conduction in order to arrive at the useful and experimentally confirmed Kelvin relations. We shall now discuss how the present-day, irreversible thermodynamic viewpoint removes this flaw in our reasoning.

Basically, we judge whether a given process is reversible or irreversible by noting the change in entropy accompanying a given change in the thermodynamic state. Thus, if  $dS > \delta Q_a/T_{\text{abs}}$ , we say the process is irreversible; or, stated in a more useful manner

$$dS_{\text{system}} = dS_{\text{across boundary}} + dS_{\text{produced inside}} \quad (19)$$

or

$$dS_s = dS_0 + dS_i = \frac{\delta Q_a}{T_{\text{abs}}} + \frac{\delta F}{T_{\text{abs}}} \quad (20)$$

TABLE 2.1—*Determination of various thermoelectric quantities applied to thermocouples.*

Given, the two constants,  $a$  and  $b$ , as determined with respect to platinum via Eq 15:

| Metal             | $a, \mu\text{V}/^\circ\text{C}$ | $b, \mu\text{V}/(^\circ\text{C})^2$ |
|-------------------|---------------------------------|-------------------------------------|
| Iron(Fe)          | +16.7                           | -0.0297                             |
| Copper(Cu)        | +2.7                            | +0.0079                             |
| Constantan(Cu-Ni) | -34.6                           | -0.0558                             |

By way of illustration, consider the following combinations of materials: iron/copper and iron/constantan, with their measuring junctions at  $200^\circ\text{C}$  and their reference junctions at  $0^\circ\text{C}$ :

Iron/copper

$$a_{\text{Fe/Cu}} = a_{\text{Fe}} - a_{\text{Cu}} = 16.7 - 2.7 = 14 \mu\text{V}/^\circ\text{C}$$

$$b_{\text{Fe/Cu}} = b_{\text{Fe}} - b_{\text{Cu}} = -0.0297 - 0.0079$$

$$b_{\text{Fe/Cu}} = -0.0376 \mu\text{V}/(^\circ\text{C})^2$$

Iron/constantan

$$a_{\text{Fe/Cu-Ni}} = a_{\text{Fe}} - a_{\text{Con}} = 16.7 - (-34.6) = 51.3 \mu\text{V}/^\circ\text{C}$$

$$b_{\text{Fe/Cu-Ni}} = b_{\text{Fe}} - b_{\text{Con}} = -0.0297 - (-0.0558)$$

$$b_{\text{Fe/Cu-Ni}} = 0.0261 \mu\text{V}/(^\circ\text{C})^2$$

Since Seebeck voltage  $E_s = aT + 1/2bT^2$ ,

Iron/copper

$$E_s = 14(200) + 1/2(-0.0376)(200)^2$$

$$E_s = 2048 \mu\text{V}$$

Iron/constantan

$$E_s = 51.3(200) + 1/2(0.0261)(200)^2$$

$$E_s = 10\,782 \mu\text{V}$$

Note how different combinations of materials give widely different thermal emf's.

Now we proceed to write expressions for  $\alpha$ ,  $\pi$ , and  $\Delta\sigma$ , to note how the separate emf's combine to give the (net) Seebeck emf: Since  $\alpha_{A,B} = a_{A,B} + b_{A,B}T =$  Seebeck coefficient

Iron/copper

$$\alpha_0 = 14 + (-0.0376)(0) = 14 \mu\text{V}/^\circ\text{C}$$

$$\alpha_{200} = 14 + (-0.0376)(200) = 6.48 \mu\text{V}/^\circ\text{C}$$

Iron/constantan

$$\alpha_0 = 51.3 + 0.0261(0) = 51.3 \mu\text{V}/^\circ\text{C}$$

$$\alpha_{200} = 51.3 + 0.0261(200) = 56.52 \mu\text{V}/^\circ\text{C}$$

Note that it is the great difference in Seebeck coefficients (thermoelectric powers) for the two combinations which accounts for the difference in thermal emf's:

$$E_s = \int_{T_R}^T \alpha_{A,B} dT$$

Since  $\pi_{A,B} = T_{\text{abs}}\alpha_{A,B} =$  Peltier coefficient = Peltier voltage

Iron/copper

$$\pi_0 = 273(14) = 3822 \mu\text{V}$$

$$\pi_{200} = 473(6.48) = 3065 \mu\text{V}$$

Iron/constantan

$$\pi_0 = 273(51.3) = 14\,005 \mu\text{V}$$

$$\pi_{200} = 473(56.52) = 26\,734 \mu\text{V}$$

TABLE 2.1—(Continued).

Note that, in the case of the iron/copper (Fe-Cu) thermocouple,  $\pi_{\text{cold}} > \pi_{\text{hot}}$ , whereas in the more usual Fe/Cu-Ni thermocouple,  $\pi_{\text{hot}} > \pi_{\text{cold}}$ .

Since  $\Delta\sigma_{A,B} = -b_{A,B}T_{\text{abs}} =$  Thomson coefficient, and

$$E_T = \int_{T_{R\text{abs}}}^{T_{\text{abs}}} \Delta\sigma dT = \frac{1}{2} b_{A,B} (T_{R\text{abs}}^2 - T_{\text{abs}}^2) = \text{Thomson voltage}$$

Iron/copper

$$E_T = -\frac{0.0376}{2} (273^2 - 473^2)$$

$$E_T = 2805 \mu\text{V}$$

Iron/constantan

$$E_T = \frac{0.0261}{2} (273^2 - 473^2)$$

$$E_T = -1947 \mu\text{V}$$

We sum the various components

$$E_S = \pi_2 - \pi_1 + \int_1^2 \Delta\sigma dT = \text{Seebeck voltage}$$

Iron/copper

$$E_S = 3065 - 3822 + 2805$$

$$E_S = 2048 \mu\text{V}$$

Iron/constantan

$$E_S = 26\,734 - 14\,005 - 1947$$

$$E_S = 10\,782 \mu\text{V}$$

These figures of course, check with the original calculations. Note that, in the Fe/Cu case, the net Thomson emf far outweighs in importance the net Peltier emf, whereas in the Fe/Cu-Ni case, the converse is true.

Hence, only in the absence of entropy within the system boundaries do we have the reversible case,  $dS_{\text{rev}} = \delta Q_q / T_{\text{abs}}$ , which may be handled adequately by classical thermodynamics in the steady and quasi-steady states. Evidently, the rate of production of entropy per unit volume,  $\xi$ , is an important quantity in irreversible thermodynamics, which may be expressed as

$$\xi = \left( \frac{1}{A dx} \right) \frac{dS_i}{dt} = \left( \frac{1}{A dx} \right) \frac{\delta F}{T_{\text{abs}} dt} \quad (21)$$

where  $A dx$  is the area times the differential length.

Another significant quantity, the product  $T_{\text{abs}}\xi$  (called the dissipation), always can be split into two terms or a sum of two terms; one associated with a flow,  $J$ , and the other associated with a force,  $X$ . Furthermore, in many simple cases a linear relation is found (by experiment) to exist between the flow and force terms so defined. For example, in the one-dimensional, isothermal, steady flow of electric charges,  $\delta Q_e/dt$  across a potential gradient,  $-dE/dx$ , it may be shown that

$$T_{\text{abs}}\xi = \left(\frac{I}{A}\right)\left(-\frac{dE}{dx}\right) = J_e X_e \quad (22)$$

where  $J_e$  and  $X_e$  represent the electric flow and force terms, respectively, as defined by the entropy production method. The term  $J_e$  represents the electric-current density and the term  $X_e$  the electric-field strength or the electromotive force, which of course are related by the linear Ohm's law (that is,  $J_e = L_e X_e$ , where  $L_e$  represents the electrical conductivity). Again, in the one-dimensional, steady flow of thermal charges,  $dQ_q/dt$ , across a temperature gradient,  $-dT/dx$ , it may be shown that

$$T_{\text{abs}}\xi = \left(\frac{Q}{A}\right)\left(\frac{1}{T_{\text{abs}}}\frac{dT}{dx}\right) = J_q X_q \quad (23)$$

where  $J_q$  and  $X_q$  represent the thermal flow and force, respectively, as defined by the entropy production method. The term  $J_q$  represents the thermal current density, and the term  $X_q$  represents the thermomotive force, which are, of course, related by the linear Fourier's law (that is,  $J_q = L_q X_q$  where  $L_q$  represents the product of the thermal conductivity and the absolute temperature). It has been found that, even in complex situations, it always may be stated that

$$T_{\text{abs}}\xi = \sum J_K X_K \quad (24)$$

When several irreversible transport processes occur simultaneously (as, for example, the electric and thermal conduction in a thermocouple), they usually will interfere with each other; therefore, the linear relations must be generalized to include the various possible interaction terms. Thus, for the combined electric and thermal effects we would write

$$J_e = L_{ee}X_e + L_{eq}X_q \quad (25)$$

$$J_q = L_{qe}X_e + L_{qq}X_q \quad (26)$$

or, in general

$$J_i = \sum L_{ij}X_j \quad (27)$$

We have just seen that an entropy production necessarily accompanies both the  $I^2R$  and heat conduction effects (that is, they are irreversible); therefore, the Kelvin relations could not follow from reversible thermodynamic theory without certain intuitive assumptions. By reasoning that the electrical and thermal currents were independent, Thomson tacitly assumed that  $L_{eq} = L_{qe}$  as we shall subsequently show. Experimentally, this reciprocal relationship often was found to be true. The American chemist, Lars Onsager, proved in 1931 from a statistical-mechanics viewpoint that the assumption

$$L_{ij} = L_{ji} \quad (28)$$

is always true when the linear relations between flows,  $J_k$ , and forces,  $X_k$ , are valid. The Onsager reciprocal relation forms the basis of irreversible thermodynamics. By applying these concepts to the processes involved in the thermocouple, we are led rationally and unambiguously to the Kelvin relations. Thus, whenever the junctions of a thermocouple are maintained at different temperatures, we expect that an electric potential difference, an electric current, and a thermal current will be present. The dissipation for this thermoelectric process is simply the sum of the electric and thermal terms previously given. That is

$$T_{\text{abs}}\xi = \frac{I}{A} \left( -\frac{dE}{dT} \right) + \frac{Q}{A} \left( \frac{1}{T_{\text{abs}}} \frac{dT}{dx} \right) \quad (29)$$

The generalized linear laws for this case also have been given as

$$J_e = L_{ee} \left( -\frac{dE}{dT} \right) + \frac{L_{eq}}{T_{\text{abs}}} \left( \frac{dT}{dx} \right) \quad (30)$$

$$J_q = L_{qe} \left( -\frac{dE}{dT} \right) + \frac{L_{qq}}{T_{\text{abs}}} \left( \frac{dT}{dx} \right) \quad (31)$$

Recalling that the Seebeck emf is determined under conditions of zero electric current, the Seebeck coefficient,  $\alpha$ , may be expressed in terms of the Onsager coefficients as

$$\alpha = \left( \frac{dE_S}{dT} \right)_{I=0} = \frac{L_{eq}}{L_{ee} T_{\text{abs}}} \quad (32)$$

Recalling that the Peltier coefficient,  $\pi$ , represents the heat absorbed, or evolved, with the passage of an electric current across an isothermal junction, this too may be expressed in terms of the Onsager coefficients as

$$\pi = \left( \frac{J_q}{J_e} \right)_{dT=0} = \frac{L_{qe}}{L_{ee}} \quad (33)$$

Finally, we recall that Thomson found experimentally (and expressed in the Kelvin relations) that the Seebeck and Peltier coefficients are related, as shown in Eq 13.

$$\pi = T_{\text{abs}} \left( \frac{dE_S}{dT} \right) \quad (34)$$

In terms of the Onsager coefficients, this requires that

$$\frac{L_{qe}}{L_{ee}} = T_{\text{abs}} \left( \frac{L_{eq}}{L_{ee} T_{\text{abs}}} \right) \quad (35)$$

$$L_{qe} = L_{eq} \quad (36)$$

which indicates that the experimental results agree with those which are predicted by the entropy production-linear law-Onsager reciprocal relation approach; in other words, by irreversible thermodynamics, without using any intuitive assumption. The Kelvin relations, also in accord with experiment, must follow.

## 2.2 Laws of Thermoelectric Circuit

Numerous investigations of thermoelectric circuits in which accurate measurements were made of the current, resistance, and electromotive force have resulted in the establishment of several basic laws. These laws have been established experimentally beyond a reasonable doubt and may be accepted in spite of any lack of a theoretical development.

### 2.2.1 Law of Homogeneous Metals

*A thermoelectric current cannot be sustained in a circuit of a single homogeneous material, however varying in cross section, by the application of heat alone.*

A consequence of this law is that two different materials are required for any thermocouple circuit. Experiments have been reported suggesting that a nonsymmetrical temperature gradient in a homogenous wire gives rise to a measurable thermoelectric emf. A preponderance of evidence indicates, however, that any emf observed in such a circuit arises from the effects of local inhomogeneities. Furthermore, any current detected in such a circuit



when the wire is heated in any way whatever is taken as evidence that the wire is inhomogenous.

### 2.2.2 Law of Intermediate Metals

*The algebraic sum of the thermoelectromotive forces in a circuit composed of any number of dissimilar materials is zero if all of the circuit is at a uniform temperature.*

A consequence of this law is that a third homogeneous material always can be added in a circuit with no effect on the net emf of the circuit so long as its extremities are at the same temperature. Therefore, it is evident that a device for measuring the thermoelectromotive force may be introduced into a circuit at any point without affecting the resultant emf, provided all of the junctions which are added to the circuit by introducing the device are all at the same temperature. It also follows that any junction whose temperature is uniform and which makes a good electrical contact does not affect the emf of the thermoelectric circuit regardless of the method employed in forming the junction (Fig. 2.1).

Another consequence of this law may be stated as follows. If the thermal emfs of any two metals with respect to a reference metal (such as  $C$ ) are known, then the emf of the combination of the two metals is the algebraic sum of their emfs against the reference metal (Fig. 2.2).

### 2.2.3 Law of Successive or Intermediate Temperatures

*If two dissimilar homogeneous metals produce a thermal emf of  $E_1$ , when the junctions are at temperatures  $T_1$  and  $T_2$ , and a thermal emf of  $E_2$ , when the junctions are at  $T_2$  and  $T_3$ , the emf generated when the junctions are at  $T_1$  and  $T_3$ , will be  $E_1 + E_2$ .*

One consequence of this law permits a thermocouple, calibrated for a given reference temperature, to be used with any other reference temperature through the use of a suitable correction (see Fig. 2.3 for a schematic example).

Another consequence of this law is that extension wires, having the same thermoelectric characteristics as those of the thermocouple wires, can be introduced in the thermocouple circuit (say from region  $T_2$  to  $T_3$  in Fig. 2.3) without affecting the net emf of the thermocouple.

## 2.3 Elementary Thermoelectric Circuits

Two continuous, dissimilar thermocouple wires extending from the measuring junction to the reference junction, when used together with cop-

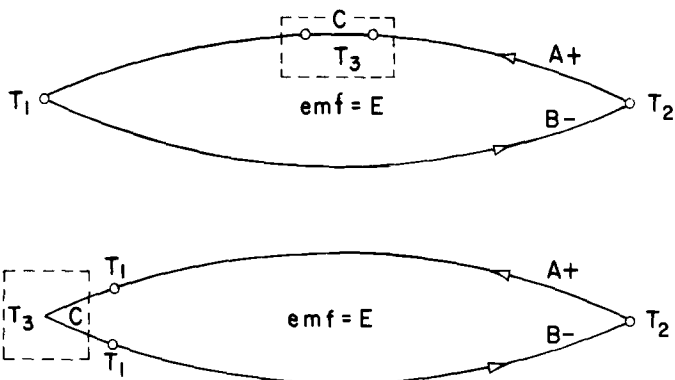


FIG. 2.1— $E$  unaffected by third material,  $C$ .

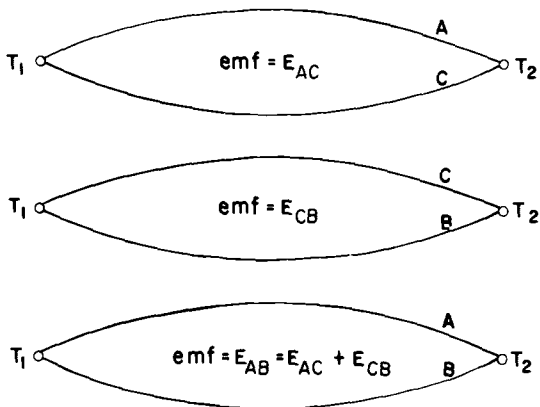


FIG. 2.2— $Emfs$  are additive for materials.

per connecting wires and a potentiometer, connected as shown in Fig. 2.4, make up the basic thermocouple circuit.

An ideal circuit is given in Fig. 2.5 for use when more than one thermocouple is involved. The usual thermocouple circuit, however, includes: measuring junctions, thermocouple extension wires, reference junctions, copper connecting wires, a selector switch, and potentiometer, as indicated in Fig. 2.6. Many different circuit arrangements of the above components are also acceptable, depending on given circumstances, and these are discussed in the appropriate sections which follow.

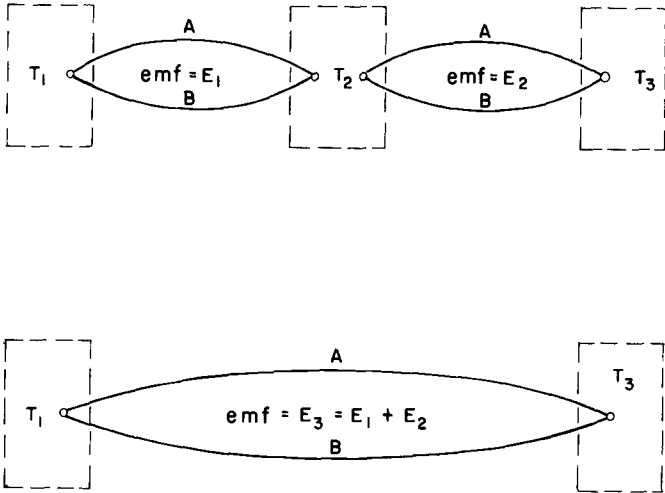
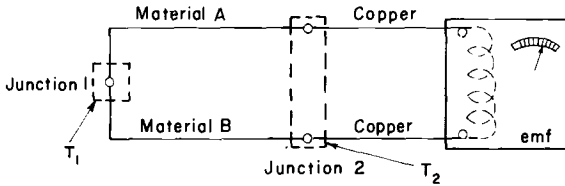
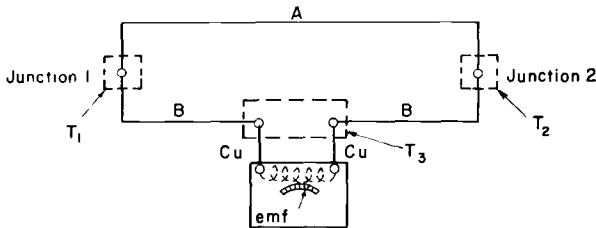


FIG. 2.3—Emfs are additive for temperature intervals.



(a) For temperature level (Junction 2 is held at a constant, known reference temperature)



(b) For temperature difference (Junctions 1 and 2 are each exposed to unknown environment temperatures)

FIG. 2.4—Several methods for introducing copper extension wires in elementary thermocouple circuits.

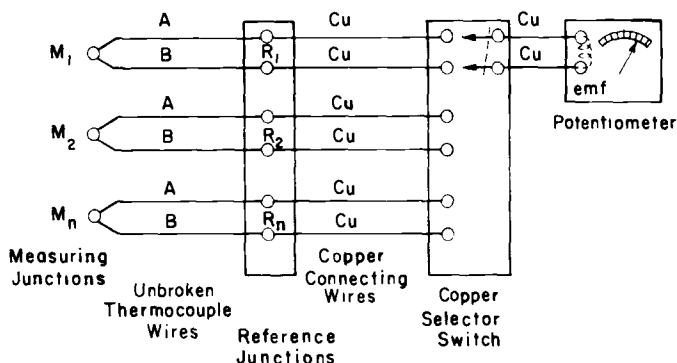


FIG. 2.5—Basic thermocouple circuit.

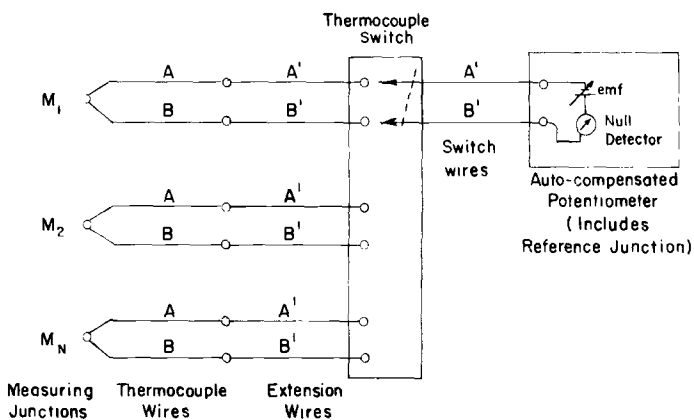


FIG. 2.6—Typical industrial thermocouple circuits.

## 2.4 Bibliography

### 2.4.1 Early Historical References

Volta, A., "On the Electricity Excited by Mere Contact of Conducting Substances of Different Kinds," *Philosophical Transactions*, 1800, p. 403.

Seebeck, T. J., "Evidence of the Thermal Current of the Combination Bi-Cu by Its Action on Magnetic Needle," *Royal Academy of Science*, Berlin, 1822-1823, p. 265.

Fourier, J. B. J., *Analytical Theory of Heat*, Gauthier-Villars et Cie., Paris, 1822; English translation by Freeman, A., Cambridge University Press, Cambridge, 1878.

Ohm, G. S., "Determination of the Laws by Which Metals Conduct the Contact Electricity,

and also a Draft for a Theory of the Voltage Apparatus," *Journal for Chemie and Physik (Schweigger's Journal)*, Vol. 46, 1826, p. 137.

Peltier, J. C. A., "Investigation of the Heat Developed by Electric Currents in Homogeneous Materials and at the Junction of Two Different Conductors," *Annalis de Chemie et de Physique*, Vol. 56 (2nd Series), 1834, p. 371.

Joule, J. P., "On the Production of Heat by Voltaic Electricity," *Proceedings of the Royal Society*, Dec. 1840.

Thomson, W., "On an Absolute Thermometric Scale Founded on Carnot's Theory of the Motive Power of Heat, and Calculated from Regnault's Observations," *Proceedings of the Cambridge Philosophical Society*, June 1848.

Clausius, R. J. E., "About the Motive Force of Heat," *Annalen der Physik und Chemie*, Vol. 79, 1850, pp. 368 and 500.

Thomson, W., "On a Mechanical Theory of Thermo-Electric Current," *Proceedings of the Royal Society of Edinburgh*, Dec. 1851.

Thomson, W., "On the Thermal Effects of Electric Currents in Unequal Heated Conductors," *Proceedings of the Royal Society*, Vol. VII, May 1854.

#### 2.4.2 Recent References

Benedict, R. P., "Thermoelectric Effects," *Electrical Manufacturing*, Feb. 1960, p. 103.

Finch, D. I., "General Principles of Thermoelectric Thermometry," *Temperature*, Vol. 3, Part 2, Reinhold, New York, 1962.

Roeser, W. F., "Thermoelectric Circuitry," *Journal of Applied Physics*, Vol. 11, 1940, p. 388.

Dike, P. H., "Thermoelectric Thermometry," *Leeds and Northrup Technical Publication EN-33A (1a)*, 3rd ed., April 1955.

Stratton, R., "On the Elementary Theory of Thermoelectric Phenomena," *British Journal of Applied Physics*, Vol. 8, Aug. 1949, p. 33.

Miller, D. G., "Thermodynamic Theory of Irreversible Processes," *American Journal of Physics*, May 1956, p. 433.

Onsager, L., "Reciprocal Relations in Irreversible Processes," *Physical Review*, Vol. 37, Feb. 1931, p. 405.

Callen, H. B., "The Application of Onsager's Reciprocal Relations to Thermoelectric, Thermomagnetic, and Galvanomagnetic Effects," *Physical Review*, Vol. 73, June 1948, p. 3149.

Hatsopoulos, G. N. and Keenan, J. H., "Analyses of the Thermoelectric Effects of Methods of Irreversible Thermodynamics," *Journal of Applied Mechanics*, Vol. 25, Dec. 1958, p. 428.

Benedict, R. P., *Fundamentals of Temperature, Pressure, and Flow Measurements*, 2nd ed., Wiley, New York, 1977.

Pollock, D. D., *The Theory and Properties of Thermocouple Elements*, ASTM STP 492, American Society for Testing and Materials, 1971.

Benedict, R. P. and Russo, R. J., "A Note on Grounded Thermocouple Circuits," *Transactions, American Society of Mechanical Engineers, Journal of Basic Engineering*, June 1972, p. 377.

Fenton, A. W., "The Theory of Thermoelectric Thermometers," United Kingdom Atomic Energy Authority, 1969, unpublished.

Fenton, A. W., "Errors in Thermoelectric Thermometers," *Proceedings, Institute of Electrical Engineers*, Vol. 116, No. 7, July 1969.

Fenton, A. W. et al., "Thermocouples: Instabilities of Seebeck Coefficients," United Kingdom Atomic Energy Authority, Report No. TRG 1447(R), Jan. 1967.

Freeman, R. J., "Distributed Seebeck Effect at High Temperature," High Temperature Thermometry Seminar, Oct. 1959, see TID 7586, Part 1.

Fenton, A. W., "A Note on How Thermocouples Work," Report No. ND-R-327(R), United Kingdom Atomic Energy Authority, April 1974.

Broomfield, G. H., "Signals from Temperature Measuring Thermocouples," *The Metallurgist and Materials Technologist*, May 1979, p. 281.

Moffat, R. J., "Thermocouple Theory and Practice," in *Fundamentals of Aerospace Instrumentation*. Vol. 6, Instrument Society of America, 1974, pp. 111-124.

**2.5 Nomenclature***Roman*

|             |                             |
|-------------|-----------------------------|
| <i>a, b</i> | Coefficients                |
| <i>A</i>    | Area                        |
| <i>E</i>    | Electric potential          |
| <i>F</i>    | Frictional loss             |
| <i>I</i>    | Electric current            |
| <i>J</i>    | Flow                        |
| <i>k</i>    | Thermal conductivity        |
| <i>L</i>    | Constant of proportionality |
| <i>Q</i>    | Heat                        |
| <i>S</i>    | Entropy                     |
| <i>t</i>    | Time                        |
| <i>T</i>    | Temperature                 |
| <i>U</i>    | Internal energy             |
| <i>W</i>    | Work                        |
| <i>x</i>    | Length or thickness         |
| <i>X</i>    | Force                       |

*Subscripts*

|                |                        |
|----------------|------------------------|
| <i>A, B, C</i> | Thermocouple materials |
| <i>e</i>       | Electrical             |
| <i>i, j, k</i> | General subscripts     |
| <i>i</i>       | Internal               |
| <i>P</i>       | Peltier                |
| <i>q</i>       | Thermal                |
| <i>R</i>       | Reference              |
| <i>S</i>       | Seebeck                |
| <i>T</i>       | Thomson                |
| abs            | Absolute               |
| rev            | Reversible             |
| 1,2            | States                 |

*Greek*

|          |                           |
|----------|---------------------------|
| $\alpha$ | Seebeck coefficient       |
| $\Delta$ | Finite difference         |
| $\pi$    | Peltier coefficient       |
| $\sigma$ | Thomson coefficient       |
| $\Sigma$ | Sum                       |
| $\xi$    | Entropy production/volume |

# Chapter 3—Thermocouple Materials

---

## 3.1 Common Thermocouple Types

The commonly used thermocouple types are identified by letter designations originally assigned by the Instrument Society of America (ISA) and adopted as an American Standard in ANSI MC 96.1. This chapter covers general application data on the atmospheres in which each thermocouple type can be used, recommended temperature ranges, limitations, etc. Physical and thermoelectric properties of the thermoelement materials used in each of these thermocouple types are also presented in this section.

The following thermocouple types are included (these are defined as having the emf-temperature relationship given in the corresponding letter-designated Table in Chapter 10 within the limits of error specified in Table 10.1 of that chapter):

*Type T*—Copper (+) versus constantan (-).

*Type J*—Iron (+) versus constantan (-).

*Type E*—Nickel-10 percent chromium (+) versus constantan (-).

*Type K*—Nickel-10 percent chromium (+) versus nickel-5 percent aluminum and silicon (-) (see note).

*Type R*—Platinum-13 percent rhodium (+) versus platinum (-).

*Type S*—Platinum-10 percent rhodium (+) versus platinum (-).

*Type B*—Platinum-30 percent rhodium (+) versus platinum-6 percent rhodium (-).

Temperature limits stated in the text are maximum values. Table 3.1 gives recommended maximum temperature limits for various gage sizes of wire. Figure 3.1 is a graphical presentation of maximum temperature limits from Table 3.1 and permits interpolation based on wire size. Table 3.2 gives nominal Seebeck coefficients for the various types. Temperature-emf equivalents and commercial limits of error for these common thermocouple types are given in Chapter 10.

### 3.1.1 General Application Data

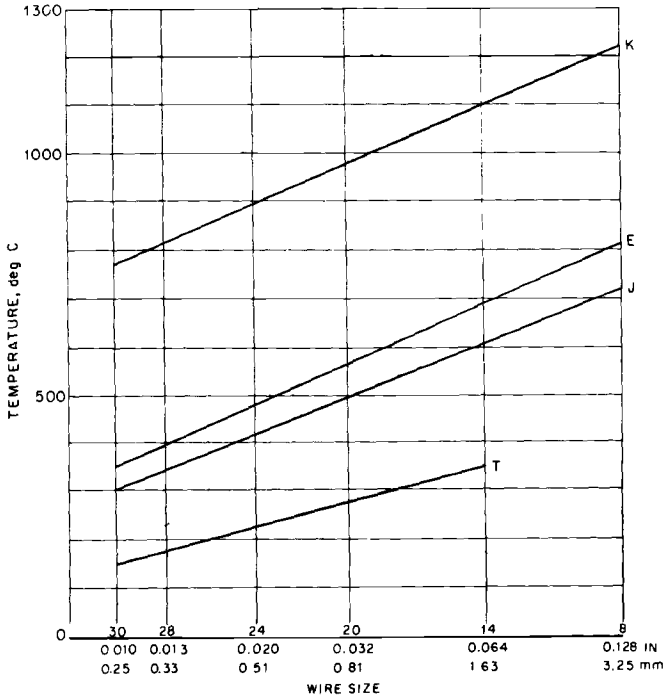
*Type T*—These thermocouples are resistant to corrosion in moist atmospheres and are suitable for subzero temperature measurements (see Table 10.1 for limits of error in the subzero region.) Their use in air or in oxidizing environments is restricted to 370°C (700°F) due to oxidation of the

TABLE 3.1—Recommended upper temperature limits for protected thermocouples.

| Thermocouple Type | Upper Temperature Limit for Various Wire Sizes (awg), °C (°F) |                                  |                                  |                                  |                                  |                                  |
|-------------------|---|----------------------------------|----------------------------------|----------------------------------|----------------------------------|----------------------------------|
|                   | No. 8 Gage, 3.25 mm (0.128 in.)                               | No. 14 Gage, 1.63 mm (0.064 in.) | No. 20 Gage, 0.81 mm (0.032 in.) | No. 24 Gage, 0.51 mm (0.020 in.) | No. 28 Gage, 0.33 mm (0.013 in.) | No. 30 Gage, 0.25 mm (0.010 in.) |
| T                 |   | 370 (700)                        | 260 (500)                        | 200 (400)                        | 200 (400)                        | 150 (300)                        |
| J                 | 760 (1400)  | 590 (1100)                       | 480 (900)                        | 370 (700)                        | 370 (700)                        | 320 (600)                        |
| E                 | 870 (1600)  | 650 (1200)                       | 540 (1000)                       | 430 (800)                        | 430 (800)                        | 370 (700)                        |
| K                 | 1260 (2300)   | 1090 (2000)                      | 980 (1800)                       | 870 (1600)                       | 870 (1600)                       | 760 (1400)                       |
| R and S           |   |                                  |                                  | 1480 (2700)                      |                                  |                                  |
| B                 |   |                                  |                                  | 1700 (3100)                      |                                  |                                  |

NOTE—This table gives the recommended upper temperature limits for the various thermocouples and wire sizes. These limits apply to protected thermocouples, that is, thermocouples in conventional closed-end protecting tubes. They do not apply to sheathed thermocouples having compacted mineral oxide insulation. Properly designed and applied sheathed thermocouples may be used at temperatures above those shown in the tables. Other literature sources should be consulted.





NOTE—This graph gives the recommended upper temperature limits for the various thermocouples and wire sizes. These limits apply to thermocouples used under the atmospheric limitations outlined in the text. They do not apply to sheathed thermocouples having compacted mineral oxide insulation. In any general recommendation of thermocouple temperature limits, it is not practicable to take into account special cases. In actual operation, there may be instances where the temperature limits recommended can be exceeded. Likewise, there may be applications where satisfactory life will not be obtained at the recommended temperature limits. However, in general, the temperature limits listed are such as to provide satisfactory thermocouple life when the wires are operated continuously at these temperatures.

FIG 3.1—Recommended upper temperature limits for types K, E, J, T thermocouples.

copper thermoelement. They may be used to higher temperatures in some other atmospheres.

They can be used in a vacuum and in oxidizing, reducing or inert atmospheres over the temperature range of  $-200$  to  $370^{\circ}\text{C}$  ( $-330$  to  $700^{\circ}\text{F}$ ). The upper temperature limit is due primarily to oxidation of the copper element.

This is the only thermocouple type for which limits of error are established in the subzero temperature range (see rates under Table 10.1, Chapter 10).

Type J—These thermocouples are suitable for use in vacuum and in oxidizing, reducing, or inert atmospheres, over the temperature range of  $0$  to  $760^{\circ}\text{C}$  ( $32$  to  $1400^{\circ}\text{F}$ ). The rate of oxidation of the iron thermoelement is rapid above  $540^{\circ}\text{C}$  ( $1000^{\circ}\text{F}$ ), and the use of heavy-gage wires is recom-

TABLE 3.2—Nominal Seebeck coefficients (thermoelectric power).

| Temperature | Thermocouple Type                 |      |      |      |      |      |      |
|-------------|-----------------------------------|------|------|------|------|------|------|
|             | E                                 | J    | K    | R    | S    | T    | B    |
| °C          | Seebeck Coefficient-Microvolts/°C |      |      |      |      |      |      |
| -190        | 27.3                              | 24.2 | 17.1 | ...  | ...  | 17.1 |      |
| -100        | 44.8                              | 41.4 | 30.6 | ...  | ...  | 28.4 |      |
| 0           | 58.5                              | 50.2 | 39.4 | ...  | ...  | 38.0 | ...  |
| 200         | 74.5                              | 55.8 | 40.0 | 8.8  | 8.5  | 53.0 | 2.0  |
| 400         | 80.0                              | 55.3 | 42.3 | 10.5 | 9.5  | ...  | 4.0  |
| 600         | 81.0                              | 58.5 | 42.6 | 11.5 | 10.3 | ...  | 6.0  |
| 800         | 78.5                              | 64.3 | 41.0 | 12.3 | 11.0 | ...  | 7.7  |
| 1000        | ...                               | ...  | 39.0 | 13.0 | 11.5 | ...  | 9.2  |
| 1200        | ...                               | ...  | 36.5 | 13.8 | 12.0 | ...  | 10.3 |
| 1400        | ...                               | ...  | ...  | 13.8 | 12.0 | ...  | 11.3 |
| 1600        | ...                               | ...  | ...  | ...  | 11.8 | ...  | 11.6 |
| °F          | Seebeck Coefficient-Microvolts/°F |      |      |      |      |      |      |
| -300        | 15.5                              | 14.4 | ...  | ...  | ...  | 9.7  |      |
| -200        | 22.0                              | 20.6 | ...  | ...  | ...  | 13.7 |      |
| -100        | 27.0                              | 24.6 | ...  | ...  | ...  | 17.3 |      |
| 32          | 32.5                              | 28.0 | 21.7 | 3.0  | 3.0  | 21.3 | ...  |
| 200         | 37.5                              | 30.1 | 23.2 | 4.1  | 4.0  | 25.7 | 0.5  |
| 400         | 41.5                              | 30.9 | 22.3 | 4.9  | 4.8  | 29.8 | 1.1  |
| 600         | 43.5                              | 30.7 | 23.1 | 5.5  | 5.1  | 32.7 | 1.8  |
| 800         | 45.0                              | 30.6 | 23.5 | 5.9  | 5.3  | ...  | 2.4  |
| 1000        | 45.0                              | 31.7 | 23.7 | 6.2  | 5.5  | ...  | 3.0  |
| 1500        | 44.0                              | 35.7 | 22.8 | 6.9  | 6.1  | ...  | 4.4  |
| 2000        | ...                               | ...  | 21.1 | 7.6  | 6.6  | ...  | 5.4  |
| 2500        | ...                               | ...  | ...  | 7.6  | 6.6  | ...  | 6.2  |
| 3000        | ...                               | ...  | ...  | 7.6  | 6.5  | ...  | 6.5  |

mended when long life is required at the higher temperatures. Type J may be used to higher temperatures in some atmospheres. However, they should not be used in sulfurous atmospheres above 540°C (1000°F).

This thermocouple is not recommended for use below the ice point because rusting and embrittlement of the iron thermoelement make its use less desirable than Type T. Limits of error have not been established for Type J thermocouples at subzero temperatures.

*Type E*—Type E thermocouples are recommended for use over the temperature range of -200 to 900°C (-330 to 1600°F) in oxidizing or inert atmospheres. In reducing atmospheres, alternately oxidizing and reducing atmospheres, marginally oxidizing atmospheres, and in vacuum, they are subject to the same limitations as Type K thermocouples.

These thermocouples are suitable for subzero temperature measurements since they are not subject to corrosion in atmospheres with high moisture content. Limits of error are shown in Table 10.1, Chapter 10.

Type E thermocouples develop the highest emf per degree of all the commonly used types and are often used primarily because of this feature.

*Type K*—Type K thermocouples are recommended for use in an oxidizing or completely inert atmosphere over the temperature range of  $-200$  to  $1260^{\circ}\text{C}$  ( $-330$  to  $2300^{\circ}\text{F}$ ). Because their oxidation resistance characteristics are better than those of Types E, J, and T thermocouples, they find widest use at temperatures above  $540^{\circ}\text{C}$  ( $1000^{\circ}\text{F}$ ).

Type K thermocouples are suitable for temperature measurements as low as  $-250^{\circ}\text{C}$  ( $-420^{\circ}\text{F}$ ), although limits of error have been established only for the temperature range given previously.

Type K thermocouples should not be used in:

1. Atmospheres that are reducing or alternately oxidizing and reducing.
2. Sulfurous atmospheres, since sulfur will attack both thermoelements and will cause rapid embrittlement and breakage of the negative thermoelement wire through intergranular corrosion.
3. Vacuum, except for short time periods, since preferential vaporization of chromium from the positive element may alter calibration.
4. Atmospheres that promote "green-rot" corrosion of the positive thermoelement. Such corrosion results from preferential oxidation of chromium when the oxygen content of the atmosphere surrounding the thermocouple is low. Green-rot corrosion can cause large negative errors in calibration and is most serious at temperature levels of  $815$  to  $1040^{\circ}\text{C}$  ( $1500$  to  $1900^{\circ}\text{F}$ ).

Green-rot corrosion frequently occurs when thermocouples are used in long unventilated protecting tubes of small diameter. It can be minimized by increasing the oxygen supply through the use of large diameter protecting tubes or ventilated protecting tubes. Another approach is to decrease the oxygen content below that which will promote preferential oxidation by inserting a "getter" to absorb the oxygen in a sealed protecting tube.

*Types R and S*—Types R and S thermocouples are recommended for continuous use in oxidizing or inert atmospheres over the temperature range of  $0$  to  $1480^{\circ}\text{C}$  ( $32$  to  $2700^{\circ}\text{F}$ ).

They should not be used in reducing atmospheres, nor those containing metallic or nonmetallic vapors. They never should be inserted directly into a metallic primary protecting tube.

*Types R and S*—Types R and S thermocouples are recommended for continuous use in oxidizing or inert atmospheres over the temperature range of  $0$  to  $1480^{\circ}\text{C}$  ( $32$  to  $2700^{\circ}\text{F}$ ).

Continued use of Types R and S thermocouples at high temperatures causes excessive grain growth which can result in mechanical failure of the platinum element. It also renders the platinum susceptible to contamination which causes a reduction in the emf output of the thermocouple.

Calibration changes also are caused by diffusion of rhodium from the alloy wire into the platinum, or by volatilization of rhodium from the alloy. All of these effects tend to produce inhomogeneity.

*Type B*—Type B thermocouples are recommended for continuous use in oxidizing or inert atmospheres over the temperature range of 870 to 1700°C (1000 to 3100°F). They are also suitable for short term use in vacuum. They should not be used in reducing atmospheres, nor those containing metallic or nonmetallic vapors. They should never be inserted directly into a metallic primary protecting tube or well.

Under corresponding conditions of temperature and environment, Type B thermocouples will show less grain growth and less drift in calibration than Types R and S thermocouples.

### 3.1.2 Properties of Thermoelement Materials

This section indicates in Tables 3.3 to 3.9 and in Figure 3.2 the physical and electrical properties of thermoelement materials as used for the common letter-designated thermocouple types (Types T, J, E, K, R, S, and B). These are typical data and are listed for information only. They are not intended for use as specifications for ordering thermocouple materials.

Thermoelement materials are designated in the tables by the established American Standard letter symbols JP, JN, etc. The first letter of the symbol designates the type of thermocouple. The second letter, P or N, denotes the positive or negative thermoelement. Typical materials to which these letter designations apply are:

|               |  |
|---------------|--|
| TP            | Copper   |
| JP            | Iron, ThermoKanthal JP <sup>1</sup>  |
| TN, JN, or EN | Constantan, Cupron <sup>2</sup> , Advance <sup>3</sup> , ThermoKanthal JN <sup>1</sup>                       |
| KP or EP      | Nickel-chrome, Chromel <sup>4</sup> , Tophel <sup>2</sup> , T-1 <sup>3</sup> , ThermoKanthal KP <sup>1</sup> |
| KN            | Nickel-silicon, Alumel <sup>4</sup> , Nial <sup>2</sup> , T-2 <sup>3</sup> , ThermoKanthal KN <sup>1</sup>   |
| RP            | Platinum-13 percent rhodium  |
| SP            | Platinum-10 percent rhodium  |
| RN or SN      | Platinum   |
| BP            | Platinum-30 percent rhodium  |
| BN            | Platinum-6 percent rhodium   |

Note that TN, JN, and EN thermoelements, as just listed, are composed of the same basic types of material. The typical data contained in the following pages are applicable to any of these thermoelements. The thermal emf of these thermoelements when referenced to platinum may differ significantly depending on the type of thermocouple of which each is intended.

It also should be noted that positive and negative thermoelements for a given type of thermocouple, as supplied by any one manufacturer, will con-

<sup>1</sup>Trademark of the Kanthal Corporation.

<sup>2</sup>Trademark of American Metal Climax Incorporated.

<sup>3</sup>Trademark of the Driver-Harris Company.

<sup>4</sup>Trademark of the Hoskins Manufacturing Company.

TABLE 3.3—Nominal chemical composition of thermoelements.

| Element    | Nominal Chemical Composition, % |                            |     |           |     |     |     |           |      |      |
|------------|---------------------------------|----------------------------|-----|-----------|-----|-----|-----|-----------|------|------|
|            | JP                              | JN, TN,<br>EN <sup>a</sup> | TP  | KP,<br>EP | KN  | RP  | SP  | RN,<br>SN | BP   | BN   |
| Iron       | 99.5                            | ...                        | ... | ...       | ... | ... | ... | ...       | ...  | ...  |
| Carbon     | ... <sup>b</sup>                | ...                        | ... | ...       | ... | ... | ... | ...       | ...  | ...  |
| Manganese  | ... <sup>b</sup>                | ...                        | ... | ...       | 2   | ... | ... | ...       | ...  | ...  |
| Sulfur     | ... <sup>b</sup>                | ...                        | ... | ...       | ... | ... | ... | ...       | ...  | ...  |
| Phosphorus | ... <sup>b</sup>                | ...                        | ... | ...       | ... | ... | ... | ...       | ...  | ...  |
| Silicon    | ... <sup>b</sup>                | ...                        | ... | ...       | 1   | ... | ... | ...       | ...  | ...  |
| Nickel     | ... <sup>b</sup>                | 45                         | ... | 90        | 95  | ... | ... | ...       | ...  | ...  |
| Copper     | ... <sup>b</sup>                | 55                         | 100 | ...       | ... | ... | ... | ...       | ...  | ...  |
| Chromium   | ... <sup>b</sup>                | ...                        | ... | 10        | ... | ... | ... | ...       | ...  | ...  |
| Aluminum   | ...                             | ...                        | ... | ...       | 2   | ... | ... | ...       | ...  | ...  |
| Platinum   | ...                             | ...                        | ... | ...       | ... | 87  | 90  | 100       | 70.4 | 93.9 |
| Rhodium    | ...                             | ...                        | ... | ...       | ... | 13  | 10  | ...       | 29.6 | 6.1  |

<sup>a</sup>Types JN, TN, and EN thermoelements usually contain small amounts of various elements for control of thermal emf, with corresponding reductions in the nickel or copper content, or both.

<sup>b</sup>Thermoelectric iron (JP) contains small but varying amounts of these elements.

TABLE 3.4—Environmental limitations of thermoelements.

| Thermoelement | Environmental Recommendations and Limitations<br>(see notes)   |
|---------------|--|
| JP            | For use in oxidizing, reducing, or inert atmospheres or in vacuum. Oxidizes rapidly above 540°C (1000°F). Will rust in moist atmospheres as in subzero applications.<br>Stable to neutron radiation transmutation. Change in composition is only 0.5 percent (increase in manganese) in 20-year period.  |
| JN, TN, EN    | Suitable for use in oxidizing, reducing, and inert atmospheres or in vacuum. Should not be used unprotected in sulfurous atmospheres above 540°C (1000°F).<br>Composition changes under neutron radiation since copper content is converted to nickel and zinc. Nickel content increases 5 percent in 20-year period.  |
| TP            | Can be used in vacuum or in oxidizing, reducing or inert atmospheres. Oxidizes rapidly above 370°C (700°F). Preferred to Type JP element for subzero use because of its superior corrosion resistance in moist atmospheres.<br>Radiation transmutation causes significant changes in composition.<br>Nickel and zinc grow into the material in amounts of 10 percent each in a 20-year period. |
| KP, EP        | For use in oxidizing or inert atmospheres. Can be used in hydrogen or cracked ammonia atmospheres if dew point is below -40°C (-40°F). Do not use unprotected in sulfurous atmospheres above 540°C (1000°F).   |

TABLE 3.4—(Continued).

| Thermoelement          | Environmental Recommendations and Limitations<br>(see notes)   |
|------------------------|--|
| KN                     | <p>Not recommended for service in vacuum at high temperatures except for short time periods because preferential vaporization of chromium will alter calibration. Large negative calibration shifts will occur if exposed to marginally oxidizing atmospheres in temperature range 815 to 1040°C (1500 to 1900°F).</p> <p>Quite stable to radiation transmutation. Composition change is less than 1 percent in 20-year period.</p> <p>Can be used in oxidizing or inert atmospheres. Do not use unprotected in sulfurous atmospheres as intergranular corrosion will cause severe embrittlement.</p>  |
| RP, SP, SN, RN, BP, BN | <p>Relatively stable to radiation transmutation. In 20-year period, iron content will increase approximately 2 percent. The manganese and cobalt contents will decrease slightly.</p> <p>For use in oxidizing or inert atmospheres. Do not use unprotected in reducing atmospheres in the presence of easily reduced oxides, atmospheres containing metallic vapors such as lead or zinc, or those containing nonmetallic vapors such as arsenic, phosphorus, or sulfur. Do not insert directly into metallic protecting tubes. Not recommended for service in vacuum at high temperatures except for short time periods.</p> <p>Types RN and SN elements are relatively stable to radiation transmutation. Types BP, BN, RP, and SP elements are unstable because of the rapid depletion of rhodium. Essentially, all the rhodium will be converted to palladium in a 10-year period.</p> |

NOTE 1—Refer to Table 3.5 for recommended upper temperature limits.

NOTE 2—Stability under neutron radiation refers to chemical composition of thermoelement, not to stability of thermal emf.

NOTE 3—Radiation transmutation rates<sup>a</sup> are based on exposure to a thermal neutron flux of  $1 \times 10^{14}$  neutrons/cm<sup>2</sup>·s.

<sup>a</sup>Browning, W. E., Jr., and Miller, C. E., Jr., "Calculated Radiation Induced Changes in Thermocouple Composition," *Temperature, Its Measurement and Control in Science and Industry*, Part 2, Rheinhold, New York, Vol. C, 1962, p. 271.

form to the calibration curve for that thermocouple within specified limits of error. However, because materials used for a given thermoelement by various manufacturers may differ slightly in thermal emf, larger errors may occur if positive and negative thermoelements from different sources are combined.

## 3.2 Extension Wires

### 3.2.1 General Information

Extension wires are inserted between the measuring junction and the reference junction and have approximately the same thermoelectric proper-

TABLE 3.5—Recommended upper temperature limits for protected thermoelements.

| Upper Temperature Limits for Various Wire Sizes (avg), °C (°F) |                                       |  |  |  |  |  |
|--|---------------------------------------|--|--|--|--|--|
| Thermoelement  | No. 8 Gage,<br>3.25 mm<br>(0.128 in.) | No. 14 Gage,<br>1.63 mm<br>(0.064 in.) | No. 20 Gage,<br>0.81 mm<br>(0.032 in.) | No. 24 Gage,<br>0.51 mm<br>(0.020 in.) | No. 28 Gage,<br>0.33 mm<br>(0.013 in.) | No. 30 Gage,<br>0.25 mm<br>(0.010 in.) |
| JP   | 760°C<br>(1400°F)                     | 593°C<br>(1100°F)                      | 482°C<br>(900°F)                       | 371°C<br>(700°F)                       | 371°C<br>(700°F)                       | 320°C<br>(600°F)                       |
| JN, TN, EN   | 871°C<br>(1600°F)                     | 649°C<br>(1200°F)                      | 538°C<br>(1000°F)                      | 427°C<br>(800°F)                       | 427°C<br>(800°F)                       | 427°C<br>(800°F)                       |
| TP   | ...                                   | 371°C<br>(700°F)                       | 260°C<br>(500°F)                       | 204°C<br>(400°F)                       | 204°C<br>(400°F)                       | 150°C<br>(300°F)                       |
| KP, EP, KN   | 1260°C<br>(2300°F)                    | 1093°C<br>(2000°F)                     | 982°C<br>(1800°F)                      | 871°C<br>(1600°F)                      | 871°C<br>(1600°F)                      | 760°C<br>(1400°F)                      |
| RP, SP, RN, SN   | ...                                   | ...                                    | ...                                    | 1482°C<br>(2700°F)                     | ...                                    | ...                                    |
| BP, BN   | ...                                   | ...                                    | ...                                    | 1705°C<br>(3100°F)                     | ...                                    | ...                                    |

NOTE—This table gives the recommended upper temperature limits for the various thermoelements and wire sizes. These limits apply to protected thermoelements, that is, thermoelements in conventional closed-end protecting tubes. They do not apply to sheathed thermoelements having compacted mineral oxide insulation. In any general recommendation of thermoelement temperature limits, it is not practicable to take into account special cases. In actual operation, there may be instances where the temperature limits recommended can be exceeded. Likewise, there may be applications where satisfactory life will not be obtained at the recommended temperature limits. However, in general, the temperature limits listed are such as to provide satisfactory thermoelement life when the wires are operated continuously at these temperatures.

TABLE 3.6—Seebeck coefficient (thermoelectric power) of thermoelements with respect to Platinum 67 (typical values).

| Thermoelement   | JN, TN,   |       | TP   | KP, EP | KN    | RP   | SP   | BP   | BN   |
|-----------------|---|-------|------|--------|-------|------|------|------|------|
|                 | JP  | EN    |      |        |       |      |      |      |      |
| Temperature, °C | Seebeck Coefficient, $\mu\text{V}/^\circ\text{C}$ |       |      |        |       |      |      |      |      |
| -190            | +6.3  | -20.9 | -4.1 | ...    | ...   | ...  | ...  | ...  | ...  |
| -100            | 14.4  | 27.0  | +1.1 | ...    | ...   | ...  | ...  | ...  | ...  |
| 0               | 17.8  | 32.2  | 5.9  | +25.7  | -13.5 | +5.5 | +5.5 | ...  | ...  |
| 200             | 14.6  | 41.0  | 12.0 | 32.7   | 7.4   | 8.5  | 8.5  | +9.2 | +7.2 |
| 400             | 9.7   | 45.5  | 16.2 | 34.6   | 7.7   | 10.5 | 9.5  | 11.7 | 7.6  |
| 600             | 11.7  | 46.8  | ...  | 33.8   | 8.8   | 11.5 | 10.0 | 13.8 | 7.9  |
| 800             | 17.8  | 46.4  | ...  | 32.2   | 8.8   | 12.5 | 11.0 | 15.8 | 8.2  |
| 1000            | ...   | ...   | ...  | 30.8   | 8.3   | 13.0 | 11.5 | 17.7 | 8.5  |
| 1200            | ...   | ...   | ...  | 29.1   | 7.4   | 14.0 | 12.0 | 19.1 | 8.7  |
| 1400            | ...   | ...   | ...  | ...    | ...   | 14.0 | 12.0 | 20.0 | 8.7  |
| 1600            | ...   | ...   | ...  | ...    | ...   | 13.5 | 12.0 | 20.4 | 8.7  |
| Temperature, °F | Seebeck Coefficient, $\mu\text{V}/^\circ\text{F}$ |       |      |        |       |      |      |      |      |
| -300            | +2.5  | -11.9 | -2.1 | ...    | ...   | ...  | ...  | ...  | ...  |
| -200            | 6.7   | 14.0  | +0.2 | ...    | ...   | ...  | ...  | ...  | ...  |
| -100            | 8.8   | 15.8  | 1.5  | ...    | ...   | ...  | ...  | ...  | ...  |
| 32              | 9.9   | 17.9  | 3.3  | +14.3  | -7.5  | +3.0 | +3.0 | ...  | ...  |
| 200             | 9.6   | 20.5  | 5.0  | 16.7   | 6.5   | 4.1  | 4.0  | +4.1 | +3.6 |
| 400             | 8.0   | 22.9  | 6.7  | 18.3   | 4.0   | 4.9  | 4.7  | 5.1  | 4.0  |
| 600             | 6.2   | 24.5  | 8.2  | 19.0   | 4.1   | 5.5  | 5.2  | 5.8  | 4.2  |
| 800             | 5.3   | 25.3  | ...  | 19.1   | 4.4   | 5.8  | 5.4  | 6.5  | 4.2  |
| 1000            | 5.7   | 26.0  | ...  | 18.9   | 4.8   | 6.2  | 5.5  | 7.4  | 4.3  |
| 1500            | 9.9   | 25.8  | ...  | 17.8   | 4.9   | 6.8  | 6.1  | 8.8  | 4.6  |
| 2000            | ...   | ...   | ...  | 16.7   | 4.3   | 7.6  | 6.6  | 10.2 | 4.8  |
| 2500            | ...   | ...   | ...  | 14.9   | 4.0   | 7.7  | 6.7  | 11.0 | 4.9  |
| 3000            | ...   | ...   | ...  | ...    | ...   | 7.6  | 6.5  | 11.3 | 4.9  |

ties as the thermocouple wires with which they are used. Table 3.10 gives comparative data on extension wires available for thermocouples in common use. Extension wires are normally available as single or duplex, solid or stranded, insulated wires in sizes ranging from 14 to 20 B&S gage. A variety of insulations and protective coverings is available in several combinations to suit the many types of environments encountered in industrial service (see Chapter 4).

Some advantages of using extension wires are:

1. Improvement in mechanical or physical properties of the thermoelectric circuit. For example, the use of stranded construction or smaller diameter solid wire may increase the flexibility of a portion of the circuit. Extension wires also may be selected to adjust the electrical resistance of the circuit.



TABLE 3.7—Typical physical

| Property   | Thermoelement         |                       |                       |                       |
|--|-----------------------|-----------------------|-----------------------|-----------------------|
|  | JP                    | JN. EN. TN            | TP                    | KP. EP                |
| <i>Melting point (solidus temperatures):</i>               |                       |                       |                       |                       |
| °C   | 1 490                 | 1 220                 | 1 083                 | 1 427                 |
| °F   | 2 715                 | 2 228                 | 1 981                 | 2 600                 |
| <i>Resistivity:</i>  |                       |                       |                       |                       |
| μΩ·cm:   |                       |                       |                       |                       |
| at 0°C   | 8.57                  | 48.9                  | 1.56                  | 70                    |
| at 20°C  | 9.67                  | 48.9                  | 1.724                 | 70.6                  |
| Ω cmil/ft:   |                       |                       |                       |                       |
| at 0°C   | 51.5                  | 294.2                 | 9.38                  | 421                   |
| at 20°C  | 58.2                  | 294                   | 10.37                 | 425                   |
| Temperature coefficient of resistance, Ω/Ω·°C (0 to 100°C) | $65 \times 10^{-4}$   | $-0.1 \times 10^{-4}$ | $43 \times 10^{-4}$   | $4.1 \times 10^{-4}$  |
| Coefficient of thermal expansion, in./in.·°C (20 to 100°C) | $11.7 \times 10^{-6}$ | $14.9 \times 10^{-6}$ | $16.6 \times 10^{-6}$ | $13.1 \times 10^{-6}$ |
| <i>Thermal conductivity at 100°C:</i>                      |                       |                       |                       |                       |
| Cal·cm/s·cm <sup>2</sup> ·°C                               | 0.162                 | 0.0506                | 0.901                 | 0.046                 |
| Btu·ft/h·ft <sup>2</sup> ·°F                               | 39.2                  | 12.2                  | 218                   | 11.1                  |
| Specific heat at 20°C, cal/g·°C                            | 0.107                 | 0.094                 | 0.092                 | 0.107                 |
| <i>Density:</i>  |                       |                       |                       |                       |
| g/cm <sup>3</sup>  | 7.86                  | 8.92                  | 8.92                  | 8.73                  |
| lb/in. <sup>3</sup>  | 0.284                 | 0.322                 | 0.322                 | 0.315                 |
| <i>Tensile strength (annealed):</i>                        |                       |                       |                       |                       |
| kgf/cm <sup>2</sup>  | 3 500                 | 5 600                 | 2 500                 | 6 700                 |
| psi  | 50 000                | 80 000                | 35 000                | 95 000                |
| Magnetic attraction  | strong                | none                  | none                  | none                  |

2. Cost improvement in thermoelectric circuitry. For example, certain base metal extension wires may be substituted for noble metal wires when the reference junction is situated at a distance from a noble metal thermocouple.

Extension wires may be separated into two categories having the following characteristics:

*Category 1*—Alloys substantially the same as used in the thermocouple. This type of extension wire normally is used with base metal thermocouples.

*Category 2*—Alloys differing from those used in the thermocouple. This type of extension wire normally is used with noble metal thermocouples and with several of the nonstandardized thermocouples (see Section 3.3).

### 3.2.2 Sources of Error

Several possible sources of error in temperature measurement accompany the use of extension wires in thermocouple circuits. Most of the errors can be avoided, however, by exercising proper precautions.

One type of error arises from the disparity in thermal emf between thermocouples and nominally identical extension wire components of Category 1.

*properties of thermoelement materials.*

| Material              |                       |                       |                       |                       |                       |
|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|
| KN                    | RP                    | SP                    | RN, SN                | BP                    | BN                    |
| 1 399                 | 1 860                 | 1 850                 | 1 769                 | 1 927                 | 1 826                 |
| 2 550                 | 3 380                 | 3 362                 | 3 216                 | 3 501                 | 3 319                 |
| 28.1                  | 19.0                  | 18.4                  | 9.83                  | ...                   | ...                   |
| 29.4                  | 19.6                  | 18.9                  | 10.4                  | 19.0                  | 17.5                  |
| 169                   | 114.3                 | 110.7                 | 59.1                  | ...                   | ...                   |
| 177                   | 117.7                 | 114.0                 | 62.4                  | 114.5                 | 106                   |
| $23.9 \times 10^{-4}$ | $15.6 \times 10^{-4}$ | $16.6 \times 10^{-4}$ | $39.2 \times 10^{-4}$ | $13.3 \times 10^{-4}$ | $20.0 \times 10^{-4}$ |
| $12.0 \times 10^{-6}$ | $9.0 \times 10^{-6}$  | $9.0 \times 10^{-6}$  | $9.0 \times 10^{-6}$  | ...                   | ...                   |
| 0.071                 | 0.088                 | 0.090                 | 0.171                 | ...                   | ...                   |
| 17.2                  | 21.3                  | 21.8                  | 41.4                  | ...                   | ...                   |
| 0.125                 | ...                   | ...                   | 0.032                 | ...                   | ...                   |
| 8.60                  | 19.61                 | 19.97                 | 21.45                 | 17.60                 | 20.55                 |
| 0.311                 | 0.708                 | 0.721                 | 0.775                 | 0.636                 | 0.743                 |
| 6 000                 | 3 200                 | 3 200                 | 1 400                 | 4 900                 | 2 800                 |
| 85 000                | 46 000                | 45 000                | 20 000                | 70 000                | 40 000                |
| moderate              | none                  | none                  | none                  | none                  | none                  |

The disparity results from the variations occurring among thermoelements lying within the standard limits of error for each type of thermocouple and extension wire. Thus, for example, it is possible that an error as great as  $\pm 4.4^\circ\text{C}$  ( $\pm 8^\circ\text{F}$ ) could occur in the Type K/KX and J/JX thermocouple-extension wire combinations, where the standard limits of error are  $\pm 2.2^\circ\text{C}$  ( $\pm 4^\circ\text{F}$ ) for the thermocouple and the extension wires treated as separate combinations. Such errors can be eliminated substantially by selecting extension wires whose emf closely matches that of the specific thermocouple, up to the maximum temperature of the thermocouple-extension wire junction.

A second source of error can arise if a temperature difference exists between the two thermoelement-extension wire junctions. Errors of this type are potentially greater in circuits employing extension wires of Category 2, where each extension element may differ significantly in emf from the corresponding thermoelement. Such errors may occur even though the extension pair emf exactly matches the thermocouple emf at each temperature. Referring to Fig. 3.3, schematically representing emf versus temperature curves for positive and negative thermoelements *P* and *N*, and corresponding extension wire elements *PX* and *NX*, the following relationships apply at any temperature *T* within the operating range of the extension wires:

TABLE 3.8—*Thermoelements—resistance to change with increasing temperature.*

| Thermo-<br>elements | Ratio of Resistance at Temperature Indicated to Resistance at 0°C (32°F) |                |                  |                  |                   |                   |                    |                    |                    |                    |  |
|---------------------|--|----------------|------------------|------------------|-------------------|-------------------|--------------------|--------------------|--------------------|--------------------|--|
|                     | 0°C<br>(32°F)  | 20°C<br>(68°F) | 200°C<br>(392°F) | 400°C<br>(752°F) | 600°C<br>(1112°F) | 800°C<br>(1472°F) | 1000°C<br>(1832°F) | 1200°C<br>(2192°F) | 1400°C<br>(2552°F) | 1500°C<br>(2732°F) |  |
| JP                  | 1.00   | 1.13           | 2.46             | 4.72             | 7.84              | 12.00             | 13.07              | ...                | ...                | ...                |  |
| JN, TN, EN          | 1.00   | 0.999          | 0.996            | 0.994            | 1.024             | 1.056             | 1.092              | ...                | ...                | ...                |  |
| TP                  | 1.00   | 1.11           | 1.86             | 2.75             | 3.70              | 4.75              | 5.96               | ...                | ...                | ...                |  |
| KP, EP              | 1.00   | 1.01           | 1.09             | 1.19             | 1.25              | 1.30              | 1.37               | 1.43               | ...                | ...                |  |
| KN                  | 1.00   | 1.05           | 1.43             | 1.64             | 1.82              | 1.98              | 2.15               | 2.32               | ...                | ...                |  |
| RP                  | 1.00   | 1.03           | 1.31             | 1.60             | 1.89              | 2.16              | 2.41               | 2.66               | 2.90               | 3.01               |  |
| SP                  | 1.00   | 1.03           | 1.33             | 1.65             | 1.95              | 2.23              | 2.50               | 2.76               | 3.01               | 3.13               |  |
| RN, SN              | 1.00   | 1.06           | 1.77             | 2.50             | 3.18              | 3.81              | 4.40               | 4.94               | 5.42               | 5.66               |  |
| BP                  | 1.00   | 1.03           | 1.26             | 1.51             | 1.76              | 1.98              | 2.20               | 2.41               | 2.62               | 2.73               |  |
| BN                  | 1.00   | 1.03           | 1.40             | 1.78             | 2.14              | 2.47              | 2.78               | 3.08               | 3.37               | 3.51               |  |

TABLE 3.9.—Nominal resistance of thermoelements.

|                |                            | Nominal Resistance, ohms per foot at 20°C (68°F) |        |            |          |        |         |         |         |         |         |  |  |  |  |
|----------------|----------------------------|--|--------|------------|----------|--------|---------|---------|---------|---------|---------|--|--|--|--|
| Awg No.        | Diameter, in. <sup>b</sup> | KN   | KP, EP | TN, JN, EN | TP       | JP     | RN, SN  | RP      | SP      | BP      | BN      |  |  |  |  |
| 6              | 0.1620                     | 0.0067   | 0.0162 | 0.0112     | 0.000395 | 0.0027 | 0.00243 | 0.00448 | 0.00438 | 0.00440 | 0.00407 |  |  |  |  |
| 9 <sup>a</sup> | 0.148                      | ...  | ...    | ...        | ...      | 0.0033 | ...     | 0.00537 | ...     | ...     | ...     |  |  |  |  |
| 8              | 0.1285                     | 0.0107   | 0.0257 | 0.0179     | 0.000628 | 0.0043 | 0.00386 | 0.00713 | 0.00697 | 0.00700 | 0.00648 |  |  |  |  |
| 10             | 0.1019                     | 0.0170   | 0.041  | 0.0283     | 0.000999 | 0.0069 | 0.00614 | 0.00113 | 0.01108 | 0.01113 | 0.01030 |  |  |  |  |
| 12             | 0.0808                     | 0.0270   | 0.065  | 0.0448     | 0.00159  | 0.0109 | 0.00976 | 0.01803 | 0.01761 | 0.01769 | 0.01637 |  |  |  |  |
| 14             | 0.0641                     | 0.0432   | 0.104  | 0.0718     | 0.00253  | 0.0174 | 0.0155  | 0.0286  | 0.0280  | 0.0281  | 0.0260  |  |  |  |  |
| 16             | 0.0508                     | 0.0683   | 0.164  | 0.113      | 0.00402  | 0.0276 | 0.0247  | 0.0456  | 0.0445  | 0.0447  | 0.0414  |  |  |  |  |
| 17             | 0.0453                     | 0.0874   | 0.209  | 0.145      | 0.00506  | 0.0349 | 0.0311  | 0.0574  | 0.0562  | 0.0564  | 0.0523  |  |  |  |  |
| 18             | 0.0403                     | 0.111  | 0.266  | 0.184      | 0.00648  | 0.0446 | 0.0399  | 0.0725  | 0.0719  | 0.0722  | 0.0669  |  |  |  |  |
| 20             | 0.0320                     | 0.173  | 0.415  | 0.287      | 0.0102   | 0.0699 | 0.0624  | 0.1149  | 0.1125  | 0.1130  | 0.1046  |  |  |  |  |
| 22             | 0.0253                     | 0.276  | 0.663  | 0.456      | 0.0161   | 0.1111 | 0.0993  | 0.1839  | 0.1790  | 0.1798  | 0.1664  |  |  |  |  |
| 23             | 0.0226                     | 0.347  | 0.833  | 0.576      | 0.0204   | 0.1401 | 0.1251  | 0.2913  | 0.2257  | 0.2267  | 0.2099  |  |  |  |  |
| 24             | 0.0201                     | 0.438  | 1.05   | 0.728      | 0.0257   | 0.1767 | 0.1578  | 0.4656  | 0.2847  | 0.2859  | 0.2647  |  |  |  |  |
| 25             | 0.0179                     | 0.553  | 1.33   | 0.918      | 0.0324   | 0.2228 | 0.1990  | 0.7414  | 0.3589  | 0.3605  | 0.3337  |  |  |  |  |
| 26             | 0.0159                     | 0.700  | 1.68   | 1.16       | 0.0408   | 0.281  | 0.2509  | 1.177   | 0.4526  | 0.4546  | 0.4208  |  |  |  |  |
| 28             | 0.0126                     | 1.11   | 2.48   | 1.85       | 0.0649   | 0.447  | 0.3989  | 1.839   | 0.7197  | 0.7229  | 0.6692  |  |  |  |  |
| 30             | 0.0100                     | 1.77   | 4.25   | 2.94       | 0.1032   | 0.710  | 0.6344  | 2.965   | 1.144   | 1.149   | 1.064   |  |  |  |  |
| 32             | 0.0080                     | 2.76   | 6.65   | 4.59       | 0.1641   | 1.13   | 1.009   | 4.708   | 1.819   | 1.827   | 1.691   |  |  |  |  |
| 34             | 0.0063                     | 4.45   | 10.7   | 7.41       | 0.2609   | 1.80   | 1.604   | 7.356   | 2.893   | 2.906   | 2.690   |  |  |  |  |
| 36             | 0.0050                     | 7.08   | 17.0   | 11.8       | 0.4148   | 2.86   | 2.550   | 12.25   | 4.600   | 4.620   | 4.277   |  |  |  |  |
| 38             | 0.0040                     | 11.1   | 26.6   | 18.4       | 0.6597   | 4.54   | 4.056   | 7.316   | 7.316   | 7.348   | 6.803   |  |  |  |  |
| 40             | 0.0031                     | 18.4   | 44.2   | 30.6       | 1.049    | 7.22   | 6.448   | 11.63   | 11.63   | 11.68   | 10.81   |  |  |  |  |

<sup>a</sup>#9 Birmingham wire gage.  
<sup>b</sup>1 in. = 25.4 mm.

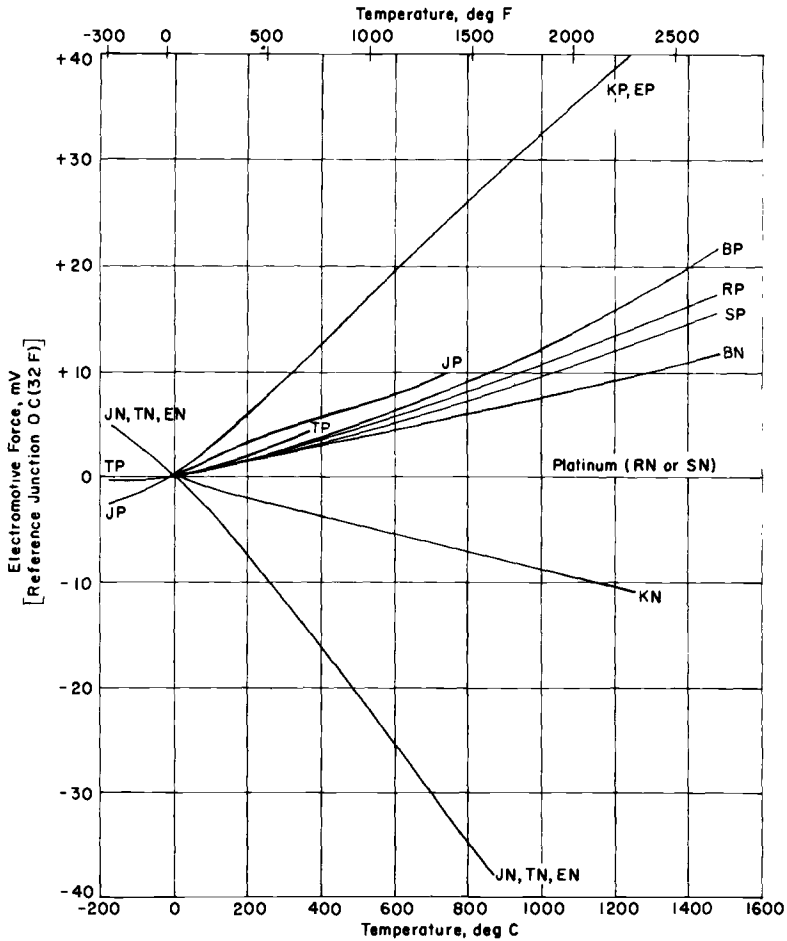


FIG. 3.2—Thermal emf of thermoelements relative to platinum.

Thermocouple output = extension pair output

That is

$$E_P - E_N = E_{PX} - E_{NX} \tag{1}$$

Rearranging to

$$E_P - E_{PX} = E_N - E_{NX} \tag{2}$$

If a temperature difference exists between the two junctions such that *P* joins *PX* at *T<sub>P</sub>*, and *N* joins *NX* at *T<sub>N</sub>*, an unwanted emf will exist across the two junctions, of magnitude

$$\Delta E = (E_P - E_{PX})_{T_P} - (E_N - E_{NX})_{T_N} \tag{3}$$

Rearranging Eq 39 according to Eq 38

$$\Delta E = (E_P - E_{PX})_{T_P} - (E_P - E_{PX})_{T_N} \quad (4)$$

The sign of  $\Delta E$  will depend on the relationship of temperature  $T_P$  to  $T_N$  and the emf relationship of  $PX$  and  $NX$  to  $P$  and  $N$ .

This  $\Delta E$  will be interpreted as an error in the output of the measuring thermocouple. Such errors do not exceed about one degree at the measuring junction, per degree of  $\Delta T$  between the thermocouple-extension wire junctions. These errors can be eliminated by equalizing the temperatures of the two junctions.

A third source of error lies in the presence of reversed polarity at the thermocouple-extension wire junctions, or at the extension wire-instrument junctions. Although a single reversal of polarity in the assembly would be noticeable, an inadvertent double reversal likewise may produce measurement errors, but could escape immediate detection.

A fourth source of error concerns the use of connectors in the thermocouple assembly. If the connector material has thermal emf characteristics which differ appreciably from those of the thermocouple extension wires, then it is important that a negligible temperature difference be maintained across the connector. This follows directly from the Law of Intermediate Metals (see Section 2.2.2). Thus, in situations where a connector made of a third metal spans a substantial temperature gradient, unwanted emfs are generated between the thermoelectric materials and the extremities of the connector, and they appear as errors in the output of the thermocouple. The magnitude of errors of this type can vary over a wide range depending on the materials involved and the temperature difference spanned by the connector.

If the emf errors arising from the use of extension wires or from other sources are to be expressed as temperature errors, the Seebeck coefficient of the thermocouple at the measuring junction temperature must be used.

A useful graphical method of evaluating error sources in thermoelectric circuits is detailed in a paper by Moffat (see Ref 1).<sup>5</sup>

### 3.3 Nonstandardized Thermocouple Types

Newer thermocouple materials are being evaluated constantly to find combinations which perform special functions more reliably than the common thermocouples. The special functions for which these newer combinations are required frequently involve very high temperatures, but also may include unusual environments such as special atmospheres or areas susceptible to vibration.

Each of the combinations described in this section has been designed to measure temperatures under specific conditions and to perform with a degree of reliability superior to other combinations under these same condi-

<sup>5</sup>The italic numbers in brackets refer to the list of references appended to this chapter.

TABLE 3.10—Extension wires for

| Thermocouple Type        | Extension Wire Type | Alloy Type         |                            |
|--------------------------|---------------------|--------------------|----------------------------|
|                          |                     | Positive           | Negative                   |
| STANDARD                 |                     |                    |                            |
| Base Metal               | Category 1          |                    |                            |
| E                        | EX                  | Ni-Cr              | Constantan                 |
| J                        | JX                  | iron               | Constantan                 |
| K <sup>c</sup>           | KX                  | Ni-Cr              | Ni-Al                      |
| T                        | TX                  | copper             | Constantan                 |
| Noble Metal              | Category 2          |                    |                            |
| B                        | BX                  | copper             | copper                     |
|                          | proprietary         | Cu-Mn <sup>f</sup> | copper                     |
| R                        | SX                  | copper             | Cu-Ni <sup>d,1</sup>       |
| S                        | SX                  | copper             | Cu-Ni <sup>d,1</sup>       |
|                          | proprietary         | Ni-Cr <sup>e</sup> | Fe-Cr <sup>e</sup>         |
| OTHER                    |                     |                    |                            |
| Refractory metal         | Category 2          |                    |                            |
| W/W-26Re                 | proprietary         | Ni-Cr <sup>e</sup> | Ni-Cr <sup>e</sup>         |
| W-5Re/W-26Re             | proprietary         | Ni-Al <sup>e</sup> | Ni-Cu <sup>e</sup>         |
| W-3Re/W-25Re             | proprietary         | Ni-Cr <sup>e</sup> | Ni-Cr <sup>e</sup>         |
| Base metal               |                     |                    |                            |
| Ni-14Cr/Ni-4Si           | Category 1          | Ni-Cr              | Ni-Si                      |
| Ni-20Cr/Ni-3Si           | Category 1          | Ni-Cr              | Ni-Si                      |
| Ni-18Mo/Ni-1Co           | Category 1          | Ni-Mo              | Ni-Co                      |
| Noble metal              |                     |                    |                            |
| Pt-20Rh/Pt-5Rh           | Category 2          | copper             | copper                     |
| Pt-40Rh/Pt-20Rh          | Category 2          | copper             | copper                     |
| Pt-13Rh/Pt-1Rh           | Category 2          | copper             | copper                     |
| Pt-15Ir/Pd               | Category 2          | base metal         | base metal                 |
| Pt-5Mo/Pt-0.1Mo          | Category 2          | copper             | Cu-Ni                      |
| Ir-40,50,60Rh/Ir         | Category 2          | copper             | AlSi 347 SS<br>or aluminum |
| 83Pd-14Pt-3Au/65Au-35Pd  | Category 2          | KP                 | KN                         |
| 55Pd-31Pt-14Au/65Au-35Pd | Category 2          | KP                 | KN                         |
|                          | Category 2          | base metal         | base metal                 |

<sup>a</sup> See also ANSI MC96.1. Reference junction 0°C (32°F).

<sup>b</sup> M denotes strong magnetic response. O denotes little or no magnetic response at room temperature.

<sup>c</sup> Includes special Type K alloys discussed in 3.3.4.1.

<sup>d</sup> Driver Harris Co.

<sup>e</sup> Hoskins Manufacturing Co.

<sup>f</sup> AMAX Specialty Metals Corp.

thermocouples mentioned in Chapter 3.

| Temperature Range      |               | Limits of Error <sup>d</sup>   |   |   |      | Magnetic <sup>b</sup><br>Response |     |
|------------------------|---------------|--|---|---|------|-----------------------------------|-----|
|                        |               | Normal   |   | Special   |      |                                   |     |
| °C                     | °F            | ± °C   | ± °F  | ± °C  | ± °F | P                                 | N   |
| <b>THERMOCOUPLES</b>   |               |  |   |   |      |                                   |     |
| 0 to 200               | 32 to 400     | 1.7  | 3.0   |   |      | O                                 | O   |
| 0 to 200               | 32 to 400     | 2.2  | 4.0   | 1.1   | 2.0  | M                                 | O   |
| 0 to 200               | 32 to 400     | 2.2  | 4.0   |   |      | O                                 | M   |
| -60 to 100             | -75 to 200    | 1.0  | 1.8   | 0.5   | 0.9  | O                                 | O   |
| 0 to 100               | 32 to 200     | $\left\{ \begin{array}{l} +0.0 \\ -3.7 \end{array} \right.$  | $\left\{ \begin{array}{l} +0.0 \\ -6.7 \end{array} \right.$ | $\left\{ \begin{array}{l} \text{measured junction} \\ >1000^{\circ}\text{C} (1830^{\circ}\text{F}) \end{array} \right.$   |      | O                                 | O   |
| 0 to 320               | 32 to 600     |  |   |   |      | ...                               | ... |
| 0 to 200               | 32 to 400     | 5.0  | 9.0   | $\left\{ \begin{array}{l} \text{measured junction} \\ >870^{\circ}\text{C} (1600^{\circ}\text{F}) \\ \text{or } \pm 1\% \end{array} \right.$  |      | O                                 | O   |
| 0 to 200               | 32 to 400     | 5.0  | 9.0   |   |      | O                                 | O   |
| 0 to 540               | 32 to 1000    | 2.8  | 5.0   |   |      | O                                 | M   |
| (whichever is greater) |               |  |   |   |      |                                   |     |
| <b>THERMOCOUPLES</b>   |               |  |   |   |      |                                   |     |
| 0 to 260               | 32 to 500     | $\left. \begin{array}{l} \pm 0.14 \text{ MV} \\ \pm 0.11 \text{ MV} \\ \pm 0.11 \text{ MV} \end{array} \right\}$ |   | $\left\{ \begin{array}{l} \text{Equivalent to} \\ \text{less than } \pm 0.5\% \\ \text{of measured} \\ \text{temperature} \\ \text{in range} \\ 1370 \text{ to } 2200^{\circ}\text{C} \\ (2500 \text{ to } 4000^{\circ}\text{F}) \end{array} \right.$ |      | O                                 | M   |
| 0 to 870               | 32 to 1600    |  |   |   |      | O                                 | M   |
| 0 to 260               | 32 to 500     |  |   |   |      | O                                 | M   |
| 0 to 200               | 32 to 400     | 2.2  | 4.0   |   |      | O                                 | M   |
| 0 to 200               | 32 to 400     | 2.2  | 4.0   |   |      | O                                 | M   |
| 0 to 200               | 32 to 400     | 2.2  | 4.0   |   |      | O                                 | M   |
| 0 to 175               | 32 to 350     | not established  |   |   |      | O                                 | O   |
| 0 to 175               | 32 to 350     | not established  |   |   |      | O                                 | O   |
| 0 to 175               | 32 to 350     | not established  |   |   |      | O                                 | O   |
| 0 to 700               | 32 to 1300    | not established  |   |   |      | ...                               | ... |
| 0 to 70                | 32 to 160     | not established  |   |   |      | O                                 | O   |
| not established        |               | not established  |   |   |      | O                                 | O   |
| at about 800           | at about 1470 | not established  |   |   |      | O                                 | M   |
| at about 800           | at about 1470 | not established  |   |   |      | O                                 | M   |
| 0 to 160               | 32 to 320     | ...  |   |   |      | ...                               | ... |



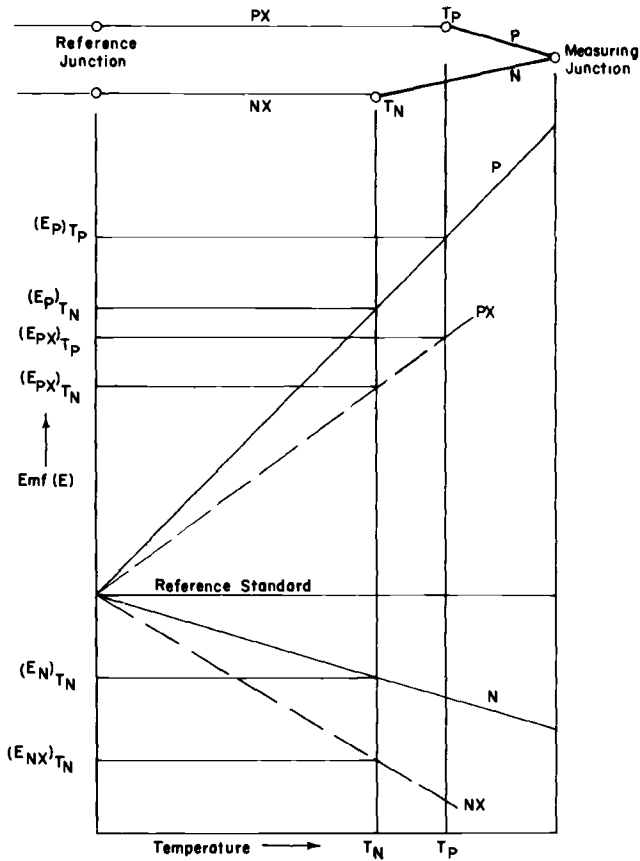


FIG. 3.3—Error due to  $\Delta T$  between the thermocouple-extension wire junctions.

tions. The properties of each combination are detailed to allow a quick selection of a combination which is most likely to be suitable for a special condition. Thermocouple compositions are given in weight percent with the positive thermoelement of the thermocouple named first.

The information on newer thermocouple materials is presented using comments, tables, and curves. The comments made for the various thermocouple systems are intended to convey information not easily shown by tables or curves. The information contained in the tables is intended to help the reader to quickly decide if a certain thermocouple system, or a specific thermocouple, is suited to his particular needs. The information given is general and nominal, and cannot be used too literally. For example, the useful maximum temperature of a thermocouple depends in part on wire size, insulation used, method of installation, atmosphere conditions, vibration present, etc. The evaluation of certain properties as good, fair, or poor is subject to wide ranges of interpretation in terms of a particular application; hence, no attempt is made to define these terms. Approximate millivolt-versus-

temperature relations for the various thermocouples are shown by curves. The curves are presented to show general temperature ranges for the various thermocouples but are not intended for use in converting emf to temperature. The reader should contact the wire manufacturer for temperature-emf tables.

The thermocouples described here are in use, and sufficient data and experience are available to warrant their inclusion. No attempt is made to include the many other thermocouple materials described in the literature which may have limited uses, or for which there are limited data, or for which there are serious problems of stability, emf reversibility, structural strength, etc.

The best source of information for a specific thermocouple in the "newer material" classification is considered to be the manufacturer of the particular thermocouple under consideration. Other useful information can be found in Ref 2.

### 3.3.1 *Platinum Types*

*3.3.1.1 Platinum-Rhodium Versus Platinum-Rhodium Thermocouples*—The standard Types R and S thermocouples can be used for temperature measurement to the melting point of platinum, 1769°C (3216°F) on a short-term basis, but, for improved service life at temperatures over 1200°C (2192°F), special platinum-rhodium thermocouples are recommended.

The platinum-40 percent rhodium versus platinum-20 percent rhodium thermocouple, called the "Land-Jewell" thermocouple, is especially useful for continuous use to 1800°C (3272°F) or occasional use to 1850°C (3362°F). However, it is seldom used where the Type B thermocouple will suffice because of lower output and greater cost.

Other thermocouples suggested for high-temperature measurement have been a platinum-13 percent rhodium versus platinum-1 percent rhodium combination and a platinum-20 percent rhodium versus platinum-5 percent rhodium combination. The former shows slightly less tendency toward mechanical failure or contamination at high temperatures than the standard Types R and S thermocouples, while the latter has properties very similar to those of the Type B thermocouple.

Figure 3.4 and Table 3.11 show the characteristics of these alloys.

All special platinum-rhodium versus platinum-rhodium thermocouples, like the standard Types R, S, and B thermocouples, show improved life at high temperatures when protected by double-bore, full-length insulators of high-purity alumina.

*3.3.1.2 Platinum-15 Percent Iridium Versus Palladium Thermocouples*—The platinum-15 percent iridium versus palladium combination was developed as a high-output noble-metal thermocouple. It combines the desirable attributes of noble metals with a high emf output as a lower cost than other noble-metal thermocouples.

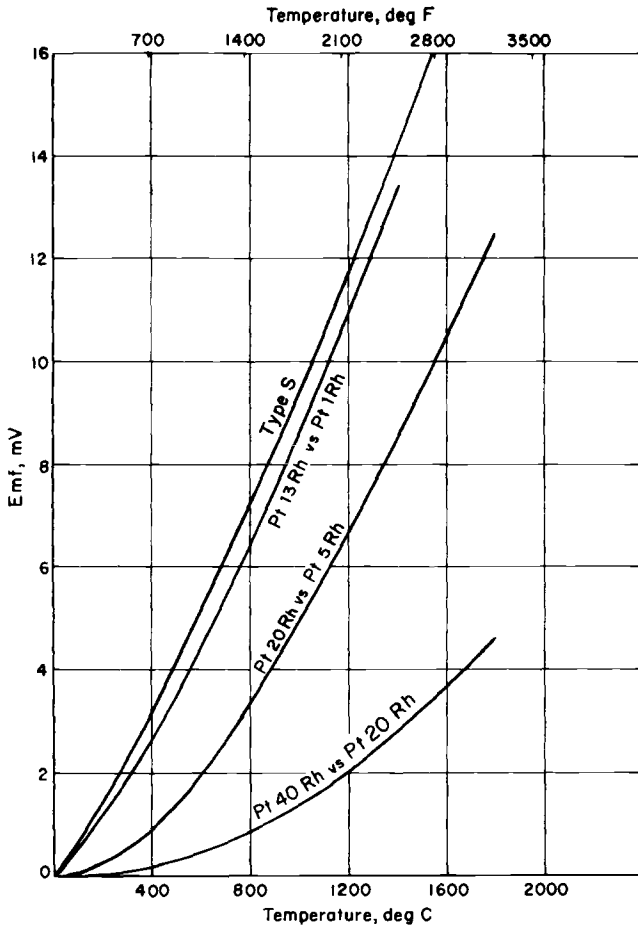


FIG. 3.4—Thermal emf of platinum-rhodium versus platinum-rhodium thermocouples.

The output becomes more linear and the Seebeck coefficient (thermoelectric power) increases with increasing temperature. In the absence of vibration, the useful range can probably be extended closer to the melting point of palladium, 1550°C (2826°F).

Figure 3.5 and Table 3.12 show the characteristics of these alloys.

Extension wires of base metals have been developed to provide a reasonable match with the thermocouple to about 700°C (1292°F).

Resistance to corrosion of the platinum-15 percent iridium alloy is better than that of the platinum-rhodium alloys in current use. Palladium is slightly less resistant to corrosion than the platinum alloy group. It will superficially oxidize at 700°C (1292°F). The oxide decomposes at about 875°C (1607°F) leaving a bright metal. When subjected to alternating oxidizing and reducing

TABLE 3.11—Platinum-rhodium versus platinum-rhodium thermocouples.

|   | Pt-20Rh Versus<br>Pt-5Rh | Pt-40Rh Versus<br>Pt-20Rh | Pt-13Rh Versus<br>Pt-1Rh |
|---|--------------------------|---------------------------|--------------------------|
| <i>Nominal operating temperature range, in:</i>       |                          |                           |                          |
| Reducing atmosphere (nonhydrogen)                     | NR <sup>a</sup>          | NR                        | NR                       |
| Wet hydrogen  | NR                       | NR                        | NR                       |
| Dry hydrogen  | NR                       | NR                        | NR                       |
| Inert atmosphere                                      | 1700°C (3092°F)          | 1800°C (3272°F)           | 1600°C (2912°F)          |
| Oxidizing atmosphere                                  | 1700°C (3092°F)          | 1800°C (3272°F)           | 1600°C (2912°F)          |
| Vacuum (short-time use)                               | 1700°C (3092°F)          | 1800°C (3272°F)           | 1600°C (2912°F)          |
| Maximum short-time temperature                        | 1770°C (3218°F)          | 1850°C (3362°F)           | 1770°C (3218°F)          |
| <i>Approximate microvolts per degree:</i>             |                          |                           |                          |
| Mean, over nominal operating range                    | 6.8/°C (12.2/°F)         | 2.5/°C (4.5/°F)           | 9.9/°C (17.8/°F)         |
| At top temperature of normal range                    | 9.9/°C (17.8/°F)         | 4.7/°C (8.45/°F)          | 12.2/°C (22.0/°F)        |
| <i>Melting temperature, nominal:</i>                  |                          |                           |                          |
| Positive thermoelement                                | 1900°C (3452°F)          | 1930°C (3520°F)           | 1865°C (3389°F)          |
| Negative thermoelement                                | 1820°C (3308°F)          | 1900°C (3452°F)           | 1771°C (3220°F)          |
| Stability with thermal cycling                        | good                     | good                      | good                     |
| High-temperature tensile properties                   | good                     | good                      | good                     |
| Stability under mechanical working                    | good                     | fair                      | good                     |
| Ductility (of most brittle thermoelement) after use   | fair                     | fair                      | fair                     |
| Resistance to handling contamination                  | fair                     | fair                      | fair                     |
| <i>Recommended extension wire, 175°C (347°F) max:</i> |                          |                           |                          |
| Positive conductor                                    | Cu                       | Cu                        | Cu                       |
| Negative conductor                                    | Cu                       | Cu                        | Cu                       |

<sup>a</sup>NR = not recommended.

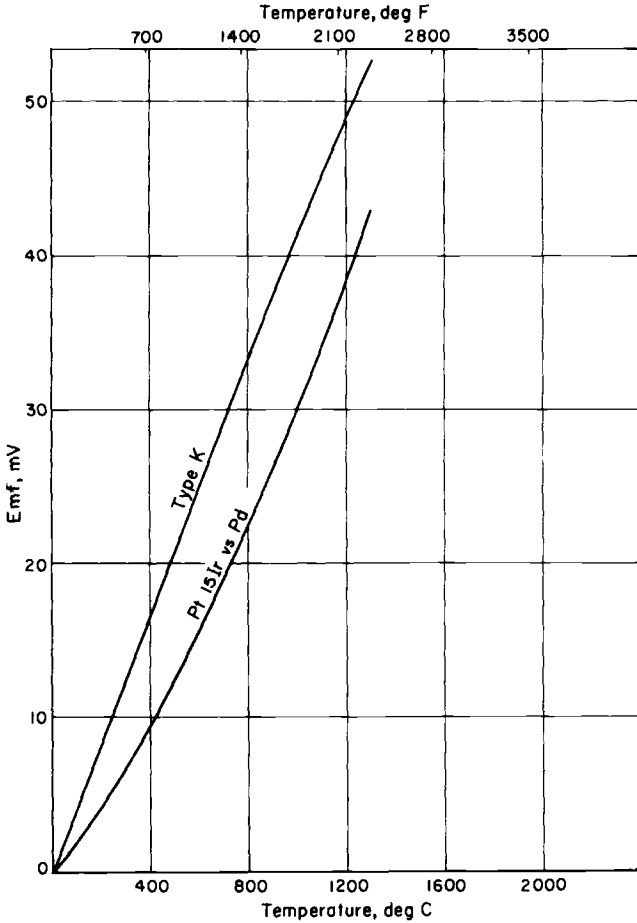


FIG. 3.5—Thermal emf of platinum-iridium versus palladium thermocouples.

atmospheres, surface blistering may result. As with all noble metals, the catalytic effect of the wires must be considered in combustible atmospheres. Its use may be preferred to base metals, however, for many applications. Both wires are ductile and may be reduced to very small sizes and still be handled with relative ease.

**3.3.1.3 Platinum-5 Percent Molybdenum Versus Platinum-0.1 Percent Molybdenum Thermocouple**—Platinum alloys containing rhodium are not suitable for use under neutron irradiation since the rhodium changes slowly to palladium. This causes a drift in the calibration of thermocouples containing rhodium. However, a thermocouple of platinum-5 percent molybdenum versus platinum-0.1 percent molybdenum is suitable for use in the helium atmosphere of a gas-cooled atomic reactor. Good stability at temperatures up

TABLE 3.12—*Platinum-iridium versus palladium thermocouple.*

|   | Pt-15Ir Versus Pd              |
|---|--------------------------------|
| <i>Nominal operating temperature range, in:</i>     |                                |
| Reducing atmosphere (nonhydrogen)                   | NR <sup>a</sup>                |
| Wet hydrogen  | NR                             |
| Dry hydrogen  | NR                             |
| Inert atmosphere                                    | 1370°C (2500°F)                |
| Oxidizing atmosphere                                | 1370°C (2500°F)                |
| Vacuum  | NR                             |
| Maximum short-time temperature                      | 1550°C (2826°F)                |
| <i>Approximate microvolts per degree:</i>           |                                |
| Mean, over nominal operating range                  | 12/°C (22/°F)                  |
| At top temperature of normal range                  | 13.6/°C (24.6/°F)              |
| <i>Melting temperature, nominal:</i>                |                                |
| Positive thermoelement                              | 1785°C (3245°F)                |
| Negative thermoelement                              | 1550°C (2826°F)                |
| Stability with thermal cycling                      | good                           |
| High-temperature tensile properties                 | fair                           |
| Stability under mechanical working                  | good                           |
| Ductility (of most brittle thermoelement) after use | good                           |
| Resistance to handling contamination                | fair                           |
| <i>Recommended extension wire:</i>                  |                                |
| Positive conductor                                  | base metal alloys <sup>b</sup> |
| Negative conductor                                  | base metal alloys <sup>b</sup> |

<sup>a</sup>NR = not recommended.

<sup>b</sup>General Electric Company.

to 1400°C (2552°F) has been reported. The output of the thermocouple is high and increases in a fairly uniform manner with increasing temperature.

Figure 3.6 and Table 3.13 show the characteristics of these alloys.

The thermocouple usually is used in an insulated metallic sheath of platinum-5 percent molybdenum alloy. The sheath may be joined to a Type 321 stainless steel sheath beyond the area of the helium atmosphere. Both the platinum-molybdenum alloy and the Type 321 stainless steel behave well under neutron irradiation and are compatible with graphite which normally is used in the reactor.

Extension wires for this thermocouple can be copper for the positive conductor and copper-1.6 percent nickel for the negative conductor. Using these materials the junctions between the thermocouple and the extension wires should be maintained below 70°C (158°F).

### 3.3.2 Iridium-Rhodium Types

**3.3.2.1 Iridium-Rhodium Versus Iridium Thermocouples**—Iridium-rhodium versus iridium thermocouples are suitable for measuring temperature

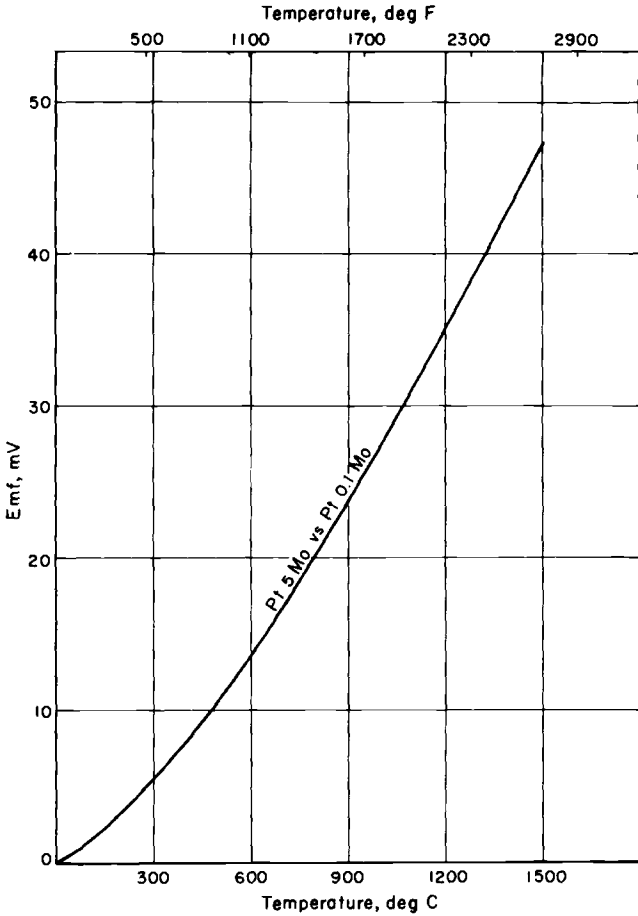


FIG. 3.6—Thermal emf of platinum-molybdenum versus platinum-molybdenum thermocouples.

to approximately 2000°C (3632°F), and generally are used above the range served by platinum-rhodium versus platinum thermocouples. They can be used in inert atmospheres and in vacuum, but not in reducing atmospheres, and they may be used in oxidizing atmospheres with shortened life.

The alloys of principal interest are those containing 40, 50, and 60 percent rhodium. They may be used for short times at maximum temperatures 2180, 2140, and 2090°C (3956, 3884, and 3794°F), these temperatures being 60°C (140°F) or more below the respective melting points.

Figure 3.7 and Table 3.14 show the characteristics of these alloys. The wires must be handled carefully. They are flexible in the fibrous (as drawn) state, but when annealed are broken easily by repeated bending.

TABLE 3.13—*Platinum-molybdenum versus platinum-molybdenum thermocouple.*

|   | Pt-5Mo Versus<br>Pt-0.1Mo |
|---|---------------------------|
| <i>Nominal operating temperature range, in:</i>     |                           |
| Reducing atmosphere (nonhydrogen)                   | NR <sup>a</sup>           |
| Wet hydrogen  | NR                        |
| Dry hydrogen  | NR                        |
| Inert atmosphere (helium)                           | 1400°C (2552°F)           |
| Oxidizing atmosphere                                | NR                        |
| Vacuum  | NR                        |
| Maximum short-time temperature                      | 1550°C (2822°F)           |
| <i>Approximate microvolts per degree:</i>           |                           |
| Mean, over nominal operating range                  | 29/°C (51.2/°F)           |
| At top temperature of normal range                  | 30/°C (54/°F)             |
| <i>Melting temperature, nominal:</i>                |                           |
| Positive thermoelement                              | 1788°C (3250°F)           |
| Negative thermoelement                              | 1770°C (3218°F)           |
| Stability with thermal cycling                      | good                      |
| High-temperature tensile properties                 | fair                      |
| Stability under mechanical working                  | good                      |
| Ductility (of most brittle thermoelement) after use | good                      |
| Resistance to handling contamination                | fair                      |
| <i>Recommended extension wire 70°C (158°F) max:</i> |                           |
| Positive conductor                                  | Cu                        |
| Negative conductor                                  | Cu-1.6Ni                  |

<sup>a</sup>NR = not recommended.

Metals said to be suitable for extension wires are 85 percent copper-15 percent nickel alloy for the positive conductor and 81 percent copper-19 percent nickel alloy for the negative conductor.<sup>6</sup>

**3.3.2.2 Iridium-Rhodium Versus Platinum-Rhodium Thermocouples**—Platinum-40 percent rhodium alloy<sup>7</sup> has been chosen by Lewis Research Center (NASA) as a substitute for an iridium thermoelement in combustor gas streams at pressures above 20 atmospheres and temperatures approaching 1600°C (2912°F). The thermocouple, consisting of a positive element of iridium-40 percent rhodium and a negative element of platinum-40 percent rhodium, showed reasonable oxidation resistance under these conditions.

Calibration to 1400°C (2552°F) showed the thermocouple output to be nearly linear and the absolute emf to be close to that of the iridium-40 percent rhodium versus iridium thermocouple.

<sup>6</sup>Johnson Matthey Incorporated.

<sup>7</sup>National Aeronautics and Space Administration Technical Brief, Nov. 1975.



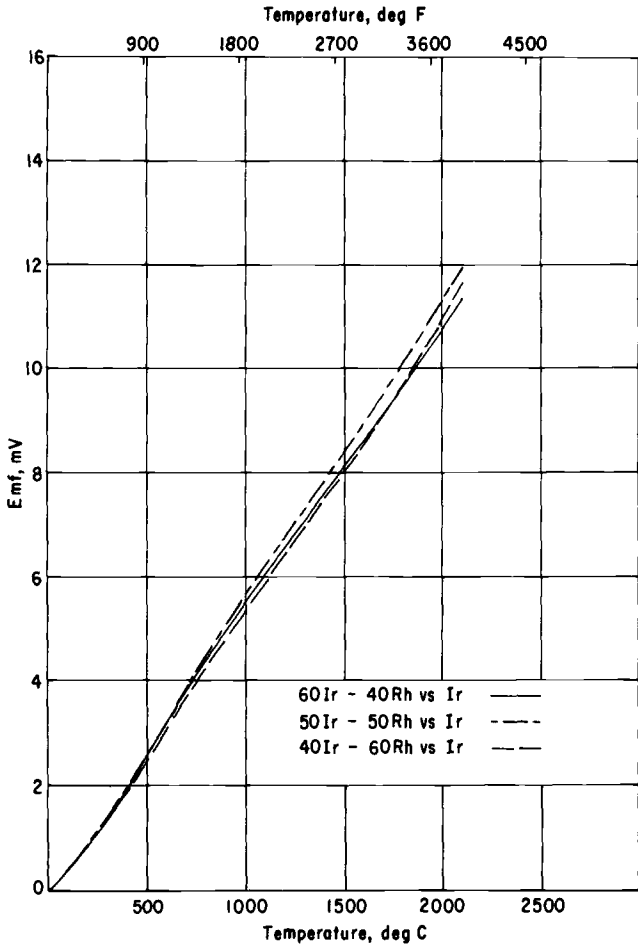


FIG. 3.7—Thermal emf of iridium-rhodium versus iridium thermocouples.

### 3.3.3 Platinel Types

3.3.3.1 *Platinel Thermocouples*—Platinel,<sup>8</sup> a noble-metal thermocouple combination, was metallurgically designed for high-temperature indication and control in turbo-prop engines. This combination approximates within reasonable tolerances the Type K thermocouple curve.

Actually, two combinations have been produced and are called Platinel I and Platinel II. The negative thermoelement in both thermocouples is a 65 percent gold-35 percent palladium alloy (Platinel 1503), but the positive one in Platinel I is composed of 83 percent palladium, 14 percent platinum, and

<sup>8</sup>Trademark of the Engelhard Industries, Inc.

TABLE 3.14—Iridium-rhodium versus iridium thermocouples.

|   | 60Ir-40Rh Versus Ir | 50Ir-50Rh Versus Ir | 40Ir-60Rh Versus Ir |
|---|---------------------|---------------------|---------------------|
| <i>Nominal operating temperature range in:</i>      |                     |                     |                     |
| Reducing atmosphere (nonhydrogen)                   |                     |                     |                     |
| Wet hydrogen  | NR <sup>a</sup>     | NR                  | NR                  |
| Dry hydrogen  | NR                  | NR                  | NR                  |
| Inert atmosphere                                    | 2100°C (3812°F)     | 2050°C (3722°F)     | 2000°C (3632°F)     |
| Oxidizing atmosphere                                | NR                  | NR                  | NR                  |
| Vacuum  | 2100°C (3812°F)     | 2050°C (3722°F)     | 2000°C (3632°F)     |
| Maximum short-time temperature                      | 2190°C (3974°F)     | 2140°C (3884°F)     | 2090°C (3794°F)     |
| <i>Approximate microvolts per degree:</i>           |                     |                     |                     |
| Mean over nominal operating range                   | 5.3°C (2.9°F)       | 5.7°C (3.2°F)       | 5.2°C (2.9°F)       |
| At top temperature of normal range                  | 5.6°C (3.1°F)       | 6.2°C (3.5°F)       | 5.0°C (2.8°F)       |
| <i>Melting temperature, nominal:</i>                |                     |                     |                     |
| Positive thermoelement                              | 2250°C (4082°F)     | 2202°C (3996°F)     | 2153°C (3907°F)     |
| Negative thermoelement                              | 2443°C (4429°F)     | 2443°C (4429°F)     | 2443°C (4429°F)     |
| Stability with thermal cycling                      | fair                | fair                | fair                |
| High-temperature tensile properties                 | ...                 | ...                 | ...                 |
| Stability under mechanical working                  | ...                 | ...                 | ...                 |
| Ductility (of more brittle thermoelement) after use | poor                | poor                | poor                |
| <i>Resistance to handling contamination:</i>        |                     |                     |                     |
| Recommended extension wire                          | ...                 | ...                 | ...                 |
| Positive conductor                                  | ...                 | ...                 | ...                 |
| Negative conductor                                  | ...                 | ...                 | ...                 |

<sup>a</sup>NR = not recommended.

3 percent gold (Platinel 1786), while that used in Platinel II contains 55 percent palladium, 31 percent platinum, and 14 percent gold (Platinel 1813). Platinel II is the preferred type and has superior mechanical fatigue properties. The thermal emfs of these combinations differ little, as shown in Fig. 3.8. Other properties are given in Table 3.15.

From Fig. 3.8 it is apparent that the emf match with the Type K thermocouple is excellent at high temperatures, but some departure occurs at low temperatures. Generally, the user of Platinel makes the connection between the thermocouple and the extension wire (Type K thermocouple wire) at an elevated temperature (800°C) where the match is good. However, if this is done, care should be taken to ensure that the junctions of both conductors

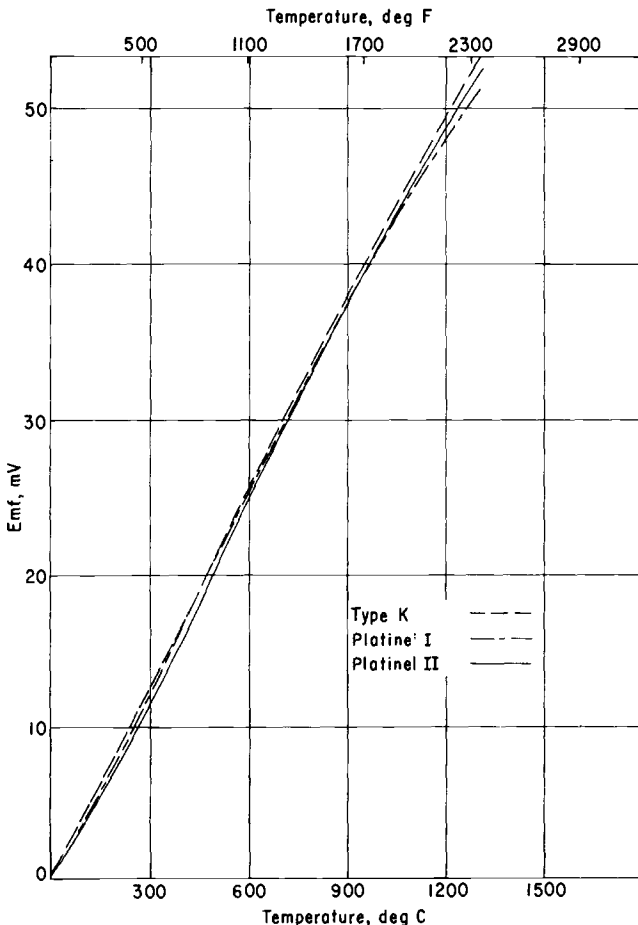


FIG. 3.8—Thermal emf of platinel thermocouples.

TABLE 3.15—*Platinel thermocouples.*

|  | Platinel II       | Platinel I        |
|--|-------------------|-------------------|
| <i>Nominal operating temperature range, in:</i>                    |                   |                   |
| Reducing atmosphere (nonhydrogen)                                  | NR <sup>b</sup>   | NR                |
| Wet hydrogen   | NR                | NR                |
| Dry hydrogen <sup>a</sup>  | 1010°C (1850°F)   | 1010°C (1850°F)   |
| Inert atmosphere   | 1260°C (2300°F)   | 1260°C (2300°F)   |
| Oxidizing atmosphere   | 1260°C (2300°F)   | 1260°C (2300°F)   |
| Vacuum   | NR                | NR                |
| Maximum short-time temperature (< 1 h)                             | 1360°C (2480°F)   | 1360°C (2480°F)   |
| <i>Approximate microvolts per degree:</i>                          |                   |                   |
| Mean, over nominal operating range (100 to 1000°C)                 | 42.5/°C (23.5/°F) | 41.9/°C (23.3/°F) |
| At top temperature of normal range (1000 to 1300°C)                | 35.5/°C (19.6/°F) | 33.1/°C (18.4/°F) |
| <i>Melting temperature, nominal:</i>                               |                   |                   |
| Positive thermoelement—solidus                                     | 1500°C (2732°F)   | 1580°C (2876°F)   |
| Negative thermoelement—solidus                                     | 1426°C (2599°F)   | 1426°C (2599°F)   |
| Stability with thermal cycling                                     | good              | good              |
| High-temperature tensile properties                                | fair              | fair              |
| Stability under mechanical working                                 | ?                 | ?                 |
| Ductility (of most brittle thermoelement) after use                | good              | good              |
| Resistance to handling contamination                               | ?                 | ?                 |
| <i>Recommended extension wire at approximately 800°C (1472°F):</i> |                   |                   |
| Positive conductor   | Type KP           | Type KP           |
| Negative conductor   | Type KN           | Type KN           |

<sup>a</sup>High-purity alumina insulators are recommended.

<sup>b</sup>NR = not recommended.

are at the same temperature. If the junction is made at a temperature where the extension wire/thermocouple emf match is not too close, then corrections should be made. Other base-metal extension wires capable of matching the emf of the Platinels very closely at low temperatures [to 160°C (320°F)] are also available.

It is recommended that precautions usually followed with the use of platinum-rhodium versus platinum thermocouples be observed when the Platinels are employed. Tests have shown that phosphorus, sulfur, and silicon have a deleterious effect on the life of the thermocouples.

### 3.3.4 Nickel-Chromium Types

**3.3.4.1 Nickel-Chromium Alloy Thermocouples**—Special nickel-chromium alloys are supplied by various manufacturers as detailed in the following paragraphs. Figure 3.9 and Table 3.16 give characteristics of these alloys.

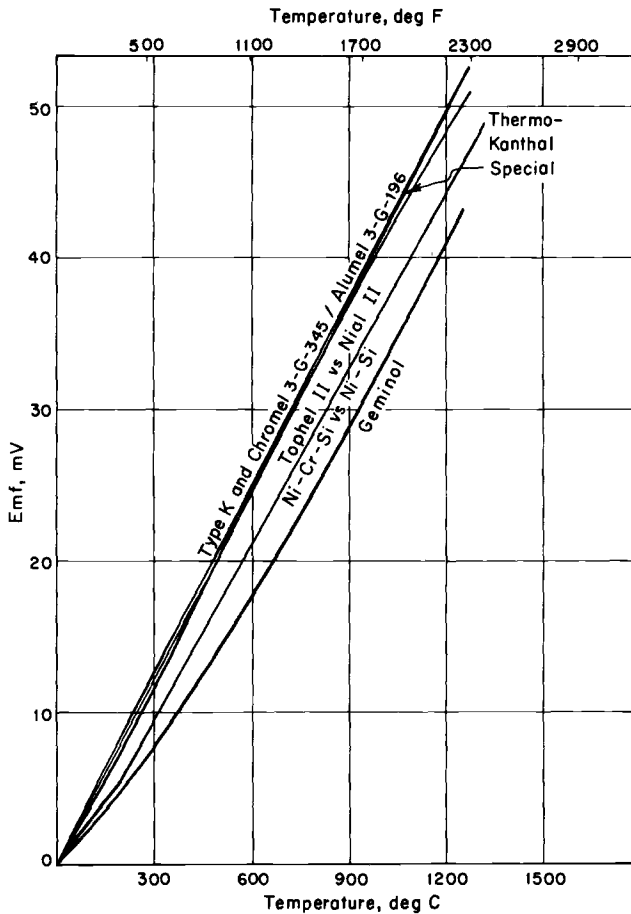


FIG. 3.9—Thermal emf of nickel-chromium alloy thermocouples.

3.3.4.1.1 *Geminol*—The Geminol<sup>9</sup> thermocouple was developed primarily for improved resistance to deterioration in reducing atmospheres.

The composition of the positive thermoelement has been adjusted specifically to combat in reducing atmospheres the destructive corrosion known as “green rot”.

The substitution of an 80 percent nickel-20 percent chromium type alloy for conventional (Type KP) 90 percent nickel-10 percent chromium alloy positive thermoelement, and a 3 percent silicon in nickel alloy for the conventional (Type KN) manganese-aluminum-silicon in nickel alloy negative thermoelement, results in a more oxidation-resisting thermocouple.

<sup>9</sup>Trademark of the Driver-Harris Company.

TABLE 3.16—Nickel-chromium alloy thermocouples.

|   | Geminal           | Thermo-Kanthal Special | Tophel II-Nial II                  | Chromel 3-G-345<br>Alumel 3-G-196 | Ni-Cr-Si/<br>Ni-Si             |
|---|-------------------|------------------------|------------------------------------|-----------------------------------|--------------------------------|
| <i>Nominal operating temperature range, in:</i>                             |                   |                        |                                    |                                   |                                |
| Reducing atmosphere (no hydrogen)   | 1205°C (2200°F)   | 1205°C (2200°F)        | 1205°C (2200°F)                    | 1205°C (2200°F)                   | 1205°C (2200°F)                |
| Wet hydrogen  | 1205°C (2200°F)   | 1205°C (2200°F)        | 1205°C (2200°F)                    | 1205°C (2200°F)                   | NR                             |
| Dry hydrogen  | 1205°C (2200°F)   | 1205°C (2200°F)        | 1205°C (2200°F)                    | 1205°C (2200°F)                   | 1205°C (2200°F)                |
| Inert atmosphere  | 1205°C (2200°F)   | 1205°C (2200°F)        | 1205°C (2200°F)                    | 1205°C (2200°F)                   | 1250°C (2280°F)                |
| Oxidizing atmosphere  | 1205°C (2200°F)   | 1205°C (2200°F)        | 1205°C (2200°F)                    | 1205°C (2200°F)                   | 1250°C (2280°F)                |
| Vacuum  | 1040°C (1904°F)   |                        | 1040°C (2000°F)                    | 1040°C (2000°F)                   | NR <sup>a</sup>                |
| Maximum short-time temperature  | 1260°C (2300°F)   | 1260°C (2300°F)        | 1260°C (2300°F)                    | 1260°C (2300°F)                   | 1300°C (2370°F)                |
| <i>Approximate microvolts per degree-Mean, over nominal operating range</i> |                   |                        |                                    |                                   |                                |
| At top temperature of normal range  | 18.7/°C (10.4/°F) | 22.6/°C (12.6/°F)      | 40. $\mu$ V/°C (22.5 $\mu$ V/°F)   | 40.7 $\mu$ V/°C (22.6 $\mu$ V/°F) | 37. $\mu$ V/°C (21 $\mu$ V/°F) |
|   | 22.2/°C (12.3/°F) | 20.0/°C (11.1/°F)      | 36 $\mu$ V/°C (20 $\mu$ V/°F)      | 36 $\mu$ V/°C (20 $\mu$ V/°F)     | 36 $\mu$ V/°C (20 $\mu$ V/°F)  |
| <i>Melting temperature, nominal:</i>  |                   |                        |                                    |                                   |                                |
| Positive thermocement   | 1400°C (2550°F)   | 1432°C (2610°F)        | 1430°C (2600°F)                    | 1430°C (2600°F)                   | 1410°C (2570°F)                |
| Negative thermocement   | 1430°C (2600°F)   | 1410°C (2570°F)        | 1400°C (2550°F)                    | 1400°C (2550°F)                   | 1340°C (2445°F)                |
| Stability with thermal cycling  | good              | good                   | good                               | good                              | good                           |
| High-temperature tensile properties   | good              | good                   | good                               | good                              | fair                           |
| Stability under mechanical working  | intermediate      | intermediate           | fair                               | fair                              | fair                           |
| Ductility (of most brittle thermocement) after use                          | good              | good                   | good                               | good                              | good                           |
| Resistance to handling contamination  | good              | good                   | good                               | good                              | good                           |
| <i>Recommended excitation wire:</i>   |                   |                        |                                    |                                   |                                |
| Positive conductor  | Geminal P         | Thermo-Kanthal P       | Tophel II or any Type K(+) Nial II | Chromel 3-G-345 or any Type K(+)  | Ni-Cr-Si                       |
| Negative conductor  | Geminal N         | Thermo-Kanthal N       |                                    | Alumel 3-G-196 and Type K(-)      | Ni-Si                          |

<sup>a</sup>NR = not recommended.

The temperature-emf curve is practically parallel to that of the conventional Type K thermocouple above 760°C (1400°F).

**3.3.4.1.2 Thermo-Kanthal special**—The Thermo-Kanthal special thermocouple was developed to give improved stability at temperatures between 982°C(1800°F) and 1260°C (2300°F) over that obtained with conventional base-metal thermocouple materials.

**3.3.4.1.3 Tophel II-Nial II**—

1. The Tophel II-Nial II thermocouple was developed for improved oxidation resistance and emf stability over the conventional Type K thermocouple alloys in both oxidizing and reducing atmospheres at elevated temperatures.

2. Tophel II, which is the positive thermoelement, is a nickel-10 percent chromium base alloy with additions to resist "green rot" attack in reducing atmospheres at elevated temperatures. The emf of Tophel II is within the standard tolerance of the conventional Type K positive thermoelement over the entire temperature range of 32 to 2300°F (0 to 1260°C). Tophel II can be matched with any acceptable Type K negative thermoelement to form a couple which is within the standard tolerance for the Type K thermocouple.

3. Nial II, which is the negative thermoelement, is a nickel-2.5 percent silicon base alloy with additions to improve the oxidation resistance and emf stability in an oxidizing atmosphere at elevated temperatures. The emf of Nial II is within the standard tolerance of the conventional Type K thermoelement between the range of 149 to 1260°C (300 to 2300°F). From 0 to 149°C (32 to 300°F), the Nial II is about 0.1 mV less negative than the conventional Type K negative thermoelement with reference to platinum.

4. The Tophel II-Nial II thermocouple meets the emf tolerances designated in ASTM Specification E 230 for the Type K thermocouple from 149 to 1093°C (300 to 2000°F). From 0 to 149°C (32 to 300°F), the Tophel II-Nial II thermocouple generates 0.1 mV (or 5 deg equivalent) less than the standard Type K thermocouple at the same temperature.

5. Tophel II-Nial II thermocouples can be used on existing instruments designed for the Type K thermocouples for temperatures sensing and control within the range of 149 to 1260°C (300 to 2300°F). If extension wire is needed, the negative extension wire should be Nial II, while the positive extension wire could either be Tophel II or any acceptable Type K (+) extension wire.

6. Through the improvements in both oxidation resistance and emf stability, Tophel II-Nial II thermocouples offers longer useful and total service life than conventional Type K thermocouples of the same size. As a corollary benefit, finer size Tophel II-Nial II thermocouples can be used to achieve equivalent or better stability than conventional Type K couples of larger sizes.

**3.3.4.1.4 Chromel 3-G-345-Alumel 3-G-196**—The Chromel 3-G-345-Alumel 3-G-196 thermocouple is designed to provide improved performance

under extreme environmental conditions where the conventional Type K thermocouple is subject to accelerated loss of stability.

More specifically, Chromel 3-G-345 is a Type K positive thermoelement in which the basic 10 percent chromium-nickel alloy is modified to give improved resistance to preferential chromium oxidation ("green rot"). At temperatures from 871 to 1038°C (1600 to 1900°F), conventional Type K positive thermoelements operating in marginally oxidizing environments are subject to embrittlement and loss of output as a result of such attack.

Under those conditions, Type K thermocouples employing Chromel 3-G-345 positive thermoelements offer greater stability than conventional Type K thermocouples. The usual precautions regarding protection of Type K thermocouples in corrosive environments apply to the special thermocouple as well.

The modified Chromel thermoelement meets the accepted curve of emf versus platinum for Type K positive thermoelements, within standard tolerances. It can be combined with either Alumel 3-G-196 or conventional Alumel to form Type K thermocouples meeting standard emf tolerances.

Alumel 3-G-196 is a Type K negative thermoelement of greatly improved oxidation resistance. It is suited to use in both reducing and oxidizing atmospheres, where its stability of output is especially advantageous in fine wire applications at high temperatures. It is nominally 2.5 silicon-nickel.

Alumel 3-G-196 meets the accepted curve of emf versus platinum for Type K negative thermoelements at all temperatures from 0 to 1260°C (32 to 2300°F). It can be combined with either Chromel 3-G-345 or regular Chromel to form thermocouples meeting standard Type K thermocouple tolerances over the entire range from 0 to 1260°C (32 to 2300°F).

Type K thermocouples employing either or both special thermoelements can be used with conventional extension wires at no sacrifice in guaranteed accuracy of the thermocouple-extension wire combination.

#### 3.3.4.1.5 *Nickel-Chromium-Silicon versus Nickel-Silicon—*

1. This combination resulted from many years of research in Australia and in the United States. Some of this work has been reported in NBS Monograph 161 [3].

2. The alloys in this combination have excellent resistance to preferential oxidation in the range 1000 to 1200°C.

3. The emf output differs from that of the Type K thermocouple but the curves have similar slopes over the elevated temperature range (see Fig. 3.9).

4. The short-term changes in the thermal emf outputs of 3.3 mm diameter nickel-chromium-silicon/nickel silicon and Type K thermocouples and of their individual thermoelements versus platinum on exposure in air at 1250°C are reported in NBS 161.

5. The long-term thermal emf drifts in 3.3 mm diameter nickel-chromium-silicon and Type K thermocouples and in their individual thermoelements versus platinum on exposure in air at 1000°C are also reported in NBS 161.



### 3.3.5 Nickel-Molybdenum Types

#### 3.3.5.1 20 Alloy and 19 Alloy<sup>10</sup> (nickel-nickel molybdenum alloys)—

1. The 20 Alloy/19 Alloy thermocouple was developed for temperature sensing and control applications at elevated temperatures in hydrogen or other reducing atmospheres. The emf table of the 20 Alloy versus the 19 Alloy does not conform to the Type K or any existing base metal thermocouples designated by ASTM Specification E 230.

2. The 19 Alloy, which is the negative thermoelement, is essentially a nickel-1 percent molybdenum alloy. Its emf versus platinum values are somewhat more negative than those of the Type K negative thermoelement within the range of 0 to 1260°C (32 to 2300°F).

3. The 20 Alloy, which is the positive thermoelement, is essentially a nickel-18 percent molybdenum alloy. Its emf versus platinum values are less positive within the range of 0 to 260°C (32 to 500°F) than the Type K positive thermoelement, but more positive within the range of 260 to 1260°C (500 to 2300°F). Figure 3.10 and Table 3.17 show the characteristics of these alloys.

4. The 20 Alloy/19 Alloy thermocouple, when properly sealed in a protection tube, offers excellent emf stability at elevated temperatures in hydrogen or other reducing atmospheres.

5. The oxidation resistance of the 20 Alloy/19 Alloy thermocouple is not good. The 20 Alloy/19 Alloy thermocouples are not recommended for use in an oxidizing atmosphere above 649°C (1200°F).

6. 20 Alloy/19 Alloy extension wire should be used in connection with the 20 Alloy/19 Alloy thermocouple.

### 3.3.6 Tungsten-Rhenium Types

There are three tungsten-rhenium thermocouple systems available—tungsten versus tungsten-26 percent rhenium, doped tungsten-3 percent rhenium versus tungsten-25 percent rhenium and doped tungsten-5 percent rhenium versus tungsten-26 percent rhenium. The price of the first combination has the lowest cost. All have been employed to 2760°C (5000°F), but general use is below 2316°C (4200°F). Applications for these couples have been found in space vehicles, nuclear reactors, and many high-temperature electronic, thermoelectric, industrial heating, and structural projects. However, when employed in a nuclear environment, the effect of transmutation of the thermal emf of the couples should be considered.

The use of tungsten in certain applications as the positive element may pose a problem, since heating tungsten to or above its recrystallization

<sup>10</sup>The 20 Alloy versus 19 Alloy thermocouple was developed by the General Electric Company. Since 1962 the Wilbur B. Driver Company has been the sole manufacturer of the 20 Alloy and the 19 Alloy.

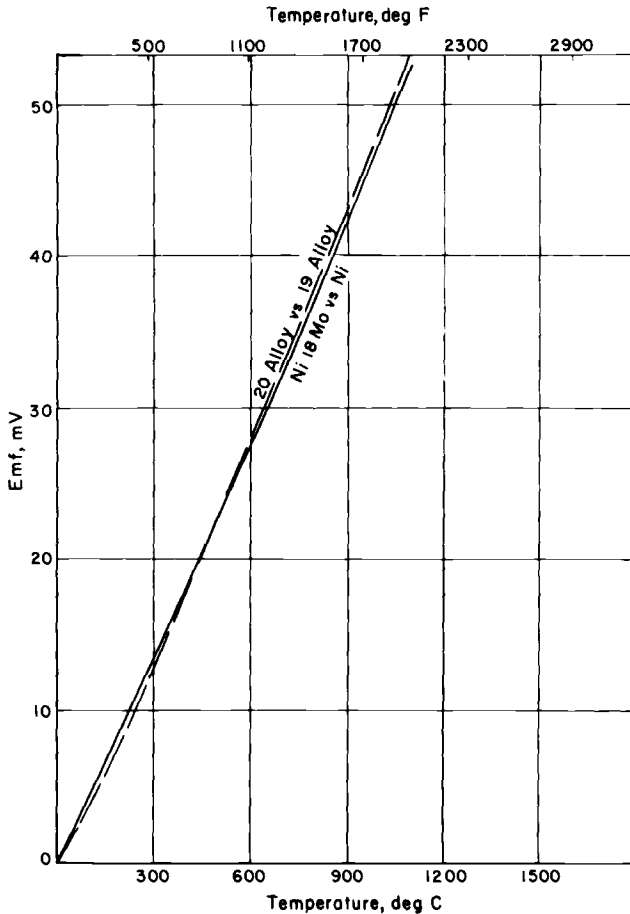


FIG. 3.10—Thermal emf of nickel versus nickel-molybdenum thermocouples.

temperature (approximately 1200°C) causes embrittlement resulting in loss of room-temperature ductility; an effect that is not experienced with the alloy leg containing high rhenium. With proper handling and usage this combination can be employed satisfactorily for long periods. One approach to the brittleness problem is to add rhenium to the tungsten thermoelement. Early research showed that the addition of 10 percent rhenium to the tungsten element did much to retain ductility after recrystallization. This much rhenium, however, greatly reduced the emf response for the thermocouple. Other techniques to retain room-temperature ductility are used by manufacturers; these include special processing and doping with the addition of 5 percent or less rhenium to the tungsten thermoelement.

Doping usually consists of using additives during the process of preparing

TABLE 3.17—Physical data and recommended applications of the 20 Alloy/19 Alloy thermocouples.

|  | 20 Alloy/19 Alloy   |
|--|---|
| <i>Nominal operating temperature range, in:</i>                          |   |
| Reducing atmosphere (nonhydrogen)  | 1205°C (2200°F)   |
| Wet hydrogen   | 1205°C (2200°F)   |
| Dry hydrogen   | 1205°C (2200°F)   |
| Inert atmosphere   | 1205°C (2200°F)   |
| Oxidizing atmosphere   | not recommended   |
| Vacuum   | 1205°C (2200°F)   |
| Maximum short time temperature   | 1260°C (2300°F)   |
| <i>Approximate microvolts per degree:</i>                                |   |
| Mean, over nominal operating range                                       | 55 $\mu\text{V}/^\circ\text{C}$ (31.0 $\mu\text{V}/^\circ\text{F}$ )                                      |
| At top temperature of normal range                                       | between the range of 1000 to 2300°F, 59 $\mu\text{V}/^\circ\text{C}$ (32.9 $\mu\text{V}/^\circ\text{F}$ ) |
| <i>Melting temperature, nominal:</i>                                     |   |
| Positive thermoelement   | 1430°C (2600°F)   |
| Negative thermoelement   | 1450°C (2640°F)   |
| General stability with thermal cycling (good, fair, poor)                | good  |
| High temperature tensile properties (good, fair, poor)                   | good  |
| Unaffected by mechanical working (good, fair, poor)                      | fair  |
| Ductility (of most brittle thermal element) after use (good, fair, poor) | fair  |
| Resistance to handling contamination (good, fair, poor)                  | good  |
| <i>Recommended extension wire:</i>                                       |   |
| Positive conductor   | 20 Alloy  |
| Negative conductor   | 19 Alloy  |

the tungsten powder and results in a unique microstructure in the finished wire. The additives essentially are eliminated during the subsequent sintering of the tungsten-rhenium powder compact. In fact, presently known analytical techniques do not disclose the presence of the additives above the background level of such substances normally present as impurities in non-doped tungsten or tungsten-rhenium alloys.

The emf response of tungsten-3 percent rhenium and tungsten-5 percent rhenium thermoelements used with thermoelements containing high percentages of rhenium is satisfactory. The thermoelectric power of the tungsten versus tungsten-26 percent rhenium, tungsten-3 percent rhenium versus tungsten-25 percent rhenium, and tungsten-5 percent rhenium versus tungsten-26 percent rhenium is comparable at lower temperatures, but drops off slightly for the latter two as the temperature is increased.

The tungsten thermoelement is not supplied to the user in a stabilized (recrystallized) condition; therefore, a small change in emf is encountered at the operating temperature. In the case of the doped tungsten-3 percent rhenium, doped tungsten-5 percent rhenium, tungsten-25 percent rhenium,

and tungsten-26 percent rhenium thermoelements, these are supplied in a stabilized (recrystallized) condition.

All three thermocouple combinations are supplied as matched pairs guaranteed to meet the emf output of producer developed tables within  $\pm 1$  percent. In addition, compensating extension wires are available for each of the three combinations with maximum service temperatures as high as  $871^{\circ}\text{C}$  ( $1600^{\circ}\text{F}$ ) for tungsten-5 percent rhenium versus tungsten-26 percent rhenium.

Important factors controlling the performance at high temperatures are: the diameter of the thermoelements (larger diameters are suitable for higher temperatures), the atmosphere (vacuum, high-purity hydrogen, or high-purity inert atmospheres required), the insulation, and sheath material. Some evidence is at hand, however, which indicates the possibility of selective vaporization of rhenium at temperatures of the order of  $1900^{\circ}\text{C}$  and higher when bare (unsheathed) tungsten-rhenium thermocouples are used in vacuum. For this reason, the vapor pressure of rhenium should be considered when a bare couple is used in a high vacuum at high temperatures. This, of course, is not a problem when these couples are protected with a suitable refractory metal sheath.

Figure 3.11 and Table 3.18 show the characteristics of these alloys.

### 3.4 Compatibility Problems at High Temperatures

In order for thermocouples to have a long life at high temperatures, it is necessary to limit reactions between the metals, the atmosphere, and the ceramic insulation. Such reactions may change the strength or corrosion-resistant properties of the alloys, the electrical output of the thermocouple, or the electrical insulation properties of the ceramic insulant.

At extremely high temperatures, reactions can be expected between almost any two materials. Table 3.19 has been included to show the temperatures at which such reactions occur between pairs of metallic elements. At lower temperatures, certain reactions do not occur and such as do occur, proceed at a slower rate. Because of potential reactions, it is important to identify the impurities and trace elements as well as the major constituents of the thermocouple components. The "free energy of formation" (Gibbs free energy) for the oxides of each element at the temperatures of interest, can be determined to predict possible oxide reactions. Other reactions may occur and attention should be given to the possible formation of the carbides, nitrides, etc. of the various elements.

Helpful data may be obtained from published reports, but, because of the importance of trace elements and impurities, the sources should be treated with caution. In some cases, the amount and types of impurities in the materials used were unknown.

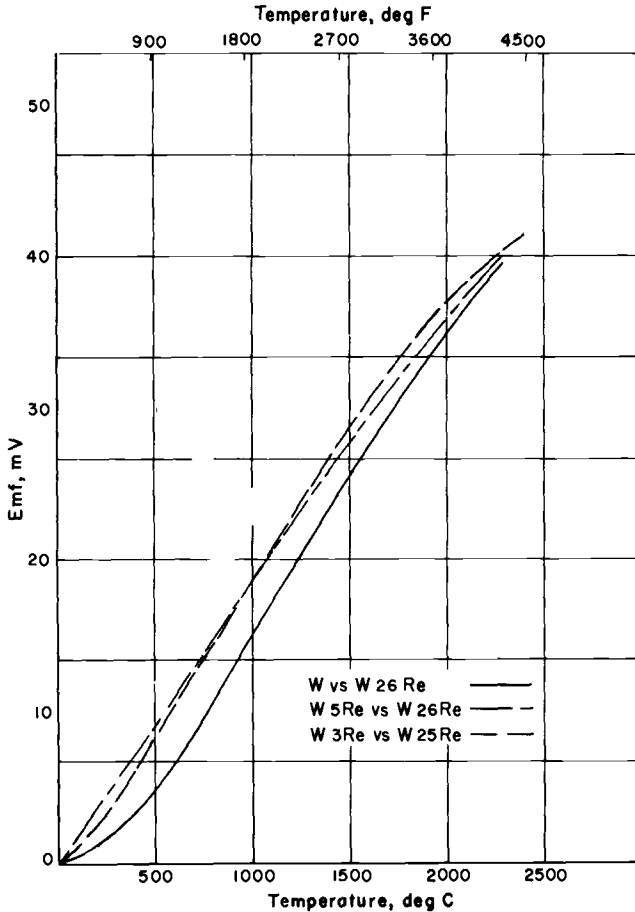


FIG. 3.11—*Thermal emf of tungsten-rhenium versus tungsten-rhenium thermocouples.*

Certain reactions may be somewhat self-limiting in that the reaction product provides a protective film against further reaction. However, spalling or chipping off of the reaction product may occur because of thermal or physical stress. Thus, the reaction rate and the use of the corrosion product as protection can be ascertained only if tested under the desired operating conditions and times.

The use of oxygen-gettering material should be considered in instances where oxygen is present in limited amounts [4]. This method has been employed with enclosed Type K thermocouples to limit the preferential oxidation of the positive thermoelement. A thin tube (or sliver) of titanium at the hottest location of the thermocouple has been used.

TABLE 3.18—Tungsten-rhenium thermocouples.

|   | W Versus W-26 Re | W-3Re Versus W-25 Re                                     | W-5Re Versus W-26 Re                                     |
|---|------------------|--|--|
| <i>Nominal operating temperature range, in:</i>                   |                  |  |  |
| Reducing atmosphere (nonhydrogen)                                 | NR <sup>a</sup>  | NR   | NR   |
| Wet hydrogen  | NR               | NR   | NR   |
| Dry hydrogen  | 2760°C (5000°F)  | 2760°C (5000°F)  | 2760°C (5000°F)  |
| Inert atmosphere  | 2760°C (5000°F)  | 2760°C (5000°F)  | 2760°C (5000°F)  |
| Oxidizing atmosphere  | NR               | NR   | NR   |
| Vacuum <sup>b</sup>   | 2760°C (5000°F)  | 2760°C (5000°F)  | 2760°C (5000°F)  |
| Maximum short-time temperature                                    | 3000°C (5430°F)  | 3000°C (5430°F)  | 3000°C (5430°F)  |
| <i>Approximate microvolts per degree:</i>                         |                  |  |  |
| Mean, over nominal operating range 0°C to 2316°C (32°F to 4200°F) | 16.7/°C (9.3/°F) | 17.1/°C (9.5/°F)   | 16.0/°C (8.9/°F)   |
| At top temperature of normal range 2316°C (4200°F)                | 12.1/°C (6.7/°F) | 9.9/°C (5.5/°F)  | 8.8/°C (4.9/°F)  |
| <i>Melting temperature, nominal:</i>                              |                  |  |  |
| Positive thermoelement  | 3410°C (6170°F)  | 3360°C (6080°F)  | 3350°C (6062°F)  |
| Negative thermoelement  | 3120°C (5648°F)  | 3120°C (5648°F)  | 3120°C (5648°F)  |
| Stability with thermal cycling                                    | good             | good   | good   |
| High-temperature tensile properties                               | good             | good   | good   |
| Stability under mechanical working                                | fair             | fair   | fair   |
| Ductility (of most brittle thermoelement after use)               | poor             | poor to good depending on atmosphere or degree of vacuum | poor to good depending on atmosphere or degree of vacuum |
| Resistance to handling contamination                              | good             | good   | good   |
| Extension wire  | available        | available  | available  |

<sup>a</sup>NR = not recommended.

<sup>b</sup>Preferential vaporization of rhenium may occur when bare (unshathed) couple is used at high temperatures and high vacuum. Check vapor pressure of rhenium at operating temperature and vacuum before using bare couple.

TABLE 3.19.—Minimum melting temperatures of binary systems.<sup>a</sup>

| Element           | W     | Re    | Os    | Ta    | Mo    | Ir    | Cb    | Ru    | Hf   | Rh    | V     | Cr    | Zr    | Pt    | Ti   | Fe    | Co    | Ni   | Si   |
|-------------------|-------|-------|-------|-------|-------|-------|-------|-------|------|-------|-------|-------|-------|-------|------|-------|-------|------|------|
| Melting Point, °F | 6170  | 5724  | 5432  | 5423  | 4730  | 4428  | 4425  | 4082  | 4030 | 3560  | 3452  | 3407  | 3353  | 3224  | 3034 | 2802  | 2723  | 2651 | 2588 |
| <i>Element:</i>   |       |       |       |       |       |       |       |       |      |       |       |       |       |       |      |       |       |      |      |
| Si                | 2550  | -2057 |       | 2525  | -2570 | 2588  | 2372  |       |      |       | -2550 | -2408 | -2480 | 1526  | 2426 | 2192  | 2183  | 1770 |      |
| Ni                | -2651 | 2651  |       | 2480  | -2398 |       | 2145  | 2651  | 2102 |       | 2198  | 2444  | -1764 | -2651 | 1727 | 2588  | -2646 |      |      |
| Co                | -2696 | -2723 | -2723 | 2331  | 2444  | -2460 | 2255  | -2550 | 2214 | -2550 | 2264  | 2552  | 1789  | -2590 | 1860 | -2696 |       |      |      |
| Fe                | 2775  | -2802 |       | -2462 | 2624  |       | 2480  | 2802  | 2372 | -2750 | 2675  | 2743  | 1705  | -2730 | 1985 |       |       |      |      |
| Ti                | -3034 | -3034 |       | -3034 | -3034 | 2687  | -3034 |       | 2985 |       | -2777 | 2525  | -2876 | 2390  |      |       |       |      |      |
| Pt                | -3224 | -3224 |       | 3224  | 3224  | -3224 | -3092 |       |      | -3224 |       | 2552  | 2165  |       |      |       |       |      |      |
| Zr                | -3020 | 2912  |       | 3308  | 2740  |       | 3164  | 2453  | 3353 |       | 2246  | -2372 |       |       |      |       |       |      |      |
| Cr                | 3038  | 3407  |       | 3092  | 3360  |       | 3020  |       |      |       | 3182  |       |       |       |      |       |       |      |      |
| V                 | 2974  | 3452  |       | 3308  | 3452  |       | 3290  |       |      |       |       |       |       |       |      |       |       |      |      |
| Rh                |       |       |       |       | 3524  |       |       |       |      |       |       |       |       |       |      |       |       |      |      |
| Hf                | 3488  | -3416 |       |       | 3506  |       |       |       |      |       |       |       |       |       |      |       |       |      |      |
| Ru                | 4001  |       |       | 3578  | 3533  |       |       |       |      |       |       |       |       |       |      |       |       |      |      |
| Cb                | -4425 | 4415  |       | -4425 | -4250 |       | 3056  |       |      |       |       |       |       |       |      |       |       |      |      |
| Ir                | -4730 | 4424  | -4406 | -4730 |       |       |       |       |      |       |       |       |       |       |      |       |       |      |      |
| Mo                |       |       |       |       |       |       |       |       |      |       |       |       |       |       |      |       |       |      |      |
| Ta                | -5423 | 4874  | -4388 |       |       |       |       |       |      |       |       |       |       |       |      |       |       |      |      |
| Os                | 4937  |       |       |       |       |       |       |       |      |       |       |       |       |       |      |       |       |      |      |
| Re                | -5070 |       |       |       |       |       |       |       |      |       |       |       |       |       |      |       |       |      |      |

<sup>a</sup> Adapted from: *Constitution of Binary Alloys* by Rodney P. Elliott, McGraw-Hill, New York, 1965.

### 3.5 References

- [1] Moffat, R. J., "Understanding Thermocouple Behavior: The Key to Precision," Paper 68-628, Instrument Society of America, Vol. 5, Oct. 1968.
- [2] Caldwell, F. R., "Thermocouple Materials," NBS Monograph 40, National Bureau of Standards, 1 March 1962.
- [3] NBS Monograph 161, National Bureau of Standards.
- [4] Neswald, R. G., "Titanium for Realists," *Space/Aeronautics*, Vol. 48, No. 5, Oct. 1967, pp. 90-99.



# Chapter 4—Typical Thermocouple Designs and Applications

---

A complete thermocouple temperature sensing assembly, in accordance with the present state of the art, consists of one or more of the following:

*A. Sensing Element Assembly*—In its most basic form this assembly includes two dissimilar wires, supported or separated or both by electrical insulation and joined at one end to form a measuring junction. Such assemblies usually fall into one of three categories; (1) those formed from wires having nonceramic insulation, (2) those with hard-fired ceramic insulators, and (3) those made from sheathed, compacted ceramic-insulated wires. This chapter will deal only with the first two. See Chapter 5 for complete details on the latter.

*B. Protecting Tube*—Ceramic and metal protecting tubes serve the purpose of protecting the sensing element assembly from the deleterious effects of hostile atmospheres and environments. In some cases, two concentrically arranged protecting tubes may be used. The one closest to the sensing element assembly is designated the primary protecting tube, while the outer tube is termed the secondary protecting tube. Combinations such as an aluminum oxide primary tube and a silicon carbide secondary tube often are used to obtain the beneficial characteristics of the combination, such as resistance to cutting flame action and ability to resist thermal and mechanical shock.

*C. Thermowell*—More critical or demanding applications may require the use of specially machined and drilled solid bar stock called thermowells for not only protection of the thermocouple, but also to withstand high pressure or stresses or erosion or both caused by material flows within containment vessels. These drilled wells, as they are sometimes called, are machined to close tolerances, and highly polished to inhibit corrosion.

*D. Terminations*—Sensing element assembly wire terminations are made to:

- (a) Terminals (usually screw type)
- (b) Connection head
  - 1. General purpose type
  - 2. Screw cover type
  - 3. Open type

- (c) Plug and jack quick-disconnect
- (d) Military standard (MS) type of connector
- (e) Miscellaneous connection devices such as crimp-on sleeves, transition fittings filled with epoxy or other potting materials, and so on.

*E. Miscellaneous Hardware*—These include:

- (a) Pipe nipple or adapter—to join the protecting tube to the head
- (b) Thermocouple gland—used primarily with sheathed, compacted ceramic-insulated thermocouple assemblies to serve the dual function of mounting and sealing-off pressure in the mounting hole (see Chapter 5). Such glands may also be used with small protecting tubes.
- (c) Threaded bushing—welded or brazed to the protecting tube and screwed into the mounting hole.

#### 4.1 Sensing Element Assemblies

Typical thermocouple element assemblies, shown in Fig. 4.1, A and B, illustrate common methods of forming the measuring junction, A—by twisting and welding (twisting provides added strength), and B—by butt-welding. C shows an assembly using nonceramic insulation such as asbestos or fiber glass. New ceramic fibers are available which extend the upper temperature limits of this form of insulation. D, E, and F show the use of various forms of hard fired ceramic insulators, double bore (D) fish-spine or ball and socket (E) and four-hole (F). Fish-spine provides flexibility, and four-hole provides for two independent sensing elements.

#### 4.2 Nonceramic Insulation

The normal function of thermocouple insulation is to provide electrical separation for the thermoelements. If this function is not provided or is compromised in any way, the indicated temperature may be in error. Insulation is affected adversely by moisture, abrasion, flexing, temperature extremes, chemical attack, and nuclear radiation. Each type of insulation has its own limitations. A knowledge of these limitations is essential, if accurate and reliable measurements are to be made.

Some insulations have a natural moisture resistance. Teflon, polyvinyl chloride (PVC), and some forms of polyimides are examples of this group. With the fiber type insulations, moisture protection results from impregnating with substances such as wax, resins, or silicone compounds. Protection from abrasion and flexing is also generally provided by impregnating materials. However, one cycle over their rated temperatures will result in a deterioration of this protection. Once the impregnating materials have been

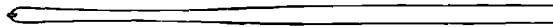
exposed to temperatures at which they vaporize there is no longer moisture or mechanical protection.

The moisture penetration problem is not confined to the sensing end of the thermocouple assembly. For example, if the thermocouple passes through hot or cold zones or through an area which becomes alternately hot and cold, condensation may produce errors in the indicated temperature, unless adequate moisture resistance is provided.

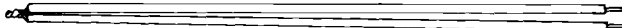
After exposure to temperatures exceeding the limitations of the insulation, whole sections of the insulation can fall away resulting in bare wire and a possible "short." Thermocouples in this condition should not be used if any flexing or abrasion is expected. It is recommended that they be discarded or that the exposed portion of the thermocouple assembly be cut off and the measuring junction reformed.



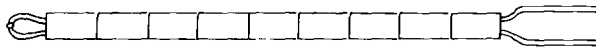
A. Bare thermocouple element, twisted and welded.



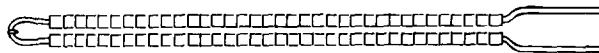
B. Butt-welded thermocouple element.



C. Thermocouple element, twisted and welded with asbestos insulation.



D. Butt-welded thermocouple element with double-bore insulators.



E. Butt-welded thermocouple element with fish-spine insulators.



F. Two butt-welded thermocouple elements with 4-hole insulators.

FIG. 4.1—Typical thermocouple element assemblies.

Insulations are rated for a maximum temperature both for continuous usage and for a single exposure. It is imperative to observe the limits when selecting an insulating material. At elevated temperatures even those insulations which remain physically intact may become conductive. Under these conditions, the output of the thermocouple may be a function of the highest temperature to which the insulation is exposed, rather than the temperature of the measuring junction. The change in insulation resistance may be permanent if caused by deterioration of organic insulants or binders which leave a carbon residue. In considering the temperature to which the insulation is exposed, it should not be assumed that this is the temperature of the measuring junction. A thermocouple may be attached to a massive specimen which is exposed to a high-temperature source to achieve a rapid heating rate. Parts of the thermocouple wires not in thermal contact with the specimen can be overheated severely while the junction remains within safe temperature limits. With this in mind, high quality insulation should be used when rapid heating rates are expected. Very little factual information is available on actual deterioration rates and magnitudes, but the condition is real, so a conservative approach is a requisite of good engineering practice.

The basic types of flexible insulations for elevated temperature usage are fiber glass, fibrous silica, and asbestos.<sup>1</sup> Of the three materials, fibrous silica has the best high-temperature electrical properties, but, because this insulation normally is not impregnated, its handling and abrasion characteristics leave something to be desired. The next best high-temperature insulation is asbestos. Because this material has very poor mechanical properties a carrier fiber or an impregnating material is added. In some instances, this carrier is cotton or another organic compound which leaves a carbon residue after exposure to a temperature at which it burns. This results in a breakdown of electrical insulation. Asbestos loses its mechanical strength after exposure to elevated temperatures and may break away from the wire with little or even no handling. A more commonly used insulation is fiber glass. It can be impregnated to provide improved moisture and mechanical characteristics within the temperature limitations of the impregnating compound. The most frequently used type of fiber glass has an upper temperature limit of approximately 500°C (900°F) for continuous use. If one is willing to sacrifice the handling characteristics, nonimpregnated fiber glass insulations are available which withstand higher temperatures.

Modern technology has led to the development of ceramic fibers which markedly increase the upper use temperature of flexible insulations. These insulations, if properly applied and handled, will allow base metal thermocouples to be used to their upper use temperatures within their limits of exposure to the environment in which they are placed. For example, Type

<sup>1</sup> Asbestos can be hazardous to health. Proper precaution should be exercised in its use.

K thermocouples can be exposed to their stated upper temperature limit, and be adequately insulated provided the environmental factors do not otherwise affect the serviceability of the insulation. The same precautions must be observed with these thermocouples as with any other thermocouple installation. The user must be knowledgeable about his application and the materials which he intends to use. These extremely high-temperature insulations should be employed without impregnants for maximum temperature service.

Chemical deterioration of insulation materials can produce a number of problems. If the environment reacts with the insulation, both the insulation and environment can be affected adversely. The insulation can be removed easily or become electrically conductive, and the process system can become contaminated. For example, some insulation materials are known to cause cracking in austenitic stainless steels.

In summary, an insulation should be selected only after considering possible exposure temperatures and heating rates, the number of temperature cycles, mechanical movement, moisture, routing of the thermocouple wire, and chemical deterioration (see Table 4.1).

Industry has established insulation color codes for standardized letter-designated thermocouple and extension wire types, as shown in Table 4.2.

### 4.3 Hard-Fired Ceramic Insulators

Hard-fired ceramic insulators most commonly used with bare thermocouple elements are mullite, aluminum oxide, and steatite, the latter being the most common material where fish-spine insulators are concerned. Single, double, and multibore insulators are available in a wide variety of sizes in both English and metric dimensions. Lengths commonly stocked by many suppliers are 1, 2, 3, 6, 12, 18, 24, and 36 in. Lengths to 72 in. are available on special order. The longer these insulators become, the more susceptible they are to breakage, so care must be exercised in handling.

It is advisable, especially in the case of precious metal thermocouple element assemblies, to keep the insulator in one piece to minimize contamination from the environment.

Hard-fired ceramic insulators are made in oval as well as circular cross-section examples of which are shown in Fig. 4.2. Properties of refractory oxides are tabulated in Table 4.3.

### 4.4 Protecting Tubes, Thermowells, and Ceramic Tubes

#### 4.4.1 Factors Affecting Choice of Protection for Thermocouples

Thermocouples must be protected from atmospheres that are not compatible with the thermocouple alloys. Protecting tubes serve the double

TABLE 4.1—Insulation characteristics.

| Insulation   | Continuous Use Temperature Limit, °C (°F) | Single Exposure Temperature Limit, °C (°F) | Moisture Resistance                            | Abrasion Resistance                |
|--|---|--|--|------------------------------------|
| Cotton   | 95 (200)                                  | 95 (200)                                   | poor   | fair                               |
| Polyvinyl  | 105 (220)                                 | 105 (220)                                  | excellent                                      | good                               |
| Enamel and cotton  | 95 (200)                                  | 95 (200)                                   | fair   | fair                               |
| Nylon  | 125 (260)                                 | 125 (260)                                  | poor   | good                               |
| Teflon <sup>d</sup>  | 205 (400)                                 | 315 (600)                                  | excellent                                      | good                               |
| Polyimide  | 315 (600)                                 | 400 (750)                                  | excellent                                      | good                               |
| Teflon and fiber glass <sup>b</sup>                                | 315 (600)                                 | 370 to 540                                 | excellent                                      | good                               |
| Fiber glass-varnish or silicone impregnation <i>E</i> <sup>c</sup> | 480 (900)                                 | (700 to 1000)                              | to 600°F<br>fair to 400°F, poor<br>above 400°F | fair to 400°F, poor<br>above 400°F |
| Fiber glass, nonimpregnated <i>S</i> <sup>d</sup>                  | 540 (1000)                                | 650 (1200)                                 | poor   | fair                               |
| Asbestos and fiber glass with silicone <sup>e</sup>                | 480 (900)                                 | 650 (1200)                                 | fair to 400°F                                  | fair to 400°F, poor<br>above 400°F |
| Felted asbestos  | 540 (1000)                                | 650 (1200)                                 | poor   | poor                               |
| Asbestos over asbestos   | 540 (1000)                                | 650 (1200)                                 | poor   | poor                               |
| Refrasil <sup>f</sup>  | 870 (1600)                                | 1100 (2000)                                | very poor                                      | very poor                          |
| Ceramic fibers (for example, Nextel <sup>g</sup> )                 | 1000 (1830)                               | 1370 (2500)                                | very poor                                      | poor                               |

<sup>a</sup> Trademark of the E. I. duPont de Nemours & Co.

<sup>b</sup> The Teflon vaporizes at 315°C (600°F) with possible toxic effects.

<sup>c</sup> *E* = electrical grade fiber glass.

<sup>d</sup> *S* = structural grade fiber glass.

<sup>e</sup> Individual wires are asbestos and overbraid is fiber glass.

<sup>f</sup> Trademark of the H. I. Thompson Co.

<sup>g</sup> Trademark of the 3M Corp.

TABLE 4.2—Color code of thermocouple and extension wire insulations.

| Thermocouple Wire |                       |        | Thermocouple Extension Wire |                       |        |
|-------------------|-----------------------|--------|-----------------------------|-----------------------|--------|
| Symbol            | Insulation Color Code |        | Symbol                      | Insulation Color Code |        |
|                   | Single                | Duplex |                             | Single <sup>b</sup>   | Duplex |
| E                 |                       | brown  | EX                          |                       | purple |
| EP                | purple                |        | EPX                         | purple                |        |
| EN                | red                   |        | ENX                         | red with purple trace |        |
| J                 |                       | brown  | JX                          |                       | black  |
| JP                | white                 |        | JPX                         | white                 |        |
| JN                | red                   |        | JNX                         | red with white trace  |        |
| K                 |                       | brown  | KX                          |                       | yellow |
| KP                | yellow                |        | KPX                         | yellow                |        |
| KN                | red                   |        | KNX                         | red with yellow trace |        |
| T                 |                       | brown  | TX                          |                       | blue   |
| TP                | blue                  |        | TPX                         | blue                  |        |
| TN                | red                   |        | TNX                         | red with blue trace   |        |
| B                 | ... <sup>a</sup>      |        | BX                          |                       | gray   |
| BP                | ... <sup>a</sup>      |        | BPX                         | gray                  |        |
| BN                | ... <sup>a</sup>      |        | BNX                         | red with gray trace   |        |
| R                 | ... <sup>a</sup>      |        | RX                          |                       | green  |
| RP                | ... <sup>a</sup>      |        | RPX                         | black                 |        |
| RN                | ... <sup>a</sup>      |        | RNX                         | red with black trace  |        |
| S                 | ... <sup>a</sup>      |        | SX                          |                       | green  |
| SP                | ... <sup>a</sup>      |        | SPX                         | black                 |        |
| SN                | ... <sup>a</sup>      |        | SNX                         | red with black trace  |        |

NOTE—For a more complete explanation of color codes see ANSI MC96.1

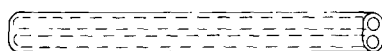
<sup>a</sup>Normally noble metal thermocouples are not insulated with colored insulations. However, if they were, the color codes of the extension wire singles but with brown duplex would apply.

<sup>b</sup>The trace colors are recommended when duplex coverings are not present, but optional when duplex coverings are applied.

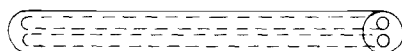
purpose of guarding the thermocouple against mechanical damage and interposing a shield between the thermocouple and its surroundings so as to maintain it as nearly as possible in its best working environment.

The conditions that must be excluded are: (a) metals (solid, liquid, or vapor) which, coming into contact with the thermocouple, would alter its chemical composition; (b) furnace gases and fumes which may attack the thermocouple materials (sulphur and its compounds are particularly deleterious); (c) materials such as silica and some of its metallic oxides, which, in contact with the thermocouple in a reducing atmosphere, are reduced, and combine with the thermocouple to attack it; and (d) electrolytes which would attack the thermocouple material.

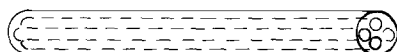
The choice of the proper protecting tube is governed by the conditions of use and by the tolerable life of the thermocouple. On many occasions the strength of the protecting tube may be more important than the long-term thermoelectric stability of the thermocouple. On the other hand, gas tight-



Oval Double Bore Insulator



Round Double Bore Insulator



Round Four Bore Insulator

FIG. 4.2—Cross-section examples of oval and circular hard-fired ceramic insulators.

ness and resistance to thermal shock may be of paramount importance. In other cases, chemical compatibility of the protecting tube with the process may be the deciding factor. The problem of “green-rot” discussed in Section 3.1.1 also should be considered. In short, careful consideration must be given to each unique application.

As important as proper selection of the material is the cleanliness of the inside of the tube. Foreign matter, especially sulphur bearing compounds, can seriously affect the serviceability of the thermocouple as well as the tube itself.

#### 4.4.2 Common Methods of Protecting Thermocouples

**4.4.2.1 Protecting Tubes**—By proper selection of material, metal protecting tubes can offer adequate mechanical protection for base metal thermocouples up to 1150°C (2100°F) in oxidizing atmospheres. It must be remembered that all metallic tubes are somewhat porous at temperatures exceeding 815°C (1500°F), so that, in some cases, it may be necessary to provide an inner tube of ceramic material otherwise damaging gaseous vapors may enter the tube and attack the thermocouple.

Typical use temperatures for protecting tubes are given next. These should be used only as a guide with careful selection of the proper material for each application.

(a) Carbon steels can be used to 540°C (1000°F) in oxidizing the atmospheres, and considerably higher if protected.



TABLE 4.3—Properties

|   | Composition   | Porosity, volume % | Fusion Temperature, °C | Maximum Normal Use Temperature, °C | Density, Bulk (b), True (t), g/cm <sup>3</sup> |
|---|---|--------------------|------------------------|------------------------------------|--|
| Sapphire crystal                                | 99.9 Al <sub>2</sub> O <sub>3</sub>   | 0                  | 2030                   | 1950                               | 3.97(t)  |
| Sintered alumina                                | 99.8 Al <sub>2</sub> O <sub>3</sub>   | 3 to 7             | 2030                   | 1900                               | 3.97(t)  |
| Sintered beryllia                               | 99.8 BeO  | 3 to 7             | 2570                   | 1900                               | 3.03(t)  |
| Sintered calcia                                 | 99.8 CaO  | 5 to 10            | 2600                   | 2000                               | 3.32(t)  |
| Chrome-alumina cermet<br>(Haynes Stellite LT-1) | 77 Cr, 23 Al <sub>2</sub> O <sub>3</sub>  | 2                  | 1850                   | 1300                               | 5.9(b)   |
| Sintered magnesia                               | 99.8 MgO  | 3 to 7             | 2800                   | 1900                               | 3.58(t)  |
| Sintered mullite                                | 72 Al <sub>2</sub> O <sub>3</sub> , 28 SiO <sub>2</sub>                                       | 3 to 10            | 1810                   | 1750                               | 3.03(t)  |
| Sintered forsterite                             | 99.5 Mg <sub>2</sub> SiO <sub>4</sub>   | 4 to 12            | 1885                   | 1750                               | 3.22(t)  |
| Sintered spinel                                 | 99.8 MgAl <sub>2</sub> O <sub>4</sub>   | 3 to 10            | 2135                   | 1850                               | 3.58(t)  |
| Sintered titania                                | 99.5 TiO <sub>2</sub>   | 3 to 7             | 1840                   | 1600                               | 4.24(t)  |
| Sintered thoria                                 | 99.8 ThO <sub>2</sub>   | 3 to 7             | 3050                   | 2500                               | 10.50(t)                                       |
| Sintered yttria                                 | 99.8 Y <sub>2</sub> O <sub>3</sub>  | 2 to 5             | 2410                   | 2000                               | 4.50(t)  |
| Sintered urania                                 | 99.8 UO <sub>2</sub>  | 3 to 10            | 2800                   | 2200                               | 10.96(t)                                       |
| Sintered stabilized<br>zirconia                 | 92 ZrO <sub>2</sub> , 4 HfO <sub>2</sub> ,<br>4 CaO   | 3 to 10            | 2550                   | 2200                               | 5.6(t)   |
| Sintered zircon                                 | 99.5 ZrSiO <sub>4</sub>   | 5 to 15            | 2420                   | 1800                               | 4.7(t)   |
| Silica glass                                    | 99.8 SiO <sub>2</sub>   | 0                  | 1710                   | 1100                               | 2.20(t)  |
| Mullite porcelain                               | 70 Al <sub>2</sub> O <sub>3</sub> , 27 SiO <sub>2</sub> ,<br>3 Mo + M <sub>2</sub> O          | 2 to 10            | 1750                   | 1400                               | 2.8(b)   |
| High alumina porcelain                          | 90-95 Al <sub>2</sub> O <sub>3</sub> , 4-7 SiO <sub>2</sub> ,<br>1 to 4 Mo + M <sub>2</sub> O | 2 to 5             | 1800                   | 1500                               | 3.75(b)  |

<sup>a</sup> Kingery, W. D., "Oxides for High Temperature Applications," *Proceedings of the International Symposium on High Temperature Technology*, McGraw-Hill, New York, 1960.

(b) Austenitic stainless steels (AISI 300 series) can be used to 870°C (1600°F), in oxidizing atmospheres. Types 316, 317, and 318 can be used in some reducing atmospheres.

(c) Ferritic stainless steels (AISI 400 series) can, with proper selection, be used as high as 1093°C (2000°F) in both oxidizing and reducing atmospheres. Martensitic types (AISI 400 series), by contrast, are limited to lower temperatures for continuous use, with the top temperature being about 675°C (1250°F) for Type 410 stainless.

(d) High-nickel alloys, Nichrome,<sup>2</sup> Inconel,<sup>3</sup> etc., can be used to 1150°C (2100°F) in oxidizing atmospheres.

<sup>2</sup>Trademark of the Driver-Harris Company.

<sup>3</sup>Trademark of the International Nickel Company.

of refractory oxides.<sup>a</sup>

| Specific Heat Capacity (cal/g/°C) 20 to 1000°C | Linear Expansion (10 <sup>-6</sup> in./in./°C) 20 to 1000°C | Thermal Conductivity (cal s <sup>-1</sup> C <sup>-1</sup> cm <sup>-2</sup> cm) |           | Modulus of Rupture, psi |                | Modulus of Elasticity, 10 <sup>6</sup> psi | Thermal Stress Resistance |
|--|---|--|-----------|-------------------------|----------------|--|---------------------------|
|  |   | At 100°C   | At 1000°C | At 20°C                 | At 1000°C      |  |                           |
| 0.26   | 8.6   | 0.072  | 0.019     | 40 000-150 000          | 30 000-100 000 | 55   | very good                 |
| 0.26   | 8.6   | 0.069  | 0.014     | 30 000                  | 22 000         | 53   | good                      |
| 0.50   | 8.9   | 0.500  | 0.046     | 20 000                  | 10 000         | 45   | excellent                 |
| 0.23   | 13.0  | 0.033  | 0.017     | ...                     | ...            | ...  | fair-poor                 |
| 0.16   | 8.9   | 0.08   | 0.05      | 45 000                  | 20 000         | 37.5                                       | excellent                 |
| 0.25   | 13.5  | 0.082  | 0.016     | 14 000                  | 12 000         | 30.5                                       | fair-poor                 |
| 0.25   | 5.3   | 0.013  | 0.008     | 12 000                  | 7 000          | 21   | good                      |
| 0.23   | 10.6  | 0.010  | 0.005     | 10 000                  | ...            | ...  | fair-poor                 |
| 0.25   | 8.8   | 0.033  | 0.013     | 12 300                  | 11 000         | 34.5                                       | fair                      |
| 0.20   | 8.7   | 0.015  | 0.008     | 8 000                   | 6 000          | ...  | fair-poor                 |
| 0.06   | 9.0   | 0.022  | 0.007     | 12 000                  | 7 000          | 21   | fair-poor                 |
| 0.13   | 9.3   | (0.02)   | ...       | ...                     | ...            | ...  | fair-poor                 |
| 0.06   | 10.0  | 0.020  | 0.007     | 12 000                  | 18 000         | 25   | fair-poor                 |
| 0.14   | 10.0  | 0.005  | 0.005     | 20 000                  | 15 000         | 22   | fair-good                 |
| 0.16   | 4.2   | 0.015  | 0.008     | 12 000                  | 6 000          | 30   | good                      |
| 0.18   | 0.5   | 0.004  | 0.012     | 15 500                  | ...            | 10.5                                       | excellent                 |
| 0.25   | 5.5   | 0.007  | 0.006     | 10 000                  | 6 000          | 10   | good                      |
| 0.26   | 7.8   | 0.05   | 0.015     | 50 000                  | ...            | 53   | very good                 |

As with carbon steels, the stainless steels and other alloy steels used for protecting tubes can be exposed to higher temperatures if properly protected.

The majority of metal protecting tubes are made from pipe sized tubing, cut to the proper length, and threaded on one end for attachment of the terminal head. The other end is closed by welding using a filler metal which is the same as the parent metal.

**4.4.2 Thermowells**—Where the thermocouple assembly is subject to high-pressure or flow-induced stresses or both, a drilled thermowell often is recommended. Although less expensive metal tubes, fabricated by plugging the end may satisfy application requirements, more stringent specifications usually dictate the choice of gun-drilled bar stock, polished and hydrostatically tested as a precaution against failure.

Examples of drilled thermowells are shown in Fig. 4.3.

**4.4.2.3 Ceramic Tubes**—Ceramic tubes are used usually at temperatures beyond the ranges of metal tubes although they are sometimes used at lower temperatures in atmospheres harmful to metal tubes.

The ceramic tube most widely used has a mullite base with certain additives to improve the mechanical and thermal shock properties. The upper temperature limit is 1650°C (3000°F).

Silicon carbide tubes are used as secondary protecting tubes. This material resists the cutting action of flames. It is not impermeable to gases and, where a dense tube is required, a nitride-bonded type material can be obtained with greatly reduced permeability.

Fused alumina tubes can be used as primary or secondary protecting tubes or both where temperatures to 1900°C (3450°F) are expected and a gas tight tube is essential. Fused alumina tubes and insulators should be used with platinum-rhodium/platinum thermocouples above 1200°C (2200°F) in order to ensure long life and attain maximum accuracy. The mullite types contain impurities which can contaminate platinum above

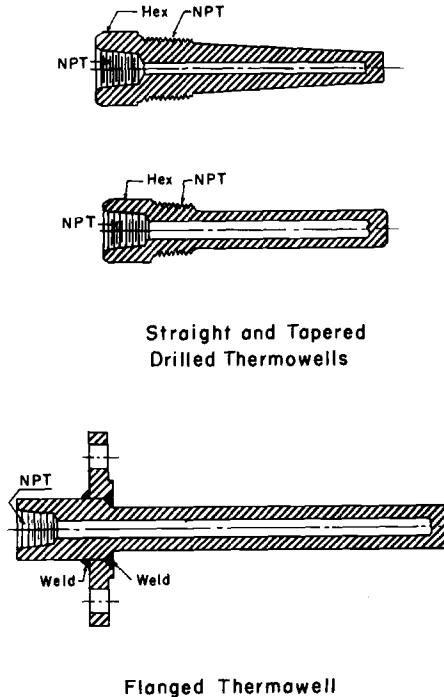


FIG. 4.3—Examples of drilled thermowells.

1200°C (2200°F). The alumina tubes are more expensive than the mullite base tubes but can be obtained impervious to most gases to 1815°C (3300°F).

**4.4.2.4 Metal-Ceramic Tubes**—“Cermets” are combinations of metals and metallic oxides which, after proper treatment, form dense, high-strength, corrosion-resistant tubes and are available for use to about 1425°C (2600°F) in most atmospheres.

## 4.5 Circuit Connections

To reduce costs and provide suitable insulation in the low-temperature parts of the thermocouple circuit, extension wire (see Section 3.2) is often used to extend the circuit to the measuring instrument. The intermediate junction between the thermocouple and extension wires must be held below the upper temperature limit of the extension wires (see Table 4.2) or considerable errors may be introduced.

Sheathed, mineral-insulated thermocouples can incorporate a transition fitting within which the extension wires are welded or brazed to the thermocouple wires. Where hard-fired ceramic insulators are used, the thermocouple wires usually terminate in a “head” which is attached to the insulator or to the protecting tube in which the insulator is housed. The interconnections are made by clamps or binding posts to permit easy replacement of the thermocouple. One assumes in such a component that, if a third metal is introduced into the circuit between the thermocouple and extension wires, no temperature gradient exists along its length. If this is so, in accordance with the law of intermediate metals, no error will result.

Industrial thermocouples often use heads of cast iron, aluminum, or die cast construction with screw covers and a temperature resistant gasket seal. Terminal blocks are commonly provided consisting of a ceramic or phenolic block and brass terminals. These assemblies are particularly likely to introduce errors due to temperature gradients, so they should be used with caution. Where phenolic terminal blocks are used, an upper temperature of about 170°C (340°F) applies.

To reduce the likelihood of thermal gradient errors, connectors of the quick disconnect type intended for use in thermocouple circuits have contacts made of thermoelectric materials matching the thermocouple conductors. Even with these connectors some errors can result when extreme gradients across the connectors are encountered. Quick disconnect connectors are more commonly used with sheathed ceramic insulated assemblies. See Chapter 5 for more details on their application.

Since any material inhomogeneity in the circuit will introduce an error in the presence of a temperature gradient, best results will be obtained by avoiding extension wires, connectors, and terminal blocks. The thermocou-

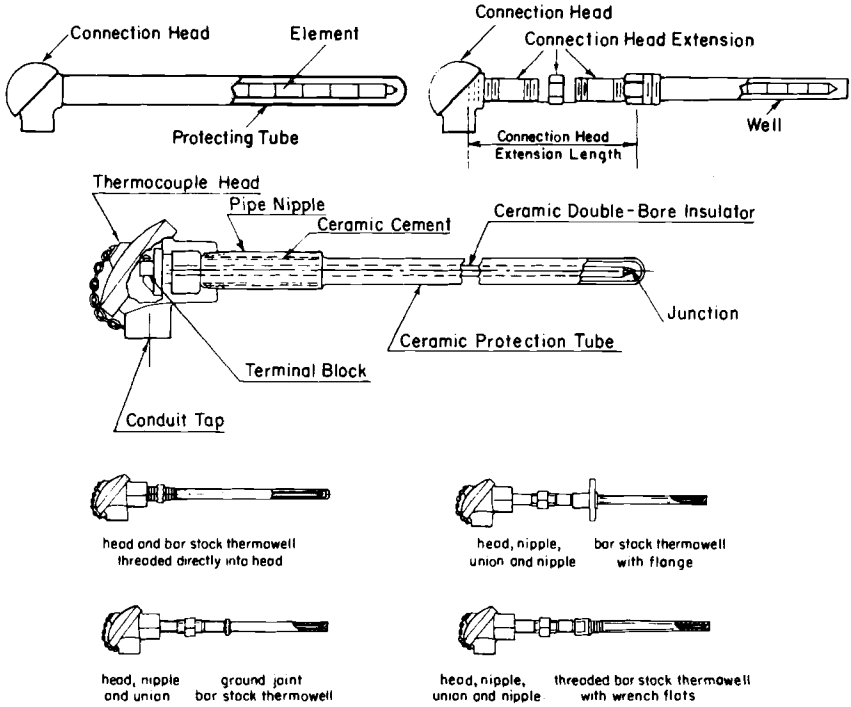


FIG. 4.4—Typical examples of thermocouple assemblies with protecting tubes.

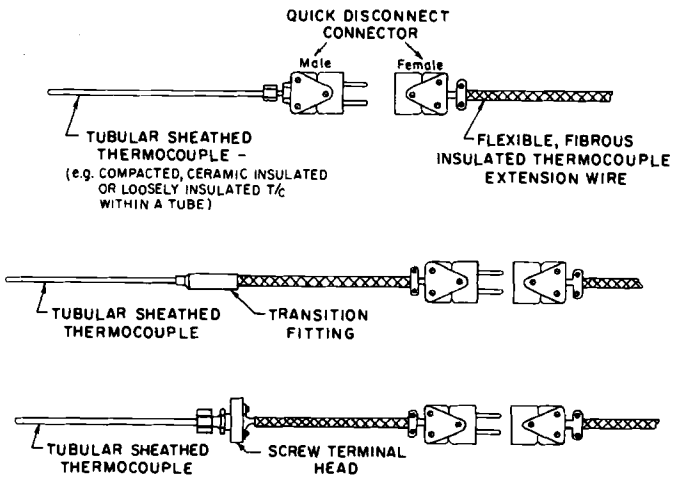


FIG. 4.5—Typical examples of thermocouple assemblies using quick disconnect connectors.

TABLE 4.4—*Selection guide for protecting tubes.*

| Application                                  | Protecting Tube Material                              |
|--|---|
| <i>Heat treating:</i>                        |   |
| <b>Annealing</b>                             |   |
| Up to 704°C (1300°F)                         | black steel   |
| Over 704°C (1300°F)                          | Inconel 600, <sup>a</sup> Type 446 SS                 |
| <b>Carburizing hardening</b>                 |   |
| Up to 816°C (1500°F)                         | black steel, Type 446 SS                              |
| 1093°C (1500 to 2000°F)                      | Inconel 600, Type 446 SS                              |
| Over 1093°C (2000°F)                         | ceramic <sup>b</sup>                                  |
| Nitriding salt baths                         | Type 446 SS   |
| Cyanide                                      | nickel (CP)   |
| Neutral                                      | Type 446 SS   |
| High speed                                   | ceramic <sup>b</sup>                                  |
| <i>Iron and steel:</i>                       |   |
| Basic oxygen furnace                         | quartz  |
| Blast furnaces                               |   |
| Downcomer                                    | Inconel 600, Type 446 SS                              |
| Stove dome                                   | silicon carbide                                       |
| Hot blast main                               | Inconel 600   |
| Stove trunk                                  | Inconel 600   |
| Stove outlet flue                            | black steel   |
| Open hearth                                  |   |
| Flues and stack                              | Inconel 600, Type 446 SS                              |
| Checkers                                     | Inconel 600, Cermets                                  |
| Waste heat boiler                            | Inconel 600, Type 446 SS                              |
| Billet heating slab heating and butt welding |   |
| Up to 1093°C (2000°F)                        | Inconel 600, Type 446 SS                              |
| Over 1093°C (2000°F)                         | silicon ceramic carbide <sup>b</sup>                  |
| Bright annealing batch                       |   |
| Top work temperature                         | not required (use bare Type J thermocouple)           |
| Bottom work temperature                      | Type 446 SS   |
| Continuous furnace section                   | Inconel 600, ceramic <sup>b</sup>                     |
| Forging                                      | silicon carbide, ceramic <sup>b</sup>                 |
| Soaking pits                                 |   |
| Up to 1093°C (2000°F)                        | Inconel 600   |
| Over 1093°C (2000°F)                         | silicon ceramic carbide <sup>b</sup>                  |
| <i>Nonferrous metals:</i>                    |   |
| Aluminum                                     |   |
| Melting                                      | cast iron (white-washed)                              |
| Heat treating                                | black steel   |
| Brass or bronze                              | not required (use dip-type thermocouple)              |
| Lead   | Type 446 SS, black steel                              |
| Magnesium                                    | black steel, cast iron                                |
| Tin  | extra heavy carbon steel                              |
| Zinc   | extra heavy carbon steel                              |
| Pickling tanks                               | chemical lead   |
| <i>Cement:</i>                               |   |
| Exit flues                                   | Inconel 600, Type 446 SS                              |
| Kilns, heating zone                          | Inconel 600   |
| <i>Ceramic:</i>                              |   |
| Kilns  | ceramic <sup>b</sup> and silicon carbide <sup>c</sup> |
| Dryers                                       | silicon carbide, black steel                          |
| Vitrous enamelling                           | Inconel 600, Type 446 SS                              |

TABLE 4.4—(Continued).

| Application  | Protecting Tube Material                                   |
|--|--|
| <i>Glass:</i>                                      |  |
| Fore hearths and feeders                           | platinum thimble   |
| Lehrs  | black steel  |
| Tanks  |  |
| Roof and wall                                      | ceramic <sup>a</sup>                                       |
| Flues and checkers                                 | Inconel 600, Type 446 SS                                   |
| <i>Paper:</i>                                      |  |
| Digesters  | Type 316 SS, Type 446 SS                                   |
| <i>Petroleum:</i>                                  |  |
| Dewaxing   | Types 304, 310, 316, 321, 347 SS, carbon steel             |
| Towers   | Types 304, 310, 316, 321, 347 SS, carbon steel             |
| Transfer lines                                     | Types 304, 310, 316, 321, 347 SS, carbon steel             |
| Factioning column                                  | Types 304, 310, 316, 321, 347 SS, carbon steel             |
| Bridgewall   | Types 304, 310, 316, 321, 347 SS, carbon steel             |
| <i>Power:</i>                                      |  |
| Coal-air mixtures                                  | 304 SS   |
| Flue gases   | black steel, Type 446 SS                                   |
| Preheaters   | black steel, Type 446 SS                                   |
| Steel lines  | Types 347 or 316 SS  |
| Water lines  | low carbon steels  |
| Boiler tubes                                       | Types 304, 309, or 310 SS                                  |
| <i>Gas producers:</i>                              |  |
| Producer gas                                       | Type 446 SS  |
| Water gas  |  |
| Carburetor   | Inconel 600, Type 446 SS                                   |
| Superheater  | Inconel 600, Type 446 SS                                   |
| Tar stills   | low carbon steels  |
| <i>Incinerators:</i>                               |  |
| Up to 1093°C (2000°F)                              | Inconel 600, Type 446 SS                                   |
| Over 1093°C (2000°F)                               | ceramic (primary) silicon carbide (secondary) <sup>a</sup> |
| <i>Food:</i>                                       |  |
| Baking ovens                                       | black steel  |
| Charretort, sugar                                  | black steel  |
| Vegetables and fruit                               | Type 304 SS  |
| <i>Chemical:</i>                                   |  |
| Acetic acid  |  |
| 10 to 50% 21°C (70°F)                              | Type 304, Hastelloy C, <sup>d</sup> Monel                  |
| 50% 100°C (212°F)                                  | Type 316, Hastelloy C, <sup>d</sup> Monel                  |
| 99% 21 to 100°C (70 to 212°F)                      | Type 430, Hastelloy C, <sup>d</sup> Monel                  |
| Alcohol, ethyl, methyl                             |  |
| 21 to 100°C (70 to 212°F)                          | Type 304   |
| Ammonia  |  |
| All concentration 21°C (70°F)                      | Types 304, 316 SS  |
| Ammonium chloride                                  |  |
| All concentration 100°C (212°F)                    | Type 316 SS, Monel   |
| Ammonium nitrate                                   |  |
| All concentration 21 to 100°C (70 to 212°F)        | Type 316 SS  |
| Ammonium sulphate, 10% to saturated, 100°C (212°F) | Type 316 SS  |

TABLE 4.4—(Continued).

| Application  | Protecting Tube Material                      |
|--|---|
| Barium chloride, all concentration, 21°C (70°F)    | Monel, Hastelloy C                            |
| Barium hydroxide, all concentration, 21°C (70°F)   | low carbon steels                             |
| Barium sulphite                                    | Nichrome, <sup>e</sup> Hastelloy C            |
| Brines   | Monel   |
| Bromine  | tantalum, Monel                               |
| Butadiene  | Type 304 SS                                   |
| Butane   | Type 304 SS                                   |
| Butylacetate                                       | Monel   |
| Butyl alcohol                                      | copper, Type 304 SS                           |
| Calcium chlorate, dilute, 21 to 66°C (70 to 150°F) |   |
| Calcium hydroxide                                  | Type 304 SS                                   |
| 10 to 20% 100°C (212°F)                            | Type 304 SS, Hastelloy C                      |
| 50% 100°C (212°F)                                  | Type 316 SS, Hastelloy C                      |
| Carbolic acid, all, 100°C (212°F)                  | Type 316 SS                                   |
| Carbon dioxide, wet or dry                         | 2017-T4 aluminum, Monel, nickel               |
| Chlorine gas                                       |   |
| Dry, 21°C (70°F)                                   | Type 316 SS, Monel                            |
| Moist, -7 to 100°C (20 to 212°F)                   | Hastelloy C                                   |
| Chromic acid, 10 to 50% 100°C (212°F)              | Type 316 SS, Hastelloy C (all concentrations) |
| Citric acid  |   |
| 15% 21°C (70°F)                                    | Type 304 SS, Hastelloy C (all concentrations) |
| 15% 100°C (212°F)                                  | Type 316 SS, Hastelloy C (all concentrations) |
| Concentrated, 100°C (212°F)                        | Type 316 SS, Hastelloy C (all concentrations) |
| Copper nitrate                                     | Types 304 SS, 316 SS                          |
| Copper sulphate                                    | Types 304 SS, 316 SS                          |
| Cresols  | Type 304 SS                                   |
| Cyanogen gas                                       | Type 304 SS                                   |
| Dow therm <sup>f</sup>                             | low carbon steels                             |
| Ether  | Type 304 SS                                   |
| Ethyl acetate                                      | Monel, Type 304 SS                            |
| Ethyl chloride, 21°C (70°F)                        | Type 304 SS, low carbon steel                 |
| Ethyl sulphate, 21°C (70°F)                        | Monel   |
| Ferric chloride, 5% 21°C (70°F) to boiling         | tantalum, Hastelloy C                         |
| Ferric sulphate, 5% 21°C (70°F)                    | Type 304 SS                                   |
| Ferrous sulphate, dilute, 21°C (70°F)              | Type 304 SS                                   |
| Formaldehyde                                       | Types 304 SS, 316 SS                          |
| Formic acid, 5% 21 to 66°C (70 to 150°F)           | Type 316 SS                                   |
| Freon  | Monel   |
| Gallic acid, 5% 21 to 66°C (70 to 150°F)           | Monel   |
| Gasoline, 21°C (70°F)                              | Type 304 SS, low carbon steel                 |
| Glucose, 21°C (70°F)                               | Type 304 SS                                   |
| Glycerine, 21°C (70°F)                             | Type 304 SS                                   |
| Glycerol   | Type 304 SS                                   |
| Hydrobromic acid, 98% 100°C (212°F)                | Hastelloy B                                   |
| Hydrochloric acid                                  |   |
| 1%, 5% 21°C (70°F)                                 | Hastelloy C                                   |
| 1%, 5% 100°C (212°F)                               | Hastelloy B                                   |
| 25% 21 to 100°C (70 to 212°F)                      | Hastelloy B                                   |
| Hydrofluoric acid, 60% 100°C (212°F)               | Hastelloy C, Monel                            |
| Hydrogen peroxide, 21 to 100°C (70 to 212°F)       | Types 316 SS, 304 SS                          |
| Hydrogen sulphide, wet and dry                     | Type 316 SS                                   |



TABLE 4.4—(Continued).

| Application                            | Protecting Tube Material     |
|--|------------------------------|
| Iodine, 21°C (70°F)                    | tantalum                     |
| Lactic acid                            |                              |
| 5% 21°C (70°F)                         | Type 304 SS, 316 SS          |
| 5% 66°C (150°F)                        | Type 316 SS                  |
| 10% 100°C (212°F)                      | tantalum                     |
| Magnesium chloride                     |                              |
| 5% 21°C (70°F)                         | Monel, nickel                |
| 5% 100°C (212°F)                       | nickel                       |
| Magnesium sulphate, hot and cold       | Monel                        |
| Muriatic acid, 21°C (70°F)             | tantalum                     |
| Naptha, 21°C (70°F)                    | Type 304 SS                  |
| Natural gas, 21°C (70°F)               | Types 304 SS, 316 SS, 317 SS |
| Nickel chloride, 21°C (70°F)           | Type 304 SS                  |
| Nickel sulphate, hot and cold          | Type 304 SS                  |
| Nitric acid                            |                              |
| 5% 21°C (70°F)                         | Types 304 SS, 316 SS         |
| 20% 21°C (70°F)                        | Types 304 SS, 316 SS         |
| 50% 100°C (70°F)                       | Types 304 SS, 316 SS         |
| 50% 100°C (212°F)                      | Types 304 SS, 316 SS         |
| 65% 100°C (212°F)                      | Type 316 SS                  |
| Concentrated, 21°C (70°F)              | Types 304 SS, 316 SS         |
| Concentrated, 100°C (212°F)            | tantalum                     |
| Nitrobenzene, 21°C (70°F)              | Type 304 SS                  |
| Oleic acid, 21°C (70°F)                | Type 316 SS                  |
| Oleum, 21°C (70°F)                     | Type 316 SS                  |
| Oxalic acid                            |                              |
| 5% hot and cold                        | Type 304 SS                  |
| 10% 100°C (212°F)                      | Monel                        |
| Oxygen                                 |                              |
| 21°C (70°F)                            | steel                        |
| Liquid                                 | SS                           |
| Elevated temperatures                  | SS                           |
| Palmitic acid                          | Type 316 SS                  |
| Pentane                                | Type 340 SS                  |
| Phenol                                 | Types 304 SS, 316 SS         |
| Phosphoric acid                        |                              |
| 1%, 5% 21°C (70°F)                     | Type 304 SS                  |
| 10% 21°C (70°F)                        | Type 316 SS                  |
| 10% 100°C (212°F)                      | Hastelloy C                  |
| 30% 21 to 100°C (70 to 212°F)          | Hastelloy B                  |
| 85% 21 to 100°C (70 to 212°F)          | Hastelloy B                  |
| Picric acid, 21°C (70°F)               | Type 304 SS                  |
| Potassium bromide, 21°C (70°F)         | Type 316 SS                  |
| Potassium carbonate, 1% 21°C (70°F)    | Types 304 SS, 316 SS         |
| Potassium chlorate, 21°C (70°F)        | Type 304 SS                  |
| Potassium hydroxide                    |                              |
| 5% 21°C (70°F)                         | Type 304 SS                  |
| 25% 100°C (212°F)                      | Type 304 SS                  |
| 60% 100°C (212°F)                      | Type 316 SS                  |
| Potassium nitrate                      |                              |
| 5% 21°C (70°F)                         | Type 304 SS                  |
| 5% 100°C (212°F)                       | Type 304 SS                  |
| Potassium permanganate, 5% 21°C (70°F) | Type 304 SS                  |
| Potassium sulphate, 5% 21°C (70°F)     | Types 304 SS, 316 SS         |
| Potassium sulphide, 21°C (70°F)        | Types 304 SS, 316 SS         |

TABLE 4.4—(Continued).

| Application                                   | Protecting Tube Material           |
|---|------------------------------------|
| Propane                                       | Type 304 SS, low carbon steel      |
| Pyrogalllic acid                              | Type 304 SS                        |
| Quinine bisulphate, dry                       | Type 316 SS                        |
| Quinine sulphate, dry                         | Type 304 SS                        |
| Seawater                                      | Monel or Hastelloy C               |
| Salicylic acid                                | nickel                             |
| Sodium bicarbonate                            |                                    |
| All concentration, 21°C (70°F)                | Type 304 SS                        |
| 5% 66°C (150°F)                               | Types 304 SS, 316 SS               |
| Sodium carbonate, 5% 21 to 66°C (70 to 150°F) | Types 304 SS, 316 SS               |
| Sodium chloride                               |                                    |
| 5% 21 to 66°C (70 to 150°F)                   | Type 316 SS                        |
| Saturated 21 to 100°C (70 to 212°F)           | Type 316 SS, Monel                 |
| Sodium fluoride, 5% 21°C (70°F)               | Monel                              |
| Sodium hydroxide                              | Types 304 SS, 316 SS, Hastelloy C  |
| Sodium hypochlorite, 5% still                 | Type 316 SS, Hastelloy C           |
| Sodium nitrate, fused                         | Type 316 SS                        |
| Sodium peroxide                               | Type 304 SS                        |
| Sodium sulphate, 21°C (70°F)                  | Types 304 SS, 316 SS               |
| Sodium sulphide, 21°C (70°F)                  | Type 316 SS                        |
| Sodium sulphite, 30% 66°C (150°F)             | Type 304 SS                        |
| Sulphur dioxide                               |                                    |
| Moist gas, 21°C (70°F)                        | Type 316 SS                        |
| Gas, 302°C (575°F)                            | Types 304 SS, 316 SS               |
| Sulphur                                       |                                    |
| Dry molten                                    | Type 304 SS                        |
| Wet   | Type 316 SS                        |
| Sulphuric acid                                |                                    |
| 5% 21 to 100°C (70 to 212°F)                  | Hastelloy B, 316 SS                |
| 10% 21 to 100°C (70 to 212°F)                 | Hastelloy B                        |
| 50% 21 to 100°C (70 to 212°F)                 | Hastelloy B                        |
| 90% 21°C (70°F)                               | Hastelloy B                        |
| 90% 100°C (212°F)                             | Hastelloy D                        |
| Tannic acid, 21°C (70°F)                      | Type 304 SS, Hastelloy B           |
| Tartaric acid                                 |                                    |
| 21°C (70°F)                                   | Type 304 SS                        |
| 66°C (150°F)                                  | Type 316 SS                        |
| Toluene                                       | 2017-T4 aluminum, low carbon steel |
| Turpentine                                    | Types 304 SS, 316 SS               |
| Whiskey and wine                              | Type 304 SS, nickel                |
| Xylene  | copper                             |
| Zinc chloride                                 | Monel                              |
| Zinc sulphate                                 |                                    |
| 5% 21°C (70°F)                                | Types 304 SS, 316 SS               |
| Saturated, 21°C (70°F)                        | Types 304 SS, 316 SS               |
| 25% 100°C (212°F)                             | Types 304 SS, 316 SS               |

<sup>a</sup>Trademark of the International Nickel Co.

<sup>b</sup>Due to susceptability to cracking, sudden thermal shocks should be avoided.

<sup>c</sup>Due to susceptability to cracking, sudden thermal shocks should be avoided.

<sup>d</sup>Trademark of the Cabot Corp.

<sup>e</sup>Trademark of the Driver-Harris Co.

<sup>f</sup>Trademark of the Dow Chemical Corp.

ple wires should be run directly to the reference junction after which copper wires are interconnected for extension to the measuring instrument.

#### 4.6 Complete Assemblies

Figures 4.4 and 4.5 show complete assemblies of the components which have been described in the foregoing sections. Many other combinations are possible. Manufacturers' catalogs may be consulted for other varieties and details.

#### 4.7 Selection Guide for Protecting Tubes

The following information in Table 4.1 has been extracted from various manufacturers' literature. It is offered as a guide to the selection of protecting tubes. Caution should be exercised in applying this information to specific situations.

#### 4.8 Bibliography

White, F. J., "Accuracy of Thermocouples in Radiant Heat Testing," *Experimental Mechanics*. Vol. 2, July 1962, p. 204.

Baker, H. D., Ryder, E. A., and Baker, N. H., *Temperature Measurement in Engineering*. Vol. 1, Wiley, New York, 1953.

McLaren, E. H. and Murdock, E. G., "New Considerations on the Preparation, Properties, and Limitations of the Standard Thermocouple for Thermometry," *Temperature, Its Measurement and Control in Science and Industry*. Reinhold, New York, Vol. 4, Part 3, 1972, p. 1543.

Benedict, R. P., *Fundamentals of Temperature, Pressure, and Flow Measurements*. Second Edition, Wiley, New York, 1977.

# Chapter 5—Sheathed, Ceramic-Insulated Thermocouples

---

## 5.1 General Considerations

Compacted ceramic insulated thermocouple material consists of three parts as shown in Fig. 5.1. This type of thermocouple is in common use because it isolates the thermocouple wires from environments that may cause rapid deterioration and provides excellent high-temperature insulation for thermocouple wires. The sheath can be made of a metal compatible with the process in which it is being used and provides mechanical protection. The material is easy to use because it forms easily, retains the bent configuration, and is readily fabricated into finished thermocouple assemblies.

## 5.2 Construction

All compacted types of thermocouples are made by similar processes. They begin with matched thermocouple wires surrounded by noncompacted ceramic insulating material held within a metal tube. By drawing, swaging, or other mechanical reduction processes the tube is reduced in diameter, and the insulation is compacted around the wires. Several options are available depending upon the material combinations selected for the temperature measurement application.

A ductile sheath and brittle refractory metal wire combination requires a design wherein the starting tubing diameter is only slightly larger than the finished size and only large enough on the inside diameter to accommodate a crushable preformed ceramic insulator with the wire strung through the insulators. This combination then would be reduced to the final diameter by one of the compaction methods usually in a single reduction pass. The process is such that the wire is neither elongated nor reduced in diameter in recognition of its brittle nature at room temperature.

A brittle sheath/brittle wire combination does not lend itself to a compacted insulation design and, therefore, is assembled as a tube-insulator-wire combination without the subsequent sheath reduction. Ductile wire/ductile sheath combinations cover the widest range of commonly used materials and offer the producer the widest choice of design approaches.

Nominal physical dimensions of sheathed ceramic insulated ther-

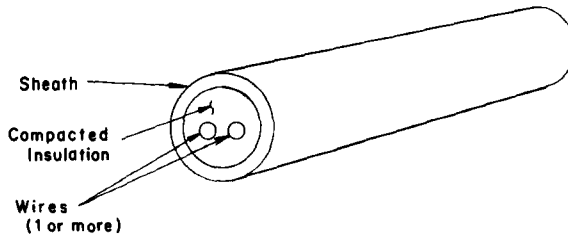


FIG. 5.1—*Compacted ceramic insulated thermocouple showing its three parts.*

mocouples are shown in Fig. 5.2. The ratios of sheath outside diameter to wire size and to sheath wall thickness offer a balance between maximum wall thickness (for protection of the sheath compacted insulant) and suitable insulation spacing for effective insulation resistance at elevated temperature. It is estimated that 90 percent of all sheathed thermocouples produced to date have used magnesium oxide (MgO) as the insulation material. Magnesium oxide is popular as a thermocouple insulator because of its overall compatibility with standard thermoelements and sheathing materials, its relative low cost, and its availability.

Aluminum, beryllium and thorium oxide insulations are also available from suppliers for use with certain wire and sheath combinations. The latter two materials are usually combined with refractory metal sheaths and thermoelements.

Because many applications of ceramic insulated thermocouples are at temperatures above 200°C (400°F), much attention must be given to cleanliness and chemical and metallurgical purity of the components. Great pains and expense having been taken to control the purity of the insulation during fabrication, the user would be foolish to abuse the sheathed material during assembly or application of the finished thermocouple. A warning heeded by the sailors and frontiersmen of early America can be applied today to the manufacture and use of sheathed thermocouples: Keep your powder clean and dry!

### 5.3 Insulation

For most practical purposes the sheathed thermocouple material should have a minimum insulation resistance of 100 megohms. This is readily obtained using dry, uncontaminated compacted ceramic. The capture of oil, oil vapors, moisture, perspiration, and lint during manufacture can cause low insulation resistance. The hygroscopic nature of the insulants, especially MgO, and capillary attraction cause rapid absorption of moisture through exposed ends of the sheath. Also, the insulation resistance of all ceramics,

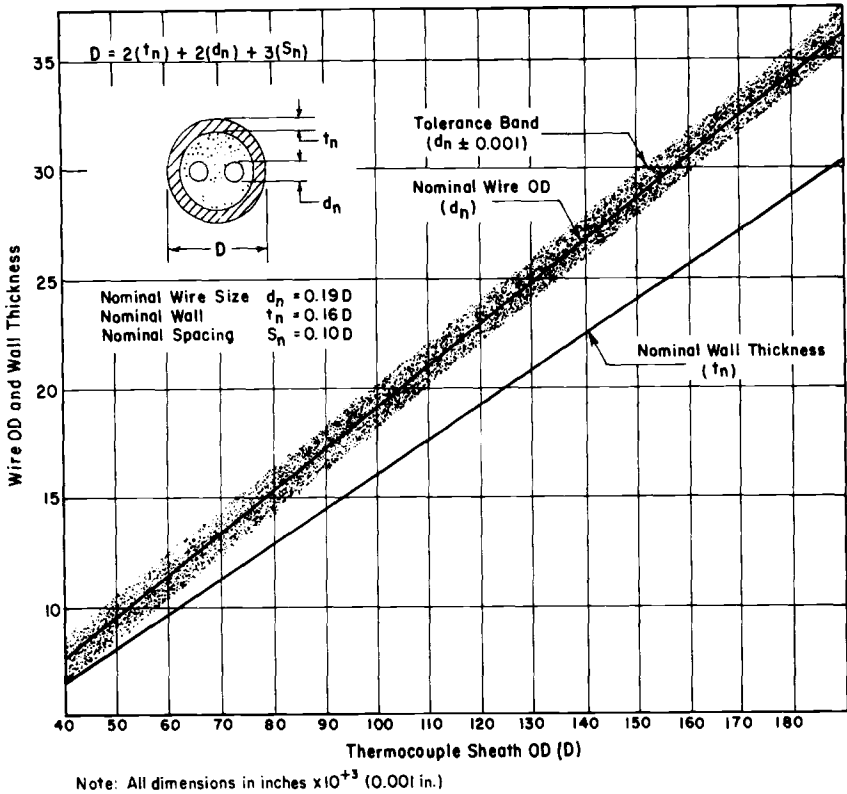


FIG. 5.2—Nominal thermocouple sheath outside diameter versus internal dimensions.

compacted and uncompact, reduces with an increase in temperature, especially if contaminated.

When purity has been maintained so that the insulation resistance is greater than 1000 megohms, special techniques are required to maintain these values. Such material exposed to 21°C (70°F) air and a relative humidity above 50 percent will experience a degradation of insulation resistance to less than 0.1 megohm in 15 min. Higher humidity will cause a more rapid degradation. The following precautions should be exercised when handling compacted ceramic insulated thermocouples:

1. Do not leave an end exposed for periods longer than one minute. Immediately seal the end, preferably immediately after heating to expel any moisture.
2. Expose ends only in a region of low relative humidity.
3. Store sealed assembly in a warm (above 38°C (100°F)) and dry (relative humidity less than 25 percent) area.

Once a surface of the compacted oxide insulator is exposed to normal ambient humidity, moisture enters and diffuses inward through the insulator. The rate of diffusion depends on the humidity, the insulation temperature, and the material and degree of compaction of the oxide. As indicated, it is usually rapid. In fact, the ultimate purity can be only maintained if all operations are performed in an inert-gas dry box [1].<sup>1</sup> After having been absorbed and diffused, the moisture is very difficult to remove. Heat added to drive out the moisture will only increase its rate of reaction (oxidation) with the sheath wall and the thermoelements. Even though the insulation resistance may be restored, the damage has been done. Failure to recognize the effect and nature of this phenomenon is responsible for the poor performance reported by many users of sheathed thermocouples.

In the special case of a brief exposure of high-density material, limited success has been achieved by moving a moderate heat source 200 to 300°C (400 to 600°F) toward the exposed end and immediate sealing with epoxy.

Some of the characteristics of the more common compacted ceramics are shown in Tables 5.1 and 5.2.

TABLE 5.1—Characteristic of insulating materials used in ceramic-packed thermocouple stock.

| Insulator                                 | Minimum Purity, % | Melting Point, °C (°F) | Approximate Usable Temperature, °C (°F) |
|---|-------------------|------------------------|---|
| Magnesia (MgO)                            | 99.4              | 2790 (5050)            | 1650 (3000)                             |
| Alumina (Al <sub>2</sub> O <sub>3</sub> ) | 99.5              | 2010 (3650)            | 1540 (2800)                             |
| Zirconia (ZrO <sub>2</sub> )              | 99.4              | 2480 (4500)            | 650 (1200)                              |
| Beryllia (BeO)                            | 99.8              | 2510 (4550)            | 2315 (4200)                             |
| Thoria (ThO <sub>2</sub> )                | 99.5              | 3290 (5950)            | 2760 (5000)                             |

TABLE 5.2—Thermal expansion coefficient of refractory insulating materials and three common metals.

| Material         | Average Coefficient of Expansion × 10 <sup>-4</sup> (25 to 700°C), °C <sup>-1</sup> |
|------------------|---|
| Copper           | 16.5  |
| Stainless steels | 13.9 to 16.4  |
| Aluminum         | 9.6   |
| Magnesium oxide  | 12.9  |
| Beryllium oxide  | 8.1   |
| Aluminum oxide   | 7.1 to 8.0  |
| Zirconium oxide  | 4.2 to 5.2  |

<sup>1</sup>The italic numbers in brackets refer to the list of references appended to this chapter.

## 5.4 Wire

The characteristics of the wires are no different from those of other thermocouples described in this manual. Since they are contained in a protective sheath and firmly held, small diameter wires can be exposed to high temperatures for long periods of time with less deterioration than that experienced by bare wire of the same size, provided they are properly fabricated and sealed.

## 5.5 Sheath

The sheath material performs several functions in the ceramic-insulated thermocouple system:

1. It holds the ceramic in compaction.
2. It shields the ceramic and thermoelements from the environment.
3. It furnishes mechanical strength to the assembly.

Since there is no sheath material suitable for all environments, a wide variety of different materials are offered. Table 5.3 shows a group of materials that can be used as sheaths and some of their characteristics. For maximum life a sheath diameter should be selected that offers the heaviest wall.

## 5.6 Combinations of Sheath, Insulation, and Wire

Precautions to be observed in selecting combinations are:

1. Be sure the sheath material will survive the environment. Remember that a thin sheath will deteriorate more rapidly than a thick one.
2. Be sure the assembly of sheath and wire is suitably annealed for optimum sheath life and stability of wire calibration.
3. Select a sheath and wire material of similar coefficients of linear expansion. For example: Platinum-rhodium and platinum have about one half the expansion of stainless or Inconel; a grounded hot junction may pull apart. The usual solution is to use hard-fired insulators in place of crushable and perhaps isolate the junction. Another solution is to use a platinum-rhodium sheath.
4. Select a sheath and wire material of similar annealing characteristics.
5. Do not use Types K, J, or E with an aluminum or copper sheath.

Table 5.4 indicates the compatibility of wire and sheath materials.

Table 5.5 gives dimensions of typical ceramic-packed stock.

## 5.7 Characteristics of the Basic Material

1. The sheath can usually be bent around a mandrel twice the sheath diameter without damage.



TABLE 5.3—Sheath materials of ceramic-packed thermocouple stock and some of their properties.

| Material               | Recommended       |                                |                      |                                    |   |
|------------------------|-------------------|--------------------------------|----------------------|------------------------------------|---|
|                        | Melting Point, °F | Recommended Maximum in Air, °F | Operating Atmosphere | Continuous Maximum Temperature, °F | Tensile Strength,* psi<br>At 200°F      At 1600°F |
| <i>Stainless steel</i> |                   |                                |                      |                                    |   |
| 304                    | 2 560             | 1 920                          | ORNV                 | 1 650                              | 68 000  |
| 309                    |                   | 2 000                          | ORNV                 | 2 000                              |   |
| 310                    | 2 560             | 2 000                          | ORNV                 | 2 100                              | 23 000  |
| 316                    | 2 500             | 1 650                          | ORNV                 | 1 700                              | 23 000  |
| 321                    | 2 550             | 1 650                          | ORNV                 | 1 600                              | 70 000  |
| 347                    | 2 600             | 1 680                          | ORNV                 | 1 600                              | 75 000  |
| 430                    | 2 700             | 1 550                          | ORNV                 | 1 200                              |   |
| 446                    | 2 700             | 2 000                          | ORNV                 | 2 000                              |   |
| Inconel                | 2 550             | 2 000                          | ONV <sup>b</sup>     | 2 100                              | 93 000  |
| Inconel X              | 2 620             | 2 500                          | ONV <sup>b</sup>     | 2 200                              | 150 000   |
| Incoloy                | 2 500             | 1 640                          |                      |                                    | 11 000  |
| Hastelloy X            | 2 350             | 2 300                          |                      |                                    | 77 000  |
| Hastelloy C            | 2 310             | 1 820                          |                      |                                    | 106 000   |
| Haynes 25              | 2 425             | 1 400                          |                      |                                    | 136 000   |
| Hastelloy B            | 2 375             | 1 400                          |                      |                                    | 147 000   |
| Monel                  | 2 460             | 1 640                          |                      |                                    | 125 000   |
| ChromeI                | 2 600             | 2 100                          | ONV                  |                                    | 90 000  |
| Copper                 | 1 990             | 600                            | ORNV                 | 600                                | 21 000  |
| Brass                  | 1 850             | 700                            |                      |                                    |   |
| Aluminum               | 1 220             | 800                            | ORNV                 | 700                                |   |
| Nichrome               | 2 550             | 2 200                          |                      | 2 000                              |   |
| Alumel                 | 2 550             | 2 100                          | ONV                  |                                    | 82 000  |
| Nickel                 | 2 647             | 1 100                          |                      |                                    |   |
| Iron                   | 2 798             | 600                            |                      |                                    |   |
| Zircaloy               | 3 350             | 1 400                          |                      |                                    |   |
| Platinum               | 3 217             | 3 000                          |                      | 3 000                              |   |
| Pt-Rh 10%              | 3 362             | 3 100                          | ON <sup>b</sup>      | 3 100                              |   |
| Niobium                | 4 474             | 1 600                          | VN                   | 3 800                              | 110 000   |
| Molybdenum             | 4 730             | 400                            | VNR                  |                                    | 137 000   |
| Molybdenum distilled   |                   | 3 100                          | ON                   | 3 000                              | 30 000  |
| Molybdenum chromalized |                   | 3 100                          | ON                   | 3 000                              |   |
| Tantalum               | 5 425             | 750                            | V                    | 5 000                              | 96 000  |
| Titanium               | 3 035             | 600                            | VN                   | 2 000                              | 22 000  |

NOTE—Symbols describing atmospheres are: O = oxidizing; R = reducing; N = neutral; V = vacuum. 32°F = 0°C

\*Scales readily in oxidizing atmosphere.

<sup>b</sup>Very sensitive to sulfur corrosion.

<sup>c</sup>After exposure to temperature of 100 h except for stainless steels; Haynes 25, W, Mo, Ta, and Nb.

TABLE 5.4.—Compatibility of wire and sheath material [6].

| Wire                    | Sheath |     |     |     |     |     |                         |                  |        |               |                |                |               |                        |
|-------------------------|--------|-----|-----|-----|-----|-----|-------------------------|------------------|--------|---------------|----------------|----------------|---------------|------------------------|
|                         | 304    | 310 | 316 | 321 | 347 | 440 | Plati-<br>num<br>Alloys | Hastel-<br>loy X | Copper | Alumi-<br>num | Inconel<br>600 | Inconel<br>702 | Tanta-<br>lum | Nio-<br>bium<br>Alloys |
| Type K                  | 1      | 1   | 1   | 1   | 1   | 1   | 1                       | 3                | 4      | 4             | 1              | 1              | 3             | 3                      |
| Type J                  | 1      | 1   | 1   | 1   | 1   | 1   | 2                       | 4                | 4      | 4             | 3              | 3              | 4             | 4                      |
| Type T                  | 1      | 1   | 1   | 1   | 1   | 1   | 2                       | 4                | 1      | 4             | 3              | 3              | 4             | 4                      |
| Type E                  | 1      | 1   | 1   | 1   | 1   | 1   | 1                       | 1                | 4      | 4             | 1              | 1              | 3             | 3                      |
| Types B, R, and S       | 1      | 1   | 1   | 1   | 1   | 1   | 1                       | 1                | 4      | 4             | 1              | 1              | 4             | 4                      |
| Tungsten rhenium alloys | 3      | 3   | 3   | 3   | 3   | 3   | 3                       | 1                | 4      | 4             | 3              | 3              | 3             | 3                      |
| Iridium rhodium alloys  | 3      | 3   | 3   | 3   | 3   | 3   | 3                       | 1                | 4      | 4             | 3              | 3              | 3             | 3                      |
| Copper                  | 3      | 4   | 3   | 3   | 3   | 4   | 4                       | 4                | 1      | 2             | 3              | 4              | 2             | 2                      |
| Nickel                  | 1      | 1   | 1   | 1   | 1   | 1   | 1                       | 1                | 4      | 4             | 1              | 1              | 3             | 3                      |
| Aluminum                | 4      | 4   | 4   | 4   | 4   | 4   | 4                       | 4                | 4      | 1             | 4              | 4              | 4             | 4                      |
| Nichrome <sup>a</sup>   | 1      | 1   | 1   | 1   | 1   | 1   | 1                       | 1                | 4      | 4             | 1              | 1              | 3             | 3                      |

NOTE.—1. Easy manufacturing and good operational compatibility.  
 2. Easy manufacturing but poor operational compatibility.  
 3. Difficult manufacturing but good operational compatibility.  
 4. Difficult manufacturing and poor operational compatibility.  
<sup>a</sup>Trademark of the Driver-Harris Co.

TABLE 5.5—Dimensions and wire sizes of typical ceramic-packed material.

| (a)                                |   |                                   |                                  |                                     |
|------------------------------------|---|-----------------------------------|----------------------------------|-------------------------------------|
| Sheath<br>Outside<br>Diameter, in. | Outside<br>Diameter<br>Tolerance, $\pm$ in. | Nominal<br>Wall<br>Thickness, in. | Approximate<br>Wire,<br>B&S gage | Nominal<br>Production<br>Length, ft |
| 0.010                              | 0.001                                       | 0.0015                            | 48                               | 250                                 |
| 0.020                              | 0.001                                       | 0.003                             | 38                               | 250                                 |
| 0.032                              | 0.001                                       | 0.005                             | 36                               | 250                                 |
| 0.040                              | 0.001                                       | 0.007                             | 34                               | 250                                 |
| 0.062                              | 0.002                                       | 0.010                             | 29                               | 150                                 |
| 0.090                              | 0.002                                       | 0.014                             | 26                               | 125                                 |
| 0.125                              | 0.002                                       | 0.018                             | 24                               | 100                                 |
| 0.188                              | 0.003                                       | 0.025                             | 18                               | 60                                  |
| 0.250                              | 0.003                                       | 0.032                             | 17                               | 40                                  |
| 0.313                              | 0.003                                       | 0.040                             | 16                               | 40                                  |
| 0.375                              | 0.003                                       | 0.049                             | 14                               | 30                                  |
| 0.430                              | 0.003                                       | 0.065                             | 13                               | 30                                  |
| 0.500                              | 0.003                                       | 0.070                             | 12                               | 30                                  |

| (b)                     |                                  |        |        |        |
|-------------------------|----------------------------------|--------|--------|--------|
| Sheath<br>Diameter, in. | Nominal Conductor Diameters, in. |        |        |        |
|                         | 1-Wire                           | 2-Wire | 3-Wire | 4-Wire |
| 0.313                   | 0.064                            | 0.051  | 0.040  | 0.040  |
| 0.250                   | 0.051                            | 0.040  | 0.032  | 0.032  |
| 0.188                   | 0.040                            | 0.032  | 0.022  | 0.022  |
| 0.125                   | 0.032                            | 0.022  | 0.011  | 0.011  |
| 0.042                   | 0.022                            | 0.011  | 0.006  | 0.006  |
| 0.040                   | 0.011                            | 0.006  | ...    | ...    |
| 0.025                   | 0.006                            | 0.004  | ...    | ...    |

NOTE—1 in. = 25.4 mm; 1 ft = 0.3048 m.

2. The life of material having a diameter of 0.81 mm (0.032 in.) or less may be limited by grain growth in the sheath wall.

3. Four wires in 1.57 mm (0.062 in.) sheath diameter and smaller are not practical to handle.

4. Two wires in 0.81 mm (0.032 in.) sheath diameter and smaller are difficult to handle but are used in laboratory environments.

Stock material and completed thermocouples are usually supplied to the end user in the fully annealed state with proper metallurgical grain size and no surface corrosion. Improper handling can easily destroy this condition. When wire is delivered coiled, it should not be uncoiled until needed for fabrication. Repeated or excessive bending will affect the annealed state. Sometimes the wire has been further heat treated after solution annealing, to control or stabilize calibration. If this is the case, further heat treatment to remove cold work will destroy these characteristics.

## 5.8 Testing

Many tests have been devised to evaluate sheathed ceramic insulated thermocouples. These tests cover the physical and metallurgical properties of the sheath and thermoelements, the electrical properties of the insulation, and the thermoelectric properties of the thermoelements.

ASTM has issued a specification E 235 [2] on sheathed thermocouples for nuclear and other high reliability applications which covers Type K thermoelements in various sheath materials, with alumina or magnesia insulations and alternative thermoelements. In Aerospace Information Report 46 [3] the Society of Automotive Engineers has covered the preparation and use of Type K thermocouples for turbojet engines, while the military has issued Mil T 22300 (Ships) and Mil T 23234 (Ships) for nuclear application of the sheathed thermocouples. In addition many government and commercial laboratories, thermocouple fabricators, and thermocouple users have issued specifications covering specific tests and test procedures for evaluating sheathed thermocouples.

Scadron [4] outlined some of the tests and tolerances that are applied for the verification of physical, electrical, and thermoelectric integrity of the sheathed thermocouple.

Most manufacturers' catalogs cover some aspects of the tests, guarantees, and procedures used to verify product integrity. Fenton et al [5] were concerned with inhomogeneity in bare and sheathed thermoelements and developed procedures and apparatus for testing for drift and inhomogeneity. National Bureau of Standards Circular 590 [6] covers thermocouple testing. While this publication applies to the bare thermoelements it is applicable to the electrical characteristics of the metal sheathed ceramic insulated material.

Table 5.6 shows various characteristics, tests, and the source of testing procedure which are applicable to sheathed ceramic-insulated thermocouples.

## 5.9 Measuring Junction

Numerous variations in measuring junction construction are possible with this type of material. The application dictates the most desirable method.

1. *Exposed or Bare Wire Junction* (Fig 5.3)—In this type of a junction the sheath and insulating material are removed to expose the thermocouple wires. These wires are joined to form a measuring junction. The junction may be of the twist-and-weld or butt-weld type. While the thermocouple will have a fast response, the exposed ceramic is not pressure tight and will pick up moisture, and the wires are subject to mechanical damage and are exposed to the environment.

2. *Grounded Junction* (Fig 5.4)—A closure is made by welding in an inert

TABLE 5.6—Various characteristics tests and the source of testing procedure applicable to sheathed ceramic-insulated thermocouples.

| Characteristics               | Tests   | Procedure  | Comments   |
|-------------------------------|---|--|--|
| PHYSICAL AND METALLURGICAL    |   |  |  |
| 1. OD of sheath               | ring gage, micrometer, or micromounts for high precision                      | good mechanical practice or transverse section per ASTM Method E 3   | tolerances per Table 29 sample preparation: requires care to prevent smear                       |
| 2. Roundness of sheath        | rotate for total indicated reading  | Vee block and dial indicator   | important for tube firing use  |
| 3. Sheath surface finish      | profilometer or roughness gage  | ANSI Standard B46.1  | also check clean finish for welding and brazing  |
| 4. Sheath wall thickness      | thread gage micrometer or metallurgical mount                                 | transverse section per ASTM Method E 3   | concerns machining, bending, welding, life: can be checked only at ends                          |
| 5. Insulation spacing         | comparator or metallurgical mount   | transverse section per ASTM Method E 3   | see electrical tests   |
| 6. Insulation compactness     | (A) tap test, (B) helium pressure, (C) dye absorption, (D) compaction density | (A) supplier catalog, (B) MIL-T-22300, (C) and (D) ASTM Method D 2771  | relative values must be related to application   |
| 7. Wire diameter              | micrometer or metallurgical mount   | visual or transverse section per ASTM Method E 3   | $\pm 1$ wire gage size (Table 29)  |
| 8. Wire surface and roundness | micrometer and visual   | 3-point diameter check   | 10% out of round max showing slight embedment of insulating material into wire                   |
| 9. Ductility and formability  | bend and visual or metallurgical mount  | ASTM E 235   | bend 90 deg only for ease of making metallurgical mount  |
| 10. Sheath integrity          | (A) water immersion, (B) hydrostatic, (C) helium leak, (D) dye penetrant      | (A) water soak with ends protected [18], (B) ASTM Method E 165, (C) ASTM Method E 235, (D) ASTM Method E 235 | (A) may use hydrostatic pressure or steam for some applications: seal weld to protect insulation |
| 11. Junction integrity        | radiographs   | ASTM Method E 235  | application for junction and 4 in. of sheath   |
| 12. Material compatibility    | thermal cycling   | ASTM Method E 235  | thermal expansion for grounded junction integrity check  |

|  |   |   |  |
|--|---|---|--|
| 13. Metallurgical integrity                | metallurgical mount                             | ASTM Method E 235   | checks grain size  |
| 14. Response time                          | thermal response test                           | gas: SAE 46, liquid [24]                                      | assesses thermal mass and welding technique  |
| 15. Uniformity of properties               | Tests 1, 2, 3, 10, 11, and 13 full length       | as noted  | use sampling procedure for large runs  |
| 16. Stability under service conditions     | application experience or life tests            | as required   | check with other users in same field   |
| CONSTANT TEMPERATURE ELECTRICAL            |   |   |  |
| 17. Insulation resistance                  | megohm meter between wires and sheath and wires | ASTM Method E 235   | 50 V for OD less than 0.061, 500 V for greater than 0.062  |
| 18. Electrical resistance (loop)           | Wheatstone bridge                               | Chapter 3   | tolerances $\pm 1$ gage size based on wire type, length and dia; also checks continuity  |
| 19. High temperature insulation resistance | megohm meter or Wheatstone bridge               |   | relative to operational requirement, effective means of testing insulation quality at expected operating temperature of thermocouple |
| 20. Dielectric strength                    | high potential generator                        |   | seldom used check for contamination and voids in insulation: voltage usually 500 V for 0.062 OD and larger                           |
| ISOTHERMAL ELECTRICAL                      |   |   |  |
| 21. Capacitance                            | capacitance bridge                              |   | test is usually not applied to thermocouples   |
| 22. Uniformity along length                | Test 17, 18, 19, 20, 21 for full length         |   | all tests are seldom necessary for single application  |
| 23. Stability under service conditions     | application experience or life tests            | check samples or full lengths coiled if necessary as required | check for experience by other users  |

TABLE 5.6—(Continued).

| Characteristics            | Tests                                 | Procedure  | Comments   |
|----------------------------|---------------------------------------|--|--|
| THERMOELECTRIC PROPERTIES  |                                       |  |  |
| 24. Emf versus temperature | potentiometer and heat or cold source | Chapter 6  | test at one or more points up to maximum use temperature                                     |
| 25. Homogeneity            | heat source and galvanometer          | NBC Circular 590 and Ref 6                       | max of $\pm 100 \mu\text{V}$ for J, K, T;<br>$\pm 25 \mu\text{V}$ for B, R, S thermoelements |
| 26. Uniformity full length | Test 24 and 25 for full length        | applying sampling procedure for large quantities | random sampling is most economical approach  |

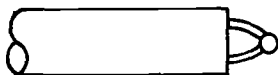


FIG. 5.3—Exposed or bare wire junction.

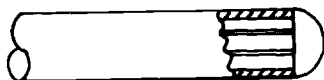


FIG. 5.4—Grounded junction.

atmosphere so that the two thermocouple wires become an integral part of the sheath weld closure. Thus, the wires are “grounded” to the sheath. This will give a slower response than exposed wire but the insulation is pressure tight, and the wires are protected from mechanical damage and from the environment.

3. *Ungrounded or Isolated Junction* (Fig. 5.5)—This type is similar to the grounded junction except that the thermocouple wires are first made into a junction which is then insulated from the sheath and the sheath closure. The closure is formed by welding without touching the thermocouple wires. Thus, the thermocouple is “ungrounded” to the sheath material. This junction has slower response than the grounded junction but is still pressure tight and protected from mechanical damage and from the environment. The strain due to differential expansion between wires and sheath may be reduced.

4. *Reduced Diameter Junction* (Fig. 5.6)—This may be either grounded or insulated and is used where fast response is required, and a heavier sheath or wires are desired for strength, life, or lower circuit resistance over the balance of the unit.



FIG. 5.5—Ungrounded or isolated junction.



FIG. 5.6—Reduced diameter junction.



### 5.10 Terminations

There are numerous ways in which thermocouples of this type can be treated at the reference end. The most common treatments are as follows:

1. *Wires Exposed and Sealed*—The sheath and the insulation are removed leaving the bare thermocouple wires exposed for a specific length. The insulating material is then sealed with epoxy to inhibit moisture absorption.

2. *Transition Fitting* (Fig 5.7)—The terminal end is provided with a fitting wherein the thermocouple wires are joined to more suitable wires. In this fitting the necessary sealant for the mineral insulant is also provided. One commercial machine produces a molded, thermoplastic transition.

3. *Terminals or Connectors*—Various types of fittings are available to facilitate external electrical connections. These include screw terminal heads, open or enclosed, and plug or jack connections (Fig. 5.8).

### 5.11 Installation of the Finished Thermocouple

Many types of installation are possible with sheathed thermocouples. Typical installations are shown in Figs. 5.9, 5.10, and 5.11. Other special flanges and adaptors are available from many thermocouple manufacturers.

### 5.12 Sheathed Thermocouple Applications

Application information for sheathed thermocouples has been well covered in the literature. Many suggested applications are made in the various suppliers catalogs. The Sannes article [7] on the application of the smaller

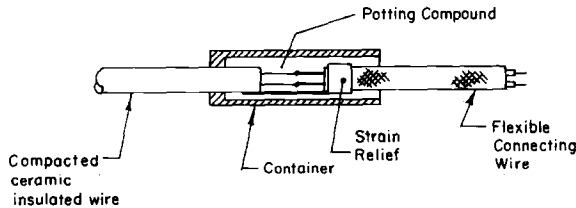


FIG. 5.7—Termination with flexible connecting wires.

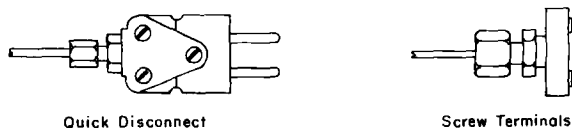


FIG. 5.8—Quick disconnect and screw terminals.

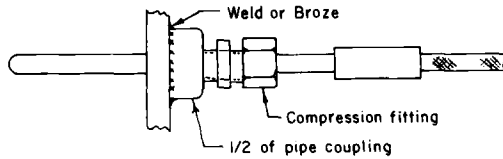


FIG. 5.9—Fittings to adapt into process line [up to  $3.48 \times 10^4$  kPa (5000 psi)].

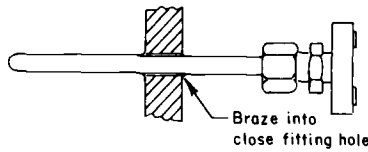


FIG. 5.10—Brazed for high pressure operation [up to  $6.89 \times 10^5$  kPa (100 000 psi)].

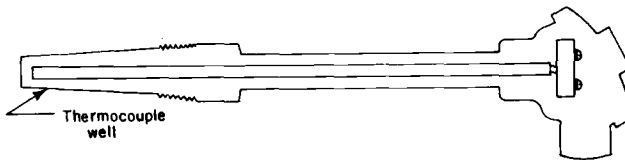


FIG. 5.11—Thermocouple in thermowell.

sheath diameters is useful. Chapter 9.2 of this manual is an excellent reference on surface temperature measurement. Gas stream performance is well documented [8-10] because of the applications to jet engines and rockets.

Nuclear reactor applications have used sheathed thermocouples extensively for monitoring and control. Johannessen [12] discussed the reliability assurance of such applications.

### 5.13 References

- [1] Bliss, P., "Fabrication of High-Reliability Sheathed Thermocouples," *Temperature, Its Measurement and Control in Science and Industry*. Vol. 4, Part 3, Section VIII-C, June 1971.
- [2] Bliss, P., "Fabrication of High-Reliability Sheathed Thermocouples," *Temperature, Its Measurement and Control in Science and Industry*, Vol 4, Part 3, Section VIII-C, Reinhold, New York, June 1971.
- [3] Committee AE-2, Society of Automotive Engineers, "The Preparation and Use of Chromel-Alumel Thermocouples for Turbojet Engines," Aerospace Information Report No. 46, 15 March 1956.
- [4] Scadron, L., "Ceramic Insulated Thermocouples," *Instruments and Control Systems*. May 1961.

- [5] Fenton, A. W., Dacey, R., and Evans, E. J., "Thermocouples: Instabilities of Seebeck Coefficient," TRG Report 1447 (R), United Kingdom Atomic Energy Authority, 1967.
- [6] Roeser, W. F. and Lonberg, S. T., "Methods of Testing Thermocouples and Thermocouples Materials," NBS Circular 590, National Bureau of Standards, 6 Feb. 1958.
- [7] Sannes, T., "Tiny Thermocouples," *Instrumentation Technology*, March 1967.
- [8] Faul, J. C., "Thermocouple Performance in Gas Streams," *Instruments and Control Systems*, Vol. 35, Dec. 1962.
- [9] Moffat, R. J., "Designing Thermocouples for Response Rate," *Transactions*, American Society of Mechanical Engineers, Feb. 1958.
- [10] Ihnat, M. E. and Hagel, W. D., "A Thermocouple System for Measuring Turbine Inlet Temperatures," *Transactions*, American Society of Mechanical Engineers, *Journal of Basic Engineering*, March 1960.
- [11] Johannessen, H. G., "Reliability Assurance in Sheathed Thermocouples for Nuclear Reactors," High Temperature Thermometry Seminar, T1D7586, Oak Ridge National Laboratory, Oak Ridge, Tenn., Aug. 1960.

# Chapter 6—Emf Measurements

---

## 6.1 General Considerations

The basic principle of thermoelectric thermometry is that a thermocouple develops an emf which is a function of the difference in temperature of its measuring junction and reference junction. If the temperature of the reference junction is known, the temperature of the measuring junction can be determined by measuring the emf generated in the circuit. The use of a thermocouple in temperature measurements, therefore, requires the use of an instrument capable of measuring emf.

There are three types of emf measuring instruments in use in industry: deflection meters (millivoltmeters), digital voltmeters, and potentiometers. Because of its limitations, the deflection meter is not used for precise measurements. Where precision and accuracy are required in the measurement of thermal emfs, either the digital voltmeter or the potentiometer is used.

Digital voltmeters can be used in most industrial applications and in making standard measurements. Digital voltmeters are very high impedance devices so that the readings are essentially independent of external circuit resistance.

When the greatest accuracy is required in measuring emfs, the potentiometer is often used. Readings are completely free from uncertainties arising from changing circuit resistance. Choice of range can be quite wide due to the very high sensitivity capability.

## 6.2 Deflection Millivoltmeters

The deflection meter consists of a galvanometer with a rigid pointer which moves over a scale graduated in millivolts or degrees. The galvanometer indicates by its deflection the magnitude of the current passing through it, and if the circuit in which it is placed includes a thermocouple, it measures the current  $I$  generated by the thermocouple in the circuit. If the circuit has a resistance  $R$  and the emf is  $E$ , by Ohm's law,  $E = RI$ . If  $R$  is kept constant,  $I$  is proportional to  $E$ , then the scale can be calibrated in terms of millivolts rather than in milli- or microamperes. This calibration holds as long as  $R$  remains constant. Any change in  $R$  introduces an error in the indicated value of  $E$ . Changes in resistance may result from changes in temperature of the thermocouple or its extension wires or of the copper galvanometer coil, from corrosion of the thermocouple wires, from changes in the depth of immersion of

the thermocouple, or from changes in contact resistance at switches or binding posts.

In general, the reference junctions of the thermocouple measuring circuit are located near the meter movement. The effect of temperature changes on these junctions is compensated for by a bimetallic spiral attached to one of the control springs of the pointer. This system maintains accurate meter calibration during changes in ambient temperature.

In spite of its limitations, the deflection meter serves a very useful purpose in a great variety of industrial measurements of temperature where the precision and accuracy required are not of a high order. Its insensitivity to small a-c signals may prove an advantage.

### 6.3 Digital Voltmeters

Two kinds of digital meters are generally available: (1) the integrating type and (2) the successive approximation type. The integrating type compares the value of the emf being measured to an internal reference voltage standard by timed charging and discharging of a reference capacitor. Measurements are relatively slow, on the order of a second, but are relatively unaffected by the presence of some types of electrical noise.

The successive approximation type digital meter operates by first estimating a voltage and comparing it with that being measured. The error is noted by the circuit, and a second approximation is made and compared, etc., until the estimated voltage equals the unknown. Solid-state circuitry enables this type of meter to display a reading within milliseconds. It is, however, susceptible to errors from electrical noise interference.

Both types of meters may display voltage, or a linearizing circuit can be included to provide readings directly in temperature.

Typical uncertainty of instruments reading in volts is 0.01 percent of range  $\pm 1$  digit. If readout is directly in temperature, uncertainty might be plus or minus several degrees for a broad range or less than  $\pm 1/2$  deg for a short range.

### 6.4 Potentiometers

#### 6.4.1 Potentiometer Theory

Accurate measurement is usually a matter of comparing an unknown quantity against a known quantity or standard—the more direct the comparison, the better. Accurate weighing, for example, often is accomplished by direct comparison against standard weights using a mechanical balance. If the measured weights are too heavy for direct comparison, lever arms may be used to multiply the forces.

The potentiometer, as the term is used here, serves a similar function in

the measurement of voltage, and, in fact, may be called a "voltage balance," the standard voltage being furnished by a standard cell, the "lever" being resistance ratios, and the galvanometer serving as the balance indicator. Since no current is drawn from the standard cell or the measured source at balance, the measurement is independent of external circuit resistance, except to the extent that this affects galvanometer or balancing mechanism sensitivity.

#### 6.4.2 Potentiometer Circuits

Figure 6.1 shows a simple potentiometer circuit which includes a resistor  $R$ , a standard cell  $S$ , a battery  $B$ , a galvanometer  $G$ , and a rheostat  $r$ .  $R$  may be a calibrated slidewire, with a known resistance, and  $R'$  a fixed resistor such that  $R$  plus  $R'$  is some simple multiple of the emf of  $S$ . If the emf of  $S$  is taken as 1.019 V, the sum of  $R$  plus  $R'$  may be chosen as 101.9. If the switch  $K$  is turned to the standard cell position, the galvanometer, in general, will deflect. The setting of rheostat  $r$ , is adjusted until the galvanometer remains at rest when  $K$  is closed. Then the drop of potential of the battery current through  $R$  and  $R'$  is exactly equal to the emf of  $S$ , so that if the current in  $R$  and  $R'$ ,  $T = 1.019/101.9$  A, or 10 mA, through each ohm of  $R$  there is then a drop of potential 0.010 V. If  $R$  is 20 ohms the total drop through the slidewire is 0.2 V.

Now if  $K$  is turned to the "thermocouple" position, a setting may be found for the sliding contact on  $R$  at which there will be no deflection of the galvanometer. At this position, the drop of potential through  $R$  of the contact is equal to the emf of the thermocouple. If balance occurs at the 5 ohm point, the emf of the thermocouple is  $0.01 \times 5 = 0.05$  V = 50 mV.

In this measurement the galvanometer has been used only as a means of detecting the presence of a current, and readings are made only when no perceptible current is passing through it. Therefore, it is not calibrated, and it is only called upon to indicate on balance with sufficient sensitivity to give the desired precision of setting of the sliding contact. An increase in the resistance of the thermocouple circuit can increase only the limits of positions of the contact between which there is no perceptible deflection, but does not affect the position of balance, nor the measured value of the emf. Since the galvanometer is used only to indicate the existence and direction of current, it is not necessary to design it to give a linear relationship between current and deflection. Zero stability is not extremely important since it is only necessary to look for departure from any equilibrium position when the key is closed to detect a need for adjustment and the direction in which it should be made. The galvanometer may be of the suspension type or an electronic null balance detector.

The calibration of an instrument of this type is stable since resistors and slidewires can be made with a high degree of stability. The emf of an un-

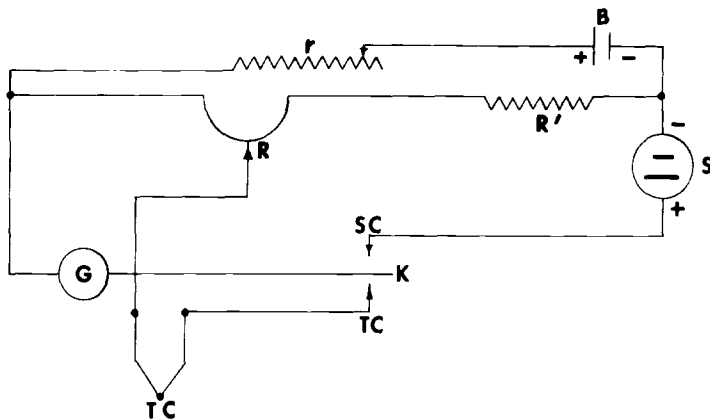


FIG. 6.1—A simple potentiometer circuit.

saturated standard cell, as used for potentiometric work, does not change more than about 0.01 percent per year and has a negligible temperature coefficient.

The usefulness of an elementary potentiometer of this sort, having its entire range across the slidewire, is limited by the resolution possible in setting and reading the position of the contact on  $R$ .

### 6.4.3 Types of Potentiometer Instruments

**6.4.3.1 Laboratory High Precision Type**—The six-dial potentiometer meets the most exacting requirements for standardizing, research and testing laboratories. It is particularly useful for precise temperature measurements in studies of specific heats, melting and boiling points, and for calibrating less precise potentiometers. It also is used for precise measurements such as required in calorimetry cryogenics. It measures emfs in the range of 0 to 1.6 V. It is essentially free of thermal emfs, and transients. Overall limits of error are typically 0.5 mV or less up to 1000 mV, and 5 mV or less up to 50 000 mV.

**6.4.3.2 Laboratory Precision Type**—The three-dial, manually operated potentiometer, also is used for precise measurements of voltage. As applied to the measurement of thermal emfs, its characteristics are such as to make it the most generally used of all the potentiometers in this field when accuracy and convenience of measurement are demanded. It is not portable in the sense in which the term is applied to self-contained potentiometers, since to attain the results of which it is capable, some parts of the circuit such as the null detector and the reference voltage source must be mounted separately. Overall limits of error are typically 1  $\mu$ V or less up to 1000  $\mu$ V, and 12  $\mu$ V or less up to 50 000  $\mu$ V.

**6.4.3.3 Portable Precision Type**—This potentiometer is a self-contained, three-dial, manually balancing instrument. It is used for precision checking of thermocouple pyrometers in laboratory and plant and for general temperature measurements. The measuring range typically extends from  $-10.1$  to  $100.1$  mV, readable to  $1 \mu\text{V}$ , and typical limits of error are: (a)  $\pm(0.03$  percent of reading plus  $3 \mu\text{V})$  without internal reference junction compensation and (b)  $\pm(0.03$  percent of reading plus  $6 \mu\text{V})$  with reference junction compensation.

An example of (a) when using an external reference junction (see Chapter 7) is as follows:

A Type K thermocouple develops  $41.269$  mV at  $1000^\circ\text{C}$  ( $1832^\circ\text{F}$ ). The thermocouple error ( $\pm 3/4$  percent) can be  $7.5^\circ\text{C}$ ; the instrument error will be  $0.0003 \times 41.269 + 0.003 = 0.015$  mV or  $0.4^\circ\text{C}$ .

The reference junction compensation (b) is provided by an additional slidewire. This slidewire is used to set the reference junction voltage to the value which corresponds to the temperature of the reference junction (obtain millivolt value from reference tables. Chapter 10).

The portable precision potentiometer is designed to measure thermocouple emfs with a precision adequate for all but the more refined laboratory applications. It includes a built-in lamp and scale galvanometer.

**6.4.3.4 Semiprecision Type**—Potentiometers are available which are similar to those used for precision potentiometry except for limits of error. They are essentially of the two-dial type with self-contained galvanometer, standard cell, and battery. They are used primarily for general temperature measurements by means of thermocouples, checking thermocouple pyrometers in laboratory and plant, and as a calibrated source of voltage.

One model has two ranges:  $-10.1$  to  $0$  mV and  $0$  to  $100.1$  mV, it is readable to  $1 \mu\text{V}$ . The limit of error is  $\pm(0.05$  percent of reading +  $20 \mu\text{V})$  without reference junction compensator and  $\pm(0.05$  percent of reading +  $40 \mu\text{V})$  with reference junction compensator.

**6.4.3.5 Recording Type**—Recording potentiometers are used widely for industrial process temperature measurement and control. These instruments balance automatically. When reliability and convenience are the prime concern, such instruments are satisfactory. However, because of potential inaccuracies in charts caused by printing limitations and humidity effects and practical limits on chart widths and scale lengths resulting in inadequate readability, they are not generally used where precision is the criterion.

## 6.5 Voltage References

Both digital meters and potentiometers require a standard voltage reference for comparison.

Digital voltmeters and moderate precision potentiometers generally use



the Zener diode, although many potentiometers still use Weston-type standard cells. High-precision potentiometers use standard cells. Two types of cells are available: saturated and unsaturated.

The saturated cell containing undissolved cadmium sulfate crystals is used in standardizing laboratories such as the National Bureau of Standards to represent the value of the volt. A typical cell has a potential of 1.01864 V at 20°C reproducible to a few microvolts. This voltage is constant for a long period of time. (As long as 60 years or more is possible with proper care of the cell.) These cells have a substantial but predictable negative temperature coefficient ranging from about  $-40 \mu\text{V}/^\circ\text{C}$  at 20°C to  $-70 \mu\text{V}/^\circ\text{C}$  at 37°C. It is, therefore, necessary to control their temperature environment very precisely, confining their usefulness to the laboratory.

Unsaturated cells have a very low temperature coefficient but a less stable voltage output. Normal voltage drift rates can be expected to be  $-20$  to  $-40 \mu\text{V}/\text{year}$ . The temperature coefficient is only a few microvolts/ $^\circ\text{C}$  between 15 and 45°C and may be either positive or negative, depending upon the chemical composition of the particular cell. Useful life of these cells may be ten years or more. As the cells age, the emf decreases. When it drops to about 1.0130 V, the potential becomes erratic; the temperature coefficient increases and excessive temperature emf hysteresis occurs.

A standard cell must be never short circuited, nor should its emf be measured with a voltmeter. In precise measurements, the balances should be made with a resistance of at least 10 000 ohms in series with the cell until the balance is well within the range of the detector scale.

For more complete information concerning standard cell characteristics and care, refer to *NBS Monograph No. 84*.

## 6.6 Reference Junction Compensation

Temperature measurement with thermocouples always requires the knowledge of the reference junction temperature. It can be either held at a constant known temperature or allowed to follow ambient temperature with the necessary compensation applied (see Chapter 7).

# Chapter 7—Reference Junctions

---

## 7.1 General Considerations

A thermocouple circuit is by its nature a differential measuring device, producing an emf which is a function of the temperatures of its two junctions. One of these junctions is at the temperature which is to be measured and is referred to as the measuring junction. The other junction is maintained at a known temperature and is referred to as the reference junction. (In a practical thermocouple circuit (see Section 2.3) copper wires are often connected to the thermocouple alloy conductors at the reference junction. The term reference junctions will be used to refer to this situation.) If these junctions are both at the same temperature, the presence of the copper “intermediate metal” introduces no change in the thermocouple’s emf. If they are not at the same temperature the analysis of the circuit is complicated. Moffat [1]<sup>1</sup> gives a helpful analytical method.

The Seebeck coefficient (thermoelectric power) of many common thermocouples is approximately constant from the ice point to the upper temperature limit of the materials (see Section 3.1.1). For such thermocouples, an uncertainty in the temperature of the reference junction will reflect a similar uncertainty in the deduced temperature of the measuring junction. However this situation does not exist for all thermocouple pairs. Notable exceptions occur in the case of the high rhodium-in-platinum alloy thermocouples [2,3]. In particular, if the reference junction of a platinum-30 percent rhodium versus platinum-6 percent rhodium (Type B) thermocouple lies within the range 0 to 50°C (32 to 122°F), a 0°C (32°F) reference junction may be assumed, and the error will not exceed 3  $\mu$ V. This represents about 0.3°C (0.5°F) error in high-temperature measurements [4].

## 7.2 Reference Junction Techniques

Three basic methods are used to take account of the reference junctions of the thermocouple circuit: (1) the junction is maintained at a fixed temperature, (2) the temperature of the reference junction is allowed to vary, and a compensating emf is introduced into the circuit or accounted for by calculation, (3) the temperature of the reference junction is allowed to vary, and

<sup>1</sup> The italic numbers in brackets refer to the list of references appended to this chapter.

compensation is made by a mechanical adjustment of the readout instrument.

Some variations of these techniques will be described in the following sections. Sources of error which are common to several techniques will be discussed in Section 7.3.

### 7.2.1 Fixed Reference Temperature

**7.2.1.1 Triple Point of Water**—A cell can be constructed in which there is an equilibrium between ice, water, and water vapor [5]. The temperature of this triple point is  $0.01^{\circ}\text{C}$  on the International Practical Temperature Scale of 1968, and it is reproducible to about  $0.0001^{\circ}\text{C}$ . Williams [6] describes a commercially available cell which is not affected by factors such as air saturation and pressure which can cause several millikelvins fluctuation in the temperature of an ice bath. To utilize such precision, extreme attention to immersion error and galvanic error is required, and the measurement system must be of the highest quality.

**7.2.1.2 Ice Point**—An ice bath, consisting of a mixture of melting, shaved ice and water, forms an easy way of bringing the reference junctions of a thermocouple to  $0^{\circ}\text{C}$  ( $32^{\circ}\text{F}$ ). If a proper technique is used, the uncertainty in the reference junction temperature can be made negligibly small. With extreme care the ice point can be reproduced to  $0.0001^{\circ}\text{C}$  [7].

A recommended form of ice bath is described in Ref 8 and is shown in Fig. 7.1. Using the illustrated construction, with 14 gage B&S iron or nickel-base alloy wires and 20 gage B&S copper and noble metal wires, immersed at least 110 mm (4.5 in.) in the water-ice mixture, Caldwell [9] found the immersion error (see Section 7.3.1) to be less than  $0.05^{\circ}\text{C}$ . Smaller diameter wires would reduce the error. If large conductors must be used, Finch [10] describes a technique which minimizes the error.

To avoid the use of mercury<sup>2</sup> in the glass tubes, the tubes may be filled with moisture-free oil. Kerosine, transformer oil and silicone oil are all suitable [11-13].<sup>3</sup> Moisture-proof insulation should extend beneath the surface of the oil to the ends of the wires where they may be connected by any means which ensures a low resistance contact (for example, welding, soldering, crimping, etc.). If the glass tubes are immersed 200 mm (8 in.) in the ice-water mixture and the oil extends to within a few millimeters of the ice-water surface, the immersion error will be negligible. Sutton [11] plots the error as a function of the wire material, diameter, and immersion depth.

If the ice bath is improperly used, serious errors can result. The largest error which is likely to occur arises due to melting of the ice at the bottom of a

<sup>2</sup>Mercury can be hazardous to health.

<sup>3</sup>Care should be taken to prevent oil contamination of that part of the thermocouples which will be exposed to high temperatures.

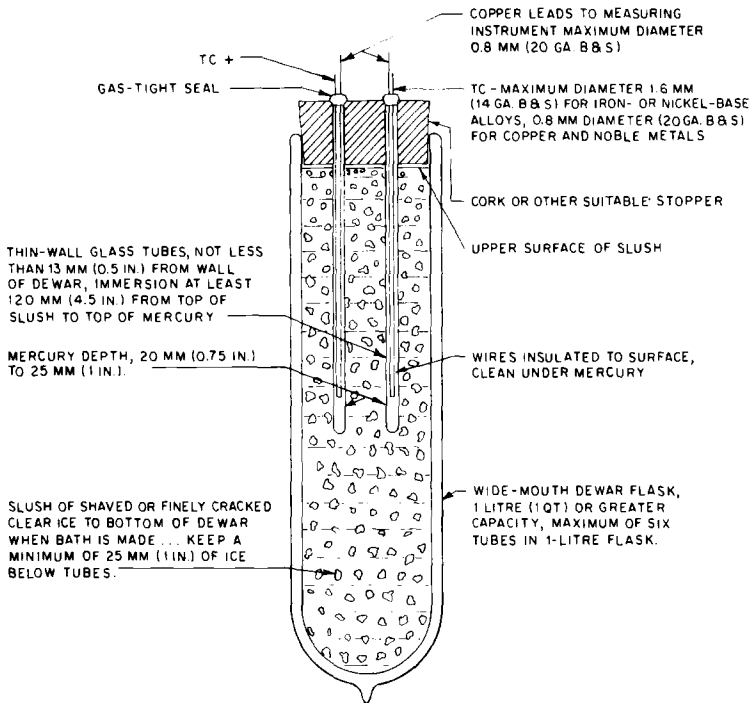


FIG. 7.1—Recommended ice bath for reference junction.

bath until the reference junctions are below the ice level and surrounded by water alone. This water may be as much as  $4^{\circ}\text{C}$  above the ice point. While an ice bath is being used excess water should be removed periodically and more ice added, so that the ice level is maintained safely below the reference junctions [8, 12].

If the ice used to prepare the bath has been stored in a freezer at a temperature below  $0^{\circ}\text{C}$ , it may freeze the surrounding water and remain at a temperature below  $0^{\circ}\text{C}$  for some time. To avoid the condition, the ice should be shaved rather than crushed and thoroughly wetted with water before placing it in the vacuum bottle [11-13].

If appreciable concentrations of salts are present in the water used to make the ice bath, the melting point can be affected. McElroy [14] investigated various combinations of tap and distilled water to determine the error introduced. He observed bath temperatures of  $+0.013^{\circ}\text{C}$  using distilled water with tap ice and  $-0.006^{\circ}\text{C}$  using tap water and tap ice. It is probable that the use of tap water will not introduce significant errors unless accuracies better than  $0.01^{\circ}\text{C}$  are required [9].

Another possible source of error is galvanic action which is discussed in Section 7.3.2.

Although the ice bath is an easy way of achieving a convenient fixed point for the reference junctions in the laboratory, the need for constant attention makes it unsuitable for industrial application where some form of automatic reference junction is desirable.

*7.2.1.3 Automatic Ice Point*—The development of the thermoelectric refrigerator (Peltier cooler) has enabled the production of practical devices in which an equilibrium between ice and water is constantly maintained [15, 16]. Since water expands 9 percent on freezing, the change of volume may be used to control the heat transfer. Substances which undergo a phase change do so without change of temperature. This is an important advantage since the system behaves as if it had an infinite thermal capacity.

This device can provide a reference medium which is maintained at a precise temperature, but careful design is necessary if this precision is to be utilized fully. The system is subject to immersion error (Section 7.3.1) and galvanic error (7.3.2) due to condensation.

Some commercially available devices provide wells into which the user may insert reference junctions formed from his own calibrated wire. Others are provided with many reference junction pairs brought out to terminals which the user may connect into his system. The latter type are subject to the wire matching error (Section 7.3.3).

If the potential errors have been successfully overcome, the error introduced into a system by these devices may be less than  $0.1^{\circ}\text{C}$ .

Automatic ice points can be used to further advantage in conjunction with a "zone box" (see 7.2.2.1).

*7.2.1.4 Constant Temperature Ovens*—A thermostatically controlled oven provides a way of holding a reference junction at an approximately constant temperature. The major advantage of this method is that one oven can be used with a large number of circuits while maintaining isolation between the circuits without the need for providing separate power supplies for each circuit.

The oven must be maintained at a temperature above the highest anticipated ambient temperature. The need for temperature uniformity within the oven and a precise temperature control system are inherent complications, in addition to the immersion error (Section 7.3.1) and the wire matching error (Section 7.3.3).

Ovens are available with rated accuracies ranging from  $0.1$  to  $0.05^{\circ}\text{C}$ . A common commercially used junction temperature is  $66^{\circ}\text{C}$  ( $150^{\circ}\text{F}$ ), although other values may be specified.

Elevated temperature reference junctions can be used with instruments or tables based on  $0^{\circ}\text{C}$  reference junctions, provided an appropriate correction is applied.

A device using two ovens is available which makes this correction automatically. To generate the necessary emf (for example,  $2.662$  mV for a Type K system with a  $66^{\circ}\text{C}$  ( $150^{\circ}\text{F}$ ) reference junction temperature) an

additional internal thermocouple is connected in series with the external thermocouple circuit. This internal thermocouple has its reference junction in the first oven and its measuring junction in the second oven. The second oven is maintained at a suitable temperature above that of the first so that the required emf is generated. The external thermocouple circuit then behaves as if its reference junction were at 0°C. The manufacturers' stated accuracies of these devices are similar to those of single oven units.

### 7.2.2 *Electrical Compensation*

If the temperature of the reference junction of a thermocouple is allowed to change, the output emf will vary in accordance with the Seebeck coefficient of the couple at the reference temperature. A compensating circuit containing a source of current, a combination of fixed resistors, and a temperature sensitive resistor (TSR) can be designed which will have a similar variation of emf as the temperature of the TSR is varied. If the reference junction of the thermocouple is coupled thermally to the TSR and the compensating circuit is connected in series with the thermocouple so that its temperature-variable emf opposes that caused by the reference junction, the thermocouple behaves as if the reference junction temperature were held constant. In addition, by suitable choice of the fixed resistors, any fixed reference junction temperature may be simulated. Since the TSR is at the temperature of the reference junction, no warmup or stabilization time is involved. Muth [17] has given a more extended description of these circuits.

The disadvantages of this arrangement include the need for a stable power source for each thermocouple circuit, the difficulty of exactly matching the Seebeck coefficient over an extended temperature range, and the addition of series resistance in the thermocouple circuit.

This principle is used in almost all self-balancing recording thermocouple potentiometers. Here the power source already is present as part of the potentiometer circuit. The Seebeck coefficient is matched adequately to allow the accuracy of the entire instrument to be typically 0.25 percent of full scale over a reasonable range of ambient temperatures.

Electric reference junction compensators are also available as small circuit modules with self-contained battery power sources or for connection to a-c power. A typical specification for a battery powered unit is compensation to  $\pm 0.3^\circ\text{C}$  over an ambient of 13 to 35°C (55 to 90°F). Improved specifications are quoted for more elaborate devices.

Some portable manually balanced potentiometers are provided with a thermometer to read the reference junction temperature and an adjustable circuit calibrated in millivolts or temperature. The control must be set manually to add the required emf to simulate an ice-point reference junction temperature.

**7.2.2.1 Zone Box**—In systems employing large numbers of thermocouples, an alternative method of dealing with the reference junctions is par-

ticularly useful. All of the thermocouples are routed to a device called a zone box where each thermocouple conductor is joined to a copper wire which is routed to the emf measuring instrument [18, 19].

Within the zone box all of the reference junctions between the thermocouples and the copper wires are insulated electrically but kept in good thermal contact with each other and with a transducer which measures the temperature within the zone box. This transducer can be a thermocouple of the same type as the measuring thermocouples with its reference junction in an automatic ice point or any of the other devices described in Section 7.2.1. The output of this thermocouple can be added to that of the measuring thermocouples, either electrically or in a data-collection computer. Several thermocouples are sometimes used in the zone box to monitor its temperature uniformity.

Alternatively, the zone box temperature can be measured by other transducers such as thermistors or resistance thermometers which need no reference temperature. In this case the measuring instrument determines the necessary correction to the thermal emfs, based on the temperature of the measuring-thermocouple reference junctions in the zone box. Several variations of this technique are described in Ref 19.

The advantage of the zone box is its simplicity. It generally requires no heaters, controls or power supplies. Since it is approximately at the ambient temperature, the immersion error (Section 7.3.1) can be made negligible with a moderate amount of thermal insulation if care is taken to avoid locations having extreme thermal gradients. The wire matching error (Section 7.3.3) should receive attention because the reference junctions are at ambient temperature and the calibration error at this temperature must be accounted for.

*7.2.2.2 Extended Uniform Temperature Zone*—To reduce the length of thermocouple wires required to reach a zone box, Sutton [11] extended the zone by the use of a piped water system. The system operates at ambient temperature. By circulating water with a low power pump, uniformity within  $0.1^{\circ}\text{C}$  between the first and last reference junction is achievable. The zone length may extend to many tens of meters.

### *7.2.3 Mechanical Reference Compensation*

To complete this account of methods used to compensate for the temperature of thermocouple reference junctions, a device used on millivolt pyrometers must be included. The millivolt pyrometer measures the thermal emf of a thermocouple circuit by measuring the current produced in a circuit of fixed and known resistance. The current operates a galvanometer with a rigid pointer which moves over a scale graduated in degrees [10]. The reference junction is at the temperature of the instrument, and hence the available thermal emf is a function of the temperature of the instrument. Compensa-

tion is often accomplished by attaching one of the hairsprings of the D'Arsonval galvanometer movement to a bimetallic thermometer element so that the electrical zero of the instrument is adjusted to correspond to the temperature of the instrument. This system is subject to the wire matching error (Section 7.3.3.), but the precision of the pyrometer seldom justifies making corrections.

### 7.3 Sources of Error

Several sources of error which may disturb the control or measurement of the reference junction temperature are discussed in this section.

#### 7.3.1 Immersion Error

Whenever reference junctions are being maintained at a temperature which differs from the ambient, heat is transferred between the reference temperature medium (oven, ice bath, etc.) and the ambient via the electrical insulation which separates the junctions from the medium and via the wires which emerge from the reference junctions. Thus the temperature of the junctions always differs from that of the reference medium to a greater or lesser degree. Caldwell [9] gives data which allow the error to be estimated for the standard type of ice bath. For other situations the error may be calculated by methods outlined in Refs 20 and 21, if the coefficients governing heat flow between the medium, the wires, and the ambient can be evaluated.

With careful design the immersion error usually can be made negligible.

#### 7.3.2 Galvanic Error

If water is allowed to contact the thermocouple alloy and copper wires of the reference junction, a galvanic cell may be set up, causing voltage drops which disturb the thermal emfs. If the reference junction is at a temperature below the dew point, the water may appear due to condensation. Insulation on both wires and precautions to avoid the accumulation of water in contact with the wires normally will prevent this error [9, 14].

#### 7.3.3 Wire Matching Error

Thermocouple wire normally is calibrated with its reference junction at 0°C, and corrections are determined to enable accurate measurements at elevated temperatures. The calibration deviation at ambient temperature is seldom of interest and usually is not determined.

Many reference junction devices are equipped with thermocouple alloy wires, and provision is made for interconnection with the user's thermocouples at ambient temperatures. If the calibration of the wire supplied with



the device differs from that of the thermocouples at the ambient temperature, a significant error can result due to the interconnection of the wires. This source of error often is overlooked, since it is assumed that if the interconnection of both wires of a thermocouple pair occurs at the same temperature no error is introduced. The existence of this error is visualized easily if the circuit is analyzed using Moffat's method [1].

A simple correction for the wire matching error can be made if the ambient temperature deviation of the wire supplied with the reference junction device is known and the user's thermocouples are calibrated at ambient temperature.

The wire matching error is avoided in those reference junction devices in which the user's wire is used to form the reference junctions.

#### 7.4 References

- [1] Moffat, R. J., "The Gradient Approach to Thermocouple Circuitry," *Temperature. Its Measurement and Control in Science and Industry*. Vol. 3, Part 2, Reinhold, New York, 1962, pp. 33-38.
- [2] Caldwell, F. R., "Thermocouple Materials," *Temperature. Its Measurement and Control in Science and Industry*. Vol. 3, Part 2, Reinhold, New York, 1962, pp. 81-134.
- [3] Zysk, E. D., "Noble Metals in Thermometry, Recent Developments," *Technical Bulletin*, Englehard Industries, Inc., Vol. 5, No. 3, 1964.
- [4] Burns, G. W. and Gallagher, J. S., "Reference Tables for the Pt-30 Percent Rh Versus Pt-6 Percent Rh Thermocouple," *Journal of Research, NBS-C Engineering and Instrumentation*, Vol. 70C, No. 2, 1966.
- [5] Stimson, H. F., "Precision Resistance Thermometry and Fixed Points," *Temperature. Its Measurement and Control in Science and Industry*. Vol. 2, Reinhold, New York, 1955, pp. 141-168.
- [6] Williams, S. B., "Triple Point of Water Temperature Reference," *Instruments and Control Systems*, Vol. 33, 1960.
- [7] Thomas, J. L., "Reproducibility of the Ice Point," *Temperature. Its Measurement and Control in Science and Industry*. Vol. 1, Reinhold, New York, 1941, pp. 159-161.
- [8] ASTM E 563, "Standard Recommended Practice for Preparation and Use of Freezing Point Reference Baths," American Society for Testing and Materials.
- [9] Caldwell, F. R., "Temperatures of Thermocouple Reference Junctions in an Ice Bath," *Journal of Research, NBS Engineering and Instrumentation*, Vol. 69C, No. 2, 1965.
- [10] Finch, D. I., "General Principles of Thermoelectric Thermometry," *Temperature, Its Measurement and Control in Science and Industry*. Vol. 3, Part 2, Reinhold, New York, 1962, pp. 3-32.
- [11] Sutton, G. R., "Thermocouple Referencing," *Temperature Measurement, 1975*; Conference Series No. 26, Chapter 4, Institute of Physics, London, pp. 188-194.
- [12] Hollander, B., "Referencing Thermocouple Junctions," *Instruments and Control Systems*, March 1973, pp. 38-39.
- [13] McElroy, D. L., and Fulkerson, W., in "Temperature Measurement and Control," *Techniques of Metals Research*. Vol. 1, Part 1, Chapter 2, *Temperature Measurement and Control*. R. F. Bunshah, Ed., Interscience, New York, 1969, pp. 175-177.
- [14] McElroy, D. L., "Progress Report I. Thermocouple Research Report for the Period, November 1, 1956 to October 31, 1957," ORNL-2467, Oak Ridge National Laboratory, Oak Ridge, Tenn..
- [15] Morgan, W. A., "Close Temperature Control of Small Volumes, A New Approach," Preprint Number 11.7-2-64, Instrument Society of America, 1964.
- [16] Feldman, C. L., "Automatic Ice-Point Thermocouple Reference Junction," *Instruments and Control Systems*, Jan. 1965, pp. 101-103.

- [17] Muth, S., Jr., "Reference Junctions," *Instruments and Control Systems*, May 1967, pp. 133-134.
- [18] Roeser, W. F., "Thermoelectric Thermometry," *Temperature. Its Measurement and Control in Science and Industry*, Vol. 1, Reinhold, New York, 1941, p. 202.
- [19] Claggett, T. J., "External Thermocouple Compensation," *Instrumentation*, Vol. 18, No. 2, Second Quarter, 1965.
- [20] Baker, H. D., Ryder, M. E., and Baker, M. A., *Temperature Measurement in Engineering*, Vol. 1, Section 7, Wiley, New York, 1953.
- [21] Bauerle, J. E., "Analysis of Immersed Thermocouple Error," *Review of Scientific Instruments*, Vol. 32, No. 3, March 1961, pp. 313-316.

# Chapter 8—Calibration of Thermocouples

---

The calibration of a thermocouple consists of the determination of its electromotive force (emf) at a sufficient number of known temperatures so that, with some accepted means of interpolation, its emf will be known over the entire temperature range in which it is to be used. The process requires a standard thermometer to indicate temperatures on a standard scale, a means for measuring the emf of the thermocouple, and a controlled environment in which the thermocouple and the standard can be brought to the same temperature. Some of the more commonly used techniques for accomplishing such calibrations will be discussed in this chapter.

Much of this material is based upon National Bureau of Standards Circular 590, *Methods of Testing Thermocouples and Thermocouple Materials*, and the calibration methods appearing in *Temperature Measurement* of the American Society of Mechanical Engineers Performance Test Codes, PTC 19.3.

## 8.1 General Considerations

### 8.1.1 Temperature Scale

The International Practical Temperature Scale of 1968 (IPTS-68) is realized and maintained by the National Bureau of Standards to provide a standard scale of temperature for use by science and industry in the United States. This scale [1,2]<sup>1</sup> was adopted by the International Committee of Weights and Measures at its meeting in October 1968 and was amended in 1975 [3]. The scale has general international acceptance, and it replaces the International Practical Temperature Scale of 1948 [4]. The IPTS-68 distinguishes between the International Practical Kelvin Temperature with the symbol  $T_{68}$  and the International Practical Celsius Temperature with the symbol  $t_{68}$ ; the relation between  $T_{68}$  and  $t_{68}$  is

$$t_{68} = T_{68} - 273.15 \text{ K}$$

The units of  $T_{68}$  and  $t_{68}$  are the kelvin, symbol K, and degree Celsius, symbol °C (formerly called centigrade). It is common practice to express values of temperature on the IPTS-68 in Kelvin temperatures below 0°C and in Celsius

<sup>1</sup>The italic numbers in brackets refer to the list of references appended to this chapter.

temperatures above 0°C. Values of Fahrenheit temperature, symbol °F, are obtained from the conversion formula

$$^{\circ}\text{F} = 9/5 \times ^{\circ}\text{C} + 32$$

The IPTS-68 is a practical, standard, empirical scale chosen in such a way that temperatures measured on it closely approximate thermodynamic temperatures. It is a practical scale because the value for a given temperature is more easily and reproducibly determined on it than on the thermodynamic scale. The scale is based on eleven reproducible equilibrium states (defining fixed points) to which numerical values are assigned, and on formulas establishing the relationship between values of International Practical Temperature and the indications of standard instruments calibrated at the defining fixed points.

The defining fixed points are established by realizing specified equilibrium states between phases of pure substances. These fixed points and the exact numerical values assigned to them are given in Table 8.1.

The standard instrument used from 13.81 K (−259.34°C) to 630.74°C is the platinum resistance thermometer. The thermometer resistor must be annealed pure platinum that is mounted in a strain-free configuration. The resistance ratio  $W(T_{68})$  of the platinum resistance thermometer, defined by

$$W(T_{68}) = R(T_{68})/R(273.15 \text{ K})$$

where  $R(T_{68})$  is the resistance at  $T_{68}$  and  $R(273.15 \text{ K})$  is the resistance at 273.15 K, must not be less than 1.39250 at  $T_{68} = 373.15 \text{ K}$ . From 630.74 to 1064.43°C the standard instrument is the platinum-10 percent rhodium versus platinum thermocouple. Above 1064.43°C, the IPTS-68 is defined by the Planck law of radiation with 1064.43°C as the reference temperature, but the type of standard instrument to be used for the measurement is not specified. However, visual and photoelectric optical pyrometers are the instruments usually used to realize the temperature scale in this region.

The procedures for interpolation lead to a division of the scale into four parts.

(a) From 13.81 to 273.15 K (−259.34 to 0°C) the temperature  $T_{68}$  is defined by the formula

$$W(T_{68}) = W_{\text{CCT-68}}(T_{68}) + \Delta W(T_{68})$$

where  $W(T_{68})$  is the resistance ratio of the platinum resistance thermometer and  $W_{\text{CCT-68}}(T_{68})$  is the resistance ratio given by a reference function [3]. The deviations  $\Delta W(T_{68})$  are calculated from measured values of  $W(T_{68})$  at the defining fixed points and the corresponding values of  $W_{\text{CCT-68}}(T_{68})$ . To obtain  $\Delta W(T_{68})$  at intermediate temperatures interpolation formulas are used. For this purpose the range between 13.81 and 273.15 K is divided into four parts; 13.81 to 20.28 K, 20.28 to 54.361 K, 54.361 to 90.188 K, and 90.188

TABLE 8.1—*Defining fixed points of The International Practical Temperature Scale of 1968.*<sup>a</sup>

| Equilibrium State  | Assigned Value of<br>International Practical<br>Temperature |                            |
|--|---|----------------------------|
|  | $T_{68}(\text{K})$  | $t_{68}(^{\circ}\text{C})$ |
| Equilibrium between the solid, liquid and vapor phases of equilibrium hydrogen (triple point of equilibrium hydrogen)                          | 13.81   | -259.34                    |
| Equilibrium between the liquid and vapor phases of equilibrium hydrogen at a pressure of 33 330.6 N/m <sup>2</sup> (25/76 standard atmosphere) | 17.042  | -256.108                   |
| Equilibrium between the liquid and vapor phases of equilibrium hydrogen (boiling point of equilibrium hydrogen)                                | 20.28   | -252.87                    |
| Equilibrium between the liquid and vapor phases of neon (boiling point of neon)  | 27.102  | -246.048                   |
| Equilibrium between the solid, liquid and vapor phases of oxygen (triple point of oxygen)  | 54.361  | -218.789                   |
| Equilibrium between the solid, liquid and vapor phases of argon (triple point of argon) <sup>b</sup>   | 83.798  | -189.352                   |
| Equilibrium between the liquid and vapor phases of oxygen (boiling point of oxygen)  | 90.188  | -182.962                   |
| Equilibrium between the solid, liquid and vapor phases of water (triple point of water)  | 273.16  | 0.01                       |
| Equilibrium between the liquid and vapor phases of water (boiling point of water)  | 373.15  | 100                        |
| Equilibrium between the solid and liquid phases of tin (freezing point of tin) <sup>c</sup>  | 505.1181  | 231.9681                   |
| Equilibrium between the solid and liquid phases of zinc (freezing point of zinc)   | 692.73  | 419.58                     |
| Equilibrium between the solid and liquid phases of silver (freezing point of silver)   | 1 235.08  | 961.93                     |
| Equilibrium between the solid and liquid phases of gold (freezing point of gold)   | 1 337.58  | 1 064.43                   |

<sup>a</sup>Except for the triple points and one equilibrium hydrogen point (17.042 K) the assigned values of temperature are for equilibrium states at a pressure  $p_0 = 1$  standard atmosphere (101 325 N/m<sup>2</sup>). In the realization of the fixed points small departures from the assigned temperatures will occur as a result of the differing immersion depths of thermometers or the failure to realize the required pressure exactly. If due allowance is made for these small temperature differences, they will not affect the accuracy of realization of the Scale. The magnitudes of these differences are given in section 111 of Ref 3.

<sup>b</sup>The triple point of argon may be used as an alternative to the condensation point of oxygen.

<sup>c</sup>The freezing point of tin ( $t' = 231.9292^{\circ}\text{C}$ , see Equation in subsection (b) on next page) may be used as an alternative to the boiling point of water.

to 273.15 K. In each part  $\Delta W(T_{68})$  is given by a polynomial [3] in  $T_{68}$ . The constants in the polynomials are determined from values of  $\Delta W(T_{68})$  at the fixed points and the condition that values of  $d \Delta W(T_{68})/d T_{68}$  given by joining polynomials must be equal at the junctions of the temperature ranges.

(b) From 0 to 630.74°C  $t_{68}$  is defined by

$$t_{68} = t' + 0.045 \left( \frac{t'}{100^\circ\text{C}} \right) \left( \frac{t'}{100^\circ\text{C}} - 1 \right) \left( \frac{t'}{419.58^\circ\text{C}} - 1 \right) \left( \frac{t'}{630.74^\circ\text{C}} - 1 \right) ^\circ\text{C}$$

where  $t'$  is defined by the formula

$$t' = \frac{1}{\alpha} \left[ W(t') - 1 \right] + \delta \left( \frac{t'}{100^\circ\text{C}} \right) \left( \frac{t'}{100^\circ\text{C}} - 1 \right) ^\circ\text{C}$$

where  $W(t') = R(t')/R(0^\circ\text{C})$ . The constants  $R(0^\circ\text{C})$ ,  $\alpha$ , and  $\delta$  are determined by measurement of the resistance of the platinum resistance thermometer at the triple point of water, the boiling point of water (or the freezing point of tin<sup>2</sup> and the freezing point of zinc. The preceding formula for  $t'$  may be also expressed as

$$W(t') = 1 + At' + Bt'^2$$

where

$$A = \alpha \left( 1 + \frac{\delta}{100^\circ\text{C}} \right) \quad \text{and} \quad B = -10^{-4} \alpha \delta ^\circ\text{C}^{-2}$$

(c) From  $630.74^\circ\text{C}$  to the gold point ( $1064.43^\circ\text{C}$ ) the temperature  $t_{68}$  is defined by the formula

$$E(t_{68}) = a + bt_{68} + ct_{68}^2$$

where  $E(t_{68})$  is the electromotive force of a standard platinum-10 percent rhodium versus platinum thermocouple when one of its junctions is at  $0^\circ\text{C}$  and the other is at the temperature  $t_{68}$ . The constants  $a$ ,  $b$ , and  $c$  are calculated from values of  $E$  at  $630.74^\circ\text{C} \pm 0.2^\circ\text{C}$ , as determined by a platinum resistance thermometer, and at the freezing points of silver and gold.

For the foregoing interpolation formula to be valid, the platinum thermoelement of the standard thermocouple must meet certain purity requirements and the values of  $E$  at  $630.74^\circ\text{C}$ , the silver point and the gold point must also satisfy certain criteria [3]. Not all Type S thermocouples will meet these requirements, but suitable thermocouples may be obtained commercially.

(d) Above the gold point the temperature  $T_{68}$  is defined by the formula

$$\frac{L_\lambda(T_{68})}{L_\lambda[T_{68}(\text{Au})]} = \frac{\exp \left[ \frac{c_2}{\lambda T_{68}(\text{Au})} \right] - 1}{\exp \left[ \frac{c_2}{\lambda T_{68}} \right] - 1}$$

<sup>2</sup>See note c, Table 8.1.

where  $L_\lambda(T_{68})$  and  $L_\lambda(T_{68}(\text{Au}))$  are the spectral concentrations at temperature  $T_{68}$  and at the freezing point of gold,  $T_{68}(\text{Au})$ , of the radiance of a blackbody at the wavelength  $\lambda$ ;  $c_2$  is defined to be 0.014388 metre kelvin and  $\lambda$  is in metres ( $\exp [x]$  is defined to be  $e^x$ ).

In addition to the defining points of the Scale, given in Table 8.1 certain other points may be useful for calibration purposes. Some of these and their reported temperatures are given in Table 8.2. Except for the triple point of benzoic acid, each temperature is for a system in equilibrium under a pressure of 1 standard atm.

### 8.1.2 Reference Thermometers

Any one of several types of thermometers, calibrated in terms of the IPTS, may be used as a reference thermometer for the calibration of thermocouples. The choice will depend upon the temperature range covered, whether a laboratory furnace or a stirred liquid bath is used, the accuracy expected of the calibration, or in cases where more than one type will suffice, the convenience or preference of the calibrating laboratory.

**8.1.2.1 Resistance Thermometers**—The standard platinum resistance thermometer is the most accurate reference for use from approximately  $-260^\circ\text{C}$  ( $-436^\circ\text{F}$ ) to  $630^\circ\text{C}$  ( $1166^\circ\text{F}$ ). In cases where an uncertainty approaching  $0.1^\circ\text{C}$  is necessary at temperatures below  $-56^\circ\text{C}$  ( $-69^\circ\text{F}$ ) or

TABLE 8.2—*Secondary reference points.*<sup>a</sup>  
The pressure<sup>b</sup> is 1 standard atm, except for the triple point of benzoic acid.

|                                     | °C       |
|-------------------------------------|----------|
| Boiling point of normal hydrogen    | −252.753 |
| Boiling point of nitrogen           | −195.806 |
| Sublimation point of carbon dioxide | −78.476  |
| Freezing point of mercury           | −38.836  |
| Freezing point of water             | 0.00     |
| Triple point of benzoic acid        | 122.37   |
| Freezing point of indium            | 156.634  |
| Freezing point of bismuth           | 271.442  |
| Freezing point of cadmium           | 321.108  |
| Freezing point of lead              | 327.502  |
| Freezing point of antimony          | 630.755  |
| Freezing point of aluminum          | 660.46   |
| Freezing point of copper            | 1 084.88 |
| Freezing point of nickel            | 1 455    |
| Freezing point of palladium         | 1 554    |
| Freezing point of platinum          | 1 769    |

<sup>a</sup>Values are extracted from Table 6 of Ref 3.

<sup>b</sup>See Ref 3 for information on the effect of pressure variation.

above about 200°C (392°F) there are few alternatives to the use of resistance thermometers as a reference.

**8.1.2.2 Liquid-in-Glass Thermometers**—This type of thermometer may be used from approximately  $-183^{\circ}\text{C}$  ( $-297^{\circ}\text{F}$ ) to  $400^{\circ}\text{C}$  ( $752^{\circ}\text{F}$ ), or even higher with special types. Generally, the accuracy of these thermometers is less below  $-56^{\circ}\text{C}$  ( $-69^{\circ}\text{F}$ ) where organic thermometric fluids are used, and above  $300^{\circ}\text{C}$  ( $572^{\circ}\text{F}$ ) where instability of the bulb glass may require frequent calibration. Specifications for ASTM liquid-in-glass thermometers are given in Ref 5.

**8.1.2.3 Types E and T Thermocouples**—Either of these types of thermocouples may be used down to a temperature of  $-183^{\circ}\text{C}$  ( $-297^{\circ}\text{F}$ ) or lower, but the attainable accuracy may be limited by the accuracy of the emf measurements and the inhomogeneity of the wire at low temperatures. The stability of the larger sizes of wire is greater than that of smaller wires under the same conditions. Twenty-four gage wire is a useful compromise between the lesser stability of smaller wire and the greater thermal conduction (greater required depth of immersion) of larger wire. Recommended upper limits are  $250^{\circ}\text{C}$  ( $482^{\circ}\text{F}$ ) for the Type E and  $200^{\circ}\text{C}$  ( $392^{\circ}\text{F}$ ) for Type T.

**8.1.2.4 Types R and S Thermocouples**—A Type S or R thermocouple is the most satisfactory reference thermometer for use in the range from  $630^{\circ}\text{C}$  ( $1166^{\circ}\text{F}$ ) up to about  $1200^{\circ}\text{C}$  ( $2192^{\circ}\text{F}$ ). Its use may be extended down to room temperature if it is desired to use the same reference over a wide range, but its sensitivity falls off appreciably as temperatures below  $200^{\circ}\text{C}$  ( $392^{\circ}\text{F}$ ) are reached. Twenty-four gage wire most commonly is used for these types of thermocouples.

**8.1.2.5 High Temperature Standards**—The IPTS-68 above  $1064^{\circ}\text{C}$  ( $1947^{\circ}\text{F}$ ) is defined by the Planck law of radiation, and the scale is usually realized by means of an optical pyrometer. The optical pyrometer [6], sighted on a blackbody cavity built into the calibration furnace, therefore, can serve as a reference thermometer for all temperatures above  $1064^{\circ}\text{C}$  ( $1947^{\circ}\text{F}$ ). On the other hand, thermocouples, calibrated on the optical pyrometer scale, can be used themselves as references. The Type B thermocouple [7] is useful up to about  $1700^{\circ}\text{C}$  ( $3092^{\circ}\text{F}$ ). Tungsten rhenium alloys can be used to higher temperatures, but the optical pyrometer more commonly is used.

### 8.1.3 Annealing

Practically all base-metal thermocouple wire is annealed or given a “stabilizing heat treatment” by the manufacturer. Such treatment generally is considered sufficient, and seldom is it found advisable to further anneal the wire before testing.

Although new platinum and platinum-rhodium thermocouple wire as sold by some manufacturers already is annealed, it has become regular practice in many laboratories to anneal all Types R, S, and B thermocouples, whether



new or previously used, before attempting an accurate calibration. This is accomplished usually by heating the thermocouple electrically in air. The entire thermocouple is supported between two binding posts, which should be close together, so that the tension in the wires and stretching while hot are kept at a minimum. The temperature of the wire is determined most conveniently with an optical pyrometer.<sup>3</sup>

There are some questions as to the optimum temperature and length of time at which such thermocouples should be annealed to produce the most constant characteristics in later use [8] and as to whether annealing for more than a few minutes is harmful or beneficial. Most of the mechanical strains are relieved during the first few minutes of heatings at 1400 to 1500°C (2552 to 2732°F), but it has been claimed that the changes in the thermal emf of a couple in later use will be smaller if the wires are heated for several hours before calibration and use. The principal objection to annealing thermocouples for a long time at high temperatures, aside from the changes in emf taking place, is that the wires are weakened mechanically as a result of grain growth. It has been found that annealing at temperatures much above 1500°C (2732°F) produces changes in the emf and leaves the wire very weak mechanically. In addition, rapid cooling [8] of the wires following annealing at elevated temperatures should be avoided since it can substantially alter the emf. Except for work of the highest precision, cooling at a rate not exceeding about 400°C/min is satisfactory. The National Bureau of Standards has adopted the procedure of annealing Types R, S, and B thermocouples for 45 min at 1450°C (2642°F), followed by 30 min at 750°C (1382°F) and then slow cooling to room temperature.

It has not been demonstrated conclusively that Types R, S, and B thermocouples after contamination can be improved materially in homogeneity by prolonged heating in air, although it is logical to suppose that certain impurities can be driven off or, through oxidation, rendered less detrimental.

#### 8.1.4 *Measurement of Emf*

One of the factors in the accuracy of the calibration of a thermocouple is the accuracy of the instrument used to measure the emf. Fortunately in most instances, an instrument is available whose performance is such that the accuracy of the calibration need not be limited by the accuracy of the emf measurements. For work of the highest accuracy it is advisable to use a potentiometer of the type designed by Diesselhorst [9], White [10], or Wenner [11], in which there are no slidewires and in which all the settings are

<sup>3</sup>The ordinary portable type of optical pyrometer is very satisfactory for this purpose. As commonly used, the magnification is too low for sighting on an object as small as the wires of noble-metal thermocouples, but this is remedied easily by lengthening the telescope tube or using an objective lens of shorter focal length.

made by means of dial switches. However, for most work on which an accuracy of  $5\ \mu\text{V}$  will suffice, slidewire potentiometers of the laboratory type are sufficiently accurate.

Electronic digital voltmeters and analog-to-digital converters that are of potentiometric or other high-impedance design and that possess sufficient accuracy may be also used. Such instruments permit fast readings of a large number of thermocouples. For a more detailed consideration of emf measurements see Chapter 6.

### 8.1.5 Homogeneity

The emf developed by a thermocouple made from homogeneous wires will be a function of the temperature difference between the measuring and the reference junction. If, however, the wires are not homogeneous, and the inhomogeneity is present in a region where a temperature gradient exists, extraneous emfs will be developed, and the output of the thermocouple will depend upon factors in addition to the temperature difference between the two junctions. The inhomogeneity of the thermocouple wire, therefore, is an important factor in accurate measurements.

Thermocouple wire now being produced is usually sufficiently homogeneous in chemical composition for most purposes. Occasionally inhomogeneity in a thermocouple may be traced to the manufacturer, but such cases are rare. More often it is introduced in the wires during tests or use. It usually is not necessary, therefore, to examine new thermocouples for inhomogeneity, but thermocouples that have been used for some time should be so examined before an accurate calibration is attempted.

While rather simple methods are available for detecting thermoelectric inhomogeneity, no satisfactory method has been devised for quantitatively determining it or the resulting errors in the measurement of temperatures. Abrupt changes in the thermoelectric power may be detected by connecting the two ends of the wire to a sensitive galvanometer and slowly moving a source of heat, such as a bunsen burner or small electric furnace, along the wire. This method is not satisfactory for detecting gradual changes in the thermoelectric power along the length of the wire. Inhomogeneity of this nature may be detected by doubling the wire and inserting it to various depths in a uniformly heated furnace, the two ends of the wire being connected to a galvanometer as before. If, for example, the doubled end of the wire is immersed 250 mm (10 in.) in a furnace with a sharp temperature gradient so that two points on the wire 500 mm (20 in.) apart are in the temperature gradient, the emf determined with the galvanometer is a measure of the difference in the thermoelectric properties of the wire at these two points.

After reasonable homogeneity of one sample of wire has been established, it may be used in testing the homogeneity of similar wires by welding the two together and inserting the junction into a heated furnace. The resulting emf

at various depths of immersion may be measured by any convenient method. Other similar methods have been described for detecting inhomogeneity [12].

Tests such as those described previously will indicate the uncertainty in temperature measurements due to inhomogeneity in the wires. For example, if a difference in emf of  $10 \mu\text{V}$  is detected along either element of a platinum-rhodium couple by heating various parts of the wire to  $600^\circ\text{C}$  ( $1112^\circ\text{F}$ ), measurements made with it are subject to an uncertainty of the order of 1 deg below  $500^\circ\text{C}$ , or 2 deg to  $1200^\circ\text{C}$ . Similarly, if an emf of  $10 \mu\text{V}$  is detected along an element of a base-metal couple with a source of heat at  $100^\circ\text{C}$ , measurements made with the thermocouple are subject to an uncertainty of the order of  $0.2^\circ\text{C}$  at this temperature. The effects of inhomogeneity in both wires may be either additive or subtractive, and, as the emf developed along an inhomogeneous wire depends upon the temperature distribution, it is evident that corrections for inhomogeneity are impracticable if not impossible.

#### 8.1.6 General Calibration Methods

The temperature-emf relation of a homogeneous [13] thermocouple is a definite physical property and therefore does not depend upon the details of the apparatus or method employed in determining this relation. Consequently, there are numerous methods of calibrating thermocouples, the choice of which depends upon the type of thermocouple, temperature range, accuracy required, size of wires, apparatus available, and personal preference. However, the emf of a thermocouple with its measuring junction at a specified temperature depends upon the temperature difference between its measuring and reference junctions. Therefore, whatever method of calibration is used, the reference junction must be maintained constant at some known temperature (see Chapter 7), and this temperature must be stated as a necessary part of the calibration results.

Thermocouple calibrations are required with various degrees of accuracy ranging from 0.1 to 5 or  $10^\circ\text{C}$ . For an accuracy of  $0.1^\circ\text{C}$ , agreement with the IPTS-68 and methods of interpolating between the calibration points become problems of prime importance, but for an accuracy of about  $10^\circ\text{C}$  comparatively simple methods of calibration usually will suffice. The most accurate calibrations in the range  $-260^\circ\text{C}$  ( $-436^\circ\text{F}$ ) to  $300^\circ\text{C}$  ( $572^\circ\text{F}$ ) are made by comparing the couples directly with a standard platinum-resistance thermometer in a stirred liquid bath. In the range 300 to  $630^\circ\text{C}$  ( $572$  to  $1166^\circ\text{F}$ ) (and below if a platinum-resistance thermometer and stirred liquid bath is not available) thermocouples are calibrated most accurately at the freezing or boiling points of pure substances. Between  $630$  and  $1064^\circ\text{C}$  ( $1166$  and  $1947^\circ\text{F}$ ), the Type S thermocouple calibrated at  $630.74^\circ\text{C}$  and the freezing points of gold and silver, serves to define the IPTS-68, and other types of thermocouples are calibrated most accurately in this range by direct comparison with a Type S thermocouple calibrated as specified. Other ther-

mocouples may be calibrated just as accurately at the fixed points as the Type S thermocouple, but interpolated values at intermediate points may depart slightly from the IPTS-68. Above 1064°C (1947°F), the most basic calibrations are made by observing the emf when one junction of the thermocouple is in a blackbody furnace, the temperature of which is measured with an optical pyrometer. However, the difficulties encountered in bringing a blackbody furnace to a uniform temperature make the direct comparison of these two types of instruments by no means a simple matter.

Although the Type S thermocouple serves to define the IPTS-68 only in the range 630.74 to 1064.43°C, this type of thermocouple calibrated at fixed points is used extensively both above and below this range as a reference thermometer in the calibration of other thermocouples. For most industrial purposes a calibration accurate to 2 or 3°C in the range room temperature to 1200°C (2192°F) is sufficient. Other thermocouples can be calibrated by comparison with such a Type S reference thermocouple almost as accurately as the calibration of the reference thermocouple is known. However, it might be pointed up that outside the range 630.74 to 1064.43°C any type of thermocouple suitable for the purpose, and calibrated to agree with the resistance thermometer or optical pyrometer in their respective ranges, has as much claim to yielding temperatures on the IPTS-68 as the Type S thermocouple. In fact, at the lower temperatures certain types of base-metal couples are definitely better adapted for precise measurements.

The calibration of couples then may be divided into two general classes, depending upon the method of determining the temperature of the measuring junction: (1) calibration at fixed points and (2) calibration by comparison with standard instruments such as thermocouples, resistance thermometers, etc.

In order to obtain the high accuracies referred to previously and usually associated with calibrations at fixed points, it is necessary to follow certain prescribed methods and to take the special precautions described in detail in the following paragraphs, but for an accuracy of about 5°C the more elaborate apparatus to be described need not be employed.

### *8.1.7 Calibration Uncertainties*

The several factors which contribute to the uncertainties in the emf versus temperature relationship for a particular thermocouple as determined by calibration may be grouped into two kinds; those influencing the observations at calibration points, and those arising from any added uncertainty as a result of interpolation between the calibration points. Errors from either of these sources of uncertainty can be reduced materially, within limits, through use of well designed equipment and careful techniques; hence, the required accuracy should be clearly understood when choosing calibration facilities.

Estimates of the uncertainties in calibrating homogeneous thermocouples by different techniques are given in Tables 8.3, 8.4, 8.5, 8.6, and 8.7. The estimates assume that reasonable care is exercised in the work. More or less accurate results are possible using the same methods, depending upon soundness of the techniques used. While excessive care is a waste when relatively crude measurements are sufficient, it should be emphasized that inadequate attention to possible sources of error is more often found to be the practice than the converse. In the following some of the important considerations associated with the various calibration methods are emphasized briefly.

*8.1.7.1 Uncertainties Using Fixed Points*—The equilibrium temperatures listed in Table 8.2 are sufficiently exact, and the materials are readily available in high enough purity, that accurate work can be done using these fixed points with no significant error being introduced by accepting the temperatures listed. Using freezing points, however, good designs of freezing point cells and furnaces are important for controlling the freezes and for providing sufficient immersion for the thermocouple, if the full potential of the method is to be realized.

Although uncertainties of the order of  $\pm 1^\circ\text{C}$  in the temperatures are assigned to the freezing points (and hence by implication to the melting points) of palladium and platinum, these contribute in only a minor way overall uncertainties of calibrations using freezing point techniques.

*8.1.7.2 Uncertainties Using Comparison Methods*—The accuracy attained at each calibration point using the comparison method will depend upon the degree to which the reference thermometer and the test thermocouple are maintained at the same temperature and the accuracy of the reference thermometer used. Comparison measurements made in stirred liquid baths usually present no special problems provided that sufficient immersion is used. Because of the high-thermal conductivity of copper, special attention

TABLE 8.3—Calibration uncertainties using fixed point techniques.

| Type | Temperature Range, $^\circ\text{C}$ | Calibration Points <sup>a</sup> | Calibration Uncertainty              |  |
|------|-------------------------------------|---------------------------------|--------------------------------------|--|
|      |                                     |                                 | At Observed Points, $^\circ\text{C}$ | Of Interpolated Values, $^\circ\text{C}$ |
| S    | 0 to 1100                           | Zn, Sb <sup>b</sup> , Ag, Au    | 0.2                                  | 0.3                                      |
| R    | 0 to 1100                           | Sn, Zn, Al, Ag, Au              | 0.2                                  | 0.5                                      |
| B    | 600 to 1100                         | Al, Ag, Au                      | 0.2                                  | 0.5                                      |
| E    | 0 to 870                            | Sn, Zn, Al                      | 0.2                                  | 0.5                                      |
| J    | 0 to 760                            | Sn, Zn, Al                      | 0.2                                  | 1.0                                      |
| K    | 0 to 1100                           | Sn, Zn, Al, Ag, Au              | 0.2                                  | 1.0                                      |

<sup>a</sup>Metal freezing points.

<sup>b</sup>Temperature measured by standard platinum resistance thermometer.

TABLE 8.4—*Calibration uncertainties using comparison techniques in laboratory furnaces (Types R or S standards).*

| Type   | Temperature Range, °C | Calibration Points <sup>a</sup> | Calibration Uncertainty |                            |
|--------|-----------------------|---------------------------------|-------------------------|----------------------------|
|        |                       |                                 | At Observed Points, °C  | Of Interpolated Values, °C |
| R or S | 0 to 1100             | about every 100°C               | 0.3                     | 0.5                        |
| B      | 600 to 1100           | about every 100°C               | 0.3                     | 0.5                        |
| E      | 0 to 870              | about every 100°C               | 0.5                     | 0.5                        |
| J      | 0 to 760              | about every 100°C               | 0.5                     | 1.0                        |
| K      | 0 to 1100             | about every 100°C               | 0.5                     | 1.0                        |

TABLE 8.5—*Calibration uncertainties using comparison techniques in stirred liquid baths.*

| Type | Temperature Range, °C | Calibration Points | Type of Standard <sup>a</sup> | Calibration Uncertainty |                            |
|------|-----------------------|--------------------|-------------------------------|-------------------------|----------------------------|
|      |                       |                    |                               | At Observed Points, °C  | Of Interpolated Values, °C |
| E    | -196 to 425           | about every 100°C  | PRT                           | 0.1                     | 0.2                        |
|      | -196 to 435           | about every 50°C   | PRT                           | 0.1                     | 0.1                        |
|      | -196 to 435           | about every 50°C   | E or T                        | 0.2                     | 0.2                        |
| T    | -56 to 200            | about every 50°C   | LIG                           | 0.1                     | 0.1                        |
|      | -196 to 250           | about every 100°C  | PRT                           | 0.1                     | 0.2                        |
|      | -196 to 250           | about every 50°C   | PRT                           | 0.1                     | 0.1                        |
|      | -196 to 250           | about every 50°C   | E or T                        | 0.2                     | 0.2                        |
|      | -56 to 200            | about every 50°C   | LIG                           | 0.1                     | 0.1                        |

<sup>a</sup>PRT = standard platinum resistance thermometer; E or T = Type E or T thermocouple; and LIG = liquid-in-glass thermometer.

TABLE 8.6—*Calibration uncertainties: tungsten-rhenium type thermocouples.*

|                    | Calibration Uncertainty |                                     |
|--------------------|-------------------------|-------------------------------------|
|                    | At Observed Points      | Of Interpolated Values <sup>a</sup> |
| Gold (1064.43°C)   | ±0.5°C                  | 1000 to 1455°C, ±2.7°C              |
| Nickel (1455°C)    | ±3.5°C                  | 1455 to 1554°C, ±4.0°C              |
| Palladium (1554°C) | ±3.0°C                  | 1554 to 1768°C, ±4.0°C              |
| Platinum (1769°C)  | ±3.0°C                  | 1768 to 2000°C, ±7.0°C              |
| Rhodium (1963°C)   | ±5.0°C                  |                                     |

<sup>a</sup>These values apply only when all five observed points are taken.

TABLE 8.7—*Calibration uncertainties using comparison techniques in special furnaces (optical pyrometer standard).*

| Type                        | Temperature Range, °C | Calibration Uncertainty |   |
|-----------------------------|-----------------------|-------------------------|---|
|                             |                       | At Observed Points, °C  | Of Interpolated Values, <sup>a</sup> °C |
| IrRh versus Ir <sup>b</sup> | 1000 to 1300          | 2                       | 3                                       |
| IrRh versus Ir <sup>b</sup> | 1300 to 1600          | 3                       | 4                                       |
| IrRh versus Ir <sup>b</sup> | 1600 to 2000          | 5                       | 8                                       |
| W versus WRe <sup>c</sup>   | 1000 to 1300          | 2                       | 3                                       |
| W versus WRe <sup>c</sup>   | 1300 to 1600          | 3                       | 4                                       |
| W versus WRe <sup>c</sup>   | 1600 to 2000          | 5                       | 8                                       |
| R, S, or B                  | 1100 to 1450          | 2                       | 3                                       |
| B                           | 1450 to 1750          | 3                       | 5                                       |

<sup>a</sup>Using difference curve from reference table with calibration points spaced every 200°C.

<sup>b</sup>40Ir60Rh versus Ir, 50Ir50Rh versus Ir, or 60Ir10Rh versus Ir.

<sup>c</sup>W versus 74W26Re, 97W3Re versus 75W25Re, or 95W5Re versus 74W26Re.

should be given to the problem of immersion when calibrating Type T thermocouples.

As higher and higher temperatures are used, the difficulties of maintaining the test and reference thermocouples at the same measured temperature are magnified whether a tube furnace, an oven with moderating block, or whatever means is used for maintaining the desired temperature. In addition, at temperatures of about 1500°C (2732°F), and higher, the choice of insulating materials becomes very important (see Chapter 4). Special attention must be paid to possible errors arising from contamination from the insulators or protection tube and from electrical leakage.

When an optical pyrometer is used as the reference thermometer, a good blackbody must be used, and the design must be such that the test thermocouple is at the same temperature as the blackbody.

## 8.2 Calibration Using Fixed Points

The indications of the Type S thermocouple calibrated at 630.74°C and the silver and gold points, as mentioned in Section 8.1.1, define the IPTS-68 between 630.74°C (1167°F) and 1064.43°C (1948°F). If such a thermocouple is calibrated also at the zinc point, a reference thermometer will result which is accurate to about 0.3°C in the range 0 to 1100°C (32 to 2012°F). While the fixed-point calibration is prescribed for defining the IPTS-68, similar methods are also useful in the calibration of other types of thermocouples. Fixed points can be used with various degrees of accuracy, ranging from 0.1 to 5°C, for the calibration of various types of thermocouples in

the range  $-260^{\circ}\text{C}$  ( $-436^{\circ}\text{F}$ ) to the melting point of platinum at  $1769^{\circ}\text{C}$  ( $3216^{\circ}\text{F}$ ). Some of the fixed points for which values have been determined accurately are listed in Section 8.1.1, Table 8.2. Because of experimental difficulties, fixed points at temperatures higher than the freezing point of copper usually are realized as melting points rather than freezing points, as described later.

### 8.2.1 Freezing Points

The emf developed by a homogeneous thermocouple at the freezing point of a metal is constant and reproducible if all of the following conditions are fulfilled: (1) the thermocouple is protected from contamination; (2) the thermocouple is immersed in the freezing-point sample sufficiently far to eliminate heating or cooling of the measuring junction by heat flow along the wires and protection tube; (3) the reference junctions are maintained at a constant and reproducible temperature; (4) the freezing-point sample is pure, and (5) the metal is maintained at essentially a uniform temperature during freezing.

Techniques for achieving these conditions are well developed [12,14,15]. Many of the metals listed in Table 8.2 of Section 8.1.1 are available commercially in high purity (99.999 percent or better) and can be used assuming the freezing point temperatures given in the table. It is essential, however, that protecting tubes and crucibles be chosen of such material (see Section 4) that the pure metals will not be contaminated. Copper and silver must be protected from oxygen contamination [12] and it is also advisable to protect aluminum and antimony; this is done usually by using covered crucibles and covering the freezing point metals with powdered graphite or by sealing the crucible in a glass tube that contains a nonoxidizing gas such as argon or helium. The choice of a suitable furnace is also important. The furnace must provide uniform heating in the region of the freezing point sample, and have adequate controls to bring the sample slowly into its freeze. Complete units consisting of freezing point sample, crucible, and furnace are available commercially. Freezing point standard samples of tin, lead, zinc, aluminum, and copper may be purchased from the National Bureau of Standards.

### 8.2.2 Melting Points

The emf of a thermocouple at the melting point of a metal may be determined with the same apparatus as that described above for freezing points, but the use of the freeze is usually more satisfactory. Melting points are used to advantage, however, when only a limited amount of material is available or at high temperatures where experimental techniques with freezing points are difficult. To apply this method [16-19], a short length of metal whose melting point is known is joined between the end of the two wires of the ther-



mocouple and placed in an electrically heated furnace the temperature of which is raised slowly. When the melting point of the metal is reached, the emf of the thermocouple remains steady for a few minutes and then drops to zero as the fused metal drops away from the junction. With good technique<sup>4</sup> the method can result in accuracies comparable to those with which the IPTS-68 is realized above 1064°C by optical pyrometry.

### 8.3 Calibration Using Comparison Methods

The calibration of a thermocouple by comparison with a reference thermometer [20] is sufficiently accurate for most purposes and can be done conveniently in most industrial and technical laboratories. The success of this method usually depends upon the ability of the observer to bring the measuring junction of the thermocouple to the same temperature as the actuating element of the reference thermometer, such as the measuring junction of a standard thermocouple or the bulb of a resistance or liquid-in-glass thermometer. The accuracy obtained is further limited by the accuracy of the reference thermometer. Of course, the reference junction temperature must be known, but this can be controlled, as described in Chapter 7. The method of bringing the measuring junction of the thermocouple to the same temperature as that of the actuating element of the reference thermometer depends upon the type of thermocouple, type of reference thermometer, and the method of heating.

#### 8.3.1 Laboratory Furnaces

The calibration procedure consists of measuring the emf of the thermocouple being calibrated at selected calibration points, the temperature of each point being measured with a reference thermometer. The number and choice of calibration points will depend on the type of thermocouple, the temperature range covered, and the accuracy required (see Sections 8.1.6 and 8.4).

*8.3.1.1 Noble-Metal Thermocouples*—Such thermocouples usually may be calibrated at temperatures from ambient up to 1200°C by comparison with either a Type S or Type R reference thermocouple in electrically heated furnaces. Above 1200°C (2192°F) the Type B thermocouple is a preferred reference thermometer because of its greater stability at high temperatures. This thermocouple may be used to 1700°C (3092°F) or higher.

One method for the comparison of two such thermocouples is based upon the simultaneous reading of the emf of the reference and the test thermocouple without waiting for the furnace to stabilize at any given temperature. The measuring junctions are maintained always at close to the same temperature

<sup>4</sup>This method is not well adapted to metals that oxidize rapidly, and, if used with materials whose melting temperature is altered by the oxide, the metal should be melted in a neutral atmosphere.

by welding them into a common bead or by wrapping them together with platinum wire or ribbon. A separate potentiometer is used to measure each emf, one connected to each thermocouple, and each potentiometer is provided with a reflecting galvanometer. The two spots of light are reflected into a single scale, the galvanometers being set in such a position that the spots coincide at the zero point on the scale when the circuits are open, and therefore also when the potentiometers are set to balance the emf of each thermocouple. Simultaneous readings are obtained by setting one potentiometer to a desired value and adjusting the other so that both spots of light pass across the zero of the scale together as the temperature of the furnace is raised or lowered.

By making observations first with a rising and then with a falling temperature, the rates of rise and fall being approximately equal, and taking the mean of the results found, several minor errors such as those due to differences in the periods of the galvanometers, etc., are eliminated or greatly reduced.

This method is particularly adapted to the calibration of thermocouples at any number of selected points. For example, if it is desired to determine the temperature of a thermocouple corresponding to 10.0 mV, this emf is set up on the potentiometer connected to the thermocouple, the emf of the reference thermocouple observed as desired above, and the temperature obtained from the emf of the reference. If it is desired to determine the emf of a thermocouple corresponding to 1000°C (1832°F), the emf of the reference thermocouple corresponding to this temperature is set up on the potentiometer connected to the reference thermocouple, and the emf of the thermocouple being calibrated is observed directly with the second potentiometer. To reduce the time required to calibrate by this method the furnace should be so constructed that it will heat or cool rapidly. Fast response is obtained in one furnace design which employs a nickel-chromium tube as the heating element [14].

A similar furnace using a silicon carbide tube as the heating element can be used to extend the calibration range upward [7]. At temperatures above 1064°C (1947°F) the IPTS-68 is defined in terms of ratios of radiation (Section 8.1.1) usually measured with a visual or a photoelectric optical pyrometer. If the test thermocouple is inserted into the back of a blackbody cavity built into the furnace, a pyrometer may be used directly as the reference thermometer. Alternatively, the Type B thermocouple can be used as the reference thermometer after it has been calibrated against a pyrometer.

The thermocouples are insulated and protected by suitable ceramic tubes (Chapter 4). It is essential that good insulation be maintained between the two potentiometers and thermocouple circuits except at the point where the junctions are welded together. The reference junctions are maintained at a known temperature (Chapter 7).

Variations of the two potentiometer method may be used to automate the calibration process when the thermocouple being calibrated and the reference thermocouple are of the same type [20]. If the emf of the reference is read with one potentiometer and the emf difference between the reference and the unknown are read with the second potentiometer, the calibration data may be recorded automatically [21, 22].

If two potentiometers are not available for taking simultaneous readings, the furnace may be brought to essentially a constant temperature, and the emf of each thermocouple read alternately on one instrument [20].

When the thermocouples are calibrated by welding or wrapping the junctions together, both would be expected to be close to the same temperature even when the temperature of the furnace is changing. If it is necessary or advisable to calibrate the thermocouples without removing them from the protecting tubes, then the junctions of the thermocouple being tested and that of the reference thermocouple should be brought as close together as possible in a uniformly heated portion of the furnace. In this case it is necessary that the furnace be brought to approximately a constant temperature before taking observations.

There are a number of other methods of heating and of bringing the junctions to approximately the same temperature, for example, inserting the thermocouples properly protected into a bath of molten metal or into holes drilled in a large metal block. The block of metal may be heated in a muffle furnace or, if made of a good thermal conductor such as copper, may be heated electrically. Tin, which has a low melting point, 232°C (450°F), and low volatility, makes a satisfactory bath material. The thermocouples should be immersed to the same depth with the junctions close together. Ceramic tubes are sufficient protection, but to avoid breakage by thermal shock when immersed in molten metal it is preferable to place them inside of secondary tubes of iron, nickel-chromium, graphite, or similar material. In all of these methods, particularly in those cases in which the junctions of the thermocouples are not brought into direct contact, it is important that the depth of immersion be sufficient to eliminate cooling or heating of the junctions by heat flow along the thermocouple and the insulating and protecting tubes. This can be determined by observing the change in the emf of the thermocouple as the depth of immersion is changed slightly. If proper precautions are taken, the accuracy yielded by any method of heating or bringing the junctions to the same temperature may be as great as that obtained by any other method.

*8.3.1.2 Base-Metal Thermocouples*—The methods of testing base-metal thermocouples above room temperature are generally the same as those just described for testing noble-metal thermocouples with the exception, in some cases, of the methods of bringing the junctions of the reference and the thermocouple being tested to the same temperature and the methods of protecting platinum-rhodium reference thermocouples from contamination. One

arrangement of bringing the junction of a platinum-rhodium reference thermocouple to the same temperature as that of a large base-metal thermocouple for accurate calibration is to insert the junction of the reference thermocouple into a small hole (about 1.5 mm (0.06 in.) in diameter) drilled in the hot junction of the base-metal thermocouple. The platinum-rhodium reference thermocouple is protected by ceramic tubes to within a few tenths of an inch of the hot junction, and the end of the ceramic tube is sealed to the thermocouple by pyrex glass or by a small amount of kaolin and water-glass cement. This prevents contamination of the reference thermocouple, with the exception of the small length of about 2.5 mm (0.1 in.) which is necessarily in contact with the base-metal thermocouple. If the furnace is uniformly heated in this region (and it is of little value to make such a test unless it is) contamination at this point will not cause any error. If the wire of the reference thermocouple becomes brittle at the junction, this part of the wire may be cut off and enough wire drawn through the softened seal to form a new junction. The seal should be examined after each test and remade if it does not appear to be good. More than one base-metal thermocouple may be welded together and the hole drilled in the composite junction. The thermocouples should be clamped in place so that the junctions remain in contact. If two potentiometers are used for taking simultaneous readings, the temperature of the furnace may be changing as much as a few degrees per minute during an observation, but if a single instrument is used for measuring the emf, the furnace temperature should be maintained practically constant during observations. When wires, insulators, and protection tubes are large, tests should be made to ensure that the depth of immersion is sufficient.

### 8.3.2 *Stirred Liquid Baths*

At temperatures below 620°C (1148°F) stirred liquid baths provide an efficient medium for bringing a thermocouple and a reference thermometer to the same temperature.

Water, petroleum oils, or other organic liquids, depending upon temperature range, are commonly used bath media. Molten salts or liquid tin are used at temperatures higher than are suitable for oil. Baths suitable for this work are described in Ref 23.

Base-metal thermocouples, either bare wire or insulated, may be calibrated accurately in such baths. Usually no special preparation of the thermocouple will be required other than to insert it to the bottom of a protection tube for immersion in the liquid bath. Borosilicate glass tubing, such as Pyrex glass, is convenient for use up to 500°C (932°F). Vitreous silica or ceramic tubing may be used to 620°C (1148°F). The tube should be closed at the immersed end and of an internal diameter such as to permit easy insertion of the thermocouple or thermocouples to be calibrated but no larger than necessary. Unfavorable heat transfer conditions in an unnecessarily

large diameter tube will require a greater depth of immersion in the bath than would a close fitting tube. If a bare wire thermocouple is being calibrated, the wires must be provided with electrical insulation over the length inserted in the protection tube. Sheathed thermocouples may be immersed directly in the bath liquid in cases where the sheath material will not be attacked by the liquid. Salt baths for use at high temperature must be provided with suitable wells into which the thermocouple protection tubes and reference thermometers may be inserted for protection from the molten salt.

The reference thermometer may be a calibrated thermocouple inserted in the protection tube with the thermocouple being calibrated, or it may be a liquid-in-glass thermometer or a resistance thermometer immersed in the bath close to the thermocouple protection tube. The choice of a reference thermometer will be governed principally by the degree of uncertainty which can be tolerated.

### 8.3.3 *Fixed Installations*

After thermocouples have been used for some time at high temperatures, it is difficult, if not impossible, to determine how much the calibrations are in error by removing them from an installation and testing in a laboratory furnace. The thermocouples are usually heterogeneous after such use and in such a condition that the emf developed by the thermocouples depends upon the temperature distribution along the wires [24]. If possible, such a thermocouple should be tested under the same conditions and in the same installation in which it is used. Although it is not usually possible to obtain as high a precision by testing the thermocouple in place as is obtained in laboratory tests, the result is far more useful in the sense of being representative of the behavior of the thermocouple [19]. The calibration is accomplished by comparing the thermocouple with a reference thermocouple.

In this case, as in the calibration of any thermocouple by comparison methods, the main objective is to bring the measuring junction to the same temperature as that of the thermocouple being tested. One method is to drill a hole in the furnace, flue, etc., at the side of each thermocouple permanently installed, large enough to permit insertion of the reference thermocouples. The hole is kept plugged, except when tests are being made. The reference thermocouple is inserted through this hole to the same depth as the thermocouple being tested with the measuring junction ends of the protecting tubes as close together as possible. Preferably a potentiometer should be used to measure the emf of the reference thermocouple.

In many installations the base-metal thermocouple and its protecting tube are mounted inside another protecting tube of iron, fire clay, carborundum, or some other refractory which is permanently cemented or fastened into the furnace wall. Frequently there is room to insert a reference thermocouple in this outer tube alongside of the fixed thermocouple. A third method, much

less satisfactory, is to wait until the furnace, flue, etc., have reached a constant temperature and make observations with the thermocouple being tested, then remove this thermocouple and insert the reference thermocouple to the same depth.

If desired, comparisons can be made, preferably by either of the first or second methods at several temperatures, and a curve obtained for each permanently installed thermocouple showing the necessary corrections to be applied to its readings. Although testing a thermocouple at one temperature yields some information, it is not safe to assume that the changes in the emf of the thermocouple are proportional to the temperature or to the emf. For example, it has been observed that a thermocouple which had changed in use by the equivalent of  $9^{\circ}\text{C}$  at  $315^{\circ}\text{C}$  ( $16^{\circ}\text{F}$  at  $599^{\circ}\text{F}$ ) had changed only the equivalent of  $6^{\circ}\text{C}$  at  $1100^{\circ}\text{C}$  ( $11^{\circ}\text{F}$  at  $2012^{\circ}\text{F}$ ).

It may be thought that the method of calibrating thermocouples under working conditions is unsatisfactory because, in most furnaces used in industrial processes, large temperature gradients exist, and there is no certainty that the reference thermocouple is at the same temperature as the thermocouple being tested. This objection, however, is not serious, because if temperature gradients do exist of such a magnitude as to cause much difference in temperature between two similarly mounted thermocouples located close together, the reading of the reference thermocouple represents the temperature of the fixed thermocouple as closely as the temperature of the latter represents that of the furnace.

Another advantage of calibrating thermocouples in the same installation in which they are used is that the thermocouple, extension wires, and indicator are tested as a unit and under the conditions of use.

#### 8.4 Interpolation Methods

An experimental thermocouple calibration consists of a series of voltage measurements determined at a finite number of known temperatures. If a test thermocouple were compared with a standard temperature instrument at 100 temperatures within a  $5^{\circ}\text{C}$  ( $10^{\circ}\text{F}$ ) range, there would be little need for interpolation between the calibration points. However, if from 4 to 10 calibration points are all that can be afforded in a given range of interest, then what is needed to characterize an individual thermocouple is a continuous relation, by means of which temperatures can be approximated with a minimum uncertainty from voltage measurements at intermediate levels. Efforts to obtain such a continuous relation appear thwarted from the start because of the small number of discrete calibration points available. However, interpolation between the calibration points is possible since the emf changes only slowly and smoothly with temperature.

One can present raw calibration data directly in terms of temperature ( $T$ ) and voltage ( $E_{\text{couple}}$ ), on a scale so chosen that the information appears well represented by a single curve (see Fig. 8.1) or by a simple mathematical

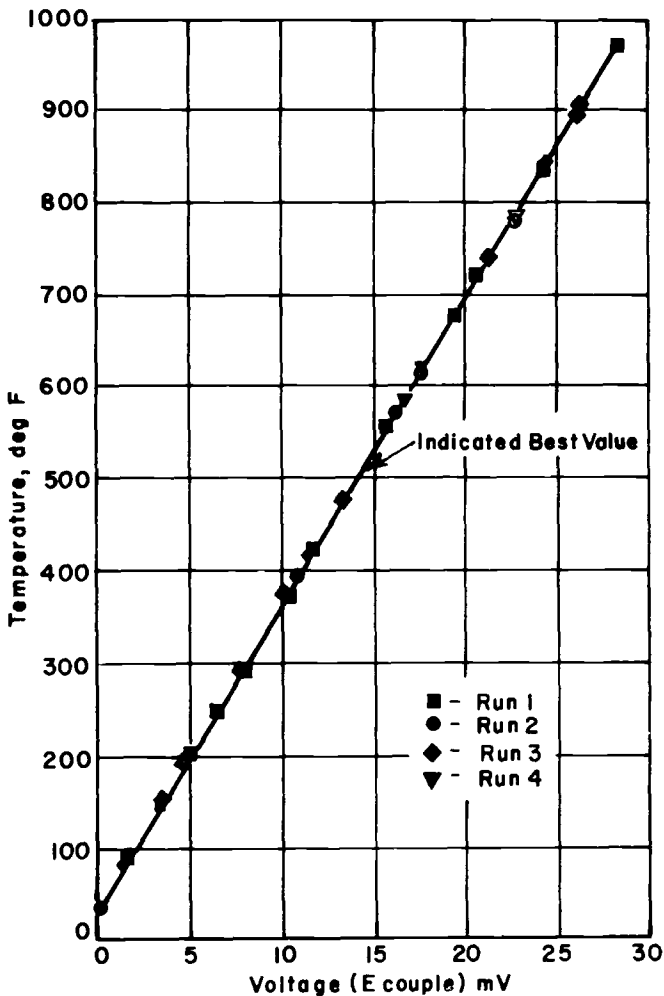


FIG. 8.1—Temperature emf plot of raw calibration data for an iron/constantan thermocouple.

equation. For example, for the highest accuracy in the range 630 to 1064°C with the Type S thermocouple, the method is that prescribed in Ref 12. An equation of the form  $e = a + bt + ct^2$ , is used where  $a$ ,  $b$ , and  $c$  are constants determined by calibration at the freezing points of gold, silver, and antimony. By calibrating the thermocouple also at the freezing point of zinc and using an equation of the form  $e = a + bt + ct^2 + dt^3$ , the temperature range can be extended down to 400°C without introducing an uncertainty of more than 0.1°C in the range 630 to 1064°C. By calibrating the thermocouple at freezing points of gold, antimony, and zinc and using an equation of

the form  $e = a + bt + ct^2$ , a calibration is obtained for the range 400 to 1100°C, which agrees with IPTS-68 to 0.5°C. However, in general, this practice of directly representing thermocouple characteristics does not yield results within the required limits of uncertainty.

A better method<sup>5</sup> is based on the use of differences between observed values and values obtained from standard reference tables. Such reference tables and the mathematical means for generating them are presented in Chapter 10 of this Manual. The data of Fig. 8.1 are replotted in Fig. 8.2 in terms of differences from the proper reference table. The maximum spread between points taken at the same level (replication), but obtained in random order with respect to time and level (randomization) is taken as the uncertainty envelope. This information, taken from Fig. 8.2 is plotted in Fig. 8.3, and constitutes a vital bit of information about the particular thermocouple and the calibration system. In lieu of an experimental determination of the uncertainty, one must rely on judgment or on the current literature for this information.

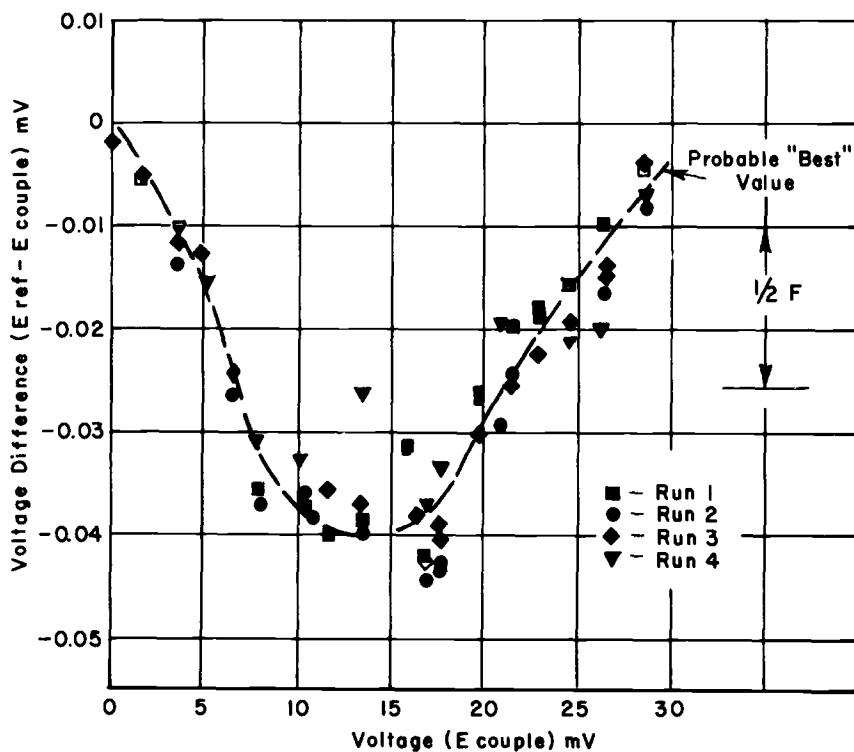


FIG. 8.2—Difference plot of raw calibration data for an iron/constantan thermocouple.

<sup>5</sup>Much of the material in this section is based on Refs 25 to 27.



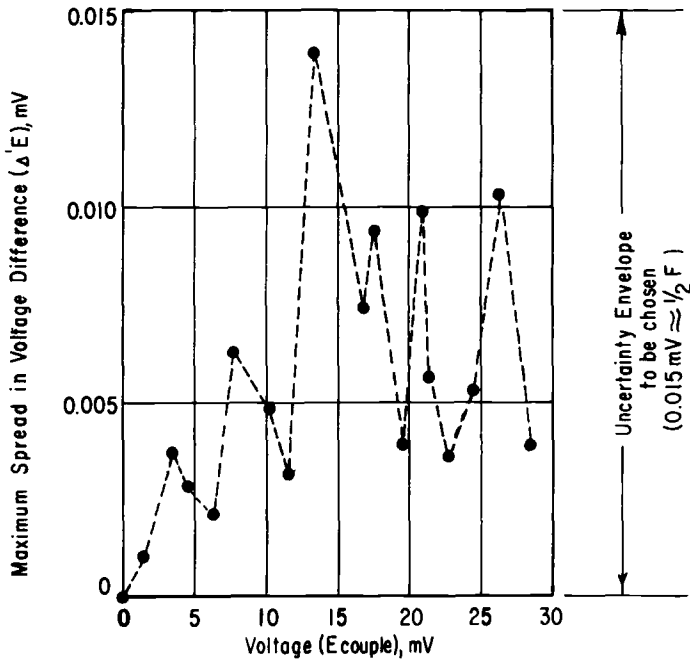


FIG. 8.3—Typical determination of uncertainty envelope (from data of Fig. 8.2).

Usually, only a single set of calibration points is available. Typical points would be those taken from one run shown in Figs. 8.1 or 8.2, and these are shown in Fig. 8.4 together with four of the many possible methods for representing the thermocouple difference characteristic. Although at first it appears that the most probable relation characterizing a given thermocouple is sensibly indeterminate from a single set of calibration points, it is an important fact that all experimental points must be contained within the uncertainty interval when the uncertainty interval is centered on the most probable interpolation equation.

Making use of this principle, together with the fact that overall experimental uncertainties are minimized by use of the least squares technique, one starts the search for the most probable interpolation equation by passing a least squares equation of the first degree through the experimental data. A check is then made to ascertain whether all experimental points are contained within the uncertainty envelope which is centered on the linear interpolation equation (see Fig. 8.5). One proceeds, according to the results of the foregoing check, to the next highest degree equation, stopping at the lowest degree least squares equation which satisfies the uncertainty requirements. For the example given here, a third degree interpolation equation is required

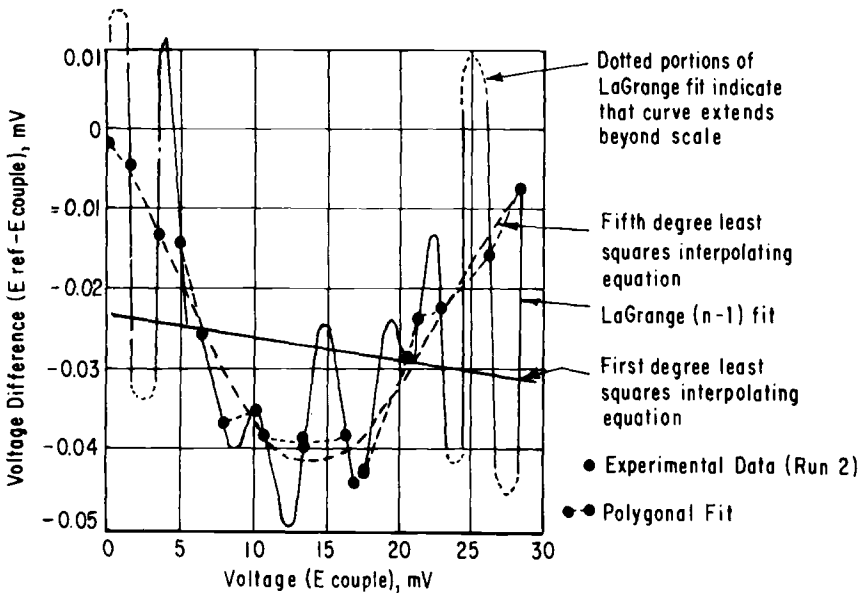


FIG. 8.4—Various possible empirical representations of the thermocouple characteristic (based on a single calibration run).

(see Fig. 8.6). By obtaining voltage differences from the least squares fit of any set of calibration points, the uncertainty in the thermocouple difference characteristic will be within one half the uncertainty interval. Generally, the form of the uncertainty envelope and the degree of the most probable least squares interpolation equation are strongly dependent on the amount of calibration data available and on the temperature range under consideration. It is recommended that the number of distinct calibration points available should be at least 2 (degree +1). The factor two is arrived at from numerical analysis reasoning. A distinct calibration point is defined arbitrarily as one which is separated, temperaturewise, from all other points in the set by as much as one tenth the difference in temperature between the maximum and minimum temperatures of the particular run. The choice of one tenth presupposes a maximum practical degree of four for the least squares interpolation equation, in keeping with the low degree requirement of numerical analysis. Indeed, if the data cannot be represented by a fourth degree interpolation equation, one should increase the uncertainty interval and start the fitting procedure again.

Thus, in general, by using the proper reference table in conjunction with a difference curve, greater precision in temperature determination by means of thermocouples can be obtained from a given number of calibration points than from the use of the calibration data alone.

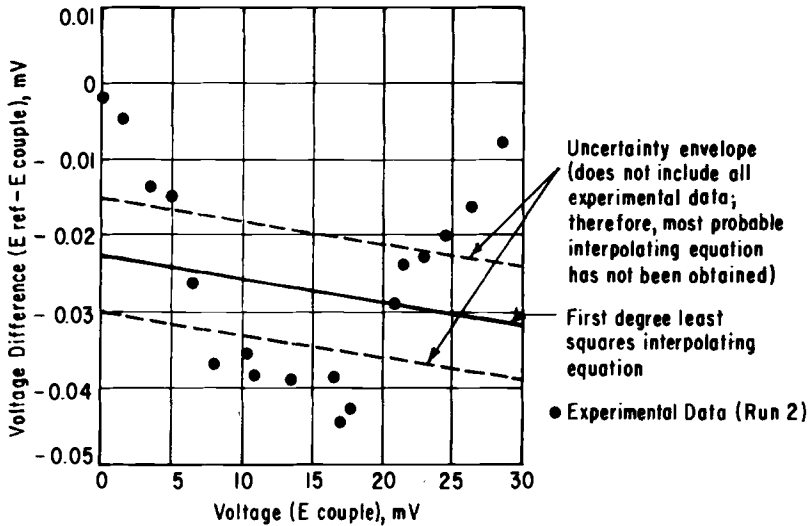


FIG. 8.5—Uncertainty envelope method for determining degree of least squares interpolating equation for a single calibration run (linear).

### 8.5 Single Thermoelement Materials

The standard method provided by ASTM for evaluating the emf characteristics of single thermoelement materials used in thermocouples for temperature measurement is designated as E 207 and is entitled "Standard Method of Thermal Emf Test of Single Thermoelement Materials by Comparison with a Secondary Standard of Similar Emf-Temperature Properties." The method covers the determination of the thermoelectromotive force of single thermoelement materials (thermoelements), against standard platinum, the cold junction being at the ice point, by comparison to the thermoelectromotive force of a working standard thermoelement of similar emf-temperature properties independently standardized with respect to the same standard platinum.

*Summary of Method*—The test thermoelements are welded to the working standard to form the test thermocouple. The method involves measuring the small electromotive force developed between the test thermoelement and the secondary working standard having emf-temperature properties similar to the thermoelement being evaluated. The thermoelectromotive force of the test thermoelement then is determined by algebraically adding this measured small emf to the known emf of the secondary working standard referenced to the standard platinum. The testing circuit is shown schematically in Fig. 8.7. Since the thermal emfs (against any reference material) of the test and standard thermoelements are similar, it is unnecessary to accurately control or

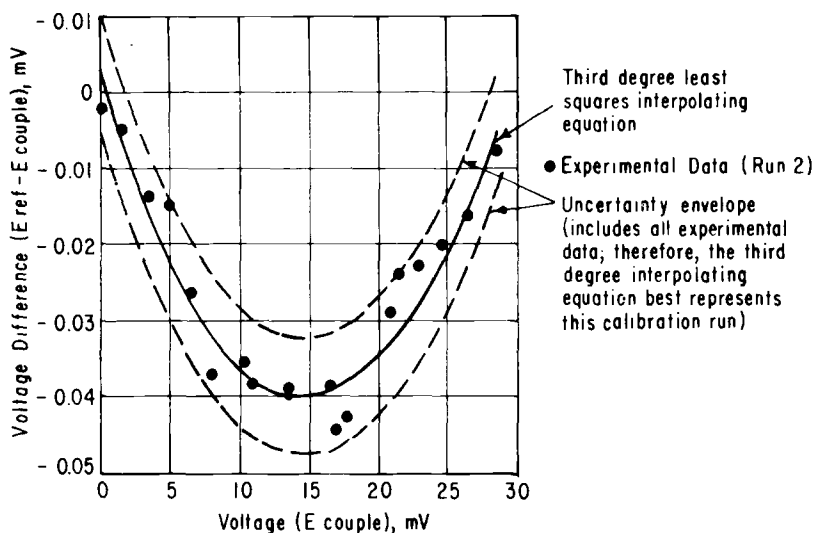


FIG. 8.6—Uncertainty envelope method for determining degree of least squares interpolating equation for a single calibration run (cubic).

measure the junction temperatures because the difference in emf changes insignificantly even for large changes in temperature at the junctions. Actually, the need for the accurate control of the measuring and reference junction temperatures is not eliminated, but merely is shifted to an accurate laboratory method which calibrates the secondary standard against the standard platinum [20].

### 8.5.1 Test Specimen

The test specimen is a length of wire, rod, ribbon, or strip of the coil or spool of the thermoelement material to be evaluated. The length is adequate to prevent the transfer of heat from the measuring junction to the reference junction during the period of test. A length of 0.6 to 1.2 m (2 to 4 ft), depending on the length of the testing medium and the transverse size of the thermoelement, is generally satisfactory. The transverse size of the specimen is limited only by the size of the test medium, the relative convenience of handling the specimens and reference thermoelement, and the maintenance of an isothermal test temperature junction.

### 8.5.2 Reference Thermoelement

A reference thermoelement is used which has emf-temperature properties similar to that of the test specimen and which previously has been standard-

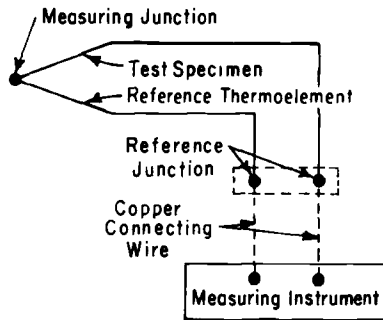


FIG. 8.7—Circuit diagram for thermal emf test.

ized thermoelectrically with respect to National Bureau of Standards Platinum 67 (Pt-67). If a large amount of testing is anticipated, a coil or spool of reference thermoelement material is reserved. This material is selected on the basis of thermoelectric uniformity, and a minimum of three samples taken from the center and the ends of the coil is calibrated against the standard platinum. The reference thermoelement and the test specimen may differ in diameter, but it is convenient for their lengths to be about equal.

### 8.5.3 Reference Junction

The reference junction temperature of the test specimen and of the reference thermoelement is controlled during the period of test by maintaining it at the ice point ( $0^{\circ}\text{C}$ ). The ice-water junction is used because it is recognized as a convenient means for maintaining a constant reference temperature. The description and maintenance of the ice point are given in Chapter 7. A reference temperature other than the ice point may be used. However, the reference thermoelement should be calibrated against standard platinum using the alternate reference temperature, or the calibration data adjusted to correspond to the alternate reference temperature.

### 8.5.4 Measuring Junction

The measuring junction consists of a welded union of the test specimen and reference thermoelement. The weldment may be prepared by any method providing a good electrical connection which can be immersed fully in the uniform temperature region of the testing medium. Any number of test specimens and reference thermoelements may be welded together provided the resulting assembly does not introduce heat losses which prevent maintaining a uniform temperature region. If separation of the reference thermoelement and test specimen cannot be maintained during the test (except

where they must make contact at the measuring junction), it is necessary that they be insulated from each other.

#### 8.5.5 *Test Temperature Medium*

For temperatures up to 300°C (570°F), appropriate liquid baths may be used. For temperatures above 150°C (300°F), electrically heated tube or muffle type furnaces are recommended for comparison testing of base metal or noble metal thermoelement materials of similar emf-temperature properties. For convenience, a separate furnace may be controlled and available for each test temperature. This eliminates lost time in changing furnace temperatures when a large volume of testing is to be done. The length of each furnace is at least 381 mm (15 in.) so as to provide a minimum depth of immersion of 178 mm (7 in.) for the test thermocouple assembly. A constant immersion depth is maintained, whether single or multiple furnaces are used. The inside diameter of the furnace tube is approximately 25 to 76 mm (1 to 3 in.), the specific diameter depending upon the size and the number of the specimens to be included in the test thermocouple assembly. The furnace provides a uniform temperature zone extending at least 76 mm (3 in.) back from the measuring junction, or further if required to contain any inhomogeneity in the test thermocouple assembly. The temperature of each furnace is controlled manually or automatically to within  $\pm 10^{\circ}\text{C}$  ( $\pm 18^{\circ}\text{F}$ ) of the desired value which is ample for comparison testing of thermoelements having compositions similar to that of the reference thermoelement.

#### 8.5.6 *Emf Indicator*

The emf generated by the thermocouple, consisting of the test specimen and the reference thermoelement is measured with instrumentation sensitive to  $\pm 0.001$  mV with an accuracy over a 2 mV range of  $\pm 1$  percent of the reading plus 0.003 mV. Any millivoltmeter, with circuitry errors taken into account, or potentiometer with a galvanometer or null indicator, providing measurements within these tolerances is acceptable. An indicator with a bidirectional scale (zero center) is convenient, but a unidirectional instrument may be used if a polarity switch is provided in the copper connecting circuit, or if the copper connecting wires to the instrument are exchanged whenever the polarity between the reference thermoelement and the test specimen is reversed.

#### 8.5.7 *Procedure*

For a furnace medium the test thermocouple assembly is inserted into the furnace so that the measuring junction extends at least 76 mm (3 in.) into the uniform temperature zone taking care there is no contact between the wires and the furnace wall. The free ends of the reference thermoelement and the test specimens are bent as required so they may be inserted into the glass

tubes of the reference junction bath. Care is exercised to minimize distorting the wires prior to testing because of the effect of cold work on emf output. After bringing the test temperature to the specified value, sufficient time is provided for the test assembly to reach steady state conditions before recording the emf generated between the test specimen and the reference thermoelement.

In a similar manner the emf generated between all other test specimens in the assembly is measured with respect to the reference thermoelement. Then the test temperature is raised to the next higher specified value, or the test assembly is advanced to the next furnace or bath having the next higher specified temperature if multiple furnaces or baths are used. A second set of readings is taken at the new temperature, and the procedure is repeated with readings taken at all specified temperatures. In all cases the readings are taken in sequence from the lowest to the highest temperature to minimize test variations between producer and consumer if any of the alloys are affected by differences in short time heating cycles. A base-metal reference thermoelement is used for one series of temperature changes only. However, if a portion of it considerably exceeding the region previously exposed to the uniform heating zone is discarded, the remainder of the reference thermoelement may be used for another test assembly. For noble metals and their alloys, reuse depends on the known stability of the material involved.

The polarity of the test specimen with respect to the reference thermoelement is determined as follows:

1. If the test specimen is connected to the positive (+) terminal of an unidirectional potentiometer and balance can be achieved, the specimen is positive to the reference thermoelement.
2. If the connections must be reversed to achieve balance, that is, the reference thermoelement must be connected to the positive terminal, the test specimen is negative to the reference thermoelement.
3. If an indicating potentiometer with a bidirectional scale is used, the test specimen to the positive (+) terminal and the reference thermoelement to the negative (-) terminal are connected. The polarity of the test specimen with respect to the reference thermoelement then will be indicated by the direction of balance of the instrument scale.

The emf of the test specimen with respect to Pt-67 is then reported for each test temperature after algebraically adding the measured emf of the test specimen versus the reference thermoelement to the known emf of the reference thermoelement versus Pt-67.

## 8.6 References

- [1] "The International Practical Temperature Scale of 1968," *Metrologia*. Vol. 5, No. 2, April 1969, pp. 34-49.

- [2] Benedict, R. P., *Technical Journal*, Leeds & Northrup Co., Vol. 6, Summer Issue, 1969.
- [3] "The International Practical Temperature Scale of 1968 Amended Edition of 1975," *Metrologia*, Vol. 12, No. 1, March 1976, pp. 7-17.
- [4] Stimson, H. F., "International Practical Temperature Scale of 1948, Text Revision of 1960," NBS Monograph 37, National Bureau of Standards, 1961.
- [5] ASTM Method E 1-71, "Standard Specifications for ASTM Thermometers," *1979 Annual Book of ASTM Standards*, Part 44, p. 505.
- [6] Kostkowski, H. J. and Lee, R. D., "Theory and Methods of Optical Pyrometry," NBS Monograph 41, National Bureau of Standards, 1962.
- [7] Burns, G. W. and Gallagher, J. S., "Reference Tables for the Pt-30% Rh Versus Pt-6% Rh Thermocouple," *Journal of Research*, National Bureau of Standards, Vol. 70C, April-June 1966.
- [8] Corruccini, R. J., "Annealing of Platinum for Thermometry," *Journal of Research*, National Bureau of Standards, Vol. 47, No. 94, 1951, RP2232.
- [9] Diesselhorst, H., "Thermokraftfreier Kompensationapparat mit fünf Dekadeu und kunstanter kleinem Widerstand," *Zeitschrift für Instrumentenkunde*, Vol. 28, No. 1, 1908.
- [10] White, W. P., "Thermokraftfreie Kompensationapparat mit kleinem Widerstand und kuanstanter Galvanometereempfindlichkeit," *Zeitschrift für Instrumenteokunde*, Vol. 27, No. 210, 1907.
- [11] Behr, L., "The Wenner Potentiometer," *Review of Scientific Instruments*, Vol. 3, No. 108, 1932.
- [12] Roeser, W. F. and Lomberger, S. T., "Methods of Testing Thermocouple Materials," NBS Circular 590, National Bureau of Standards, 1958.
- [13] Finch, D. I., "General Principles of Thermoelectric Thermometry," *Temperature, Its Measurement and Control in Science and Industry*, Vol. 3, Part 2, Reinhold, New York, 1962, p. 3.
- [14] McLaren, E. H., "The Freezing Points of High Purity Metals as Precision Temperature Standards," *Temperature, Its Measurement and Control in Science and Industry*, Vol. 3, Part 1, Reinhold, New York, 1962, p. 185.
- [15] Trabold, W. G., *Temperature, Its Measurement and Control in Science and Industry*, Vol. 3, Part 2, Reinhold, New York, p. 45.
- [16] Fairchild, C. O., Hoover, W. H., and Peters, M. F., "A New Determination of the Melting Point of Palladium," *Journal of Research*, National Bureau of Standards, Vol. 2, No. 931, 1929, RP 65.
- [17] Barber, C. R., "The Calibration of the Platinum/13% Rhodium-Platinum Thermocouple Over the Liquid Steel Temperature Range," *Journal of the Iron and Steel Institute*, Vol. 147, No. 205, 1943.
- [18] Bedford, R. E., "Reference Tables for Platinum-20% Rhodium/Platinum-5% Rhodium Thermocouples," *Review of Scientific Instruments*, Vol. 35, No. 1177, 1964.
- [19] Quigley, H. C., "Resume of Thermocouple Checking Procedures," *Instruments*, Vol. 25, No. 616, 1952.
- [20] ASTM Method E 220, "Standard Method for Calibration of Thermocouples by Comparison Techniques," *1979 Annual Book of ASTM Standards*, Part 44, p. 605.
- [21] "Automatic Thermocouple Comparator," *Technical News Bulletin*, National Bureau of Standards, Vol. 47, No. 5, May 1963, p. 82.
- [22] Toenshoff, D. A., "Automatic Calibration of Thermocouples," *Technical Bulletin*, Englehard Industries, Vol. 2, No. 3, Dec. 1961, p. 88.
- [23] ASTM Method E 77, "Standard Method for Verification and Calibration of Liquid-in-Glass Thermometers," *1979 Annual Book of ASTM Standards*, Part 44, p. 566.
- [24] Dahl, A. I., "Stability of Base-Metal Thermocouples in Air from 800 to 2200°F," *Journal of Research*, National Bureau of Standards, Vol. 24, No. 205, 1940, RP 1278.
- [25] Benedict, R. P. and Ashby, F. H., "Empirical Determination of Thermocouple Characteristics," *Transactions*, American Society of Mechanical Engineers, *Journal of Engineering for Power*, Jan. 1963, p. 9.
- [26] Benedict, R. P., "Engineering Analysis of Experimental Data," *Transactions*, American Society of Mechanical Engineers, *Journal of Engineering for Power*, Jan. 1969, p. 21.
- [27] Benedict, R. P. and Godett, T. M., "A Note on Obtaining Temperatures From Thermocouple EMF Measurements," *Transactions*, American Society of Mechanical Engineers, *Journal of Engineering for Power*, Oct. 1975, p. 516.



- [28] McLaren, E. H., and Murdock, E. G., "New Considerations on the Preparation, Properties and Limitations of the Standard Thermocouple for Thermometry," *Temperature*. Instrument Society of America, Vol. 4, Part 3, 1972, p. 1543.

### *Bibliography*

*Temperature, Its Measurement and Control in Science and Industry*. Vol. 1, Reinhold, New York, 1941, Vol. 3, Parts 1 and 2, 1962, Vol. 4, Parts 1, 2, and 3, 1972.

*ASME Performance Test Codes, Instruments and Apparatus Supplement, Part 3, Temperature Measurement*, American Society of Mechanical Engineers, New York, 1973.

Benedict, R. P., *Fundamentals of Temperature, Pressure, and Flow Measurement*, Second Edition, Wiley, New York, 1977.

ASTM E 563, Preparation and Use of Freezing Point Reference Baths, American Society for Testing and Materials.

# Chapter 9—Installation Effects

---

## 9.1 Temperature Measurement in Fluids

Fluids are divided readily into two types, compressible and incompressible, or more simply into gases and liquids. However, many concepts involved in the measurement of temperatures in fluids are common to both types, and these are discussed first.

### 9.1.1 Response

No instrument responds instantly to a change in its environment. Thus in a region where temperature is changing, a thermocouple will not be at the temperature of its environment and, hence, cannot indicate the true temperature. The simplified temperature changes considered here are the step change and the ramp change. In the step change, the temperature of the environment shifts instantaneously from  $T_1$  to  $T_2$ . In the ramp change, the environment temperature shifts linearly with time from  $T_1$  to  $T_2$ .

It is common practice to characterize the response of a temperature sensor by a first order thermal time constant  $\tau$  which is defined as:

$$\tau = \frac{\rho V c}{h A} \quad (1)$$

where  $\rho$  is density,  $V$  is volume, and  $c$  is specific heat, all of the sensor; while  $h$  is the heat transfer coefficient, and  $A$  is the area of the fluid film surrounding the sensor.

A solution of the first order, first degree, linear, differential equation [1,2]<sup>1</sup> resulting from a heat balance between the fluid film surrounding the sensor and the sensor itself is

$$T = C e^{-t/\tau} + \frac{1}{\tau} e^{-t/\tau} \int_0^t T_e e^{t'/\tau} dt \quad (2)$$

where  $T$  is the sensor temperature, and  $T_e$  is the environment temperature, both at time  $t$ , and  $C$  is a constant of integration.

<sup>1</sup>The italic numbers in brackets refer to the list of references appended to this chapter.

For a ramp change in temperature (as is found in a furnace being heated at a uniform rate) Eq 2 reduces to

$$(T_e - T) = R\tau \tag{3}$$

Equation 3 states that if an element is immersed for a long time in an environment whose temperature is rising at a constant rate  $R = dT_e/dt$ , then  $\tau$  is the interval between the time when the environment reaches a given temperature and the time when the element indicates this temperature.

For a step change in temperature (as when a thermocouple is plunged into a constant temperature bath), Eq 2 reduces to

$$(T_e - T) = (T_e - T_1)e^{-t/\tau} \tag{4}$$

Equation 4 states that if an element is plunged into a constant-temperature environment,  $\tau$  is the time required for the temperature difference between the environment and the element to be reduced to  $1/e$  of the initial difference. Note that for practical purposes the sensor will reach the new temperature after approximately 5 time constants. See Fig. 9.1 for a graphical presentation of these equations.

Below a Mach number of 0.4, the time constant hardly is affected by the fluid velocity. The size of the temperature change affects  $\tau$  because physical properties are not necessarily linear functions of temperature. Wormser [3]

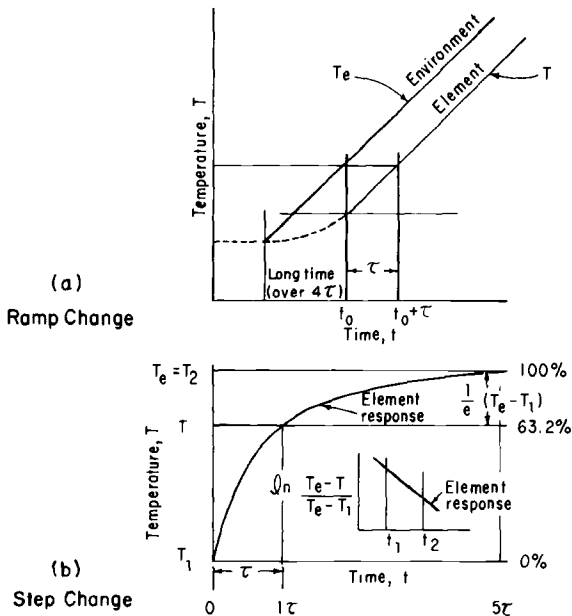


FIG. 9.1—Graphical presentation of ramp and step changes.

considers these effects in greater detail. Scadron and Warshawsky [4] present convenient nomographs for determining the time constant in the presence of heat transfer. Fluid turbulence tends to reduce the time constant by increasing the film coefficient.

If the sensor is contained in a thermowell the response time is increased because of the extra mass and the additional heat transfer coefficient involved. It may be necessary to consider the response as a second order function in which case a dead time is observed before the sensor responds to a step temperature change. However, Coon and Looney [5,6] state that the response time usually is represented adequately by the first order time constant  $\tau$ .

To achieve the best response time, the measuring junction should be in intimate contact with the well tip. Spring loading is sometimes used to accomplish this.

The response time usually is measured in liquids by plunging the thermocouple assembly into a well-stirred bath held at constant temperature. If the response time is of the same order as the immersion time, the velocity of immersion or depth of immersion or both become important parameters in the measurement. Reference 7 indicates a method for standardizing the liquid baths used in this determination.

For the response time in gases, the literature should be consulted [8,9]. Manufacturers sometimes can supply this information for simple conditions.

Multijunctions [10] and electrical networks [11] have been used successfully to improve the response of a thermocouple.

### 9.1.2 Recovery

Whenever a gas moves with an appreciable velocity, in addition to the thermal energy in the form of random translational kinetic energy of the molecules, some of its thermal energy is in the form of directed kinetic energy of fluid flow. The static temperature is a measure of the random kinetic energy, while the dynamic temperature is a measure of the directed kinetic energy. The total temperature is a concept (not a measurement) which sums the static and the dynamic temperatures. Such a total temperature would be sensed by an adiabatic probe which completely stagnates an ideal gas. Thus

$$T_{\text{adi, ideal}} = T_t = T + \frac{V^2}{2Jg_c c_p} = T + T_v \quad (5)$$

where

- $T_t$  = total temperature,
- $T$  = static temperature,
- $T_v$  = dynamic temperature,

$V$  = directed fluid velocity,  
 $J$  = mechanical equivalent of heat,  
 $g_c$  = standard acceleration of gravity, and  
 $c_p$  = specific heat at constant pressure.

In real fluids, an adiabatic recovery factor ( $\alpha$ ) generally is defined such that

$$T_{\text{adi}} = T + \alpha T_V \quad (6)$$

where  $\alpha$  may be more or less than one depending on the relative importance of thermal conductance and thermal capacitance in the boundary layers surrounding the sensor. Since the Prandtl number is the ratio of these two effects, it is common to express recoveries in terms of the Prandtl number. See Refs 12, 13, 14, and 15 for more information on the recovery factor.

A real sensor immersed in a real fluid tends to radiate to its surroundings. Also there is a tendency for a conductive heat transfer along the probe stem. These two effects are balanced by a convective heat transfer between the probe and the fluid. In addition, real probes do not always stagnate a moving fluid effectively. To account for these realities in temperature measurement in moving fluids, a dynamic correction factor ( $K$ ) is defined as

$$T_{\text{probe}} = T + K T_V \quad (7)$$

where  $K$  corrects for impact, viscosity, and conductivity effects in the fluid, and radiation and conduction effects in the probe.  $K$  may take on any value depending on the relative importance of these effects. Variations of  $K$  between  $\pm 35$  cannot be ruled out. Therefore, the factor  $K T_V$  can far outweigh all other factors such as calibration deviations.

### 9.1.3 Thermowells

Protecting tubes or thermowells (see Chapter 4) or both often are used to separate the measuring junction of a thermocouple from the fluid whose temperature is of interest. Such devices are used to avoid contamination of the thermoelements, to provide safety in case of high pressure installations, to provide strength in the case of significant fluid bending forces in the thermocouple, etc. Thermocouples installed in wells can be withdrawn for inspection, calibration, and replacement. A thermocouple in a well responds more slowly to changes in fluid temperature. Typical wells and their strength requirements are defined in Ref 16.

The depth of immersion in the fluid is an important consideration. One method of checking for adequacy of immersion is to increase the depth of immersion of the thermocouple well assembly in a constant temperature bath until the thermocouple output becomes constant. A minimum immersion depth of ten times the well outside diameter is a rule of thumb often used.

### 9.1.4 Thermal Analysis of an Installation

A thermocouple installation may give an indication which differs from the fluid temperature which is to be measured because:

1. The boundary walls are at a temperature different from that of the fluid.
2. There may be a temperature gradient along the well.
3. The fluid may be flowing with an appreciable velocity.
4. The thermocouple may be improperly calibrated.

Item 4 has been covered in Chapter 8 and will not be considered further here.

Basically, the thermocouple temperature is the result of a heat balance between the various modes of heat transfer.

$$q_c = q_r + q_k \quad (8)$$

where  $q$  indicates rate of heat transfer and the subscripts  $c$ ,  $r$ , and  $k$  signify, respectively, convection, radiation, and conduction. An equation has been developed to describe this heat balance mathematically [17] as

$$\frac{d^2T}{dx^2} + a_1(x) \frac{dT_x}{dx} - a_2(x, y) T_x = -a_2 a_3(x, y) \quad (9)$$

where  $a_1(x) = dA_k/A_k dx$  which indicates the effect of a change in cross-sectional area of the well;  $a_2(x, y) = dA_c(h_r + h_c)/kA_k dx$  which indicates the effect of radiation coefficient ( $h_r$ ), convection coefficient ( $h_c$ ), conductivity ( $k$ ), surface area for convection ( $A_c$ ) and cross-sectional area for conduction ( $A_k$ );  $a_3(x, y) = (h_c T_{adi} + h_r T_w)/(h_c + h_r)$  which relates the heat transfer coefficients to the adiabatic fluid temperature ( $T_{adi}$ ) and the surrounding wall temperature ( $T_w$ ),

Various solutions are possible for Eq 9 depending on the assumptions one is willing to make. Three simplified solutions are:

1. *Overall Linearization*—When the radiation coefficient is based on an average well temperature, the result is

$$\frac{T_x - a_3}{T_w - a_3} = \frac{e^{mx}}{1 + e^{2mL}} + \frac{e^{-mx}}{1 + e^{-2mL}} \quad (10)$$

where

$$m = \left( \frac{4D(h_r + h_c)}{k(D^2 - d^2)} \right)^{1/2}$$

Typical values for  $h_r$ ,  $h_c$ , and  $k$  are given in Ref 17. This approach leads to quick, approximate answers whenever the fluid can be considered transparent to radiation.

2. *Tip Solution*—When conduction effects are neglected along the well or protecting tube, Eq 9 reduces to

$$T_{\text{tip}} = a_3 \quad (11)$$

which can be solved at once since  $h_r$  and  $h_c$  are available in the literature (see Ref 17). This approximation normally would give tip temperatures which are too high since conduction tends to reduce  $T_{\text{tip}}$ .

3. *Stepwise Linearization*—This is the usual solution to Eq 9. Detailed equations are beyond the scope of this manual, but briefly one divides the well, lengthwise, into a number of elements. The temperature at the center of each element is taken to represent the temperature of that entire element. The heat balance equation is applied successively to one element after another until a match between tip and base temperature is achieved. Each installation is different. Each must be evaluated carefully to determine if the installation is capable of yielding temperatures within the allowable uncertainties.

## 9.2 Surface Temperature Measurement

### 9.2.1 General Remarks

There is no easy method of attaching a thermocouple to a surface so that it can be guaranteed to indicate the true surface temperature. To do this, it would be necessary to mount the measuring junction so that it could attain but not affect the surface temperature. In most cases, the presence of the thermocouple (or any alternative transducer) will cause a perturbation of the temperature distribution at the point of attachment, and thus it only will indicate the perturbed temperature.

9.2.1.1 *Measurement Error*—In many cases, a significant difference will exist between the indicated temperature and the “true” surface temperature, that is, the temperature that the surface would reach if no thermocouple were present. This difference is normally termed a “measurement error,” but it should not be confused with calibration or extension wire errors which are common to all thermocouple measurements. The relationship between the indicated and true surface temperature is often defined by the equation

$$Z = \frac{T_s - T_i}{T_s - T_a} \quad (12)$$

where

$Z$  = installation factor,

$T_s$  = true surface temperature,

$T_i$  = indicated surface temperature, and

$T_a$  = temperature of the surroundings or coolant.

Equation 12 expresses the measurement error  $T_s - T_i$  as a fraction of the difference between the surface and ambient temperatures.

The value of  $Z$  for a particular installation may be calculated or found by experiment; however, as several simplifying assumptions normally are made in any theoretical derivation, experimental verification is necessary if an accurate value of  $Z$  is required.

**9.2.1.2 Installation Types**—There are two basic types of surface thermocouple installation: the permanent, which is used to give a continuous history of the surface temperature, and the temporary, normally made with a sensing probe in mechanical contact with the surface to obtain spot readings. The basic principles for accurate measurement are similar for both types, but the probe type of sensors are more susceptible to measurement errors and generally have a lower accuracy.

## 9.2.2 Installation Methods

The method of attaching the thermocouple to the surface is governed by considerations of the metallurgical and thermal properties of the materials, their relative sizes, and the modes of heat transfer at the surface. Common methods are shown in Fig. 9.2.

**9.2.2.1 Permanent Installations**—For thin materials, the thermocouple junction is attached either directly to the surface (Fig. 9.2a) or is mounted in a heat collecting pad (Fig. 9.2b). It may be welded, brazed, cemented, or clamped to the surface. Good mechanical support of the leads is necessary so that no stresses are applied to the junction.

For thicker materials, the thermocouple junction may be peened into the surface or installed in a groove (Fig. 9.2c). The groove may be filled so that the surface is restored to its original profile. A thermocouple in a groove normally will have its junction below the surface and will indicate the subsurface temperature. A similar technique used with tubes is shown in Fig. 9.2d.

The configuration shown in Fig. 9.2e may be used where rapid response is required, as the junction can be made very thin by electroplating or mechanical polishing techniques [18-22].

Several installation methods are illustrated in the literature cited, particularly in Refs 23 and 24.

Metal sheathed thermocouples are suited particularly to surface measurements, especially for severe environments. They combine good strength and small size, and the measuring junction may be reduced in diameter or flattened to achieve good response with small errors.

**9.2.2.2 Measuring Junctions**—The measuring junction may be formed in several ways, each having its own advantages and disadvantages.

The bead junction commonly is used. The temperature indicated is a function of the temperatures where the wires leave the bead [25,26] so that the bead should be small, and the wires should leave the bead as close to the sur-



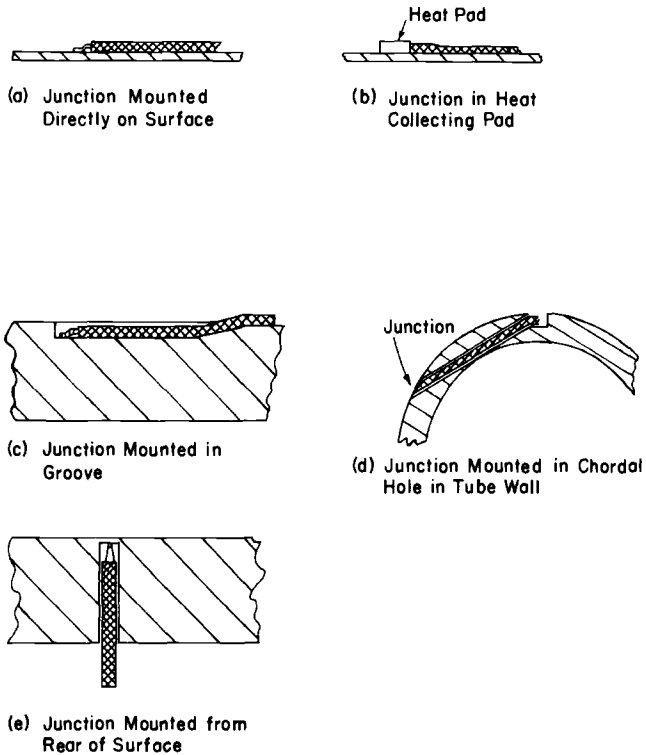


FIG. 9.2—Common attachment methods.

face as possible. This may be accomplished by using a flattened bead. Good thermal contact between the bead and the surface is essential, especially if there are temperature gradients. If the surface is a material of poor thermal conductivity, it may be advantageous to mount the measuring junction in a heat collecting pad, or button, which has a good conductivity [27].

The simplest junction is shown in Fig. 9.3 in which a single wire is brought to the surface which acts as the second thermoelement. The circuit is completed with a wire of the same material as the surface. This technique usually involves calibration of the wire/surface-material thermocouple. This calibration may not be very reproducible since the surface material is probably not an alloy with controlled thermoelectric properties. It, however, does provide a junction exactly at the surface, and the perturbation errors (see Section 9.2.3) can be reduced to a very low value [18, 28, 29].

A common variation is the separated junction in which each wire is joined separately to the surface (which must be an electrical conductor). This type, which is really two series junctions, has the advantage that the two junctions

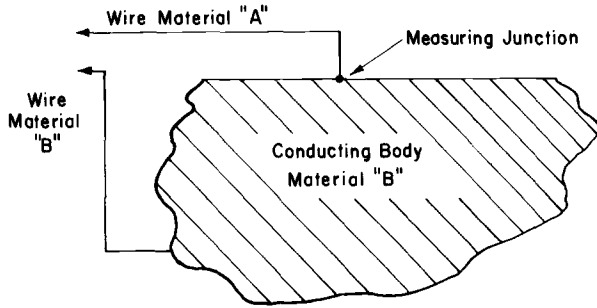


FIG. 9.3—"Single wire" thermocouple.

form a part of the surface. The output of such a thermocouple is a weighted mean of the two individual junction temperatures, of the form

$$e_0 = e_m + (b_1 - b_2) \frac{(T_1 - T_2)}{2} \quad (13)$$

where

- $T_1$  and  $T_2$  = junction temperatures,
- $e_0$  = measured output,
- $e_m$  = output which would be measured if both junctions were at the mean temperature  $(T_1 + T_2)/2$ , and
- $b_1$  and  $b_2$  = Seebeck coefficients of the two thermocouple wires versus the surface material.

Moffat [30] gives a graphical method of analysis.

Thus, the output will be greater or less than the mean depending upon which wire is at the higher temperature. The output generally cannot be calculated, as neither  $T_1$ ,  $T_2$ , nor the relationship between each wire and the surface will be known. There will be, therefore, an uncertainty in the measured temperature if temperature gradients exist. This error is minimized if the wires are bonded to the surface as close together as possible, to reduce  $(T_1 - T_2)$ . This type of junction has been shown to be more accurate than a bead junction [31,32].

**9.2.2.3 Probes**—It is often desirable to know the temperature distribution over a surface or to make a spot check at one particular point. These measurements are made with a probe containing a thermocouple junction which is held in mechanical contact with the surface. The configuration of the junction is based on the intended application, and several types are commercially available. The probes are in most cases held normal to the surface, and for ease in use should be spring-loaded, which also reduces the error.

Probes are subject to the same errors as permanent installations, but the

designer has no control over the conditions of use, and so the errors associated with this type of measurement may be significant. Since the probe provides a heat conducting path from the surface, thermal resistance due to oxide or dirt causes an additional error.

Correction factors [33] for several types of junctions range from 0.013 to 0.168, but in general must be determined for specific conditions.

The size of the junction should be as small as possible. Several types of junction are illustrated in Fig. 9.4. The junction types in order of decreasing measurement error are: grounded, exposed, button, and separated.

In order to reduce measurement errors, probes with an auxiliary heater have been used [34,35]. The probe thermocouple is heated to the surface temperature so that no temperature gradients are set up when the probe is applied to the surface. One form of probe uses two thermocouples (Fig. 9.5). Equality of the auxiliary and surface junction temperatures indicates that no heat is being transferred along the probe and that the surface junction is at the surface temperature. With this type of probe, the two junctions must be very close, and the response to a change in heater power must be fast or an error can occur in transient measurements. A probe which is controlled automatically has been described recently [36,37]. It is claimed to have an accuracy of  $\frac{3}{8}$  percent and can be used to  $760^{\circ}\text{C}$  ( $1400^{\circ}\text{F}$ ) on a variety of materials, with a measurement time of less than one second. Sasaki and Kamanda [38] used a different approach and eliminated the auxiliary junction. The surface junction was arranged to contact the surface at two second intervals only. The heater input was modulated over a twenty second period and adjusted so that the maxima and minima were above and below the surface temperature. At contact the surface junction temperature changed due to heat exchange unless the two temperatures were equal. With this method the surface temperature of glass bulbs was determined with an accuracy of  $0.3^{\circ}\text{C}$  ( $0.5^{\circ}\text{F}$ ).

**9.2.2.4 Moving Surfaces**—Surface temperatures of moving bodies are measured by several methods. A junction mounted in a probe may be held against the body [39], but this method results in errors caused by friction. In metal cutting investigations, the metal body and the cutting tool are used as the thermocouple materials. The output of this type of junction has been investigated extensively and has been analyzed by Shu et al [40]. Slip-rings to

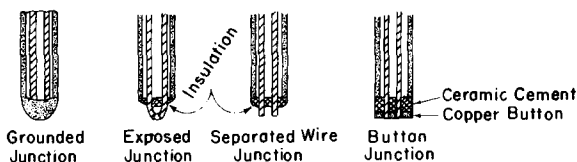


FIG. 9.4—Types of junction using metal sheathed thermocouples.

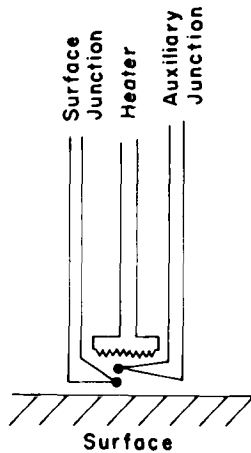


FIG. 9.5—*Thermocouple probe with auxiliary heater. diagrammatic arrangement.*

rotating members, intermittent and sliding contacts have been used also. A general review of such installations is given in Ref 24.

**9.2.2.5 Current Carrying Surfaces**—A technique of eliminating errors caused by voltage drop in surfaces heated by the passage of d-c current has been described by Dutton and Lee [41]. A three-wire thermocouple forming two junctions is used (Fig. 9.6), and the emfs due to the voltage drop in the surface are balanced out during successive reversals of current. When the balance is correct, the thermocouple output is constant regardless of the direction of the heating current.

This technique is also useful for surfaces carrying large alternating currents. In other cases, filters will suffice to attenuate the a-c component. Self-balancing potentiometers usually are affected adversely if the a-c pickup level is high. Galvanometric instruments are normally insensitive to ac and present no problem unless the current is high enough to damage the coils. If the thermocouple junction is not isolated from the surface, voltages appearing between the surface and the instrument ground (common-mode voltages) cause an error with some instruments.

### 9.2.3 Sources of Error

When a thermocouple is attached to a surface, its presence alters the heat transfer characteristics of the surface and normally will change the temperature distribution. This causes an error which will be referred to as perturbation error.

**9.2.3.1**—The causes of perturbation error can be broken down into the following:

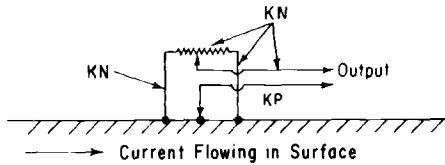


FIG. 9.6—Three wire Type K thermocouple to compensate for voltage drop induced by surface current. (Other materials may be used.)

The heat transfer characteristics of the surface are changed by the installation, that is, the surface emissivity or effective thermal conductivity will be altered or the wires may act as fins providing additional heat transfer paths.

Thermal contact resistance between the junction and the surface will cause a temperature gradient which will prevent the measuring junction from attaining the correct temperature if heat is being exchanged between the surface and its surrounding.

If temperature gradients exist, there will be an error due to uncertainty in the exact position of the junction or junctions relative to the surface [25, 26].

The response time of the thermocouple installation introduces errors during transient conditions [42, 43] (see also Section 9.1.1). The response time will be that of the surface installation and not of the thermocouple alone.

Although not discussed in this chapter, the errors associated with any thermocouple measurement, such as deviations from standard emf and lead wire errors, must be taken also into consideration [44, 45].

#### 9.2.4 Error Determination

The perturbation error must be determined if the surface temperature must be known with a high degree of accuracy. The installation should be designed to minimize this error, but in many cases materials and size make compromises necessary, so that an ideal design cannot be achieved. The error, and hence the correction factor, can be determined by the following methods.

**9.2.4.1 Steady State Conditions**—The direct calculation of the error involves solving the heat flow equation for the measuring junction and surface geometry. Normally simplifying assumptions are made, and the results must be interpreted in relation to them. The calculations show clearly the major sources of error and indicate means of reducing errors to a minimum [46–50].

Analog methods of solving the heat transfer equations using resistance or resistance-capacitance networks indicate the overall temperature distribution and show the perturbation effect of the thermocouple clearly. They are, how-

ever, difficult to make flexible, and so a number of analog models are required if a range of heat transfer conditions is to be studied [49-52].

Relaxation methods of solving the heat transfer equations have been used to calculate the temperature distribution; this method is attractive if a computer is available to perform the considerable amount of arithmetic required.

Direct experimental measurement on the installation is often the only satisfactory way to accurately determine the error. Care must be taken to simulate the service conditions exactly as a change in a variable can significantly affect the error. The major problem is to determine the true surface temperature. This is discussed extensively in the literature [19,52-57].

*9.2.4.2 Transient Conditions*—If surface temperatures are changing, the response of the thermocouple attachment may cause a significant error. The response time of the thermocouple alone will have little significance for surface measurements if the heat transfer path between the surface and the measuring junction is poor or adds thermal mass.

The time required to change the measuring junction temperature causes the thermocouple output to lag the surface temperature in time and decreases its amplitude [32,42,43]. The response time may be determined experimentally from the response to step or ramp functions of surface temperature change.

*A. Insulated Thermocouple Normal to an Electrically Heated Surface*—For surfaces with changing temperatures a bead thermocouple attached normal to an electrically heated surface and insulated from the ambient has been analyzed by Quant and Fink [59] and Green and Hunt [60].

The analysis showed that in order to obtain a rapid response with a small, steady-state error, it is necessary to use a small junction bead with good surface contact, small diameter wires, and good insulation between the wires and the surroundings.

*B. Surface Heated by Radiation*—Thermocouples mounted on a surface subject to radiant heating at temperature-rise rates up to 17°C/s were investigated by White [31]. His results showed that a separated-junction thermocouple produced the least error.

The thermocouple errors increased with increasing plate thickness and with increasing rates of temperature rise. Furthermore, the amount of bare thermocouple wire between the junction and the insulation should be a minimum.

Kovacs and Mesler [60] investigated the response of very fast surface thermocouples subject to radiant heating as a function of size and type of junction. Junctions were formed by electroplating or mechanical abrasion. Very thin junctions were subject to an overshoot error for high rates of temperature rise, as heat could not be transmitted back through the thermocouple to sub-surface layers fast enough. On the other hand, too thick a junction corresponded to a junction beneath the surface. The junction thickness should be

of the same order of magnitude as the distance between the two thermocouple wires to avoid overshooting.

*C. Surface Subject to Aerodynamic Heating*—An analysis and design of a thermocouple installation which can be mounted in a thin-metal skin subjected to aerodynamic heating is given in Ref 61. A finite difference calculation of the distorted temperature field indicated that errors due to insulation resistance at high temperatures were of the same order of magnitude as those due to the uncertainty of the exact junction location.

### 9.2.5 Procedures for Minimizing Error

The examples quoted in the preceding section have been treated separately. It is generally impossible to extrapolate from one set of conditions to another unless the installation is identical. The analyses show procedures that should be followed to reduce measurement errors. These are:

- A. Use the smallest possible installation to avoid perturbation errors.
- B. Bring the thermocouple wires away from the junction along an isotherm for at least 20 wire diameters to reduce conduction errors. The use of thermocouple materials with low thermal conductivity also will reduce this error.
- C. Locate the measuring junction as close to the surface as possible rather than above or below it.
- D. Design the installation so that it causes a minimum disturbance of any fluid flow or change in the emissivity of the surface, to avoid changes in convective or radiative heat transfer.
- E. Design the installation so that the total response is fast enough to cause negligible lag for the transients expected in service.
- F. Reduce the thermal resistance between the measuring junction and the surface to as low a value as possible. If the surface has a low thermal conductivity, a heat collecting pad may be used.

### 9.2.6 Commercial Surface Thermocouples

Many surface installations are custom engineered, but industry does offer several standard surface thermocouples intended for specific applications [39,62].

*9.2.6.1 Surface Types*—Figure 9.7 shows several types which are mounted on the surface. Type *a* is a gasket thermocouple which normally is mounted on a stud and Type *b* is a rivet head. The clamp attachment, Type *c*, is used on pipelines and will be reasonably accurate if the pipe is lagged thermally. The weldable pad attachment, Type *d*, is used on boiler or superheater tubes and uses a metal sheathed thermocouple with a grounded junction. The sheath and pad materials are chosen to be compatible with the boiler

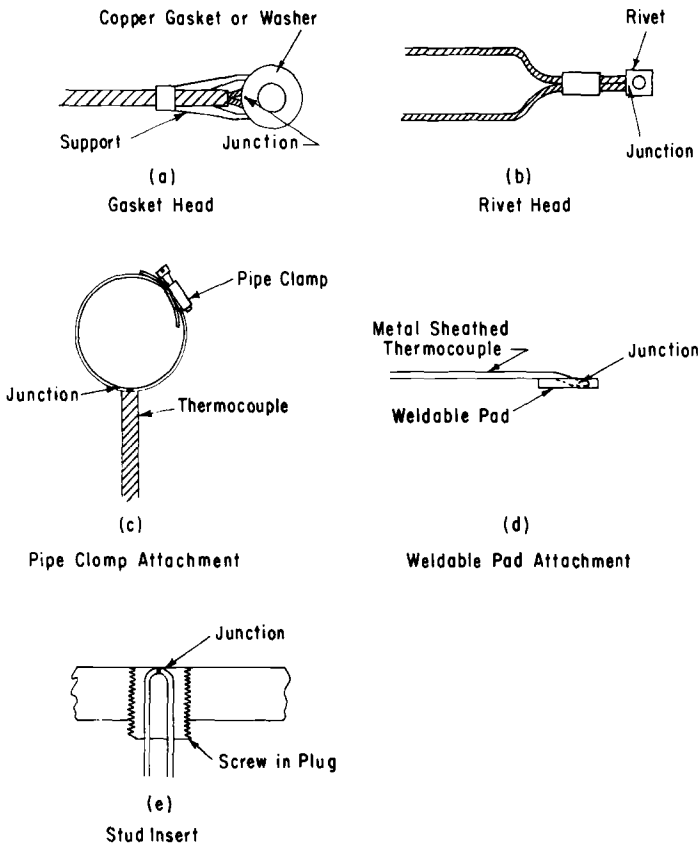


FIG. 9.7—Commercially available types of surface thermocouples.

environment. An accuracy of  $\pm 2$  percent is claimed for these thermocouples ( $\pm 1$  percent if a correction factor supplied by the manufacturer is used).

For installations where it is possible to mount the thermocouples in the surface, stud- or rivet-mounted plugs similar to Type *e* are offered by several manufacturers. Variations of this type have been used extensively for heat transfer measurements [46, 63] and for applications requiring very rapid response such as the measurement of surface temperatures in gun barrels and rocket exhaust chambers. The material of the plug must match the material of the surface, otherwise significant errors can be introduced [64], especially for materials with low thermal conductivity.

**9.2.6.2 Probe Types**—Probe type thermocouples for temporary or spot readings are offered usually as a complete package consisting of a thermocouple head which contains the measuring junction, a hand probe, and an indicating millimeter calibrated in degrees. The measuring junctions are



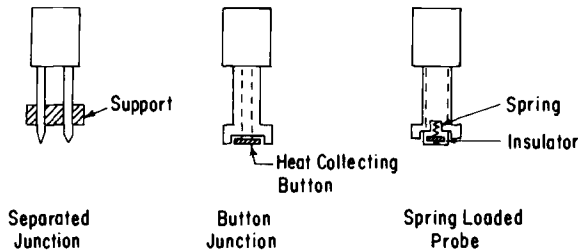


FIG. 9.8—Commercial probe thermocouple junctions.

normally interchangeable so that one instrument can be used with a variety of heads. The type of head will depend on the surface characteristics. Common types are shown in Fig. 9.8.

The separated-junction probe is used on electrically conducting surfaces only. Dirt or oxide layers will introduce a thermal resistance error or even prevent the completion of the circuit. For greatest convenience, the two wires should be separately spring-loaded against the surface. The button type of junction must be held carefully as any deviation from the normal will cause a change in the height of the junction above the surface, and the readings will be inconsistent. The spring-loaded type of junction is available in several forms and has been adapted for measurements on moving surfaces [39].

The accuracy obtainable with these probes is not high. However, the errors can be reduced to 2 or 3 percent for good conducting surfaces in still air cooled by natural convection. If the surface is a poor thermal conductor or the rate of heat transfer is high, the error will be considerably higher than this.

For rotating or moving surfaces, probe instruments utilizing a junction spring-loaded against the surface are used. Heat generated by friction causes an error which can be significant. (Bowden and Ridler [65] have shown that the temperatures may reach the melting point of one of the metals.)

A heated thermocouple probe instrument for measuring the temperature of wires or filaments is described by Bensen and Horne [66], and a wire temperature meter [67] has been marketed recently.

### 9.3 References

- [1] Harper, D. R., "Thermometric Lag," NBS Scientific Paper 185, National Bureau of Standards, March 1912.
- [2] Benedict, R. P., *Fundamentals of Temperature, Pressure, and Flow Measurements*, Second Edition, Wiley, New York, 1977.
- [3] Wormser, A. F., "Experimental Determination of Thermocouple Time Constants," National AERO Meeting Paper 158D, Society of Automotive Engineers, April 1960.
- [4] Scadron, M. D. and Warshawsky, I., "Experimental Determination of Time Constants and Nusselt Numbers for Bare-Wire Thermocouples," NACA TN 2599, National Advisory Committee for Aeronautics, Jan. 1952.

- [5] Coon, G. A., "Response of Temperature-Sensing-Element Analyses," *Transactions, American Society of Mechanical Engineers*, Nov. 1957, p. 1857.
- [6] Looney, R., "Method for Presenting the Response of Temperature-Measuring Systems," *Transactions, American Society of Mechanical Engineers*, Nov. 1957, p. 1851.
- [7] Murdock, J. W., Foltz, C. J., and Gregory, C., "A Practical Method of Determining Response Time of Thermometers in Liquid Baths," *Transactions, American Society of Mechanical Engineers, Journal of Engineering for Power*, Jan. 1963, p. 27.
- [8] Caldwell, F. R., Olsen, L. O., and Freeze, P. D., "Intercomparison of Thermocouple Response Data," SAE Paper 158F, Society of Automotive Engineers, April, 1960.
- [9] Hornfeck, A. J., "Response Characteristics of Thermometer Elements," *Transactions, American Society of Mechanical Engineers*, Feb. 1949, p. 121.
- [10] Benedict, R. P., *Fundamentals of Temperature, Pressure, and Flow Measurements*, Second Edition, Wiley, New York, 1977, p. 280.
- [11] Shepard, C. E. and Warshawsky, I., "Electrical Techniques for Compensation of Thermal Time Lag of Thermocouples and Resistance Thermometer Elements," NACA TN 2703, National Advisory Committee for Aeronautics, Jan. 1952.
- [12] Benedict, R. P., *Fundamentals of Temperature, Pressure, and Flow Measurements*, Second Edition, Wiley, New York, 1977, p. 213.
- [13] Roughton, J. E., "Design of Thermometer Pockets for Steam Mains," *Proceedings 1965-1966*, Institute of Mechanical Engineers, Vol. 180, Part 1, No. 39.
- [14] Faul, J. C., "Thermocouple Performance in Gas Streams," *Instruments and Control Systems*, Dec. 1962.
- [15] Werner, F. D., "Total Temperature Measurement," ASME Paper 58-AU-17, American Society of Mechanical Engineers.
- [16] "Temperature Measurement," ASME PTC 19.3, American Society of Mechanical Engineers, 1974.
- [17] Benedict, R. P. and Murdock, J. W., "Steady-State Thermal Analysis of a Thermometer Well," *Transactions, American Society of Mechanical Engineers, Journal of Engineering for Power*, July 1963, p. 235.
- [18] Bendersby, D., "A Special Thermocouple for Measuring Transient Temperatures," *Mechanical Engineering*, Vol. 75, No. 2, Feb. 1953, p. 117.
- [19] Powell, W. B. and Price, T. W., "A Method for the Determination of Local Heat Flux from Transient Temperature Measurements," *Transactions, Instrument Society of America*, Vol. 3, No. 3, July 1964, p. 246.
- [20] Moeller, C. E., "Thermocouples for the Measurement of Transient Surface Temperatures," *Temperature, Its Measurement and Control in Science and Industry*, Vol. 3, Part 2, Reinhold, New York, 1962, p. 617.
- [21] Ongkiehong, L. and Van Duijn, J., "Construction of a Thermocouple for Measuring Surface Temperatures," *Journal of Scientific Instruments*, Vol. 37, June 1960, p. 221.
- [22] Vigor, C. W. and Hornaday, J. R., "A Thermocouple for a Measurement of Temperature Transients in Forging Dies," *Temperature, Its Measurement and Control in Science and Industry*, Vol. 3, Part 2, Reinhold, New York, 1962, p. 625.
- [23] Baker, H. D., Ryder, E. A., and Baker, N. H., *Temperature Measurement in Engineering*, Vol. 1, Wiley, New York, 1953, Chapters 8, 11, 12.
- [24] Baker, H. D., Ryder, E. A., and Baker, N. H., *Temperature Measurement in Engineering*, Vol. 2, Wiley, New York, 1961.
- [25] Bailey, N. P., "The Response of Thermocouples," *Mechanical Engineering*, Vol. 53, No. 11, Nov. 1931, p. 797.
- [26] McCann, J. A., "Temperature Measurement Theory," KAPL-2067-2, 1962, Office of Technical Service, Department of Commerce, Washington, D.C.
- [27] Chapman, A. J., *Heat Transfer*, McMillan, New York, 1960.
- [28] Bailey, N. P., "The Measurement of Surface Temperatures, Accuracies Obtainable with Thermocouples," *Mechanical Engineering*, Vol. 54, Aug. 1932, p. 553.
- [29] Baker, H. D., Ryder, E. A., and Baker, N. H., *Temperature Measurement in Engineering*, Vol. 1, Wiley, New York, 1961, p. 90.
- [30] Moffat, R. J., "The Gradient Approach to Thermocouple Circuitry," *Temperature, Its Measurement and Control in Science and Industry*, Vol. 3, Part 2, Reinhold, New York, 1962, pp. 33-38.

- [31] White, F. J., "Accuracy of Thermocouples in Radiant Heat Testing," *Experimental Mechanics*, Vol. 2, July 1962, p. 204.
- [32] Moen, W. K., "Surface Temperature Measurements," *Instruments and Control Systems*, Vol. 33, Jan. 1960, p. 71.
- [33] Otter, A. J., "Thermocouples and Surface Temperature Measurement," AECL-3062, March 1968, SDDO, AECL, Chalk River, Ont., Canada.
- [34] Roeser, W. F. and Mueller, E. F., "Measurement of Surface Temperatures," *Bureau of Standards Journal of Research*, Vol. 5, No. 4, Oct. 1930, p. 793.
- [35] Sasaki, N., "A New Method for Surface Temperature Measurement," *Review of Scientific Instruments*, Vol. 21, No. 1, Jan. 1950, p. 1.
- [36] Robertson, D. and Sterbutzel, G. A., "An Accurate Surface Temperature Measuring System," *Proceedings of IEEE Industrial Heating Conference of Philadelphia*, April 1969. See also *Leeds and Northrup Technical Journal*, Issue 7, Summer 1969.
- [37] "A Probe for the Instantaneous Measurement of Surface Temperature," RTD-TDR-63-4015, OTS, Department of Commerce, Washington, D.C.
- [38] Sasaki, N. and Kamanda, A., "A Recording Device for Surface Temperature Measurements," *Review of Scientific Instruments*, Vol. 23, No. 6, June 1952, p. 261.
- [39] "Unusual Thermocouples and Accessories," *Instruments and Control Systems*, Vol. 36, No. 8, Aug. 1963, p. 133.
- [40] Shu, H. H., Gaylard, E. W., and Hughes, W. F., "The Relation Between the Rubbing Interface Temperature Distribution and Dynamic Thermocouple Temperature," *Transactions ASME Journal of Basic Engineering*, Vol. 86, Series D, No. 3, Sept. 1964, p. 417.
- [41] Dutton, R. and Lee, E. C., "Surface-Temperature Measurement of Current-Carrying Objects," *Journal. Instrument Society of America*, Vol. 6, No. 12, Dec. 1959, p. 49.
- [42] Jakob, M., *Heat Transfer*, Vol. 2, Wiley, New York, 1957, p. 183.
- [43] Caldwell, W. I., Coon, G. A., and Zoss, L. M., *Frequency Response for Process Control*, McGraw-Hill, New York, 1959, p. 295.
- [44] "Thermocouples and Thermocouple Extension Wires," *Recommended Practice RPI-7*, Instrument Society of America, 7 July 1959.
- [45] Finch, D. I., "General Principles of Thermoelectric Thermometry," *Temperature. Its Measurement and Control in Science and Industry*, Vol. 3, Part 2, Reinhold, New York, p. 3.
- [46] Jakob, M., *Heat Transfer*, Vol. 2, Wiley, New York, 1957, p. 153.
- [47] Chapman, A. J., *Heat Transfer*, McMillan, New York, 1960.
- [48] Boelter, L. M. K. et al, "An Investigation of Aircraft Heaters XXVIII-Equations for Steady State Temperature Distribution Caused by Thermal Sources in Flat Plates Applied to Calculation of Thermocouple Errors, Heat Meter Corrections, and Heat Transfer by Pin-Fin Plates," Technical Note 1452, National Advisory Committee for Aeronautics, 1944.
- [49] Schneider, P. J., *Conduction Heat Transfer*, Addison-Wesley, Cambridge, Mass., 1955, p. 176.
- [50] Fitts, R. L., Flemons, R. S., and Rogers, J. T., "Study of Temperature Distribution in a Finned Nuclear Fuel Sheath by Electrical Analogue and Mathematic Analysis (Revision)," R65CAP1, 19 Jan. 1965, Canadian General Electric, Peterborough, Ont.
- [51] Chan, K. S. and Rushton, K. R., "The Simulation of Boundary Conditions in Heat Conduction Problems in a Resistance-Capacitance Electrical Analogue," *Journal of Scientific Instruments*, Vol. 41, No. 9, Sept. 1964, p. 535.
- [52] Brindley, J. H., "Calibration of Surface-Attached Thermocouples on a Flat-Plate Fuel Element by Electrical Analogue and Analytical Techniques," *Transactions of the American Nuclear Society*, Vol. 6, No. 2, Nov. 1963, p. 333.
- [53] Boelter, L. M. K. and Lockhart, R. W., "Thermocouple Conduction Error Observed in Measuring Surface Temperatures," Technical Note 2427, National Advisory Committee for Aeronautics, 1946.
- [54] Stoll, A. M. and Hardy, J. D., "Direct Experimental Comparison of Several Surface Temperature Measuring Devices," *Review of Scientific Instruments*, Vol. 20, No. 9, Sept. 1949, p. 678.
- [55] Oetken, E. R., "Evaluation of Surface-Attached Thermocouples During Forced Convection Heat Transfer," IDO-16889, OTS, Department of Commerce, Washington, D.C.

- [56] Sudar, S., "Calibration of OMRE Fuel-Element Surface Thermocouple Assembly," NAA-SR-Memo 3671, 1959.
- [57] Browning, W. E. and Hemphill, H. L., "Thermocouples for Measurement of the Surface Temperature of Nuclear Fuel Elements," *Temperature. Its Measurement and Control in Science and Industry*, Vol. 3, Part 2, Reinhold, New York, p. 723.
- [58] Quant, E. R. and Fink, E. W., "Experimental and Theoretical Analysis of the Transient Response of Surface Bonded Thermocouples," *Bettis Technical Review*, WAPD-BT-19, Reactor Technology, June 1960, p. 31.
- [59] Green, S. J. and Hunt, T. W., "Accuracy and Response of Thermocouples for Surface and Fluid Temperature Measurements," *Temperature, Its Measurement and Control in Science and Industry*, Vol. 3, Part 2, Reinhold, New York, p. 695.
- [60] Kovacs, A. and Mesler, R. B., "Making and Testing Small Surface Thermocouples for Fast Response," *Review of Scientific Instruments*, Vol. 35, No. 4, April 1964, p. 485.
- [61] "Design and Construction of a Unit for Measuring Metal Skin Temperatures, Phase I, Theoretical Analysis and Design," SC-4461 (RR), Dec. 1960, OTS, Department of Commerce, Washington, D.C.
- [62] See Thermocouple Manufacturers' Catalogs.
- [63] Sellers, J. P., "Thermocouple Probes for Evaluating Local Heat Transfer Coefficients in Rocket Motors," *Temperature, Its Measurement and Control in Science and Industry*, Vol. 3, Part 2, Reinhold, New York, p. 673.
- [64] Nanigan, J., "Thermal Properties of Thermocouples," *Instruments and Control Systems*, Vol. 36, No. 10, Oct. 1963, p. 87.
- [65] Bowden, F. P. and Ridler, K. E. W., "Physical Properties of Surfaces III. The Surface Temperature of Sliding Metals," *Proceedings*, Royal Society, London A, Vol. 154, 1936, p. 644.
- [66] Bensen, J. and Horne, R., "Surface Temperature of Filaments and Thin Sheets," *Instruments and Control Systems*, Vol. 35, No. 10, Part 1, Oct. 1962, p. 115.
- [67] Report No. 152, British Iron and Steel Research Organization.
- [68] Lovuola, V. J., "Preventing Noise in Grounded Thermocouple Measurements," *Instruments and Control Systems*, Jan. 1980, p. 31.
- [69] Dean, R. C. et al, *Aerodynamic Measurements*, M.I.T. Press, Cambridge, Mass., 1953, Eighth printing, 1963.

# Chapter 10—Reference Tables for Thermocouples

---

The practical use of thermocouples in industrial and laboratory applications requires that the thermocouple conform to an established temperature—electromotive-force relationship within acceptable limits of error. Since the thermocouple in a thermoelectric thermometer system is usually expendable, conformance to established temperature-emf relationships is necessary in order to permit interchangeability.

Section 10.2 consists of reference tables that give temperature-emf relationships for the thermocouple types most commonly used in industry. These are identified as thermocouple Types B, E, J, K, R, S, and T, as defined in ANSI Standard MC96.1.

Data in these tables are based upon absolute electrical units and the International Practical Temperature Scale of 1968. All temperature emf data contained in Section 10.2 have been extracted from ASTM Standard E 230.

Reference tables giving temperature emf relationships for single leg thermoelements referenced to platinum (NBS Pt 67) are not included in this manual but are contained in ASTM Standard E 230.

## 10.1 Thermocouple Types and Limits of Error

### 10.1.1 Thermocouple Types

The letter symbols identifying each reference table are those defined in ANSI Standard MC96.1. These symbols which are used in common throughout industry, identify the following thermocouple calibrations:

*Type B*—Platinum-30 percent rhodium (+) versus platinum 6 percent rhodium (−).

*Type E*—Nickel-10 percent chromium (+) versus constantan (−).

*Type J*—Iron (+) versus constantan (−).

*Type K*—Nickel-10 percent chromium (+) versus nickel-5 percent aluminum and silicon (−).<sup>1</sup>

*Type R*—Platinum-13 percent rhodium (+) versus platinum (−).

*Type S*—Platinum-10 percent rhodium (+) versus platinum (−).

*Type T*—Copper (+) versus constantan (−).

<sup>1</sup>Silicon, or aluminum and silicon, may be present in combination with other elements.

Detailed information covering the advantages and limitations of each of these thermocouple types, their recommended temperature ranges, and detailed physical properties of the thermoelements comprising them are contained in Section 3.1 of this manual.

### 10.1.2 Limits of Error

The limits of error for the common letter designated thermocouple types, as listed in Table 10.1 are taken from ASTM E 230. Most manufacturers supply thermocouples and thermocouple wire to these limits of error or better.

## 10.2 Thermocouples Reference Tables

Following is a list of the reference tables included in this section:

| Table Number | Thermocouple Type | Temperature Range |
|--------------|-------------------|-------------------|
| 10.2         | B                 | 0 to + 3308°F     |
| 10.3         | B                 | 0 to + 1820°C     |
| 10.4         | E                 | -454 to + 1832°F  |
| 10.5         | E                 | -270 to + 1000°C  |
| 10.6         | J                 | -350 to + 2192°F  |
| 10.7         | J                 | -210 to + 1200°C  |
| 10.8         | K                 | -454 to + 2500°F  |
| 10.9         | K                 | -270 to + 1372°C  |
| 10.10        | R                 | -58 to + 3214°F   |
| 10.11        | R                 | -50 to + 1768°C   |
| 10.12        | S                 | -58 to + 3214°F   |
| 10.13        | S                 | -50 to + 1768°C   |
| 10.14        | T                 | -454 to + 752°F   |
| 10.15        | T                 | -270 to + 400°C   |

## 10.3 Generation of Smooth Temperature-Emf Relationships

### 10.3.1 Need for Smooth Temperature-Emf Relationship

A table of reference values for use with thermocouples should be capable of easy and unique generation to facilitate its use in computer and similar applications. Furthermore, the reference values should agree closely with the characteristics of the thermocouple type under study, so that differences will change only slowly and smoothly with temperature level.

Reference Tables 10.2 to 10.15 give values to three decimal places only, and this roundoff in table values results in inherent discontinuities in the temperature-emf relationship as represented by the tables.

This section provides means for generating smooth, continuous tem-

TABLE 10.1—Limits of error for thermocouples.

| Type   | Temperature Range |              | Limits of Error |             |               |             |
|--------|-------------------|--------------|-----------------|-------------|---------------|-------------|
|        | °F                | °C           | Standard        |             | Special       |             |
|        |                   |              | °F              | °C (Note 2) | °F            | °C (Note 2) |
| B      | 1600 to 3100      | 871 to 1705  | ± 1/2 percent   |             |               |             |
| E      | 32 to 600         | 0 to 316     | ± 3° F          |             | ± 2 1/4 ° F   |             |
|        | 600 to 1600       | 316 to 871   | ± 1/2 percent   |             | ± 3/8 percent |             |
| J      | 32 to 530         | 0 to 277     | ± 4° F          |             | ± 2° F        |             |
|        | 530 to 1400       | 277 to 760   | ± 3/4 percent   |             | ± 3/8 percent |             |
| K      | 32 to 530         | 0 to 277     | ± 4° F          |             | ± 2° F        |             |
|        | 530 to 2300       | 277 to 1260  | ± 3/4 percent   |             | ± 3/8 percent |             |
| R or S | 32 to 1000        | 0 to 538     | ± 2 1/2 ° F     |             |               |             |
|        | 1000 to 2700      | 538 to 1482  | ± 1/4 percent   |             |               |             |
| T      | -300 to -150      | -184 to -101 | ± 2 percent     |             | ± 1 percent   |             |
|        | -150 to -75       | -101 to -59  | ± 1 1/2 ° F     |             | ± 3/4 ° F     |             |
|        | -75 to 200        | -59 to 93    | ± 3/4 percent   |             | ± 3/8 percent |             |
|        | 200 to 700        | 93 to 371    |                 |             |               |             |

NOTE 1—In this table the limits of error for each type of thermocouple apply only over the temperature range for which the wire size in question is recommended (see Table 3.5). These limits of error should be applied only to standard wire sizes. The same limits may not be obtainable in special sizes.

NOTE 2—Where limits of error are given in percent, the percentage applies to the temperature being measured when expressed in degrees Fahrenheit. To determine the limit of error in degrees Celsius, multiply the limit of error in degrees Fahrenheit by 5/9.

NOTE 3—Limits of error apply to thermocouples as supplied by the manufacturer. The calibration of a thermocouple may change during use. The magnitude of the change depends upon such factors as temperature, the length of time, and the conditions under which it was used.

NOTE 4—Type T wire cannot be expected to meet the limits of error at temperatures below the ice point unless so specified at time of purchase. Selection is usually required.

TABLE 10.2—Type B thermocouples (deg F-millivolts).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit* |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|------------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
| DEG F   | 0      | 1                                  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |                                    |        |        |        |        |        |        |        |        |        |                             |  |
| 0   | 0.006  | 0.006                              | 0.006  | 0.006  | 0.005  | 0.005  | 0.005  | 0.005  | 0.004  | 0.004  | 0.004  | 0                           |  |
| 10  | 0.004  | 0.004                              | 0.003  | 0.003  | 0.003  | 0.003  | 0.003  | 0.002  | 0.002  | 0.002  | 0.002  | 10                          |  |
| 20  | 0.002  | 0.002                              | 0.002  | 0.001  | 0.001  | 0.001  | 0.001  | 0.001  | 0.001  | 0.000  | 0.000  | 20                          |  |
| 30  | 0.000  | 0.000                              | 0.000  | -0.000 | -0.000 | -0.000 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | 30                          |  |
| 40  | -0.001 | -0.001                             | -0.001 | -0.001 | -0.001 | -0.001 | -0.002 | -0.002 | -0.002 | -0.002 | -0.002 | 40                          |  |
| 50  | -0.002 | -0.002                             | -0.002 | -0.002 | -0.002 | -0.002 | -0.002 | -0.002 | -0.002 | -0.002 | -0.002 | 50                          |  |
| 60  | -0.002 | -0.002                             | -0.002 | -0.003 | -0.003 | -0.003 | -0.003 | -0.003 | -0.003 | -0.003 | -0.003 | 60                          |  |
| 70  | -0.003 | -0.003                             | -0.003 | -0.003 | -0.003 | -0.003 | -0.003 | -0.002 | -0.002 | -0.002 | -0.002 | 70                          |  |
| 80  | -0.002 | -0.002                             | -0.002 | -0.002 | -0.002 | -0.002 | -0.002 | -0.002 | -0.002 | -0.002 | -0.002 | 80                          |  |
| 90  | -0.002 | -0.002                             | -0.002 | -0.002 | -0.002 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | 90                          |  |
| 100   | -0.001 | -0.001                             | -0.001 | -0.001 | -0.000 | -0.000 | -0.000 | -0.000 | 0.000  | 0.000  | 0.000  | 100                         |  |
| 110   | 0.000  | 0.000                              | 0.001  | 0.001  | 0.001  | 0.001  | 0.001  | 0.001  | 0.002  | 0.002  | 0.002  | 110                         |  |
| 120   | 0.002  | 0.002                              | 0.002  | 0.002  | 0.003  | 0.003  | 0.003  | 0.003  | 0.003  | 0.004  | 0.004  | 120                         |  |
| 130   | 0.004  | 0.004                              | 0.004  | 0.005  | 0.005  | 0.005  | 0.005  | 0.005  | 0.006  | 0.006  | 0.006  | 130                         |  |
| 140   | 0.006  | 0.006                              | 0.007  | 0.007  | 0.007  | 0.007  | 0.008  | 0.008  | 0.008  | 0.009  | 0.009  | 140                         |  |
| 150   | 0.009  | 0.009                              | 0.009  | 0.010  | 0.010  | 0.010  | 0.011  | 0.011  | 0.011  | 0.012  | 0.012  | 150                         |  |
| 160   | 0.012  | 0.012                              | 0.013  | 0.013  | 0.013  | 0.014  | 0.014  | 0.014  | 0.015  | 0.015  | 0.015  | 160                         |  |
| 170   | 0.015  | 0.016                              | 0.016  | 0.016  | 0.017  | 0.017  | 0.017  | 0.018  | 0.018  | 0.019  | 0.019  | 170                         |  |
| 180   | 0.019  | 0.019                              | 0.020  | 0.020  | 0.021  | 0.021  | 0.021  | 0.022  | 0.022  | 0.023  | 0.023  | 180                         |  |
| 190   | 0.023  | 0.023                              | 0.024  | 0.024  | 0.025  | 0.025  | 0.026  | 0.026  | 0.027  | 0.027  | 0.027  | 190                         |  |
| 200   | 0.027  | 0.028                              | 0.028  | 0.029  | 0.029  | 0.030  | 0.030  | 0.031  | 0.031  | 0.032  | 0.032  | 200                         |  |
| 210   | 0.032  | 0.033                              | 0.033  | 0.034  | 0.034  | 0.035  | 0.035  | 0.036  | 0.036  | 0.037  | 0.037  | 210                         |  |
| 220   | 0.037  | 0.038                              | 0.038  | 0.039  | 0.039  | 0.040  | 0.041  | 0.041  | 0.042  | 0.042  | 0.043  | 220                         |  |
| 230   | 0.043  | 0.043                              | 0.044  | 0.044  | 0.045  | 0.046  | 0.046  | 0.047  | 0.047  | 0.048  | 0.049  | 230                         |  |
| 240   | 0.049  | 0.049                              | 0.050  | 0.050  | 0.051  | 0.052  | 0.052  | 0.053  | 0.053  | 0.054  | 0.055  | 240                         |  |
| 250   | 0.055  | 0.055                              | 0.056  | 0.057  | 0.057  | 0.058  | 0.058  | 0.059  | 0.060  | 0.060  | 0.061  | 250                         |  |
| 260   | 0.061  | 0.062                              | 0.062  | 0.063  | 0.064  | 0.064  | 0.065  | 0.066  | 0.067  | 0.067  | 0.068  | 260                         |  |
| 270   | 0.068  | 0.069                              | 0.069  | 0.070  | 0.071  | 0.071  | 0.072  | 0.073  | 0.074  | 0.074  | 0.075  | 270                         |  |
| 280   | 0.075  | 0.076                              | 0.077  | 0.077  | 0.078  | 0.079  | 0.080  | 0.080  | 0.081  | 0.082  | 0.083  | 280                         |  |
| 290   | 0.083  | 0.083                              | 0.084  | 0.085  | 0.086  | 0.086  | 0.087  | 0.088  | 0.089  | 0.090  | 0.090  | 290                         |  |
| 300   | 0.090  | 0.091                              | 0.092  | 0.093  | 0.094  | 0.094  | 0.095  | 0.096  | 0.097  | 0.098  | 0.099  | 300                         |  |
| 310   | 0.099  | 0.099                              | 0.100  | 0.101  | 0.102  | 0.103  | 0.104  | 0.104  | 0.105  | 0.106  | 0.107  | 310                         |  |
| 320   | 0.107  | 0.108                              | 0.109  | 0.110  | 0.111  | 0.111  | 0.112  | 0.113  | 0.114  | 0.115  | 0.116  | 320                         |  |
| 330   | 0.116  | 0.117                              | 0.118  | 0.119  | 0.120  | 0.120  | 0.121  | 0.122  | 0.123  | 0.124  | 0.125  | 330                         |  |
| 340   | 0.125  | 0.126                              | 0.127  | 0.128  | 0.129  | 0.130  | 0.131  | 0.132  | 0.133  | 0.134  | 0.135  | 340                         |  |
| 350   | 0.135  | 0.136                              | 0.137  | 0.138  | 0.138  | 0.139  | 0.140  | 0.141  | 0.142  | 0.143  | 0.144  | 350                         |  |
| 360   | 0.144  | 0.145                              | 0.146  | 0.147  | 0.148  | 0.149  | 0.151  | 0.152  | 0.153  | 0.154  | 0.155  | 360                         |  |
| 370   | 0.155  | 0.156                              | 0.157  | 0.158  | 0.159  | 0.160  | 0.161  | 0.162  | 0.163  | 0.164  | 0.165  | 370                         |  |
| 380   | 0.165  | 0.166                              | 0.167  | 0.168  | 0.169  | 0.171  | 0.172  | 0.173  | 0.174  | 0.175  | 0.176  | 380                         |  |
| 390   | 0.176  | 0.177                              | 0.178  | 0.179  | 0.180  | 0.182  | 0.183  | 0.184  | 0.185  | 0.186  | 0.187  | 390                         |  |
| 400   | 0.187  | 0.188                              | 0.189  | 0.191  | 0.192  | 0.193  | 0.194  | 0.195  | 0.196  | 0.197  | 0.199  | 400                         |  |
| 410   | 0.199  | 0.200                              | 0.201  | 0.202  | 0.203  | 0.205  | 0.206  | 0.207  | 0.208  | 0.209  | 0.210  | 410                         |  |
| 420   | 0.210  | 0.212                              | 0.213  | 0.214  | 0.215  | 0.217  | 0.218  | 0.219  | 0.220  | 0.221  | 0.223  | 420                         |  |
| 430   | 0.223  | 0.224                              | 0.225  | 0.226  | 0.228  | 0.229  | 0.230  | 0.231  | 0.233  | 0.234  | 0.235  | 430                         |  |
| 440   | 0.235  | 0.236                              | 0.236  | 0.239  | 0.240  | 0.242  | 0.243  | 0.244  | 0.245  | 0.247  | 0.248  | 440                         |  |
| 450   | 0.248  | 0.249                              | 0.251  | 0.252  | 0.253  | 0.254  | 0.256  | 0.257  | 0.258  | 0.260  | 0.261  | 450                         |  |
| 460   | 0.261  | 0.262                              | 0.264  | 0.265  | 0.266  | 0.268  | 0.269  | 0.271  | 0.272  | 0.273  | 0.275  | 460                         |  |
| 470   | 0.275  | 0.276                              | 0.277  | 0.279  | 0.280  | 0.281  | 0.283  | 0.284  | 0.286  | 0.287  | 0.288  | 470                         |  |
| 480   | 0.288  | 0.290                              | 0.291  | 0.293  | 0.294  | 0.295  | 0.297  | 0.298  | 0.300  | 0.301  | 0.303  | 480                         |  |
| 490   | 0.303  | 0.304                              | 0.305  | 0.307  | 0.308  | 0.310  | 0.311  | 0.313  | 0.314  | 0.315  | 0.317  | 490                         |  |
| 500   | 0.317  | 0.318                              | 0.320  | 0.321  | 0.323  | 0.324  | 0.326  | 0.327  | 0.329  | 0.330  | 0.332  | 500                         |  |
| 510   | 0.332  | 0.333                              | 0.335  | 0.336  | 0.338  | 0.339  | 0.341  | 0.342  | 0.344  | 0.345  | 0.347  | 510                         |  |
| 520   | 0.347  | 0.348                              | 0.350  | 0.351  | 0.353  | 0.355  | 0.356  | 0.358  | 0.359  | 0.361  | 0.362  | 520                         |  |
| 530   | 0.362  | 0.364                              | 0.365  | 0.367  | 0.369  | 0.370  | 0.372  | 0.373  | 0.375  | 0.376  | 0.378  | 530                         |  |
| 540   | 0.378  | 0.380                              | 0.381  | 0.383  | 0.384  | 0.386  | 0.388  | 0.389  | 0.391  | 0.392  | 0.394  | 540                         |  |
| 550   | 0.394  | 0.396                              | 0.397  | 0.399  | 0.401  | 0.402  | 0.404  | 0.405  | 0.407  | 0.409  | 0.410  | 550                         |  |
| 560   | 0.410  | 0.412                              | 0.414  | 0.415  | 0.417  | 0.419  | 0.420  | 0.422  | 0.424  | 0.425  | 0.427  | 560                         |  |
| 570   | 0.427  | 0.429                              | 0.431  | 0.432  | 0.434  | 0.436  | 0.437  | 0.439  | 0.441  | 0.442  | 0.444  | 570                         |  |
| 580   | 0.444  | 0.446                              | 0.448  | 0.449  | 0.451  | 0.453  | 0.455  | 0.456  | 0.458  | 0.460  | 0.462  | 580                         |  |
| 590   | 0.462  | 0.463                              | 0.465  | 0.467  | 0.469  | 0.470  | 0.472  | 0.474  | 0.476  | 0.477  | 0.479  | 590                         |  |
| 600   | 0.479  | 0.481                              | 0.483  | 0.485  | 0.486  | 0.488  | 0.490  | 0.492  | 0.494  | 0.495  | 0.497  | 600                         |  |
| 610   | 0.497  | 0.499                              | 0.501  | 0.503  | 0.504  | 0.506  | 0.508  | 0.510  | 0.512  | 0.514  | 0.515  | 610                         |  |
| 620   | 0.515  | 0.517                              | 0.519  | 0.521  | 0.523  | 0.525  | 0.527  | 0.528  | 0.530  | 0.532  | 0.534  | 620                         |  |
| 630   | 0.534  | 0.536                              | 0.538  | 0.540  | 0.542  | 0.544  | 0.545  | 0.547  | 0.549  | 0.551  | 0.553  | 630                         |  |
| 640   | 0.553  | 0.555                              | 0.557  | 0.559  | 0.561  | 0.563  | 0.565  | 0.566  | 0.568  | 0.570  | 0.572  | 640                         |  |

\* Converted from degrees Celsius (IPTS 1968).



166 THE USE OF THERMOCOUPLES IN TEMPERATURE MEASUREMENT

TABLE 10.2—Type B thermocouples (continued).

| EMF in Absolute Millivolts                    |       | Temperature in Degrees Fahrenheit* |       |       |       |       |       |       |       |       |       | Reference Junctions at 32 F |  |
|---|-------|------------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-----------------------------|--|
| DEG F   | 0     | 1                                  | 2     | 3     | 4     | 5     | 6     | 7     | 8     | 9     | 10    | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |       |                                    |       |       |       |       |       |       |       |       |       |                             |  |
| 650   | 0.572 | 0.574                              | 0.576 | 0.578 | 0.580 | 0.582 | 0.584 | 0.586 | 0.588 | 0.590 | 0.592 | 650                         |  |
| 660   | 0.592 | 0.594                              | 0.596 | 0.598 | 0.600 | 0.602 | 0.604 | 0.606 | 0.608 | 0.610 | 0.612 | 660                         |  |
| 670   | 0.612 | 0.614                              | 0.616 | 0.618 | 0.620 | 0.622 | 0.624 | 0.626 | 0.628 | 0.630 | 0.632 | 670                         |  |
| 680   | 0.632 | 0.634                              | 0.636 | 0.638 | 0.640 | 0.642 | 0.644 | 0.646 | 0.648 | 0.650 | 0.652 | 680                         |  |
| 690   | 0.652 | 0.654                              | 0.656 | 0.658 | 0.661 | 0.663 | 0.665 | 0.667 | 0.669 | 0.671 | 0.673 | 690                         |  |
| 700   | 0.673 | 0.675                              | 0.677 | 0.679 | 0.682 | 0.684 | 0.686 | 0.688 | 0.690 | 0.692 | 0.694 | 700                         |  |
| 710   | 0.694 | 0.696                              | 0.699 | 0.701 | 0.703 | 0.705 | 0.707 | 0.709 | 0.711 | 0.714 | 0.716 | 710                         |  |
| 720   | 0.716 | 0.718                              | 0.720 | 0.722 | 0.724 | 0.727 | 0.729 | 0.731 | 0.733 | 0.735 | 0.737 | 720                         |  |
| 730   | 0.737 | 0.740                              | 0.742 | 0.744 | 0.746 | 0.748 | 0.751 | 0.753 | 0.755 | 0.757 | 0.759 | 730                         |  |
| 740   | 0.759 | 0.762                              | 0.764 | 0.766 | 0.768 | 0.771 | 0.773 | 0.775 | 0.777 | 0.780 | 0.782 | 740                         |  |
| 750   | 0.782 | 0.784                              | 0.786 | 0.789 | 0.791 | 0.793 | 0.795 | 0.798 | 0.800 | 0.802 | 0.804 | 750                         |  |
| 760   | 0.804 | 0.807                              | 0.809 | 0.811 | 0.814 | 0.816 | 0.818 | 0.821 | 0.823 | 0.825 | 0.827 | 760                         |  |
| 770   | 0.827 | 0.830                              | 0.832 | 0.834 | 0.837 | 0.839 | 0.841 | 0.844 | 0.846 | 0.848 | 0.851 | 770                         |  |
| 780   | 0.851 | 0.853                              | 0.855 | 0.858 | 0.860 | 0.862 | 0.865 | 0.867 | 0.870 | 0.872 | 0.874 | 780                         |  |
| 790   | 0.874 | 0.877                              | 0.879 | 0.881 | 0.884 | 0.886 | 0.889 | 0.891 | 0.893 | 0.896 | 0.898 | 790                         |  |
| 800   | 0.898 | 0.901                              | 0.903 | 0.905 | 0.908 | 0.910 | 0.913 | 0.915 | 0.918 | 0.920 | 0.922 | 800                         |  |
| 810   | 0.922 | 0.925                              | 0.927 | 0.930 | 0.932 | 0.935 | 0.937 | 0.939 | 0.942 | 0.944 | 0.947 | 810                         |  |
| 820   | 0.947 | 0.949                              | 0.952 | 0.954 | 0.957 | 0.959 | 0.962 | 0.964 | 0.967 | 0.969 | 0.972 | 820                         |  |
| 830   | 0.972 | 0.974                              | 0.977 | 0.979 | 0.982 | 0.984 | 0.987 | 0.989 | 0.992 | 0.994 | 0.997 | 830                         |  |
| 840   | 0.997 | 0.999                              | 1.002 | 1.004 | 1.007 | 1.009 | 1.012 | 1.014 | 1.017 | 1.020 | 1.022 | 840                         |  |
| 850   | 1.022 | 1.025                              | 1.027 | 1.030 | 1.032 | 1.035 | 1.037 | 1.040 | 1.043 | 1.045 | 1.048 | 850                         |  |
| 860   | 1.048 | 1.050                              | 1.053 | 1.056 | 1.058 | 1.061 | 1.063 | 1.066 | 1.069 | 1.071 | 1.074 | 860                         |  |
| 870   | 1.074 | 1.076                              | 1.079 | 1.082 | 1.084 | 1.087 | 1.090 | 1.092 | 1.095 | 1.097 | 1.100 | 870                         |  |
| 880   | 1.100 | 1.102                              | 1.105 | 1.108 | 1.111 | 1.113 | 1.116 | 1.119 | 1.121 | 1.124 | 1.127 | 880                         |  |
| 890   | 1.127 | 1.129                              | 1.132 | 1.135 | 1.137 | 1.140 | 1.143 | 1.145 | 1.148 | 1.151 | 1.153 | 890                         |  |
| 900   | 1.153 | 1.156                              | 1.159 | 1.162 | 1.164 | 1.167 | 1.170 | 1.172 | 1.175 | 1.176 | 1.181 | 900                         |  |
| 910   | 1.181 | 1.183                              | 1.186 | 1.189 | 1.192 | 1.194 | 1.197 | 1.200 | 1.203 | 1.205 | 1.208 | 910                         |  |
| 920   | 1.208 | 1.211                              | 1.214 | 1.216 | 1.219 | 1.222 | 1.225 | 1.228 | 1.230 | 1.233 | 1.236 | 920                         |  |
| 930   | 1.236 | 1.239                              | 1.241 | 1.244 | 1.247 | 1.250 | 1.253 | 1.255 | 1.258 | 1.261 | 1.264 | 930                         |  |
| 940   | 1.264 | 1.267                              | 1.270 | 1.272 | 1.275 | 1.278 | 1.281 | 1.284 | 1.287 | 1.289 | 1.292 | 940                         |  |
| 950   | 1.292 | 1.295                              | 1.298 | 1.301 | 1.304 | 1.307 | 1.309 | 1.312 | 1.315 | 1.318 | 1.321 | 950                         |  |
| 960   | 1.321 | 1.324                              | 1.327 | 1.330 | 1.332 | 1.335 | 1.338 | 1.341 | 1.344 | 1.347 | 1.350 | 960                         |  |
| 970   | 1.350 | 1.353                              | 1.356 | 1.359 | 1.361 | 1.364 | 1.367 | 1.370 | 1.373 | 1.376 | 1.379 | 970                         |  |
| 980   | 1.379 | 1.382                              | 1.385 | 1.388 | 1.391 | 1.394 | 1.397 | 1.400 | 1.403 | 1.406 | 1.409 | 980                         |  |
| 990   | 1.409 | 1.411                              | 1.414 | 1.417 | 1.420 | 1.423 | 1.426 | 1.429 | 1.432 | 1.435 | 1.438 | 990                         |  |
| 1000  | 1.438 | 1.441                              | 1.444 | 1.447 | 1.450 | 1.453 | 1.456 | 1.459 | 1.462 | 1.465 | 1.468 | 1000                        |  |
| 1010  | 1.468 | 1.471                              | 1.474 | 1.477 | 1.480 | 1.483 | 1.487 | 1.490 | 1.493 | 1.496 | 1.499 | 1010                        |  |
| 1020  | 1.499 | 1.502                              | 1.505 | 1.508 | 1.511 | 1.514 | 1.517 | 1.520 | 1.523 | 1.526 | 1.529 | 1020                        |  |
| 1030  | 1.529 | 1.532                              | 1.536 | 1.539 | 1.542 | 1.545 | 1.548 | 1.551 | 1.554 | 1.557 | 1.560 | 1030                        |  |
| 1040  | 1.560 | 1.563                              | 1.566 | 1.570 | 1.573 | 1.576 | 1.579 | 1.582 | 1.585 | 1.588 | 1.591 | 1040                        |  |
| 1050  | 1.591 | 1.595                              | 1.598 | 1.601 | 1.604 | 1.607 | 1.610 | 1.613 | 1.617 | 1.620 | 1.623 | 1050                        |  |
| 1060  | 1.623 | 1.626                              | 1.629 | 1.632 | 1.636 | 1.639 | 1.642 | 1.645 | 1.648 | 1.652 | 1.655 | 1060                        |  |
| 1070  | 1.655 | 1.658                              | 1.661 | 1.664 | 1.668 | 1.671 | 1.674 | 1.677 | 1.680 | 1.684 | 1.687 | 1070                        |  |
| 1080  | 1.687 | 1.690                              | 1.693 | 1.696 | 1.700 | 1.703 | 1.705 | 1.709 | 1.713 | 1.716 | 1.719 | 1080                        |  |
| 1090  | 1.719 | 1.722                              | 1.726 | 1.729 | 1.732 | 1.735 | 1.739 | 1.742 | 1.745 | 1.748 | 1.752 | 1090                        |  |
| 1100  | 1.752 | 1.755                              | 1.758 | 1.762 | 1.765 | 1.768 | 1.771 | 1.775 | 1.778 | 1.781 | 1.785 | 1100                        |  |
| 1110  | 1.785 | 1.788                              | 1.791 | 1.795 | 1.798 | 1.801 | 1.804 | 1.808 | 1.811 | 1.814 | 1.818 | 1110                        |  |
| 1120  | 1.818 | 1.821                              | 1.824 | 1.828 | 1.831 | 1.834 | 1.838 | 1.841 | 1.844 | 1.848 | 1.851 | 1120                        |  |
| 1130  | 1.851 | 1.855                              | 1.858 | 1.861 | 1.865 | 1.868 | 1.871 | 1.875 | 1.878 | 1.882 | 1.885 | 1130                        |  |
| 1140  | 1.885 | 1.888                              | 1.892 | 1.895 | 1.898 | 1.902 | 1.905 | 1.909 | 1.912 | 1.915 | 1.919 | 1140                        |  |
| 1150  | 1.919 | 1.922                              | 1.926 | 1.929 | 1.933 | 1.936 | 1.939 | 1.943 | 1.946 | 1.950 | 1.953 | 1150                        |  |
| 1160  | 1.953 | 1.957                              | 1.960 | 1.963 | 1.967 | 1.970 | 1.974 | 1.977 | 1.981 | 1.984 | 1.988 | 1160                        |  |
| 1170  | 1.988 | 1.991                              | 1.995 | 1.998 | 2.002 | 2.005 | 2.009 | 2.012 | 2.015 | 2.019 | 2.022 | 1170                        |  |
| 1180  | 2.022 | 2.026                              | 2.029 | 2.033 | 2.036 | 2.040 | 2.043 | 2.047 | 2.051 | 2.054 | 2.058 | 1180                        |  |
| 1190  | 2.058 | 2.061                              | 2.065 | 2.068 | 2.072 | 2.075 | 2.079 | 2.082 | 2.086 | 2.089 | 2.093 | 1190                        |  |
| 1200  | 2.093 | 2.096                              | 2.100 | 2.104 | 2.107 | 2.111 | 2.114 | 2.118 | 2.121 | 2.125 | 2.129 | 1200                        |  |
| 1210  | 2.128 | 2.132                              | 2.136 | 2.139 | 2.143 | 2.146 | 2.150 | 2.154 | 2.157 | 2.161 | 2.164 | 1210                        |  |
| 1220  | 2.164 | 2.168                              | 2.172 | 2.175 | 2.179 | 2.182 | 2.185 | 2.190 | 2.193 | 2.197 | 2.201 | 1220                        |  |
| 1230  | 2.201 | 2.204                              | 2.208 | 2.211 | 2.215 | 2.219 | 2.222 | 2.226 | 2.230 | 2.233 | 2.237 | 1230                        |  |
| 1240  | 2.237 | 2.241                              | 2.244 | 2.248 | 2.252 | 2.255 | 2.259 | 2.263 | 2.266 | 2.270 | 2.274 | 1240                        |  |
| 1250  | 2.274 | 2.277                              | 2.281 | 2.285 | 2.288 | 2.292 | 2.296 | 2.299 | 2.303 | 2.307 | 2.311 | 1250                        |  |
| 1260  | 2.311 | 2.314                              | 2.318 | 2.322 | 2.325 | 2.329 | 2.333 | 2.337 | 2.340 | 2.344 | 2.348 | 1260                        |  |
| 1270  | 2.348 | 2.351                              | 2.355 | 2.359 | 2.363 | 2.366 | 2.370 | 2.374 | 2.378 | 2.381 | 2.385 | 1270                        |  |
| 1280  | 2.385 | 2.389                              | 2.393 | 2.396 | 2.400 | 2.404 | 2.408 | 2.412 | 2.415 | 2.419 | 2.423 | 1280                        |  |
| 1290  | 2.423 | 2.427                              | 2.430 | 2.434 | 2.438 | 2.442 | 2.446 | 2.449 | 2.453 | 2.457 | 2.461 | 1290                        |  |

\* Converted from degrees Celsius (IPTS 1968).

TABLE 10.2—Type B thermocouples (continued).

| EMF in Absolute Millivolts                    |       | Temperature in Degrees Fahrenheit* |       |       |       |       |       |       |       |       |       | Reference Junctions at 32 F |  |
|---|-------|------------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-----------------------------|--|
| DEG F   | 0     | 1                                  | 2     | 3     | 4     | 5     | 6     | 7     | 8     | 9     | 10    | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |       |                                    |       |       |       |       |       |       |       |       |       |                             |  |
| 1.300   | 2.461 | 2.465                              | 2.465 | 2.477 | 2.476 | 2.480 | 2.484 | 2.486 | 2.491 | 2.495 | 2.499 | 1.300                       |  |
| 1.310   | 2.469 | 2.503                              | 2.507 | 2.511 | 2.515 | 2.518 | 2.522 | 2.526 | 2.530 | 2.534 | 2.538 | 1.310                       |  |
| 1.320   | 2.538 | 2.562                              | 2.566 | 2.565 | 2.553 | 2.557 | 2.561 | 2.565 | 2.569 | 2.573 | 2.576 | 1.320                       |  |
| 1.330   | 2.576 | 2.580                              | 2.584 | 2.588 | 2.592 | 2.596 | 2.600 | 2.604 | 2.608 | 2.612 | 2.615 | 1.330                       |  |
| 1.340   | 2.615 | 2.619                              | 2.623 | 2.627 | 2.631 | 2.635 | 2.639 | 2.643 | 2.647 | 2.651 | 2.655 | 1.340                       |  |
| 1.350   | 2.655 | 2.659                              | 2.663 | 2.667 | 2.670 | 2.674 | 2.678 | 2.682 | 2.686 | 2.690 | 2.694 | 1.350                       |  |
| 1.360   | 2.694 | 2.698                              | 2.702 | 2.706 | 2.710 | 2.714 | 2.718 | 2.722 | 2.726 | 2.730 | 2.734 | 1.360                       |  |
| 1.370   | 2.734 | 2.738                              | 2.742 | 2.746 | 2.750 | 2.754 | 2.758 | 2.762 | 2.766 | 2.770 | 2.774 | 1.370                       |  |
| 1.380   | 2.774 | 2.778                              | 2.782 | 2.786 | 2.790 | 2.794 | 2.798 | 2.802 | 2.806 | 2.810 | 2.814 | 1.380                       |  |
| 1.390   | 2.814 | 2.818                              | 2.822 | 2.826 | 2.830 | 2.835 | 2.839 | 2.843 | 2.847 | 2.851 | 2.855 | 1.390                       |  |
| 1.400   | 2.855 | 2.859                              | 2.863 | 2.867 | 2.871 | 2.875 | 2.879 | 2.883 | 2.887 | 2.892 | 2.896 | 1.400                       |  |
| 1.410   | 2.896 | 2.900                              | 2.904 | 2.908 | 2.912 | 2.916 | 2.920 | 2.924 | 2.928 | 2.933 | 2.937 | 1.410                       |  |
| 1.420   | 2.937 | 2.941                              | 2.945 | 2.949 | 2.953 | 2.957 | 2.961 | 2.966 | 2.970 | 2.974 | 2.978 | 1.420                       |  |
| 1.430   | 2.978 | 2.982                              | 2.986 | 2.990 | 2.995 | 2.999 | 3.003 | 3.007 | 3.011 | 3.015 | 3.019 | 1.430                       |  |
| 1.440   | 3.019 | 3.024                              | 3.028 | 3.032 | 3.036 | 3.040 | 3.045 | 3.049 | 3.053 | 3.057 | 3.061 | 1.440                       |  |
| 1.450   | 3.061 | 3.065                              | 3.070 | 3.074 | 3.078 | 3.082 | 3.086 | 3.091 | 3.095 | 3.099 | 3.103 | 1.450                       |  |
| 1.460   | 3.103 | 3.107                              | 3.112 | 3.116 | 3.120 | 3.124 | 3.129 | 3.133 | 3.137 | 3.141 | 3.146 | 1.460                       |  |
| 1.470   | 3.146 | 3.150                              | 3.154 | 3.158 | 3.163 | 3.167 | 3.171 | 3.175 | 3.180 | 3.184 | 3.188 | 1.470                       |  |
| 1.480   | 3.188 | 3.192                              | 3.197 | 3.201 | 3.205 | 3.209 | 3.214 | 3.218 | 3.222 | 3.227 | 3.231 | 1.480                       |  |
| 1.490   | 3.231 | 3.235                              | 3.239 | 3.244 | 3.248 | 3.252 | 3.257 | 3.261 | 3.265 | 3.269 | 3.274 | 1.490                       |  |
| 1.500   | 3.274 | 3.278                              | 3.282 | 3.287 | 3.291 | 3.295 | 3.300 | 3.304 | 3.308 | 3.313 | 3.317 | 1.500                       |  |
| 1.510   | 3.317 | 3.321                              | 3.326 | 3.330 | 3.334 | 3.339 | 3.343 | 3.347 | 3.352 | 3.356 | 3.361 | 1.510                       |  |
| 1.520   | 3.361 | 3.365                              | 3.369 | 3.374 | 3.378 | 3.382 | 3.387 | 3.391 | 3.395 | 3.400 | 3.404 | 1.520                       |  |
| 1.530   | 3.404 | 3.409                              | 3.413 | 3.417 | 3.422 | 3.426 | 3.431 | 3.435 | 3.439 | 3.444 | 3.448 | 1.530                       |  |
| 1.540   | 3.448 | 3.453                              | 3.457 | 3.461 | 3.466 | 3.470 | 3.475 | 3.479 | 3.484 | 3.488 | 3.492 | 1.540                       |  |
| 1.550   | 3.492 | 3.497                              | 3.501 | 3.506 | 3.510 | 3.515 | 3.519 | 3.523 | 3.527 | 3.532 | 3.537 | 1.550                       |  |
| 1.560   | 3.537 | 3.541                              | 3.546 | 3.550 | 3.555 | 3.559 | 3.564 | 3.568 | 3.573 | 3.577 | 3.581 | 1.560                       |  |
| 1.570   | 3.581 | 3.586                              | 3.590 | 3.595 | 3.599 | 3.604 | 3.608 | 3.613 | 3.617 | 3.622 | 3.626 | 1.570                       |  |
| 1.580   | 3.626 | 3.631                              | 3.635 | 3.640 | 3.644 | 3.649 | 3.653 | 3.658 | 3.662 | 3.667 | 3.671 | 1.580                       |  |
| 1.590   | 3.672 | 3.676                              | 3.681 | 3.685 | 3.690 | 3.694 | 3.699 | 3.703 | 3.708 | 3.712 | 3.717 | 1.590                       |  |
| 1.600   | 3.717 | 3.721                              | 3.726 | 3.731 | 3.735 | 3.740 | 3.744 | 3.749 | 3.753 | 3.758 | 3.762 | 1.600                       |  |
| 1.610   | 3.762 | 3.767                              | 3.772 | 3.776 | 3.781 | 3.785 | 3.790 | 3.795 | 3.799 | 3.804 | 3.808 | 1.610                       |  |
| 1.620   | 3.808 | 3.813                              | 3.818 | 3.822 | 3.827 | 3.831 | 3.836 | 3.841 | 3.845 | 3.850 | 3.854 | 1.620                       |  |
| 1.630   | 3.854 | 3.859                              | 3.864 | 3.868 | 3.873 | 3.877 | 3.882 | 3.887 | 3.891 | 3.896 | 3.901 | 1.630                       |  |
| 1.640   | 3.901 | 3.905                              | 3.910 | 3.915 | 3.919 | 3.924 | 3.929 | 3.933 | 3.938 | 3.943 | 3.947 | 1.640                       |  |
| 1.650   | 3.947 | 3.952                              | 3.957 | 3.961 | 3.966 | 3.971 | 3.975 | 3.980 | 3.985 | 3.989 | 3.994 | 1.650                       |  |
| 1.660   | 3.994 | 3.999                              | 4.003 | 4.008 | 4.013 | 4.017 | 4.022 | 4.027 | 4.031 | 4.036 | 4.041 | 1.660                       |  |
| 1.670   | 4.041 | 4.046                              | 4.050 | 4.055 | 4.060 | 4.064 | 4.069 | 4.074 | 4.079 | 4.083 | 4.088 | 1.670                       |  |
| 1.680   | 4.088 | 4.093                              | 4.098 | 4.102 | 4.107 | 4.112 | 4.117 | 4.121 | 4.126 | 4.131 | 4.136 | 1.680                       |  |
| 1.690   | 4.136 | 4.140                              | 4.145 | 4.150 | 4.155 | 4.159 | 4.164 | 4.169 | 4.174 | 4.178 | 4.183 | 1.690                       |  |
| 1.700   | 4.183 | 4.188                              | 4.193 | 4.198 | 4.202 | 4.207 | 4.212 | 4.217 | 4.221 | 4.226 | 4.231 | 1.700                       |  |
| 1.710   | 4.231 | 4.236                              | 4.241 | 4.245 | 4.250 | 4.255 | 4.260 | 4.265 | 4.269 | 4.274 | 4.279 | 1.710                       |  |
| 1.720   | 4.279 | 4.284                              | 4.289 | 4.294 | 4.298 | 4.303 | 4.308 | 4.313 | 4.318 | 4.323 | 4.327 | 1.720                       |  |
| 1.730   | 4.327 | 4.332                              | 4.337 | 4.342 | 4.347 | 4.352 | 4.357 | 4.361 | 4.366 | 4.371 | 4.376 | 1.730                       |  |
| 1.740   | 4.376 | 4.381                              | 4.386 | 4.391 | 4.395 | 4.400 | 4.405 | 4.410 | 4.415 | 4.420 | 4.425 | 1.740                       |  |
| 1.750   | 4.425 | 4.430                              | 4.435 | 4.439 | 4.444 | 4.449 | 4.454 | 4.459 | 4.464 | 4.469 | 4.474 | 1.750                       |  |
| 1.760   | 4.474 | 4.479                              | 4.484 | 4.488 | 4.493 | 4.498 | 4.503 | 4.508 | 4.513 | 4.518 | 4.523 | 1.760                       |  |
| 1.770   | 4.523 | 4.528                              | 4.533 | 4.538 | 4.543 | 4.548 | 4.552 | 4.557 | 4.562 | 4.567 | 4.572 | 1.770                       |  |
| 1.780   | 4.572 | 4.577                              | 4.582 | 4.587 | 4.592 | 4.597 | 4.602 | 4.607 | 4.612 | 4.617 | 4.622 | 1.780                       |  |
| 1.790   | 4.622 | 4.627                              | 4.632 | 4.637 | 4.642 | 4.647 | 4.652 | 4.657 | 4.662 | 4.667 | 4.672 | 1.790                       |  |
| 1.800   | 4.672 | 4.677                              | 4.682 | 4.687 | 4.692 | 4.697 | 4.702 | 4.707 | 4.712 | 4.717 | 4.722 | 1.800                       |  |
| 1.810   | 4.722 | 4.727                              | 4.732 | 4.737 | 4.742 | 4.747 | 4.752 | 4.757 | 4.762 | 4.767 | 4.772 | 1.810                       |  |
| 1.820   | 4.772 | 4.777                              | 4.782 | 4.787 | 4.792 | 4.797 | 4.802 | 4.807 | 4.812 | 4.817 | 4.822 | 1.820                       |  |
| 1.830   | 4.823 | 4.828                              | 4.833 | 4.838 | 4.843 | 4.848 | 4.853 | 4.858 | 4.863 | 4.868 | 4.873 | 1.830                       |  |
| 1.840   | 4.873 | 4.878                              | 4.883 | 4.888 | 4.894 | 4.899 | 4.904 | 4.909 | 4.914 | 4.919 | 4.924 | 1.840                       |  |
| 1.850   | 4.924 | 4.929                              | 4.934 | 4.939 | 4.945 | 4.950 | 4.955 | 4.960 | 4.965 | 4.970 | 4.975 | 1.850                       |  |
| 1.860   | 4.975 | 4.980                              | 4.985 | 4.991 | 4.996 | 5.001 | 5.006 | 5.011 | 5.016 | 5.021 | 5.027 | 1.860                       |  |
| 1.870   | 5.027 | 5.032                              | 5.037 | 5.042 | 5.047 | 5.052 | 5.057 | 5.063 | 5.068 | 5.073 | 5.078 | 1.870                       |  |
| 1.880   | 5.078 | 5.083                              | 5.088 | 5.094 | 5.099 | 5.104 | 5.109 | 5.114 | 5.119 | 5.125 | 5.130 | 1.880                       |  |
| 1.890   | 5.130 | 5.135                              | 5.140 | 5.145 | 5.150 | 5.156 | 5.161 | 5.166 | 5.171 | 5.176 | 5.182 | 1.890                       |  |
| 1.900   | 5.182 | 5.187                              | 5.192 | 5.197 | 5.202 | 5.208 | 5.213 | 5.218 | 5.223 | 5.229 | 5.234 | 1.900                       |  |
| 1.910   | 5.234 | 5.239                              | 5.244 | 5.249 | 5.255 | 5.260 | 5.265 | 5.270 | 5.276 | 5.281 | 5.286 | 1.910                       |  |
| 1.920   | 5.286 | 5.291                              | 5.297 | 5.302 | 5.307 | 5.312 | 5.318 | 5.323 | 5.328 | 5.333 | 5.339 | 1.920                       |  |
| 1.930   | 5.339 | 5.344                              | 5.349 | 5.354 | 5.360 | 5.365 | 5.370 | 5.376 | 5.381 | 5.386 | 5.391 | 1.930                       |  |
| 1.940   | 5.391 | 5.397                              | 5.402 | 5.407 | 5.413 | 5.418 | 5.423 | 5.428 | 5.434 | 5.439 | 5.444 | 1.940                       |  |
| DEG F   | 0     | 1                                  | 2     | 3     | 4     | 5     | 6     | 7     | 8     | 9     | 10    | DEG F                       |  |

\* Converted from degrees Celsius (IPTS 1968).

TABLE 10.2—Type B thermocouples (continued).

| EMF in Absolute Millivolts                    |       | Temperature in Degrees Fahrenheit* |       |       |       |       |       |       |       |       |       | Reference Junctions at 32 F |  |
|---|-------|------------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-----------------------------|--|
| DEG F   | 0     | 1                                  | 2     | 3     | 4     | 5     | 6     | 7     | 8     | 9     | 10    | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |       |                                    |       |       |       |       |       |       |       |       |       |                             |  |
| 1950  | 5.444 | 5.450                              | 5.455 | 5.460 | 5.466 | 5.471 | 5.476 | 5.482 | 5.487 | 5.492 | 5.497 | 1950                        |  |
| 1960  | 5.497 | 5.503                              | 5.508 | 5.513 | 5.519 | 5.524 | 5.529 | 5.535 | 5.540 | 5.545 | 5.551 | 1960                        |  |
| 1970  | 5.551 | 5.556                              | 5.561 | 5.567 | 5.572 | 5.578 | 5.583 | 5.588 | 5.594 | 5.599 | 5.604 | 1970                        |  |
| 1980  | 5.604 | 5.610                              | 5.615 | 5.620 | 5.626 | 5.631 | 5.637 | 5.642 | 5.647 | 5.653 | 5.658 | 1980                        |  |
| 1990  | 5.658 | 5.663                              | 5.669 | 5.674 | 5.680 | 5.685 | 5.690 | 5.696 | 5.701 | 5.707 | 5.712 | 1990                        |  |
| 2000  | 5.712 | 5.717                              | 5.723 | 5.728 | 5.734 | 5.739 | 5.744 | 5.750 | 5.755 | 5.761 | 5.766 | 2000                        |  |
| 2010  | 5.766 | 5.771                              | 5.777 | 5.782 | 5.788 | 5.793 | 5.799 | 5.804 | 5.810 | 5.815 | 5.820 | 2010                        |  |
| 2020  | 5.820 | 5.826                              | 5.831 | 5.837 | 5.842 | 5.848 | 5.853 | 5.859 | 5.864 | 5.869 | 5.875 | 2020                        |  |
| 2030  | 5.875 | 5.880                              | 5.886 | 5.891 | 5.897 | 5.902 | 5.908 | 5.913 | 5.919 | 5.924 | 5.930 | 2030                        |  |
| 2040  | 5.930 | 5.935                              | 5.941 | 5.946 | 5.951 | 5.957 | 5.962 | 5.968 | 5.973 | 5.979 | 5.984 | 2040                        |  |
| 2050  | 5.984 | 5.990                              | 5.995 | 6.001 | 6.006 | 6.012 | 6.017 | 6.023 | 6.028 | 6.034 | 6.039 | 2050                        |  |
| 2060  | 6.039 | 6.045                              | 6.051 | 6.056 | 6.062 | 6.067 | 6.073 | 6.078 | 6.084 | 6.089 | 6.095 | 2060                        |  |
| 2070  | 6.095 | 6.100                              | 6.106 | 6.111 | 6.117 | 6.122 | 6.128 | 6.134 | 6.139 | 6.145 | 6.150 | 2070                        |  |
| 2080  | 6.150 | 6.156                              | 6.161 | 6.167 | 6.172 | 6.178 | 6.184 | 6.189 | 6.195 | 6.200 | 6.206 | 2080                        |  |
| 2090  | 6.206 | 6.211                              | 6.217 | 6.223 | 6.228 | 6.234 | 6.239 | 6.245 | 6.250 | 6.256 | 6.262 | 2090                        |  |
| 2100  | 6.262 | 6.267                              | 6.273 | 6.278 | 6.284 | 6.290 | 6.295 | 6.301 | 6.306 | 6.312 | 6.318 | 2100                        |  |
| 2110  | 6.318 | 6.323                              | 6.329 | 6.334 | 6.340 | 6.346 | 6.351 | 6.357 | 6.362 | 6.368 | 6.374 | 2110                        |  |
| 2120  | 6.374 | 6.379                              | 6.385 | 6.391 | 6.396 | 6.402 | 6.408 | 6.413 | 6.419 | 6.424 | 6.430 | 2120                        |  |
| 2130  | 6.430 | 6.436                              | 6.441 | 6.447 | 6.453 | 6.458 | 6.464 | 6.470 | 6.475 | 6.481 | 6.487 | 2130                        |  |
| 2140  | 6.487 | 6.492                              | 6.498 | 6.504 | 6.509 | 6.515 | 6.521 | 6.526 | 6.532 | 6.538 | 6.543 | 2140                        |  |
| 2150  | 6.543 | 6.549                              | 6.555 | 6.560 | 6.566 | 6.572 | 6.577 | 6.583 | 6.589 | 6.594 | 6.600 | 2150                        |  |
| 2160  | 6.600 | 6.606                              | 6.612 | 6.617 | 6.623 | 6.629 | 6.634 | 6.640 | 6.646 | 6.651 | 6.657 | 2160                        |  |
| 2170  | 6.657 | 6.663                              | 6.669 | 6.674 | 6.680 | 6.686 | 6.692 | 6.697 | 6.703 | 6.709 | 6.714 | 2170                        |  |
| 2180  | 6.714 | 6.720                              | 6.726 | 6.732 | 6.737 | 6.743 | 6.749 | 6.755 | 6.760 | 6.766 | 6.772 | 2180                        |  |
| 2190  | 6.772 | 6.778                              | 6.783 | 6.789 | 6.795 | 6.801 | 6.806 | 6.812 | 6.818 | 6.824 | 6.829 | 2190                        |  |
| 2200  | 6.829 | 6.835                              | 6.841 | 6.847 | 6.852 | 6.858 | 6.864 | 6.870 | 6.876 | 6.881 | 6.887 | 2200                        |  |
| 2210  | 6.887 | 6.893                              | 6.899 | 6.904 | 6.910 | 6.916 | 6.922 | 6.928 | 6.933 | 6.939 | 6.945 | 2210                        |  |
| 2220  | 6.945 | 6.951                              | 6.957 | 6.962 | 6.968 | 6.974 | 6.980 | 6.986 | 6.991 | 6.997 | 7.003 | 2220                        |  |
| 2230  | 7.003 | 7.009                              | 7.015 | 7.021 | 7.026 | 7.032 | 7.038 | 7.044 | 7.050 | 7.055 | 7.061 | 2230                        |  |
| 2240  | 7.061 | 7.067                              | 7.073 | 7.079 | 7.085 | 7.090 | 7.096 | 7.102 | 7.108 | 7.114 | 7.120 | 2240                        |  |
| 2250  | 7.120 | 7.126                              | 7.131 | 7.137 | 7.143 | 7.149 | 7.155 | 7.161 | 7.167 | 7.172 | 7.178 | 2250                        |  |
| 2260  | 7.178 | 7.184                              | 7.190 | 7.196 | 7.202 | 7.208 | 7.213 | 7.219 | 7.225 | 7.231 | 7.237 | 2260                        |  |
| 2270  | 7.237 | 7.243                              | 7.249 | 7.255 | 7.260 | 7.266 | 7.272 | 7.278 | 7.284 | 7.290 | 7.296 | 2270                        |  |
| 2280  | 7.296 | 7.302                              | 7.308 | 7.314 | 7.319 | 7.325 | 7.331 | 7.337 | 7.343 | 7.349 | 7.355 | 2280                        |  |
| 2290  | 7.355 | 7.361                              | 7.367 | 7.373 | 7.378 | 7.384 | 7.390 | 7.396 | 7.402 | 7.408 | 7.414 | 2290                        |  |
| 2300  | 7.414 | 7.420                              | 7.426 | 7.432 | 7.438 | 7.444 | 7.450 | 7.456 | 7.461 | 7.467 | 7.473 | 2300                        |  |
| 2310  | 7.473 | 7.479                              | 7.485 | 7.491 | 7.497 | 7.503 | 7.509 | 7.515 | 7.521 | 7.527 | 7.533 | 2310                        |  |
| 2320  | 7.533 | 7.539                              | 7.545 | 7.551 | 7.557 | 7.563 | 7.569 | 7.575 | 7.581 | 7.587 | 7.593 | 2320                        |  |
| 2330  | 7.592 | 7.598                              | 7.604 | 7.610 | 7.616 | 7.622 | 7.628 | 7.634 | 7.640 | 7.646 | 7.652 | 2330                        |  |
| 2340  | 7.652 | 7.658                              | 7.664 | 7.670 | 7.676 | 7.682 | 7.688 | 7.694 | 7.700 | 7.706 | 7.712 | 2340                        |  |
| 2350  | 7.712 | 7.718                              | 7.724 | 7.730 | 7.736 | 7.742 | 7.748 | 7.754 | 7.760 | 7.766 | 7.772 | 2350                        |  |
| 2360  | 7.772 | 7.778                              | 7.784 | 7.790 | 7.796 | 7.802 | 7.808 | 7.814 | 7.820 | 7.827 | 7.833 | 2360                        |  |
| 2370  | 7.833 | 7.839                              | 7.845 | 7.851 | 7.857 | 7.863 | 7.869 | 7.875 | 7.881 | 7.887 | 7.893 | 2370                        |  |
| 2380  | 7.893 | 7.899                              | 7.905 | 7.911 | 7.917 | 7.923 | 7.929 | 7.935 | 7.941 | 7.947 | 7.953 | 2380                        |  |
| 2390  | 7.953 | 7.959                              | 7.966 | 7.972 | 7.978 | 7.984 | 7.990 | 7.996 | 8.002 | 8.008 | 8.014 | 2390                        |  |
| 2400  | 8.014 | 8.020                              | 8.026 | 8.032 | 8.038 | 8.044 | 8.051 | 8.057 | 8.063 | 8.069 | 8.075 | 2400                        |  |
| 2410  | 8.075 | 8.081                              | 8.087 | 8.093 | 8.099 | 8.105 | 8.111 | 8.117 | 8.124 | 8.130 | 8.136 | 2410                        |  |
| 2420  | 8.136 | 8.142                              | 8.148 | 8.154 | 8.160 | 8.166 | 8.172 | 8.179 | 8.185 | 8.191 | 8.197 | 2420                        |  |
| 2430  | 8.197 | 8.203                              | 8.209 | 8.215 | 8.221 | 8.227 | 8.234 | 8.240 | 8.246 | 8.252 | 8.258 | 2430                        |  |
| 2440  | 8.258 | 8.264                              | 8.270 | 8.276 | 8.283 | 8.289 | 8.295 | 8.301 | 8.307 | 8.313 | 8.319 | 2440                        |  |
| 2450  | 8.319 | 8.326                              | 8.332 | 8.338 | 8.344 | 8.350 | 8.356 | 8.362 | 8.369 | 8.375 | 8.381 | 2450                        |  |
| 2460  | 8.381 | 8.387                              | 8.393 | 8.399 | 8.405 | 8.412 | 8.418 | 8.424 | 8.430 | 8.436 | 8.442 | 2460                        |  |
| 2470  | 8.442 | 8.449                              | 8.455 | 8.461 | 8.467 | 8.473 | 8.479 | 8.486 | 8.492 | 8.498 | 8.504 | 2470                        |  |
| 2480  | 8.504 | 8.510                              | 8.516 | 8.522 | 8.529 | 8.535 | 8.541 | 8.547 | 8.554 | 8.560 | 8.566 | 2480                        |  |
| 2490  | 8.566 | 8.572                              | 8.578 | 8.585 | 8.591 | 8.597 | 8.603 | 8.609 | 8.616 | 8.622 | 8.628 | 2490                        |  |
| 2500  | 8.628 | 8.634                              | 8.640 | 8.647 | 8.653 | 8.659 | 8.665 | 8.671 | 8.678 | 8.684 | 8.690 | 2500                        |  |
| 2510  | 8.690 | 8.696                              | 8.702 | 8.709 | 8.715 | 8.721 | 8.727 | 8.733 | 8.740 | 8.746 | 8.752 | 2510                        |  |
| 2520  | 8.752 | 8.758                              | 8.765 | 8.771 | 8.777 | 8.783 | 8.790 | 8.796 | 8.802 | 8.808 | 8.814 | 2520                        |  |
| 2530  | 8.814 | 8.821                              | 8.827 | 8.833 | 8.839 | 8.846 | 8.852 | 8.858 | 8.864 | 8.871 | 8.877 | 2530                        |  |
| 2540  | 8.877 | 8.883                              | 8.889 | 8.896 | 8.902 | 8.908 | 8.914 | 8.921 | 8.927 | 8.933 | 8.939 | 2540                        |  |
| 2550  | 8.939 | 8.946                              | 8.952 | 8.958 | 8.964 | 8.971 | 8.977 | 8.983 | 8.989 | 8.996 | 9.002 | 2550                        |  |
| 2560  | 9.002 | 9.008                              | 9.015 | 9.021 | 9.027 | 9.033 | 9.040 | 9.046 | 9.052 | 9.058 | 9.064 | 2560                        |  |
| 2570  | 9.065 | 9.071                              | 9.077 | 9.084 | 9.090 | 9.096 | 9.102 | 9.109 | 9.115 | 9.121 | 9.128 | 2570                        |  |
| 2580  | 9.128 | 9.134                              | 9.140 | 9.146 | 9.153 | 9.159 | 9.165 | 9.172 | 9.178 | 9.184 | 9.191 | 2580                        |  |
| 2590  | 9.191 | 9.197                              | 9.203 | 9.209 | 9.216 | 9.222 | 9.228 | 9.235 | 9.241 | 9.247 | 9.254 | 2590                        |  |

\* Converted from degrees Celsius (IPTS 1968).

TABLE 10.2—Type B thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit* |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|------------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
| DEG F   | 0      | 1                                  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |
| THERMoeLECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |                                    |        |        |        |        |        |        |        |        |        |                             |  |
| 2600  | 9.254  | 9.260                              | 9.266  | 9.273  | 9.279  | 9.285  | 9.291  | 9.298  | 9.304  | 9.310  | 9.317  | 2600                        |  |
| 2610  | 9.317  | 9.323                              | 9.329  | 9.336  | 9.342  | 9.348  | 9.355  | 9.361  | 9.367  | 9.374  | 9.380  | 2610                        |  |
| 2620  | 9.380  | 9.386                              | 9.393  | 9.399  | 9.405  | 9.412  | 9.418  | 9.424  | 9.431  | 9.437  | 9.443  | 2620                        |  |
| 2630  | 9.443  | 9.450                              | 9.456  | 9.462  | 9.469  | 9.475  | 9.481  | 9.488  | 9.494  | 9.500  | 9.507  | 2630                        |  |
| 2640  | 9.507  | 9.513                              | 9.519  | 9.526  | 9.532  | 9.538  | 9.545  | 9.551  | 9.558  | 9.564  | 9.570  | 2640                        |  |
| 2650  | 9.570  | 9.577                              | 9.583  | 9.589  | 9.596  | 9.602  | 9.608  | 9.615  | 9.621  | 9.627  | 9.634  | 2650                        |  |
| 2660  | 9.634  | 9.640                              | 9.647  | 9.653  | 9.659  | 9.666  | 9.672  | 9.678  | 9.685  | 9.691  | 9.697  | 2660                        |  |
| 2670  | 9.697  | 9.704                              | 9.710  | 9.717  | 9.723  | 9.729  | 9.736  | 9.742  | 9.748  | 9.755  | 9.761  | 2670                        |  |
| 2680  | 9.761  | 9.768                              | 9.774  | 9.780  | 9.787  | 9.793  | 9.800  | 9.806  | 9.812  | 9.819  | 9.825  | 2680                        |  |
| 2690  | 9.825  | 9.831                              | 9.838  | 9.844  | 9.851  | 9.857  | 9.863  | 9.870  | 9.876  | 9.883  | 9.889  | 2690                        |  |
| 2700  | 9.889  | 9.895                              | 9.902  | 9.908  | 9.915  | 9.921  | 9.927  | 9.934  | 9.940  | 9.947  | 9.953  | 2700                        |  |
| 2710  | 9.953  | 9.959                              | 9.966  | 9.972  | 9.979  | 9.985  | 9.991  | 9.998  | 10.004 | 10.011 | 10.017 | 2710                        |  |
| 2720  | 10.017 | 10.023                             | 10.030 | 10.036 | 10.043 | 10.049 | 10.056 | 10.062 | 10.068 | 10.075 | 10.081 | 2720                        |  |
| 2730  | 10.081 | 10.088                             | 10.094 | 10.100 | 10.107 | 10.113 | 10.120 | 10.126 | 10.133 | 10.139 | 10.145 | 2730                        |  |
| 2740  | 10.145 | 10.152                             | 10.158 | 10.165 | 10.171 | 10.178 | 10.184 | 10.190 | 10.197 | 10.203 | 10.210 | 2740                        |  |
| 2750  | 10.210 | 10.216                             | 10.223 | 10.229 | 10.235 | 10.242 | 10.248 | 10.255 | 10.261 | 10.268 | 10.274 | 2750                        |  |
| 2760  | 10.274 | 10.280                             | 10.287 | 10.293 | 10.300 | 10.306 | 10.313 | 10.319 | 10.325 | 10.332 | 10.338 | 2760                        |  |
| 2770  | 10.338 | 10.345                             | 10.351 | 10.358 | 10.364 | 10.371 | 10.377 | 10.383 | 10.390 | 10.396 | 10.403 | 2770                        |  |
| 2780  | 10.403 | 10.409                             | 10.416 | 10.422 | 10.429 | 10.435 | 10.441 | 10.448 | 10.454 | 10.461 | 10.467 | 2780                        |  |
| 2790  | 10.467 | 10.474                             | 10.480 | 10.487 | 10.493 | 10.500 | 10.506 | 10.512 | 10.519 | 10.525 | 10.532 | 2790                        |  |
| 2800  | 10.532 | 10.538                             | 10.545 | 10.551 | 10.558 | 10.564 | 10.571 | 10.577 | 10.584 | 10.590 | 10.596 | 2800                        |  |
| 2810  | 10.596 | 10.603                             | 10.609 | 10.616 | 10.622 | 10.629 | 10.635 | 10.642 | 10.648 | 10.655 | 10.661 | 2810                        |  |
| 2820  | 10.661 | 10.668                             | 10.674 | 10.680 | 10.687 | 10.693 | 10.700 | 10.706 | 10.713 | 10.719 | 10.726 | 2820                        |  |
| 2830  | 10.726 | 10.732                             | 10.739 | 10.745 | 10.752 | 10.758 | 10.765 | 10.771 | 10.778 | 10.784 | 10.790 | 2830                        |  |
| 2840  | 10.790 | 10.797                             | 10.803 | 10.810 | 10.816 | 10.823 | 10.829 | 10.836 | 10.842 | 10.849 | 10.855 | 2840                        |  |
| 2850  | 10.855 | 10.862                             | 10.868 | 10.875 | 10.881 | 10.888 | 10.894 | 10.901 | 10.907 | 10.914 | 10.920 | 2850                        |  |
| 2860  | 10.920 | 10.926                             | 10.933 | 10.939 | 10.946 | 10.952 | 10.959 | 10.965 | 10.972 | 10.978 | 10.985 | 2860                        |  |
| 2870  | 10.985 | 10.991                             | 10.998 | 11.004 | 11.011 | 11.017 | 11.024 | 11.030 | 11.037 | 11.043 | 11.050 | 2870                        |  |
| 2880  | 11.050 | 11.056                             | 11.063 | 11.069 | 11.076 | 11.082 | 11.089 | 11.095 | 11.102 | 11.108 | 11.115 | 2880                        |  |
| 2890  | 11.115 | 11.121                             | 11.128 | 11.134 | 11.141 | 11.147 | 11.154 | 11.160 | 11.166 | 11.173 | 11.179 | 2890                        |  |
| 2900  | 11.179 | 11.186                             | 11.192 | 11.199 | 11.205 | 11.212 | 11.218 | 11.225 | 11.231 | 11.238 | 11.244 | 2900                        |  |
| 2910  | 11.244 | 11.251                             | 11.257 | 11.264 | 11.270 | 11.277 | 11.283 | 11.290 | 11.296 | 11.303 | 11.309 | 2910                        |  |
| 2920  | 11.309 | 11.316                             | 11.322 | 11.329 | 11.335 | 11.342 | 11.348 | 11.355 | 11.361 | 11.368 | 11.374 | 2920                        |  |
| 2930  | 11.374 | 11.381                             | 11.387 | 11.394 | 11.400 | 11.407 | 11.413 | 11.420 | 11.426 | 11.433 | 11.439 | 2930                        |  |
| 2940  | 11.439 | 11.446                             | 11.452 | 11.459 | 11.465 | 11.472 | 11.478 | 11.485 | 11.491 | 11.498 | 11.504 | 2940                        |  |
| 2950  | 11.504 | 11.511                             | 11.517 | 11.524 | 11.530 | 11.537 | 11.543 | 11.550 | 11.556 | 11.563 | 11.569 | 2950                        |  |
| 2960  | 11.569 | 11.576                             | 11.582 | 11.589 | 11.595 | 11.602 | 11.608 | 11.615 | 11.621 | 11.628 | 11.634 | 2960                        |  |
| 2970  | 11.634 | 11.641                             | 11.647 | 11.654 | 11.660 | 11.667 | 11.673 | 11.680 | 11.686 | 11.693 | 11.699 | 2970                        |  |
| 2980  | 11.699 | 11.706                             | 11.712 | 11.719 | 11.725 | 11.732 | 11.738 | 11.745 | 11.751 | 11.758 | 11.764 | 2980                        |  |
| 2990  | 11.764 | 11.771                             | 11.777 | 11.784 | 11.790 | 11.797 | 11.803 | 11.810 | 11.816 | 11.823 | 11.829 | 2990                        |  |
| 3000  | 11.829 | 11.836                             | 11.842 | 11.849 | 11.855 | 11.862 | 11.868 | 11.875 | 11.881 | 11.888 | 11.894 | 3000                        |  |
| 3010  | 11.894 | 11.901                             | 11.907 | 11.914 | 11.920 | 11.927 | 11.933 | 11.940 | 11.946 | 11.953 | 11.959 | 3010                        |  |
| 3020  | 11.959 | 11.966                             | 11.972 | 11.979 | 11.985 | 11.992 | 11.998 | 12.005 | 12.011 | 12.018 | 12.024 | 3020                        |  |
| 3030  | 12.024 | 12.031                             | 12.037 | 12.044 | 12.050 | 12.057 | 12.063 | 12.070 | 12.076 | 12.083 | 12.089 | 3030                        |  |
| 3040  | 12.089 | 12.096                             | 12.102 | 12.109 | 12.115 | 12.121 | 12.128 | 12.134 | 12.141 | 12.147 | 12.154 | 3040                        |  |
| 3050  | 12.154 | 12.160                             | 12.167 | 12.173 | 12.180 | 12.186 | 12.193 | 12.199 | 12.206 | 12.212 | 12.219 | 3050                        |  |
| 3060  | 12.219 | 12.225                             | 12.232 | 12.238 | 12.245 | 12.251 | 12.258 | 12.264 | 12.271 | 12.277 | 12.284 | 3060                        |  |
| 3070  | 12.284 | 12.290                             | 12.297 | 12.303 | 12.310 | 12.316 | 12.323 | 12.329 | 12.336 | 12.342 | 12.349 | 3070                        |  |
| 3080  | 12.349 | 12.355                             | 12.362 | 12.368 | 12.374 | 12.381 | 12.387 | 12.394 | 12.400 | 12.407 | 12.413 | 3080                        |  |
| 3090  | 12.413 | 12.420                             | 12.426 | 12.433 | 12.439 | 12.446 | 12.452 | 12.459 | 12.465 | 12.472 | 12.478 | 3090                        |  |
| 3100  | 12.478 | 12.485                             | 12.491 | 12.498 | 12.504 | 12.511 | 12.517 | 12.523 | 12.530 | 12.536 | 12.543 | 3100                        |  |
| 3110  | 12.543 | 12.549                             | 12.556 | 12.562 | 12.569 | 12.575 | 12.582 | 12.588 | 12.595 | 12.601 | 12.608 | 3110                        |  |
| 3120  | 12.608 | 12.614                             | 12.621 | 12.627 | 12.633 | 12.640 | 12.646 | 12.653 | 12.659 | 12.666 | 12.672 | 3120                        |  |
| 3130  | 12.672 | 12.679                             | 12.685 | 12.692 | 12.698 | 12.705 | 12.711 | 12.718 | 12.724 | 12.730 | 12.737 | 3130                        |  |
| 3140  | 12.737 | 12.743                             | 12.750 | 12.756 | 12.763 | 12.769 | 12.775 | 12.782 | 12.789 | 12.795 | 12.801 | 3140                        |  |
| 3150  | 12.801 | 12.808                             | 12.814 | 12.821 | 12.827 | 12.834 | 12.840 | 12.847 | 12.853 | 12.860 | 12.866 | 3150                        |  |
| 3160  | 12.866 | 12.872                             | 12.879 | 12.885 | 12.892 | 12.898 | 12.905 | 12.911 | 12.918 | 12.924 | 12.930 | 3160                        |  |
| 3170  | 12.930 | 12.937                             | 12.943 | 12.950 | 12.956 | 12.963 | 12.969 | 12.976 | 12.982 | 12.988 | 12.995 | 3170                        |  |
| 3180  | 12.995 | 13.001                             | 13.008 | 13.014 | 13.021 | 13.027 | 13.034 | 13.040 | 13.046 | 13.053 | 13.059 | 3180                        |  |
| 3190  | 13.059 | 13.066                             | 13.072 | 13.079 | 13.085 | 13.091 | 13.098 | 13.104 | 13.111 | 13.117 | 13.124 | 3190                        |  |
| 3200  | 13.124 | 13.130                             | 13.136 | 13.143 | 13.149 | 13.156 | 13.162 | 13.169 | 13.175 | 13.181 | 13.188 | 3200                        |  |
| 3210  | 13.188 | 13.194                             | 13.201 | 13.207 | 13.213 | 13.220 | 13.226 | 13.233 | 13.239 | 13.246 | 13.252 | 3210                        |  |
| 3220  | 13.252 | 13.258                             | 13.265 | 13.271 | 13.278 | 13.284 | 13.290 | 13.297 | 13.303 | 13.310 | 13.316 | 3220                        |  |
| 3230  | 13.316 | 13.322                             | 13.329 | 13.335 | 13.342 | 13.348 | 13.354 | 13.361 | 13.367 | 13.374 | 13.380 | 3230                        |  |
| 3240  | 13.380 | 13.387                             | 13.393 | 13.399 | 13.406 | 13.412 | 13.418 | 13.425 | 13.431 | 13.438 | 13.444 | 3240                        |  |

\* Converted from degrees Celsius (IPTS 1968).

TABLE 10.2—Type B thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit <sup>a</sup> |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
| DEG F   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                             |  |
| 3,250   | 13.444 | 13.450   | 13.457 | 13.463 | 13.470 | 13.476 | 13.482 | 13.489 | 13.495 | 13.502 | 13.508 | 3,250                       |  |
| 3,260   | 13.508 | 13.514   | 13.521 | 13.527 | 13.533 | 13.540 | 13.546 | 13.553 | 13.559 | 13.565 | 13.572 | 3,260                       |  |
| 3,270   | 13.572 | 13.576   | 13.585 | 13.591 | 13.597 | 13.604 | 13.610 | 13.616 | 13.623 | 13.629 | 13.635 | 3,270                       |  |
| 3,280   | 13.635 | 13.642   | 13.648 | 13.655 | 13.661 | 13.667 | 13.674 | 13.680 | 13.686 | 13.693 | 13.699 | 3,280                       |  |
| 3,290   | 13.699 | 13.706   | 13.712 | 13.718 | 13.725 | 13.731 | 13.737 | 13.744 | 13.750 | 13.756 | 13.763 | 3,290                       |  |
| 3,300   | 13.763 | 13.769   | 13.775 | 13.782 | 13.788 | 13.794 | 13.801 | 13.807 | 13.814 |        |        | 3,300                       |  |
| DEG F   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |

<sup>a</sup> Converted from degrees Celsius (ITS 1968).

TABLE 10.3—Type B thermocouples (deg C-millivolts).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Celsius (IPTS 1968) |        |        |        |        |        |        |        |        |        | Reference Junctions at 0 C |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------------------------|--|
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                            |  |
| 0   | 0.000  | -0.000                                     | -0.000 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.002 | -0.002 | -0.002 | 0                          |  |
| 10  | -0.002 | -0.002                                     | -0.002 | -0.002 | -0.002 | -0.002 | -0.002 | -0.002 | -0.003 | -0.003 | -0.003 | 10                         |  |
| 20  | -0.003 | -0.003                                     | -0.003 | -0.003 | -0.003 | -0.002 | -0.002 | -0.002 | -0.002 | -0.002 | -0.002 | 20                         |  |
| 30  | -0.002 | -0.002                                     | -0.002 | -0.002 | -0.002 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.000 | 30                         |  |
| 40  | -0.000 | -0.000                                     | -0.000 | 0.000  | 0.000  | 0.001  | 0.001  | 0.001  | 0.002  | 0.002  | 0.002  | 40                         |  |
| 50  | 0.002  | 0.003                                      | 0.003  | 0.003  | 0.004  | 0.004  | 0.004  | 0.005  | 0.005  | 0.006  | 0.006  | 50                         |  |
| 60  | 0.006  | 0.007                                      | 0.007  | 0.008  | 0.008  | 0.009  | 0.009  | 0.010  | 0.010  | 0.011  | 0.011  | 60                         |  |
| 70  | 0.011  | 0.012                                      | 0.012  | 0.013  | 0.014  | 0.014  | 0.015  | 0.015  | 0.016  | 0.017  | 0.017  | 70                         |  |
| 80  | 0.017  | 0.018                                      | 0.019  | 0.020  | 0.020  | 0.021  | 0.022  | 0.022  | 0.023  | 0.024  | 0.025  | 80                         |  |
| 90  | 0.025  | 0.026                                      | 0.026  | 0.027  | 0.028  | 0.029  | 0.030  | 0.031  | 0.031  | 0.032  | 0.033  | 90                         |  |
| 100   | 0.033  | 0.034                                      | 0.035  | 0.036  | 0.037  | 0.038  | 0.039  | 0.040  | 0.041  | 0.042  | 0.043  | 100                        |  |
| 110   | 0.043  | 0.044                                      | 0.045  | 0.046  | 0.047  | 0.048  | 0.049  | 0.050  | 0.051  | 0.052  | 0.053  | 110                        |  |
| 120   | 0.053  | 0.055                                      | 0.056  | 0.057  | 0.058  | 0.059  | 0.060  | 0.062  | 0.063  | 0.064  | 0.065  | 120                        |  |
| 130   | 0.065  | 0.066                                      | 0.068  | 0.069  | 0.070  | 0.071  | 0.073  | 0.074  | 0.075  | 0.077  | 0.078  | 130                        |  |
| 140   | 0.078  | 0.079                                      | 0.081  | 0.082  | 0.083  | 0.085  | 0.086  | 0.088  | 0.089  | 0.091  | 0.092  | 140                        |  |
| 150   | 0.092  | 0.093                                      | 0.095  | 0.096  | 0.098  | 0.099  | 0.101  | 0.102  | 0.104  | 0.106  | 0.107  | 150                        |  |
| 160   | 0.107  | 0.109                                      | 0.110  | 0.112  | 0.113  | 0.115  | 0.117  | 0.118  | 0.120  | 0.122  | 0.123  | 160                        |  |
| 170   | 0.123  | 0.125                                      | 0.127  | 0.128  | 0.130  | 0.132  | 0.133  | 0.135  | 0.137  | 0.139  | 0.140  | 170                        |  |
| 180   | 0.140  | 0.142                                      | 0.144  | 0.146  | 0.148  | 0.149  | 0.151  | 0.153  | 0.155  | 0.157  | 0.159  | 180                        |  |
| 190   | 0.159  | 0.161                                      | 0.163  | 0.164  | 0.166  | 0.168  | 0.170  | 0.172  | 0.174  | 0.176  | 0.178  | 190                        |  |
| 200   | 0.178  | 0.180                                      | 0.182  | 0.184  | 0.186  | 0.188  | 0.190  | 0.192  | 0.194  | 0.197  | 0.199  | 200                        |  |
| 210   | 0.199  | 0.201                                      | 0.203  | 0.205  | 0.207  | 0.209  | 0.211  | 0.214  | 0.216  | 0.218  | 0.220  | 210                        |  |
| 220   | 0.220  | 0.222                                      | 0.225  | 0.227  | 0.229  | 0.231  | 0.234  | 0.236  | 0.238  | 0.240  | 0.243  | 220                        |  |
| 230   | 0.243  | 0.245                                      | 0.247  | 0.250  | 0.252  | 0.254  | 0.257  | 0.259  | 0.262  | 0.264  | 0.266  | 230                        |  |
| 240   | 0.266  | 0.269                                      | 0.271  | 0.274  | 0.276  | 0.279  | 0.281  | 0.284  | 0.286  | 0.289  | 0.291  | 240                        |  |
| 250   | 0.291  | 0.294                                      | 0.296  | 0.299  | 0.301  | 0.304  | 0.307  | 0.309  | 0.312  | 0.314  | 0.317  | 250                        |  |
| 260   | 0.317  | 0.320                                      | 0.322  | 0.325  | 0.328  | 0.330  | 0.333  | 0.336  | 0.338  | 0.341  | 0.344  | 260                        |  |
| 270   | 0.344  | 0.347                                      | 0.349  | 0.352  | 0.355  | 0.358  | 0.360  | 0.363  | 0.366  | 0.369  | 0.372  | 270                        |  |
| 280   | 0.372  | 0.375                                      | 0.377  | 0.380  | 0.383  | 0.386  | 0.389  | 0.392  | 0.395  | 0.398  | 0.401  | 280                        |  |
| 290   | 0.401  | 0.404                                      | 0.406  | 0.409  | 0.412  | 0.415  | 0.418  | 0.421  | 0.424  | 0.427  | 0.431  | 290                        |  |
| 300   | 0.431  | 0.434                                      | 0.437  | 0.440  | 0.443  | 0.446  | 0.449  | 0.452  | 0.455  | 0.458  | 0.462  | 300                        |  |
| 310   | 0.462  | 0.465                                      | 0.468  | 0.471  | 0.474  | 0.477  | 0.481  | 0.484  | 0.487  | 0.490  | 0.494  | 310                        |  |
| 320   | 0.494  | 0.497                                      | 0.500  | 0.503  | 0.507  | 0.510  | 0.513  | 0.517  | 0.520  | 0.523  | 0.527  | 320                        |  |
| 330   | 0.527  | 0.530                                      | 0.533  | 0.537  | 0.540  | 0.544  | 0.547  | 0.550  | 0.554  | 0.557  | 0.561  | 330                        |  |
| 340   | 0.561  | 0.564                                      | 0.568  | 0.571  | 0.575  | 0.578  | 0.582  | 0.585  | 0.589  | 0.592  | 0.596  | 340                        |  |
| 350   | 0.596  | 0.599                                      | 0.603  | 0.606  | 0.610  | 0.614  | 0.617  | 0.621  | 0.625  | 0.628  | 0.632  | 350                        |  |
| 360   | 0.632  | 0.636                                      | 0.639  | 0.643  | 0.647  | 0.650  | 0.654  | 0.658  | 0.661  | 0.665  | 0.669  | 360                        |  |
| 370   | 0.669  | 0.673                                      | 0.677  | 0.680  | 0.684  | 0.688  | 0.692  | 0.696  | 0.699  | 0.703  | 0.707  | 370                        |  |
| 380   | 0.707  | 0.711                                      | 0.715  | 0.719  | 0.723  | 0.727  | 0.730  | 0.734  | 0.738  | 0.742  | 0.746  | 380                        |  |
| 390   | 0.746  | 0.750                                      | 0.754  | 0.758  | 0.762  | 0.766  | 0.770  | 0.774  | 0.778  | 0.782  | 0.786  | 390                        |  |
| 400   | 0.786  | 0.790                                      | 0.794  | 0.799  | 0.803  | 0.807  | 0.811  | 0.815  | 0.819  | 0.823  | 0.827  | 400                        |  |
| 410   | 0.827  | 0.832                                      | 0.836  | 0.840  | 0.844  | 0.848  | 0.853  | 0.857  | 0.861  | 0.865  | 0.870  | 410                        |  |
| 420   | 0.870  | 0.874                                      | 0.878  | 0.882  | 0.887  | 0.891  | 0.895  | 0.900  | 0.904  | 0.908  | 0.913  | 420                        |  |
| 430   | 0.913  | 0.917                                      | 0.921  | 0.926  | 0.930  | 0.935  | 0.939  | 0.943  | 0.948  | 0.952  | 0.957  | 430                        |  |
| 440   | 0.957  | 0.961                                      | 0.966  | 0.970  | 0.975  | 0.979  | 0.984  | 0.988  | 0.993  | 0.997  | 1.002  | 440                        |  |
| 450   | 1.002  | 1.006                                      | 1.011  | 1.015  | 1.020  | 1.025  | 1.029  | 1.034  | 1.039  | 1.043  | 1.048  | 450                        |  |
| 460   | 1.048  | 1.052                                      | 1.057  | 1.062  | 1.066  | 1.071  | 1.076  | 1.081  | 1.085  | 1.090  | 1.095  | 460                        |  |
| 470   | 1.095  | 1.100                                      | 1.104  | 1.109  | 1.114  | 1.119  | 1.123  | 1.128  | 1.133  | 1.138  | 1.143  | 470                        |  |
| 480   | 1.143  | 1.148                                      | 1.152  | 1.157  | 1.162  | 1.167  | 1.172  | 1.177  | 1.182  | 1.187  | 1.192  | 480                        |  |
| 490   | 1.192  | 1.197                                      | 1.202  | 1.206  | 1.211  | 1.216  | 1.221  | 1.226  | 1.231  | 1.236  | 1.241  | 490                        |  |
| 500   | 1.241  | 1.246                                      | 1.252  | 1.257  | 1.262  | 1.267  | 1.272  | 1.277  | 1.282  | 1.287  | 1.292  | 500                        |  |
| 510   | 1.292  | 1.297                                      | 1.303  | 1.308  | 1.313  | 1.318  | 1.323  | 1.328  | 1.334  | 1.339  | 1.344  | 510                        |  |
| 520   | 1.344  | 1.349                                      | 1.354  | 1.360  | 1.365  | 1.370  | 1.375  | 1.381  | 1.386  | 1.391  | 1.397  | 520                        |  |
| 530   | 1.397  | 1.402                                      | 1.407  | 1.413  | 1.418  | 1.423  | 1.429  | 1.434  | 1.439  | 1.445  | 1.450  | 530                        |  |
| 540   | 1.450  | 1.456                                      | 1.461  | 1.467  | 1.472  | 1.477  | 1.483  | 1.488  | 1.494  | 1.499  | 1.505  | 540                        |  |
| 550   | 1.505  | 1.510                                      | 1.516  | 1.521  | 1.527  | 1.532  | 1.538  | 1.544  | 1.549  | 1.555  | 1.560  | 550                        |  |
| 560   | 1.560  | 1.566                                      | 1.571  | 1.577  | 1.583  | 1.588  | 1.594  | 1.600  | 1.605  | 1.611  | 1.617  | 560                        |  |
| 570   | 1.617  | 1.622                                      | 1.628  | 1.634  | 1.639  | 1.645  | 1.651  | 1.657  | 1.662  | 1.668  | 1.674  | 570                        |  |
| 580   | 1.674  | 1.680                                      | 1.685  | 1.691  | 1.697  | 1.703  | 1.709  | 1.715  | 1.720  | 1.726  | 1.732  | 580                        |  |
| 590   | 1.732  | 1.738                                      | 1.744  | 1.750  | 1.756  | 1.762  | 1.767  | 1.773  | 1.779  | 1.785  | 1.791  | 590                        |  |
| 600   | 1.791  | 1.797                                      | 1.803  | 1.809  | 1.815  | 1.821  | 1.827  | 1.833  | 1.839  | 1.845  | 1.851  | 600                        |  |
| 610   | 1.851  | 1.857                                      | 1.863  | 1.869  | 1.875  | 1.882  | 1.888  | 1.894  | 1.900  | 1.906  | 1.912  | 610                        |  |
| 620   | 1.912  | 1.918                                      | 1.924  | 1.931  | 1.937  | 1.943  | 1.949  | 1.955  | 1.961  | 1.968  | 1.974  | 620                        |  |
| 630   | 1.974  | 1.980                                      | 1.986  | 1.993  | 1.999  | 2.005  | 2.011  | 2.018  | 2.024  | 2.030  | 2.036  | 630                        |  |
| 640   | 2.036  | 2.043                                      | 2.049  | 2.055  | 2.062  | 2.068  | 2.074  | 2.081  | 2.087  | 2.094  | 2.100  | 640                        |  |
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |

TABLE 10.3—Type B thermocouples (continued).

| EMF in Absolute Millivolts                    |       | Temperature in Degrees Celsius (IPTS 1968) |       |       |       |       |       |       |       |       |       | Reference Junctions at 0 C |  |
|---|-------|--|-------|-------|-------|-------|-------|-------|-------|-------|-------|----------------------------|--|
| DEG C   | 0     | 1  | 2     | 3     | 4     | 5     | 6     | 7     | 8     | 9     | 10    | DEG C                      |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |       |  |       |       |       |       |       |       |       |       |       |                            |  |
| 650   | 2.100 | 2.106                                      | 2.113 | 2.119 | 2.126 | 2.132 | 2.139 | 2.145 | 2.151 | 2.158 | 2.164 | 650                        |  |
| 660   | 2.164 | 2.171                                      | 2.177 | 2.184 | 2.190 | 2.197 | 2.203 | 2.210 | 2.216 | 2.223 | 2.230 | 660                        |  |
| 670   | 2.230 | 2.236                                      | 2.243 | 2.249 | 2.256 | 2.263 | 2.269 | 2.276 | 2.282 | 2.289 | 2.296 | 670                        |  |
| 680   | 2.296 | 2.302                                      | 2.309 | 2.316 | 2.322 | 2.329 | 2.336 | 2.343 | 2.349 | 2.356 | 2.363 | 680                        |  |
| 690   | 2.363 | 2.369                                      | 2.376 | 2.383 | 2.390 | 2.396 | 2.403 | 2.410 | 2.417 | 2.424 | 2.430 | 690                        |  |
| 700   | 2.430 | 2.437                                      | 2.444 | 2.451 | 2.458 | 2.465 | 2.472 | 2.478 | 2.485 | 2.492 | 2.499 | 700                        |  |
| 710   | 2.499 | 2.506                                      | 2.513 | 2.520 | 2.527 | 2.534 | 2.541 | 2.548 | 2.555 | 2.562 | 2.569 | 710                        |  |
| 720   | 2.569 | 2.576                                      | 2.583 | 2.590 | 2.597 | 2.604 | 2.611 | 2.618 | 2.625 | 2.632 | 2.639 | 720                        |  |
| 730   | 2.639 | 2.646                                      | 2.653 | 2.660 | 2.667 | 2.674 | 2.681 | 2.688 | 2.696 | 2.703 | 2.710 | 730                        |  |
| 740   | 2.710 | 2.717                                      | 2.724 | 2.732 | 2.739 | 2.746 | 2.753 | 2.760 | 2.768 | 2.775 | 2.782 | 740                        |  |
| 750   | 2.782 | 2.789                                      | 2.797 | 2.804 | 2.811 | 2.818 | 2.826 | 2.833 | 2.840 | 2.848 | 2.855 | 750                        |  |
| 760   | 2.855 | 2.862                                      | 2.869 | 2.877 | 2.884 | 2.892 | 2.899 | 2.906 | 2.914 | 2.921 | 2.928 | 760                        |  |
| 770   | 2.928 | 2.936                                      | 2.943 | 2.951 | 2.958 | 2.966 | 2.973 | 2.980 | 2.988 | 2.995 | 3.003 | 770                        |  |
| 780   | 3.003 | 3.010                                      | 3.018 | 3.025 | 3.033 | 3.040 | 3.048 | 3.055 | 3.063 | 3.070 | 3.078 | 780                        |  |
| 790   | 3.073 | 3.086                                      | 3.093 | 3.101 | 3.108 | 3.116 | 3.124 | 3.131 | 3.139 | 3.146 | 3.154 | 790                        |  |
| 800   | 3.154 | 3.162                                      | 3.169 | 3.177 | 3.185 | 3.192 | 3.200 | 3.208 | 3.215 | 3.223 | 3.231 | 800                        |  |
| 810   | 3.231 | 3.239                                      | 3.246 | 3.254 | 3.262 | 3.269 | 3.277 | 3.285 | 3.293 | 3.301 | 3.308 | 810                        |  |
| 820   | 3.308 | 3.316                                      | 3.324 | 3.332 | 3.340 | 3.347 | 3.355 | 3.363 | 3.371 | 3.379 | 3.387 | 820                        |  |
| 830   | 3.387 | 3.395                                      | 3.402 | 3.410 | 3.418 | 3.426 | 3.434 | 3.442 | 3.450 | 3.458 | 3.466 | 830                        |  |
| 840   | 3.466 | 3.474                                      | 3.482 | 3.490 | 3.498 | 3.506 | 3.514 | 3.522 | 3.530 | 3.538 | 3.546 | 840                        |  |
| 850   | 3.546 | 3.554                                      | 3.562 | 3.570 | 3.578 | 3.586 | 3.594 | 3.602 | 3.610 | 3.618 | 3.626 | 850                        |  |
| 860   | 3.626 | 3.634                                      | 3.643 | 3.651 | 3.659 | 3.667 | 3.675 | 3.683 | 3.691 | 3.700 | 3.708 | 860                        |  |
| 870   | 3.708 | 3.716                                      | 3.724 | 3.732 | 3.741 | 3.749 | 3.757 | 3.765 | 3.773 | 3.782 | 3.790 | 870                        |  |
| 880   | 3.790 | 3.798                                      | 3.806 | 3.815 | 3.823 | 3.831 | 3.840 | 3.848 | 3.856 | 3.865 | 3.873 | 880                        |  |
| 890   | 3.873 | 3.881                                      | 3.890 | 3.898 | 3.906 | 3.915 | 3.923 | 3.931 | 3.940 | 3.948 | 3.957 | 890                        |  |
| 900   | 3.957 | 3.965                                      | 3.973 | 3.982 | 3.990 | 3.999 | 4.007 | 4.016 | 4.024 | 4.032 | 4.041 | 900                        |  |
| 910   | 4.041 | 4.049                                      | 4.058 | 4.066 | 4.075 | 4.083 | 4.092 | 4.100 | 4.109 | 4.117 | 4.126 | 910                        |  |
| 920   | 4.126 | 4.135                                      | 4.143 | 4.152 | 4.160 | 4.169 | 4.177 | 4.186 | 4.195 | 4.203 | 4.212 | 920                        |  |
| 930   | 4.212 | 4.220                                      | 4.229 | 4.238 | 4.246 | 4.255 | 4.264 | 4.272 | 4.281 | 4.290 | 4.298 | 930                        |  |
| 940   | 4.298 | 4.307                                      | 4.316 | 4.325 | 4.333 | 4.342 | 4.351 | 4.359 | 4.368 | 4.377 | 4.386 | 940                        |  |
| 950   | 4.386 | 4.394                                      | 4.403 | 4.412 | 4.421 | 4.430 | 4.438 | 4.447 | 4.456 | 4.465 | 4.474 | 950                        |  |
| 960   | 4.474 | 4.483                                      | 4.491 | 4.500 | 4.509 | 4.518 | 4.527 | 4.536 | 4.545 | 4.553 | 4.562 | 960                        |  |
| 970   | 4.562 | 4.571                                      | 4.580 | 4.589 | 4.598 | 4.607 | 4.616 | 4.625 | 4.634 | 4.643 | 4.652 | 970                        |  |
| 980   | 4.652 | 4.661                                      | 4.670 | 4.679 | 4.688 | 4.697 | 4.706 | 4.715 | 4.724 | 4.733 | 4.742 | 980                        |  |
| 990   | 4.742 | 4.751                                      | 4.760 | 4.769 | 4.778 | 4.787 | 4.796 | 4.805 | 4.814 | 4.823 | 4.833 | 990                        |  |
| 1000  | 4.833 | 4.842                                      | 4.851 | 4.860 | 4.869 | 4.878 | 4.887 | 4.897 | 4.906 | 4.915 | 4.924 | 1000                       |  |
| 1010  | 4.924 | 4.933                                      | 4.942 | 4.952 | 4.961 | 4.970 | 4.979 | 4.989 | 4.998 | 5.007 | 5.016 | 1010                       |  |
| 1020  | 5.016 | 5.025                                      | 5.035 | 5.044 | 5.053 | 5.063 | 5.072 | 5.081 | 5.090 | 5.100 | 5.109 | 1020                       |  |
| 1030  | 5.109 | 5.118                                      | 5.128 | 5.137 | 5.146 | 5.156 | 5.165 | 5.174 | 5.184 | 5.193 | 5.202 | 1030                       |  |
| 1040  | 5.202 | 5.212                                      | 5.221 | 5.231 | 5.240 | 5.249 | 5.259 | 5.268 | 5.278 | 5.287 | 5.297 | 1040                       |  |
| 1050  | 5.297 | 5.306                                      | 5.316 | 5.325 | 5.334 | 5.344 | 5.353 | 5.363 | 5.372 | 5.382 | 5.391 | 1050                       |  |
| 1060  | 5.391 | 5.401                                      | 5.410 | 5.420 | 5.429 | 5.439 | 5.449 | 5.458 | 5.468 | 5.477 | 5.487 | 1060                       |  |
| 1070  | 5.487 | 5.496                                      | 5.506 | 5.516 | 5.525 | 5.535 | 5.544 | 5.554 | 5.564 | 5.573 | 5.583 | 1070                       |  |
| 1080  | 5.583 | 5.593                                      | 5.602 | 5.612 | 5.621 | 5.631 | 5.641 | 5.651 | 5.660 | 5.670 | 5.680 | 1080                       |  |
| 1090  | 5.680 | 5.689                                      | 5.699 | 5.709 | 5.718 | 5.728 | 5.738 | 5.748 | 5.757 | 5.767 | 5.777 | 1090                       |  |
| 1100  | 5.777 | 5.787                                      | 5.796 | 5.806 | 5.816 | 5.826 | 5.836 | 5.845 | 5.855 | 5.865 | 5.875 | 1100                       |  |
| 1110  | 5.875 | 5.885                                      | 5.895 | 5.904 | 5.914 | 5.924 | 5.934 | 5.944 | 5.954 | 5.964 | 5.973 | 1110                       |  |
| 1120  | 5.973 | 5.983                                      | 5.993 | 6.003 | 6.013 | 6.023 | 6.033 | 6.043 | 6.053 | 6.063 | 6.073 | 1120                       |  |
| 1130  | 6.073 | 6.083                                      | 6.093 | 6.102 | 6.112 | 6.122 | 6.132 | 6.142 | 6.152 | 6.162 | 6.172 | 1130                       |  |
| 1140  | 6.172 | 6.182                                      | 6.192 | 6.202 | 6.212 | 6.222 | 6.232 | 6.242 | 6.252 | 6.263 | 6.273 | 1140                       |  |
| 1150  | 6.273 | 6.283                                      | 6.293 | 6.303 | 6.313 | 6.323 | 6.333 | 6.343 | 6.353 | 6.364 | 6.374 | 1150                       |  |
| 1160  | 6.374 | 6.384                                      | 6.394 | 6.404 | 6.414 | 6.424 | 6.435 | 6.445 | 6.455 | 6.465 | 6.475 | 1160                       |  |
| 1170  | 6.475 | 6.485                                      | 6.496 | 6.506 | 6.516 | 6.526 | 6.536 | 6.547 | 6.557 | 6.567 | 6.577 | 1170                       |  |
| 1180  | 6.577 | 6.588                                      | 6.598 | 6.608 | 6.618 | 6.629 | 6.639 | 6.649 | 6.659 | 6.670 | 6.680 | 1180                       |  |
| 1190  | 6.680 | 6.690                                      | 6.701 | 6.711 | 6.721 | 6.732 | 6.742 | 6.752 | 6.763 | 6.773 | 6.783 | 1190                       |  |
| 1200  | 6.783 | 6.794                                      | 6.804 | 6.814 | 6.825 | 6.835 | 6.846 | 6.856 | 6.866 | 6.877 | 6.887 | 1200                       |  |
| 1210  | 6.887 | 6.898                                      | 6.908 | 6.918 | 6.929 | 6.939 | 6.950 | 6.960 | 6.971 | 6.981 | 6.991 | 1210                       |  |
| 1220  | 6.991 | 7.002                                      | 7.012 | 7.023 | 7.033 | 7.044 | 7.054 | 7.065 | 7.075 | 7.086 | 7.096 | 1220                       |  |
| 1230  | 7.096 | 7.107                                      | 7.117 | 7.128 | 7.138 | 7.149 | 7.159 | 7.170 | 7.181 | 7.191 | 7.202 | 1230                       |  |
| 1240  | 7.202 | 7.212                                      | 7.223 | 7.233 | 7.244 | 7.255 | 7.265 | 7.276 | 7.286 | 7.297 | 7.308 | 1240                       |  |
| 1250  | 7.308 | 7.318                                      | 7.329 | 7.339 | 7.350 | 7.361 | 7.371 | 7.382 | 7.393 | 7.403 | 7.414 | 1250                       |  |
| 1260  | 7.414 | 7.425                                      | 7.435 | 7.446 | 7.457 | 7.467 | 7.478 | 7.489 | 7.500 | 7.510 | 7.521 | 1260                       |  |
| 1270  | 7.521 | 7.532                                      | 7.542 | 7.553 | 7.564 | 7.575 | 7.585 | 7.596 | 7.607 | 7.618 | 7.628 | 1270                       |  |
| 1280  | 7.628 | 7.639                                      | 7.650 | 7.661 | 7.671 | 7.682 | 7.693 | 7.704 | 7.715 | 7.725 | 7.736 | 1280                       |  |
| 1290  | 7.736 | 7.747                                      | 7.758 | 7.769 | 7.780 | 7.790 | 7.801 | 7.812 | 7.823 | 7.834 | 7.845 | 1290                       |  |
| DEG C   | 0     | 1  | 2     | 3     | 4     | 5     | 6     | 7     | 8     | 9     | 10    | DEG C                      |  |

TABLE 10.3—Type B thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Celsius (IPTS 1968) |        |        |        |        |        |        |        |        |        | Reference Junctions at 0 C |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------------------------|--|
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                            |  |
| 1.300   | 7.845  | 7.855                                      | 7.866  | 7.877  | 7.888  | 7.899  | 7.910  | 7.921  | 7.932  | 7.943  | 7.953  | 1.300                      |  |
| 1.310   | 7.953  | 7.964                                      | 7.975  | 7.986  | 7.997  | 8.008  | 8.019  | 8.030  | 8.041  | 8.052  | 8.063  | 1.310                      |  |
| 1.320   | 8.063  | 8.074                                      | 8.085  | 8.096  | 8.107  | 8.118  | 8.128  | 8.139  | 8.150  | 8.161  | 8.172  | 1.320                      |  |
| 1.330   | 8.172  | 8.183                                      | 8.194  | 8.205  | 8.216  | 8.227  | 8.238  | 8.249  | 8.261  | 8.272  | 8.283  | 1.330                      |  |
| 1.340   | 8.283  | 8.294                                      | 8.305  | 8.316  | 8.327  | 8.338  | 8.349  | 8.360  | 8.371  | 8.382  | 8.393  | 1.340                      |  |
| 1.350   | 8.393  | 8.404                                      | 8.415  | 8.426  | 8.437  | 8.449  | 8.460  | 8.471  | 8.482  | 8.493  | 8.504  | 1.350                      |  |
| 1.360   | 8.504  | 8.515                                      | 8.526  | 8.538  | 8.549  | 8.560  | 8.571  | 8.582  | 8.593  | 8.604  | 8.616  | 1.360                      |  |
| 1.370   | 8.616  | 8.627                                      | 8.638  | 8.649  | 8.660  | 8.671  | 8.683  | 8.694  | 8.705  | 8.716  | 8.727  | 1.370                      |  |
| 1.380   | 8.727  | 8.738                                      | 8.750  | 8.761  | 8.772  | 8.783  | 8.795  | 8.806  | 8.817  | 8.828  | 8.839  | 1.380                      |  |
| 1.390   | 8.839  | 8.851                                      | 8.862  | 8.873  | 8.884  | 8.896  | 8.907  | 8.918  | 8.929  | 8.941  | 8.952  | 1.390                      |  |
| 1.400   | 8.952  | 8.963                                      | 8.974  | 8.986  | 8.997  | 9.008  | 9.020  | 9.031  | 9.042  | 9.053  | 9.065  | 1.400                      |  |
| 1.410   | 9.065  | 9.076                                      | 9.087  | 9.099  | 9.110  | 9.121  | 9.133  | 9.144  | 9.155  | 9.167  | 9.178  | 1.410                      |  |
| 1.420   | 9.178  | 9.189                                      | 9.201  | 9.212  | 9.223  | 9.235  | 9.246  | 9.257  | 9.269  | 9.280  | 9.291  | 1.420                      |  |
| 1.430   | 9.291  | 9.303                                      | 9.314  | 9.326  | 9.337  | 9.348  | 9.360  | 9.371  | 9.382  | 9.394  | 9.405  | 1.430                      |  |
| 1.440   | 9.405  | 9.417                                      | 9.428  | 9.439  | 9.451  | 9.462  | 9.474  | 9.485  | 9.497  | 9.508  | 9.519  | 1.440                      |  |
| 1.450   | 9.519  | 9.531                                      | 9.542  | 9.554  | 9.565  | 9.577  | 9.588  | 9.599  | 9.611  | 9.622  | 9.634  | 1.450                      |  |
| 1.460   | 9.634  | 9.645                                      | 9.657  | 9.668  | 9.680  | 9.691  | 9.703  | 9.714  | 9.726  | 9.737  | 9.748  | 1.460                      |  |
| 1.470   | 9.748  | 9.760                                      | 9.771  | 9.783  | 9.794  | 9.806  | 9.817  | 9.829  | 9.840  | 9.852  | 9.863  | 1.470                      |  |
| 1.480   | 9.863  | 9.875                                      | 9.886  | 9.898  | 9.909  | 9.921  | 9.933  | 9.944  | 9.956  | 9.967  | 9.979  | 1.480                      |  |
| 1.490   | 9.979  | 9.990                                      | 10.002 | 10.013 | 10.025 | 10.036 | 10.048 | 10.059 | 10.071 | 10.082 | 10.094 | 1.490                      |  |
| 1.500   | 10.094 | 10.106                                     | 10.117 | 10.129 | 10.140 | 10.152 | 10.163 | 10.175 | 10.187 | 10.198 | 10.210 | 1.500                      |  |
| 1.510   | 10.210 | 10.221                                     | 10.233 | 10.244 | 10.256 | 10.268 | 10.279 | 10.291 | 10.302 | 10.314 | 10.325 | 1.510                      |  |
| 1.520   | 10.325 | 10.337                                     | 10.349 | 10.360 | 10.372 | 10.383 | 10.395 | 10.407 | 10.418 | 10.430 | 10.441 | 1.520                      |  |
| 1.530   | 10.441 | 10.453                                     | 10.465 | 10.476 | 10.488 | 10.500 | 10.511 | 10.523 | 10.534 | 10.546 | 10.558 | 1.530                      |  |
| 1.540   | 10.558 | 10.569                                     | 10.581 | 10.593 | 10.604 | 10.616 | 10.627 | 10.639 | 10.651 | 10.662 | 10.674 | 1.540                      |  |
| 1.550   | 10.674 | 10.686                                     | 10.697 | 10.709 | 10.721 | 10.732 | 10.744 | 10.756 | 10.767 | 10.779 | 10.790 | 1.550                      |  |
| 1.560   | 10.790 | 10.802                                     | 10.814 | 10.825 | 10.837 | 10.849 | 10.860 | 10.872 | 10.884 | 10.895 | 10.907 | 1.560                      |  |
| 1.570   | 10.907 | 10.919                                     | 10.930 | 10.942 | 10.954 | 10.965 | 10.977 | 10.989 | 11.000 | 11.012 | 11.024 | 1.570                      |  |
| 1.580   | 11.024 | 11.035                                     | 11.047 | 11.059 | 11.070 | 11.082 | 11.094 | 11.105 | 11.117 | 11.129 | 11.141 | 1.580                      |  |
| 1.590   | 11.141 | 11.152                                     | 11.164 | 11.176 | 11.187 | 11.199 | 11.211 | 11.222 | 11.234 | 11.246 | 11.257 | 1.590                      |  |
| 1.600   | 11.257 | 11.269                                     | 11.281 | 11.292 | 11.304 | 11.316 | 11.328 | 11.339 | 11.351 | 11.363 | 11.374 | 1.600                      |  |
| 1.610   | 11.374 | 11.386                                     | 11.398 | 11.409 | 11.421 | 11.433 | 11.444 | 11.456 | 11.468 | 11.480 | 11.491 | 1.610                      |  |
| 1.620   | 11.491 | 11.503                                     | 11.515 | 11.526 | 11.538 | 11.550 | 11.561 | 11.573 | 11.585 | 11.597 | 11.608 | 1.620                      |  |
| 1.630   | 11.608 | 11.620                                     | 11.632 | 11.643 | 11.655 | 11.667 | 11.678 | 11.690 | 11.702 | 11.714 | 11.725 | 1.630                      |  |
| 1.640   | 11.725 | 11.737                                     | 11.749 | 11.760 | 11.772 | 11.784 | 11.795 | 11.807 | 11.819 | 11.830 | 11.842 | 1.640                      |  |
| 1.650   | 11.842 | 11.854                                     | 11.866 | 11.877 | 11.889 | 11.901 | 11.912 | 11.924 | 11.936 | 11.947 | 11.959 | 1.650                      |  |
| 1.660   | 11.959 | 11.971                                     | 11.983 | 11.994 | 12.006 | 12.018 | 12.029 | 12.041 | 12.053 | 12.064 | 12.076 | 1.660                      |  |
| 1.670   | 12.076 | 12.088                                     | 12.099 | 12.111 | 12.123 | 12.134 | 12.146 | 12.158 | 12.170 | 12.181 | 12.193 | 1.670                      |  |
| 1.680   | 12.193 | 12.205                                     | 12.216 | 12.228 | 12.240 | 12.251 | 12.263 | 12.275 | 12.286 | 12.298 | 12.310 | 1.680                      |  |
| 1.690   | 12.310 | 12.321                                     | 12.333 | 12.345 | 12.356 | 12.368 | 12.380 | 12.391 | 12.403 | 12.415 | 12.426 | 1.690                      |  |
| 1.700   | 12.426 | 12.438                                     | 12.450 | 12.461 | 12.473 | 12.485 | 12.496 | 12.508 | 12.520 | 12.531 | 12.543 | 1.700                      |  |
| 1.710   | 12.543 | 12.555                                     | 12.566 | 12.578 | 12.590 | 12.601 | 12.613 | 12.624 | 12.636 | 12.648 | 12.659 | 1.710                      |  |
| 1.720   | 12.659 | 12.671                                     | 12.683 | 12.694 | 12.706 | 12.718 | 12.729 | 12.741 | 12.752 | 12.764 | 12.776 | 1.720                      |  |
| 1.730   | 12.776 | 12.787                                     | 12.799 | 12.811 | 12.822 | 12.834 | 12.845 | 12.857 | 12.869 | 12.880 | 12.892 | 1.730                      |  |
| 1.740   | 12.892 | 12.903                                     | 12.915 | 12.927 | 12.938 | 12.950 | 12.961 | 12.973 | 12.985 | 12.996 | 13.008 | 1.740                      |  |
| 1.750   | 13.008 | 13.019                                     | 13.031 | 13.043 | 13.054 | 13.066 | 13.077 | 13.089 | 13.100 | 13.112 | 13.124 | 1.750                      |  |
| 1.760   | 13.124 | 13.135                                     | 13.147 | 13.158 | 13.170 | 13.181 | 13.193 | 13.204 | 13.216 | 13.228 | 13.239 | 1.760                      |  |
| 1.770   | 13.239 | 13.251                                     | 13.262 | 13.274 | 13.285 | 13.297 | 13.308 | 13.320 | 13.331 | 13.343 | 13.354 | 1.770                      |  |
| 1.780   | 13.354 | 13.366                                     | 13.378 | 13.389 | 13.401 | 13.412 | 13.424 | 13.435 | 13.447 | 13.458 | 13.470 | 1.780                      |  |
| 1.790   | 13.470 | 13.481                                     | 13.493 | 13.504 | 13.516 | 13.527 | 13.539 | 13.550 | 13.562 | 13.573 | 13.585 | 1.790                      |  |
| 1.800   | 13.585 | 13.596                                     | 13.607 | 13.619 | 13.630 | 13.642 | 13.653 | 13.665 | 13.676 | 13.688 | 13.699 | 1.800                      |  |
| 1.810   | 13.699 | 13.711                                     | 13.722 | 13.733 | 13.745 | 13.756 | 13.768 | 13.779 | 13.791 | 13.802 | 13.814 | 1.810                      |  |
| 1.820   | 13.814 |  |        |        |        |        |        |        |        |        |        | 1.820                      |  |
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |



174 THE USE OF THERMOCOUPLES IN TEMPERATURE MEASUREMENT

TABLE 10.4—Type E thermocouples (deg F-millivolts).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit <sup>a</sup> |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
| DEG F   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                             |  |
| -450  | -9.830 | -9.832   | -9.833 | -9.834 | -9.835 |        |        |        |        |        |        | -450                        |  |
| -440  | -9.809 | -9.812   | -9.814 | -9.817 | -9.819 | -9.821 | -9.823 | -9.825 | -9.827 | -9.829 | -9.830 | -440                        |  |
| -430  | -9.775 | -9.779   | -9.783 | -9.786 | -9.790 | -9.793 | -9.797 | -9.800 | -9.803 | -9.806 | -9.809 | -430                        |  |
| -420  | -9.729 | -9.734   | -9.739 | -9.744 | -9.749 | -9.753 | -9.758 | -9.762 | -9.767 | -9.771 | -9.775 | -420                        |  |
| -410  | -9.672 | -9.678   | -9.684 | -9.690 | -9.696 | -9.702 | -9.708 | -9.713 | -9.719 | -9.724 | -9.729 | -410                        |  |
| -400  | -9.604 | -9.611   | -9.619 | -9.626 | -9.633 | -9.639 | -9.646 | -9.653 | -9.659 | -9.666 | -9.672 | -400                        |  |
| -390  | -9.526 | -9.534   | -9.542 | -9.550 | -9.558 | -9.566 | -9.574 | -9.582 | -9.589 | -9.597 | -9.604 | -390                        |  |
| -380  | -9.437 | -9.446   | -9.455 | -9.464 | -9.473 | -9.482 | -9.491 | -9.500 | -9.509 | -9.517 | -9.526 | -380                        |  |
| -370  | -9.338 | -9.348   | -9.358 | -9.368 | -9.378 | -9.388 | -9.398 | -9.408 | -9.418 | -9.427 | -9.437 | -370                        |  |
| -360  | -9.229 | -9.241   | -9.252 | -9.263 | -9.274 | -9.285 | -9.296 | -9.306 | -9.317 | -9.327 | -9.338 | -360                        |  |
| -350  | -9.112 | -9.124   | -9.136 | -9.148 | -9.160 | -9.172 | -9.184 | -9.195 | -9.207 | -9.218 | -9.229 | -350                        |  |
| -340  | -8.986 | -8.999   | -9.012 | -9.025 | -9.038 | -9.050 | -9.063 | -9.075 | -9.088 | -9.100 | -9.112 | -340                        |  |
| -330  | -8.852 | -8.866   | -8.880 | -8.893 | -8.907 | -8.920 | -8.934 | -8.947 | -8.960 | -8.973 | -8.986 | -330                        |  |
| -320  | -8.710 | -8.725   | -8.739 | -8.754 | -8.768 | -8.782 | -8.796 | -8.810 | -8.824 | -8.838 | -8.852 | -320                        |  |
| -310  | -8.561 | -8.576   | -8.591 | -8.606 | -8.621 | -8.636 | -8.651 | -8.666 | -8.681 | -8.696 | -8.710 | -310                        |  |
| -300  | -8.404 | -8.420   | -8.436 | -8.452 | -8.468 | -8.483 | -8.499 | -8.514 | -8.530 | -8.545 | -8.561 | -300                        |  |
| -290  | -8.240 | -8.257   | -8.273 | -8.290 | -8.306 | -8.323 | -8.339 | -8.355 | -8.372 | -8.388 | -8.404 | -290                        |  |
| -280  | -8.069 | -8.086   | -8.104 | -8.121 | -8.138 | -8.155 | -8.172 | -8.189 | -8.206 | -8.223 | -8.240 | -280                        |  |
| -270  | -7.891 | -7.909   | -7.927 | -7.945 | -7.963 | -7.981 | -7.999 | -8.016 | -8.034 | -8.051 | -8.069 | -270                        |  |
| -260  | -7.707 | -7.726   | -7.744 | -7.763 | -7.781 | -7.800 | -7.818 | -7.837 | -7.855 | -7.873 | -7.891 | -260                        |  |
| -250  | -7.516 | -7.535   | -7.555 | -7.574 | -7.593 | -7.612 | -7.631 | -7.650 | -7.669 | -7.688 | -7.707 | -250                        |  |
| -240  | -7.319 | -7.339   | -7.359 | -7.379 | -7.399 | -7.418 | -7.438 | -7.458 | -7.477 | -7.497 | -7.516 | -240                        |  |
| -230  | -7.116 | -7.137   | -7.157 | -7.178 | -7.198 | -7.218 | -7.239 | -7.259 | -7.279 | -7.299 | -7.319 | -230                        |  |
| -220  | -6.907 | -6.928   | -6.949 | -6.970 | -6.991 | -7.012 | -7.033 | -7.054 | -7.075 | -7.095 | -7.116 | -220                        |  |
| -210  | -6.692 | -6.714   | -6.735 | -6.757 | -6.779 | -6.800 | -6.822 | -6.843 | -6.864 | -6.886 | -6.907 | -210                        |  |
| -200  | -6.471 | -6.494   | -6.516 | -6.538 | -6.560 | -6.582 | -6.604 | -6.626 | -6.648 | -6.670 | -6.692 | -200                        |  |
| -190  | -6.245 | -6.268   | -6.291 | -6.314 | -6.336 | -6.359 | -6.382 | -6.404 | -6.427 | -6.449 | -6.471 | -190                        |  |
| -180  | -6.013 | -6.037   | -6.060 | -6.084 | -6.107 | -6.130 | -6.153 | -6.176 | -6.199 | -6.222 | -6.245 | -180                        |  |
| -170  | -5.776 | -5.800   | -5.824 | -5.848 | -5.872 | -5.896 | -5.919 | -5.943 | -5.967 | -5.990 | -6.013 | -170                        |  |
| -160  | -5.534 | -5.559   | -5.583 | -5.607 | -5.632 | -5.656 | -5.680 | -5.704 | -5.728 | -5.752 | -5.776 | -160                        |  |
| -150  | -5.287 | -5.312   | -5.337 | -5.362 | -5.386 | -5.411 | -5.436 | -5.460 | -5.485 | -5.510 | -5.534 | -150                        |  |
| -140  | -5.034 | -5.060   | -5.085 | -5.111 | -5.136 | -5.161 | -5.186 | -5.212 | -5.237 | -5.262 | -5.287 | -140                        |  |
| -130  | -4.777 | -4.803   | -4.829 | -4.855 | -4.880 | -4.906 | -4.932 | -4.958 | -4.983 | -5.009 | -5.034 | -130                        |  |
| -120  | -4.515 | -4.541   | -4.567 | -4.594 | -4.620 | -4.646 | -4.672 | -4.699 | -4.725 | -4.751 | -4.777 | -120                        |  |
| -110 <sup>A</sup>                             | -4.248 | -4.274   | -4.301 | -4.328 | -4.355 | -4.382 | -4.408 | -4.435 | -4.462 | -4.488 | -4.515 | -110                        |  |
| -100  | -3.976 | -4.003   | -4.031 | -4.058 | -4.085 | -4.112 | -4.139 | -4.167 | -4.194 | -4.221 | -4.248 | -100                        |  |
| -90   | -3.700 | -3.728   | -3.755 | -3.783 | -3.811 | -3.838 | -3.866 | -3.894 | -3.921 | -3.949 | -3.976 | -90                         |  |
| -80   | -3.419 | -3.447   | -3.476 | -3.504 | -3.532 | -3.560 | -3.588 | -3.616 | -3.644 | -3.672 | -3.700 | -80                         |  |
| -70   | -3.134 | -3.163   | -3.192 | -3.220 | -3.249 | -3.277 | -3.306 | -3.334 | -3.363 | -3.391 | -3.419 | -70                         |  |
| -60   | -2.845 | -2.874   | -2.903 | -2.932 | -2.961 | -2.990 | -3.019 | -3.048 | -3.077 | -3.106 | -3.134 | -60                         |  |
| -50   | -2.552 | -2.581   | -2.611 | -2.640 | -2.670 | -2.699 | -2.728 | -2.758 | -2.787 | -2.816 | -2.845 | -50                         |  |
| -40   | -2.254 | -2.284   | -2.314 | -2.344 | -2.374 | -2.404 | -2.433 | -2.463 | -2.493 | -2.522 | -2.552 | -40                         |  |
| -30   | -1.953 | -1.983   | -2.014 | -2.044 | -2.074 | -2.104 | -2.134 | -2.164 | -2.194 | -2.224 | -2.254 | -30                         |  |
| -20   | -1.648 | -1.678   | -1.709 | -1.740 | -1.770 | -1.801 | -1.831 | -1.862 | -1.892 | -1.923 | -1.953 | -20                         |  |
| -10   | -1.339 | -1.370   | -1.401 | -1.432 | -1.463 | -1.494 | -1.525 | -1.555 | -1.586 | -1.617 | -1.648 | -10                         |  |
| 0   | -1.026 | -1.057   | -1.089 | -1.120 | -1.151 | -1.183 | -1.214 | -1.245 | -1.276 | -1.308 | -1.339 | 0                           |  |
| 0   | -1.026 | -0.994   | -0.963 | -0.931 | -0.900 | -0.868 | -0.836 | -0.805 | -0.773 | -0.741 | -0.709 | 0                           |  |
| 10  | -0.709 | -0.677   | -0.645 | -0.613 | -0.581 | -0.549 | -0.517 | -0.485 | -0.453 | -0.421 | -0.389 | 10                          |  |
| 20  | -0.389 | -0.357   | -0.324 | -0.292 | -0.260 | -0.227 | -0.195 | -0.163 | -0.130 | -0.098 | -0.065 | 20                          |  |
| 30  | -0.065 | -0.033   | 0.000  | 0.033  | 0.065  | 0.098  | 0.131  | 0.163  | 0.196  | 0.229  | 0.262  | 30                          |  |
| 40  | 0.262  | 0.293  | 0.327  | 0.360  | 0.393  | 0.426  | 0.459  | 0.492  | 0.525  | 0.558  | 0.591  | 40                          |  |
| 50  | 0.591  | 0.624  | 0.658  | 0.691  | 0.724  | 0.757  | 0.790  | 0.824  | 0.857  | 0.890  | 0.924  | 50                          |  |
| 60  | 0.924  | 0.957  | 0.990  | 1.024  | 1.057  | 1.091  | 1.124  | 1.158  | 1.192  | 1.225  | 1.259  | 60                          |  |
| 70  | 1.259  | 1.292  | 1.326  | 1.360  | 1.394  | 1.427  | 1.461  | 1.495  | 1.529  | 1.563  | 1.597  | 70                          |  |
| 80  | 1.597  | 1.631  | 1.665  | 1.699  | 1.733  | 1.767  | 1.801  | 1.835  | 1.869  | 1.903  | 1.937  | 80                          |  |
| 90  | 1.937  | 1.972  | 2.006  | 2.040  | 2.075  | 2.109  | 2.143  | 2.178  | 2.212  | 2.247  | 2.281  | 90                          |  |
| 100   | 2.281  | 2.316  | 2.350  | 2.385  | 2.419  | 2.454  | 2.489  | 2.523  | 2.558  | 2.593  | 2.627  | 100                         |  |
| 110   | 2.627  | 2.662  | 2.697  | 2.732  | 2.767  | 2.802  | 2.837  | 2.872  | 2.907  | 2.942  | 2.977  | 110                         |  |
| 120   | 2.977  | 3.012  | 3.047  | 3.082  | 3.117  | 3.152  | 3.187  | 3.222  | 3.258  | 3.293  | 3.329  | 120                         |  |
| 130   | 3.329  | 3.364  | 3.399  | 3.435  | 3.470  | 3.506  | 3.541  | 3.577  | 3.612  | 3.648  | 3.683  | 130                         |  |
| 140   | 3.683  | 3.719  | 3.755  | 3.790  | 3.826  | 3.862  | 3.898  | 3.933  | 3.969  | 4.005  | 4.041  | 140                         |  |

<sup>a</sup> Converted from degrees Celsius (IPTS 1968)

TABLE 10.4—Type E thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit* |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|------------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
| DEG F   | 0      | 1                                  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |                                    |        |        |        |        |        |        |        |        |        |                             |  |
| 150   | 4.041  | 4.077                              | 4.113  | 4.149  | 4.185  | 4.221  | 4.257  | 4.293  | 4.329  | 4.365  | 4.401  | 150                         |  |
| 160   | 4.401  | 4.437                              | 4.474  | 4.510  | 4.546  | 4.582  | 4.619  | 4.655  | 4.691  | 4.728  | 4.764  | 160                         |  |
| 170   | 4.764  | 4.801                              | 4.837  | 4.874  | 4.910  | 4.947  | 4.983  | 5.020  | 5.056  | 5.093  | 5.130  | 170                         |  |
| 180   | 5.130  | 5.166                              | 5.203  | 5.240  | 5.277  | 5.314  | 5.350  | 5.387  | 5.424  | 5.461  | 5.498  | 180                         |  |
| 190   | 5.498  | 5.535                              | 5.572  | 5.609  | 5.646  | 5.683  | 5.720  | 5.757  | 5.794  | 5.832  | 5.869  | 190                         |  |
| 200   | 5.869  | 5.906                              | 5.943  | 5.981  | 6.018  | 6.055  | 6.092  | 6.130  | 6.167  | 6.205  | 6.242  | 200                         |  |
| 210   | 6.242  | 6.280                              | 6.317  | 6.355  | 6.392  | 6.430  | 6.467  | 6.505  | 6.543  | 6.580  | 6.618  | 210                         |  |
| 220   | 6.618  | 6.656                              | 6.693  | 6.731  | 6.769  | 6.807  | 6.845  | 6.882  | 6.920  | 6.958  | 6.996  | 220                         |  |
| 230   | 6.996  | 7.034                              | 7.072  | 7.110  | 7.148  | 7.186  | 7.224  | 7.262  | 7.300  | 7.339  | 7.377  | 230                         |  |
| 240   | 7.377  | 7.415                              | 7.453  | 7.491  | 7.530  | 7.568  | 7.606  | 7.645  | 7.683  | 7.721  | 7.760  | 240                         |  |
| 250   | 7.760  | 7.798                              | 7.837  | 7.875  | 7.914  | 7.952  | 7.991  | 8.029  | 8.068  | 8.106  | 8.145  | 250                         |  |
| 260   | 8.145  | 8.184                              | 8.222  | 8.261  | 8.300  | 8.338  | 8.377  | 8.416  | 8.455  | 8.494  | 8.532  | 260                         |  |
| 270   | 8.532  | 8.571                              | 8.610  | 8.649  | 8.688  | 8.727  | 8.766  | 8.805  | 8.844  | 8.883  | 8.922  | 270                         |  |
| 280   | 8.922  | 8.961                              | 9.000  | 9.039  | 9.078  | 9.118  | 9.157  | 9.196  | 9.235  | 9.274  | 9.314  | 280                         |  |
| 290   | 9.314  | 9.353                              | 9.392  | 9.432  | 9.471  | 9.510  | 9.550  | 9.589  | 9.629  | 9.668  | 9.708  | 290                         |  |
| 300   | 9.708  | 9.747                              | 9.787  | 9.826  | 9.866  | 9.905  | 9.945  | 9.984  | 10.024 | 10.064 | 10.103 | 300                         |  |
| 310   | 10.103 | 10.143                             | 10.183 | 10.223 | 10.262 | 10.302 | 10.342 | 10.382 | 10.421 | 10.461 | 10.501 | 310                         |  |
| 320   | 10.501 | 10.541                             | 10.581 | 10.621 | 10.661 | 10.701 | 10.741 | 10.781 | 10.821 | 10.861 | 10.901 | 320                         |  |
| 330   | 10.901 | 10.941                             | 10.981 | 11.021 | 11.061 | 11.101 | 11.142 | 11.182 | 11.222 | 11.262 | 11.302 | 330                         |  |
| 340   | 11.302 | 11.343                             | 11.383 | 11.423 | 11.464 | 11.504 | 11.544 | 11.585 | 11.625 | 11.665 | 11.706 | 340                         |  |
| 350   | 11.706 | 11.746                             | 11.787 | 11.827 | 11.868 | 11.908 | 11.949 | 11.989 | 12.030 | 12.070 | 12.111 | 350                         |  |
| 360   | 12.111 | 12.152                             | 12.192 | 12.233 | 12.273 | 12.314 | 12.355 | 12.396 | 12.436 | 12.477 | 12.518 | 360                         |  |
| 370   | 12.518 | 12.559                             | 12.599 | 12.640 | 12.681 | 12.722 | 12.763 | 12.804 | 12.844 | 12.885 | 12.926 | 370                         |  |
| 380   | 12.926 | 12.967                             | 13.008 | 13.049 | 13.090 | 13.131 | 13.172 | 13.213 | 13.254 | 13.295 | 13.336 | 380                         |  |
| 390   | 13.336 | 13.378                             | 13.419 | 13.460 | 13.501 | 13.542 | 13.583 | 13.624 | 13.666 | 13.707 | 13.748 | 390                         |  |
| 400   | 13.748 | 13.789                             | 13.831 | 13.872 | 13.913 | 13.955 | 13.996 | 14.037 | 14.079 | 14.120 | 14.161 | 400                         |  |
| 410   | 14.161 | 14.203                             | 14.244 | 14.286 | 14.327 | 14.368 | 14.410 | 14.451 | 14.493 | 14.534 | 14.576 | 410                         |  |
| 420   | 14.576 | 14.618                             | 14.659 | 14.701 | 14.742 | 14.784 | 14.826 | 14.867 | 14.909 | 14.950 | 14.992 | 420                         |  |
| 430   | 14.992 | 15.034                             | 15.076 | 15.117 | 15.159 | 15.201 | 15.243 | 15.284 | 15.326 | 15.368 | 15.410 | 430                         |  |
| 440   | 15.410 | 15.451                             | 15.493 | 15.535 | 15.577 | 15.619 | 15.661 | 15.703 | 15.745 | 15.787 | 15.829 | 440                         |  |
| 450   | 15.829 | 15.871                             | 15.912 | 15.954 | 15.996 | 16.038 | 16.080 | 16.123 | 16.165 | 16.207 | 16.249 | 450                         |  |
| 460   | 16.249 | 16.291                             | 16.333 | 16.375 | 16.417 | 16.459 | 16.501 | 16.544 | 16.586 | 16.628 | 16.670 | 460                         |  |
| 470   | 16.670 | 16.712                             | 16.755 | 16.797 | 16.839 | 16.881 | 16.924 | 16.966 | 17.008 | 17.051 | 17.093 | 470                         |  |
| 480   | 17.093 | 17.135                             | 17.178 | 17.220 | 17.262 | 17.305 | 17.347 | 17.389 | 17.432 | 17.474 | 17.517 | 480                         |  |
| 490   | 17.517 | 17.559                             | 17.602 | 17.644 | 17.687 | 17.729 | 17.772 | 17.814 | 17.857 | 17.899 | 17.942 | 490                         |  |
| 500   | 17.942 | 17.984                             | 18.027 | 18.070 | 18.112 | 18.155 | 18.197 | 18.240 | 18.283 | 18.325 | 18.368 | 500                         |  |
| 510   | 18.368 | 18.411                             | 18.453 | 18.496 | 18.539 | 18.581 | 18.624 | 18.667 | 18.710 | 18.752 | 18.795 | 510                         |  |
| 520   | 18.795 | 18.838                             | 18.881 | 18.924 | 18.966 | 19.009 | 19.052 | 19.095 | 19.138 | 19.181 | 19.223 | 520                         |  |
| 530   | 19.223 | 19.266                             | 19.309 | 19.352 | 19.395 | 19.438 | 19.481 | 19.524 | 19.567 | 19.610 | 19.653 | 530                         |  |
| 540   | 19.653 | 19.696                             | 19.739 | 19.782 | 19.825 | 19.868 | 19.911 | 19.954 | 19.997 | 20.040 | 20.083 | 540                         |  |
| 550   | 20.083 | 20.126                             | 20.169 | 20.212 | 20.256 | 20.299 | 20.342 | 20.385 | 20.428 | 20.471 | 20.514 | 550                         |  |
| 560   | 20.514 | 20.558                             | 20.601 | 20.644 | 20.687 | 20.730 | 20.774 | 20.817 | 20.860 | 20.903 | 20.947 | 560                         |  |
| 570   | 20.947 | 20.990                             | 21.033 | 21.076 | 21.120 | 21.163 | 21.206 | 21.250 | 21.293 | 21.336 | 21.380 | 570                         |  |
| 580   | 21.380 | 21.423                             | 21.466 | 21.510 | 21.553 | 21.597 | 21.640 | 21.683 | 21.727 | 21.770 | 21.814 | 580                         |  |
| 590   | 21.814 | 21.857                             | 21.901 | 21.944 | 21.987 | 22.031 | 22.074 | 22.118 | 22.161 | 22.205 | 22.248 | 590                         |  |
| 600   | 22.248 | 22.292                             | 22.336 | 22.379 | 22.423 | 22.466 | 22.510 | 22.553 | 22.597 | 22.640 | 22.684 | 600                         |  |
| 610   | 22.684 | 22.728                             | 22.771 | 22.815 | 22.859 | 22.902 | 22.946 | 22.989 | 23.033 | 23.077 | 23.120 | 610                         |  |
| 620   | 23.120 | 23.164                             | 23.208 | 23.252 | 23.295 | 23.339 | 23.383 | 23.426 | 23.470 | 23.514 | 23.558 | 620                         |  |
| 630   | 23.558 | 23.601                             | 23.645 | 23.689 | 23.733 | 23.777 | 23.820 | 23.864 | 23.908 | 23.952 | 23.996 | 630                         |  |
| 640   | 23.996 | 24.039                             | 24.083 | 24.127 | 24.171 | 24.215 | 24.259 | 24.302 | 24.346 | 24.390 | 24.434 | 640                         |  |
| 650   | 24.434 | 24.478                             | 24.522 | 24.566 | 24.610 | 24.654 | 24.698 | 24.742 | 24.786 | 24.829 | 24.873 | 650                         |  |
| 660   | 24.873 | 24.917                             | 24.961 | 25.005 | 25.049 | 25.093 | 25.137 | 25.181 | 25.225 | 25.269 | 25.313 | 660                         |  |
| 670   | 25.313 | 25.357                             | 25.401 | 25.445 | 25.490 | 25.534 | 25.578 | 25.622 | 25.666 | 25.710 | 25.754 | 670                         |  |
| 680   | 25.754 | 25.798                             | 25.842 | 25.886 | 25.930 | 25.974 | 26.019 | 26.063 | 26.107 | 26.151 | 26.195 | 680                         |  |
| 690   | 26.195 | 26.239                             | 26.283 | 26.328 | 26.372 | 26.416 | 26.460 | 26.504 | 26.549 | 26.593 | 26.637 | 690                         |  |
| 700   | 26.637 | 26.681                             | 26.725 | 26.770 | 26.814 | 26.858 | 26.902 | 26.947 | 26.991 | 27.035 | 27.079 | 700                         |  |
| 710   | 27.079 | 27.124                             | 27.168 | 27.212 | 27.256 | 27.301 | 27.345 | 27.389 | 27.434 | 27.478 | 27.522 | 710                         |  |
| 720   | 27.522 | 27.566                             | 27.611 | 27.655 | 27.699 | 27.744 | 27.788 | 27.832 | 27.877 | 27.921 | 27.966 | 720                         |  |
| 730   | 27.966 | 28.010                             | 28.054 | 28.099 | 28.143 | 28.187 | 28.232 | 28.276 | 28.321 | 28.365 | 28.409 | 730                         |  |
| 740   | 28.409 | 28.454                             | 28.498 | 28.543 | 28.587 | 28.632 | 28.676 | 28.720 | 28.765 | 28.809 | 28.854 | 740                         |  |
| 750   | 28.854 | 28.898                             | 28.943 | 28.987 | 29.032 | 29.076 | 29.121 | 29.165 | 29.210 | 29.254 | 29.299 | 750                         |  |
| 760   | 29.299 | 29.343                             | 29.388 | 29.432 | 29.477 | 29.521 | 29.566 | 29.610 | 29.655 | 29.699 | 29.744 | 760                         |  |
| 770   | 29.744 | 29.788                             | 29.833 | 29.878 | 29.922 | 29.967 | 30.011 | 30.056 | 30.100 | 30.145 | 30.190 | 770                         |  |
| 780   | 30.190 | 30.234                             | 30.279 | 30.323 | 30.368 | 30.412 | 30.457 | 30.502 | 30.546 | 30.591 | 30.636 | 780                         |  |
| 790   | 30.636 | 30.680                             | 30.725 | 30.769 | 30.814 | 30.859 | 30.903 | 30.948 | 30.993 | 31.037 | 31.082 | 790                         |  |

\* Converted from degrees Celsius (IPTS 1968)

TABLE 10.4—Type E thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit* |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|------------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
| DEG F   | 0      | 1                                  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |                                    |        |        |        |        |        |        |        |        |        |                             |  |
| 800   | 31.082 | 31.127                             | 31.171 | 31.216 | 31.261 | 31.305 | 31.350 | 31.395 | 31.439 | 31.484 | 31.529 | 800                         |  |
| 810   | 31.529 | 31.573                             | 31.618 | 31.663 | 31.707 | 31.752 | 31.797 | 31.842 | 31.886 | 31.931 | 31.976 | 810                         |  |
| 820   | 31.976 | 32.020                             | 32.065 | 32.110 | 32.155 | 32.199 | 32.244 | 32.289 | 32.334 | 32.378 | 32.423 | 820                         |  |
| 830   | 32.423 | 32.468                             | 32.513 | 32.557 | 32.602 | 32.647 | 32.692 | 32.736 | 32.781 | 32.826 | 32.871 | 830                         |  |
| 840   | 32.871 | 32.916                             | 32.960 | 33.005 | 33.050 | 33.095 | 33.140 | 33.184 | 33.229 | 33.274 | 33.319 | 840                         |  |
| 850   | 33.319 | 33.364                             | 33.408 | 33.453 | 33.498 | 33.543 | 33.588 | 33.632 | 33.677 | 33.722 | 33.767 | 850                         |  |
| 860   | 33.767 | 33.812                             | 33.857 | 33.901 | 33.946 | 33.991 | 34.036 | 34.081 | 34.126 | 34.171 | 34.215 | 860                         |  |
| 870   | 34.215 | 34.260                             | 34.305 | 34.350 | 34.395 | 34.440 | 34.484 | 34.529 | 34.574 | 34.619 | 34.664 | 870                         |  |
| 880   | 34.664 | 34.709                             | 34.754 | 34.798 | 34.843 | 34.888 | 34.933 | 34.978 | 35.023 | 35.068 | 35.113 | 880                         |  |
| 890   | 35.113 | 35.157                             | 35.202 | 35.247 | 35.292 | 35.337 | 35.382 | 35.427 | 35.472 | 35.517 | 35.562 | 890                         |  |
| 900   | 35.562 | 35.606                             | 35.651 | 35.696 | 35.741 | 35.786 | 35.831 | 35.876 | 35.921 | 35.966 | 36.011 | 900                         |  |
| 910   | 36.011 | 36.056                             | 36.100 | 36.145 | 36.190 | 36.235 | 36.280 | 36.325 | 36.370 | 36.415 | 36.460 | 910                         |  |
| 920   | 36.460 | 36.505                             | 36.550 | 36.595 | 36.640 | 36.684 | 36.729 | 36.774 | 36.819 | 36.864 | 36.909 | 920                         |  |
| 930   | 36.909 | 36.954                             | 36.999 | 37.044 | 37.089 | 37.134 | 37.179 | 37.224 | 37.269 | 37.314 | 37.359 | 930                         |  |
| 940   | 37.358 | 37.403                             | 37.448 | 37.493 | 37.538 | 37.583 | 37.628 | 37.673 | 37.718 | 37.763 | 37.808 | 940                         |  |
| 950   | 37.808 | 37.853                             | 37.898 | 37.943 | 37.988 | 38.033 | 38.078 | 38.123 | 38.168 | 38.213 | 38.257 | 950                         |  |
| 960   | 38.257 | 38.302                             | 38.347 | 38.392 | 38.437 | 38.482 | 38.527 | 38.572 | 38.617 | 38.662 | 38.707 | 960                         |  |
| 970   | 38.707 | 38.752                             | 38.797 | 38.842 | 38.887 | 38.932 | 38.977 | 39.022 | 39.067 | 39.112 | 39.157 | 970                         |  |
| 980   | 39.157 | 39.202                             | 39.247 | 39.292 | 39.336 | 39.381 | 39.426 | 39.471 | 39.516 | 39.561 | 39.606 | 980                         |  |
| 990   | 39.606 | 39.651                             | 39.696 | 39.741 | 39.786 | 39.831 | 39.876 | 39.921 | 39.966 | 40.011 | 40.056 | 990                         |  |
| 1000  | 40.056 | 40.101                             | 40.146 | 40.191 | 40.236 | 40.280 | 40.325 | 40.370 | 40.415 | 40.460 | 40.505 | 1000                        |  |
| 1010  | 40.505 | 40.550                             | 40.595 | 40.640 | 40.685 | 40.730 | 40.775 | 40.820 | 40.865 | 40.910 | 40.955 | 1010                        |  |
| 1020  | 40.955 | 41.000                             | 41.045 | 41.090 | 41.134 | 41.179 | 41.224 | 41.269 | 41.314 | 41.359 | 41.404 | 1020                        |  |
| 1030  | 41.404 | 41.449                             | 41.494 | 41.539 | 41.584 | 41.629 | 41.674 | 41.719 | 41.764 | 41.809 | 41.853 | 1030                        |  |
| 1040  | 41.853 | 41.898                             | 41.943 | 41.988 | 42.033 | 42.078 | 42.123 | 42.168 | 42.213 | 42.258 | 42.303 | 1040                        |  |
| 1050  | 42.303 | 42.348                             | 42.392 | 42.437 | 42.482 | 42.527 | 42.572 | 42.617 | 42.662 | 42.707 | 42.752 | 1050                        |  |
| 1060  | 42.752 | 42.797                             | 42.842 | 42.887 | 42.931 | 42.976 | 43.021 | 43.066 | 43.111 | 43.156 | 43.201 | 1060                        |  |
| 1070  | 43.201 | 43.246                             | 43.290 | 43.335 | 43.380 | 43.425 | 43.470 | 43.515 | 43.560 | 43.605 | 43.650 | 1070                        |  |
| 1080  | 43.650 | 43.694                             | 43.739 | 43.784 | 43.829 | 43.874 | 43.919 | 43.964 | 44.009 | 44.053 | 44.098 | 1080                        |  |
| 1090  | 44.098 | 44.143                             | 44.188 | 44.233 | 44.278 | 44.323 | 44.367 | 44.412 | 44.457 | 44.502 | 44.547 | 1090                        |  |
| 1100  | 44.547 | 44.592                             | 44.636 | 44.681 | 44.726 | 44.771 | 44.816 | 44.861 | 44.905 | 44.950 | 44.995 | 1100                        |  |
| 1110  | 44.995 | 45.040                             | 45.085 | 45.130 | 45.174 | 45.219 | 45.264 | 45.309 | 45.354 | 45.399 | 45.443 | 1110                        |  |
| 1120  | 45.443 | 45.488                             | 45.533 | 45.578 | 45.622 | 45.667 | 45.712 | 45.757 | 45.802 | 45.846 | 45.891 | 1120                        |  |
| 1130  | 45.891 | 45.936                             | 45.981 | 46.025 | 46.070 | 46.115 | 46.160 | 46.205 | 46.249 | 46.294 | 46.339 | 1130                        |  |
| 1140  | 46.339 | 46.384                             | 46.428 | 46.473 | 46.518 | 46.563 | 46.607 | 46.652 | 46.697 | 46.742 | 46.786 | 1140                        |  |
| 1150  | 46.786 | 46.831                             | 46.876 | 46.921 | 46.965 | 47.010 | 47.055 | 47.099 | 47.144 | 47.189 | 47.234 | 1150                        |  |
| 1160  | 47.234 | 47.279                             | 47.323 | 47.368 | 47.413 | 47.457 | 47.502 | 47.547 | 47.592 | 47.636 | 47.681 | 1160                        |  |
| 1170  | 47.681 | 47.725                             | 47.770 | 47.815 | 47.859 | 47.904 | 47.949 | 47.993 | 48.038 | 48.083 | 48.127 | 1170                        |  |
| 1180  | 48.127 | 48.172                             | 48.217 | 48.261 | 48.306 | 48.351 | 48.395 | 48.440 | 48.484 | 48.529 | 48.574 | 1180                        |  |
| 1190  | 48.574 | 48.618                             | 48.663 | 48.708 | 48.752 | 48.797 | 48.842 | 48.886 | 48.931 | 48.975 | 49.020 | 1190                        |  |
| 1200  | 49.020 | 49.065                             | 49.109 | 49.154 | 49.198 | 49.243 | 49.288 | 49.332 | 49.377 | 49.421 | 49.466 | 1200                        |  |
| 1210  | 49.466 | 49.510                             | 49.555 | 49.600 | 49.644 | 49.689 | 49.733 | 49.778 | 49.822 | 49.867 | 49.911 | 1210                        |  |
| 1220  | 49.911 | 49.956                             | 50.000 | 50.045 | 50.090 | 50.134 | 50.179 | 50.223 | 50.268 | 50.313 | 50.357 | 1220                        |  |
| 1230  | 50.357 | 50.401                             | 50.446 | 50.490 | 50.535 | 50.579 | 50.624 | 50.668 | 50.713 | 50.757 | 50.802 | 1230                        |  |
| 1240  | 50.802 | 50.846                             | 50.891 | 50.935 | 50.980 | 51.024 | 51.069 | 51.113 | 51.157 | 51.202 | 51.246 | 1240                        |  |
| 1250  | 51.246 | 51.291                             | 51.335 | 51.380 | 51.424 | 51.469 | 51.513 | 51.557 | 51.602 | 51.646 | 51.691 | 1250                        |  |
| 1260  | 51.691 | 51.735                             | 51.780 | 51.824 | 51.868 | 51.913 | 51.957 | 52.002 | 52.046 | 52.090 | 52.135 | 1260                        |  |
| 1270  | 52.135 | 52.179                             | 52.223 | 52.268 | 52.312 | 52.357 | 52.401 | 52.445 | 52.490 | 52.534 | 52.578 | 1270                        |  |
| 1280  | 52.578 | 52.623                             | 52.667 | 52.711 | 52.756 | 52.800 | 52.844 | 52.889 | 52.933 | 52.977 | 53.022 | 1280                        |  |
| 1290  | 53.022 | 53.066                             | 53.110 | 53.155 | 53.199 | 53.243 | 53.288 | 53.332 | 53.376 | 53.420 | 53.465 | 1290                        |  |
| 1300  | 53.465 | 53.509                             | 53.553 | 53.597 | 53.642 | 53.686 | 53.730 | 53.774 | 53.819 | 53.863 | 53.907 | 1300                        |  |
| 1310  | 53.907 | 53.951                             | 53.996 | 54.040 | 54.084 | 54.128 | 54.173 | 54.217 | 54.261 | 54.305 | 54.349 | 1310                        |  |
| 1320  | 54.349 | 54.394                             | 54.438 | 54.482 | 54.526 | 54.570 | 54.615 | 54.659 | 54.703 | 54.747 | 54.791 | 1320                        |  |
| 1330  | 54.791 | 54.835                             | 54.880 | 54.924 | 54.968 | 55.012 | 55.056 | 55.100 | 55.145 | 55.189 | 55.233 | 1330                        |  |
| 1340  | 55.233 | 55.277                             | 55.321 | 55.365 | 55.409 | 55.453 | 55.498 | 55.542 | 55.586 | 55.630 | 55.674 | 1340                        |  |
| 1350  | 55.674 | 55.718                             | 55.762 | 55.806 | 55.850 | 55.894 | 55.938 | 55.982 | 56.026 | 56.071 | 56.115 | 1350                        |  |
| 1360  | 56.115 | 56.159                             | 56.203 | 56.247 | 56.291 | 56.335 | 56.379 | 56.423 | 56.467 | 56.511 | 56.555 | 1360                        |  |
| 1370  | 56.555 | 56.599                             | 56.643 | 56.687 | 56.731 | 56.775 | 56.819 | 56.863 | 56.907 | 56.951 | 56.995 | 1370                        |  |
| 1380  | 56.995 | 57.039                             | 57.083 | 57.127 | 57.171 | 57.215 | 57.259 | 57.303 | 57.347 | 57.391 | 57.434 | 1380                        |  |
| 1390  | 57.434 | 57.478                             | 57.522 | 57.566 | 57.610 | 57.654 | 57.698 | 57.742 | 57.786 | 57.830 | 57.873 | 1390                        |  |
| 1400  | 57.873 | 57.917                             | 57.961 | 58.005 | 58.049 | 58.093 | 58.137 | 58.181 | 58.225 | 58.269 | 58.312 | 1400                        |  |
| 1410  | 58.312 | 58.356                             | 58.400 | 58.444 | 58.488 | 58.531 | 58.575 | 58.619 | 58.663 | 58.707 | 58.750 | 1410                        |  |
| 1420  | 58.750 | 58.794                             | 58.838 | 58.882 | 58.926 | 58.969 | 59.013 | 59.057 | 59.101 | 59.144 | 59.188 | 1420                        |  |
| 1430  | 59.188 | 59.232                             | 59.276 | 59.319 | 59.363 | 59.407 | 59.451 | 59.494 | 59.538 | 59.582 | 59.626 | 1430                        |  |
| 1440  | 59.626 | 59.669                             | 59.713 | 59.757 | 59.800 | 59.844 | 59.888 | 59.932 | 59.975 | 60.019 | 60.063 | 1440                        |  |
| DEG F   | 0      | 1                                  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |

\* Converted from degrees Celsius (IPTS 1968).

TABLE 10.4—Type E thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit* |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|------------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
| DEG F   | 0      | 1                                  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |                                    |        |        |        |        |        |        |        |        |        |                             |  |
| 1.450   | 60.063 | 60.106                             | 60.150 | 60.194 | 60.237 | 60.281 | 60.325 | 60.368 | 60.412 | 60.455 | 60.499 | 1.450                       |  |
| 1.460   | 60.499 | 60.543                             | 60.586 | 60.630 | 60.674 | 60.717 | 60.761 | 60.804 | 60.848 | 60.892 | 60.935 | 1.460                       |  |
| 1.470   | 60.935 | 60.979                             | 61.022 | 61.066 | 61.109 | 61.153 | 61.197 | 61.240 | 61.284 | 61.327 | 61.371 | 1.470                       |  |
| 1.480   | 61.371 | 61.414                             | 61.458 | 61.501 | 61.545 | 61.588 | 61.632 | 61.675 | 61.719 | 61.762 | 61.806 | 1.480                       |  |
| 1.490   | 61.806 | 61.849                             | 61.893 | 61.936 | 61.980 | 62.023 | 62.067 | 62.110 | 62.154 | 62.197 | 62.240 | 1.490                       |  |
| 1.500   | 62.240 | 62.284                             | 62.327 | 62.371 | 62.414 | 62.458 | 62.501 | 62.544 | 62.588 | 62.631 | 62.675 | 1.500                       |  |
| 1.510   | 62.675 | 62.718                             | 62.761 | 62.805 | 62.848 | 62.892 | 62.935 | 62.978 | 63.022 | 63.065 | 63.108 | 1.510                       |  |
| 1.520   | 63.108 | 63.152                             | 63.195 | 63.238 | 63.282 | 63.325 | 63.368 | 63.412 | 63.455 | 63.498 | 63.542 | 1.520                       |  |
| 1.530   | 63.542 | 63.585                             | 63.628 | 63.671 | 63.715 | 63.758 | 63.801 | 63.844 | 63.888 | 63.931 | 63.974 | 1.530                       |  |
| 1.540   | 63.974 | 64.017                             | 64.061 | 64.104 | 64.147 | 64.190 | 64.234 | 64.277 | 64.320 | 64.363 | 64.406 | 1.540                       |  |
| 1.550   | 64.406 | 64.450                             | 64.493 | 64.536 | 64.579 | 64.622 | 64.665 | 64.709 | 64.752 | 64.795 | 64.838 | 1.550                       |  |
| 1.560   | 64.838 | 64.881                             | 64.924 | 64.967 | 65.011 | 65.054 | 65.097 | 65.140 | 65.183 | 65.226 | 65.269 | 1.560                       |  |
| 1.570   | 65.269 | 65.312                             | 65.355 | 65.398 | 65.441 | 65.484 | 65.528 | 65.571 | 65.614 | 65.657 | 65.700 | 1.570                       |  |
| 1.580   | 65.700 | 65.743                             | 65.786 | 65.829 | 65.872 | 65.915 | 65.958 | 66.001 | 66.044 | 66.087 | 66.130 | 1.580                       |  |
| 1.590   | 66.130 | 66.173                             | 66.216 | 66.259 | 66.302 | 66.345 | 66.387 | 66.430 | 66.473 | 66.516 | 66.559 | 1.590                       |  |
| 1.600   | 66.559 | 66.602                             | 66.645 | 66.688 | 66.731 | 66.774 | 66.817 | 66.859 | 66.902 | 66.945 | 66.988 | 1.600                       |  |
| 1.610   | 66.988 | 67.031                             | 67.074 | 67.117 | 67.159 | 67.202 | 67.245 | 67.288 | 67.331 | 67.374 | 67.416 | 1.610                       |  |
| 1.620   | 67.416 | 67.459                             | 67.502 | 67.545 | 67.588 | 67.630 | 67.673 | 67.716 | 67.759 | 67.801 | 67.844 | 1.620                       |  |
| 1.630   | 67.844 | 67.887                             | 67.930 | 67.972 | 68.015 | 68.058 | 68.101 | 68.143 | 68.186 | 68.229 | 68.271 | 1.630                       |  |
| 1.640   | 68.271 | 68.314                             | 68.357 | 68.399 | 68.442 | 68.485 | 68.527 | 68.570 | 68.613 | 68.655 | 68.698 | 1.640                       |  |
| 1.650   | 68.698 | 68.740                             | 68.783 | 68.826 | 68.868 | 68.911 | 68.953 | 68.996 | 69.039 | 69.081 | 69.124 | 1.650                       |  |
| 1.660   | 69.124 | 69.166                             | 69.209 | 69.251 | 69.294 | 69.337 | 69.379 | 69.422 | 69.464 | 69.507 | 69.549 | 1.660                       |  |
| 1.670   | 69.549 | 69.592                             | 69.634 | 69.677 | 69.719 | 69.762 | 69.804 | 69.847 | 69.889 | 69.931 | 69.974 | 1.670                       |  |
| 1.680   | 69.974 | 70.016                             | 70.059 | 70.101 | 70.144 | 70.186 | 70.228 | 70.271 | 70.313 | 70.356 | 70.398 | 1.680                       |  |
| 1.690   | 70.398 | 70.440                             | 70.483 | 70.525 | 70.567 | 70.610 | 70.652 | 70.694 | 70.737 | 70.779 | 70.821 | 1.690                       |  |
| 1.700   | 70.821 | 70.864                             | 70.906 | 70.948 | 70.991 | 71.033 | 71.075 | 71.118 | 71.160 | 71.202 | 71.244 | 1.700                       |  |
| 1.710   | 71.244 | 71.287                             | 71.329 | 71.371 | 71.413 | 71.456 | 71.498 | 71.540 | 71.582 | 71.624 | 71.667 | 1.710                       |  |
| 1.720   | 71.667 | 71.709                             | 71.751 | 71.793 | 71.835 | 71.878 | 71.920 | 71.962 | 72.004 | 72.046 | 72.088 | 1.720                       |  |
| 1.730   | 72.088 | 72.130                             | 72.173 | 72.215 | 72.257 | 72.299 | 72.341 | 72.383 | 72.425 | 72.467 | 72.509 | 1.730                       |  |
| 1.740   | 72.509 | 72.551                             | 72.593 | 72.635 | 72.678 | 72.720 | 72.762 | 72.804 | 72.846 | 72.888 | 72.930 | 1.740                       |  |
| 1.750   | 72.930 | 72.972                             | 73.014 | 73.056 | 73.098 | 73.140 | 73.182 | 73.224 | 73.266 | 73.308 | 73.350 | 1.750                       |  |
| 1.760   | 73.350 | 73.392                             | 73.434 | 73.475 | 73.517 | 73.559 | 73.601 | 73.643 | 73.685 | 73.727 | 73.769 | 1.760                       |  |
| 1.770   | 73.769 | 73.811                             | 73.853 | 73.895 | 73.937 | 73.978 | 74.020 | 74.062 | 74.104 | 74.146 | 74.188 | 1.770                       |  |
| 1.780   | 74.188 | 74.229                             | 74.271 | 74.313 | 74.355 | 74.397 | 74.439 | 74.480 | 74.522 | 74.564 | 74.606 | 1.780                       |  |
| 1.790   | 74.606 | 74.648                             | 74.689 | 74.731 | 74.773 | 74.815 | 74.857 | 74.898 | 74.940 | 74.982 | 75.024 | 1.790                       |  |
| 1.800   | 75.024 | 75.065                             | 75.107 | 75.149 | 75.191 | 75.232 | 75.274 | 75.316 | 75.357 | 75.399 | 75.441 | 1.800                       |  |
| 1.810   | 75.441 | 75.483                             | 75.524 | 75.566 | 75.608 | 75.649 | 75.691 | 75.733 | 75.774 | 75.816 | 75.858 | 1.810                       |  |
| 1.820   | 75.858 | 75.899                             | 75.941 | 75.983 | 76.024 | 76.066 | 76.108 | 76.149 | 76.191 | 76.233 | 76.274 | 1.820                       |  |
| 1.830   | 76.274 | 76.316                             | 76.358 |        |        |        |        |        |        |        |        | 1.830                       |  |
| DEG F   | 0      | 1                                  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |

\* Converted from degrees Celsius (IPTS 1968).

178 THE USE OF THERMOCOUPLES IN TEMPERATURE MEASUREMENT

TABLE 10.5—Type E thermocouples (deg C-millivolts).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Celsius (IPTS 1968) |        |        |        |        |        |        |        |        |        | Reference Junctions at 0 C |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------------------------|--|
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |
| THERMoeLECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                            |  |
| -270  | -9.835 |  |        |        |        |        |        |        |        |        |        | -270                       |  |
| -260  | -9.797 | -9.802                                     | -9.808 | -9.813 | -9.817 | -9.821 | -9.825 | -9.828 | -9.831 | -9.833 | -9.835 | -260                       |  |
| -250  | -9.719 | -9.728                                     | -9.737 | -9.746 | -9.754 | -9.762 | -9.770 | -9.777 | -9.784 | -9.791 | -9.797 | -250                       |  |
| -240  | -9.604 | -9.617                                     | -9.630 | -9.642 | -9.654 | -9.666 | -9.677 | -9.688 | -9.699 | -9.709 | -9.719 | -240                       |  |
| -230  | -9.455 | -9.472                                     | -9.488 | -9.503 | -9.519 | -9.534 | -9.549 | -9.563 | -9.577 | -9.591 | -9.604 | -230                       |  |
| -220  | -9.274 | -9.293                                     | -9.313 | -9.332 | -9.350 | -9.368 | -9.386 | -9.404 | -9.421 | -9.438 | -9.455 | -220                       |  |
| -210  | -9.063 | -9.085                                     | -9.107 | -9.129 | -9.151 | -9.172 | -9.193 | -9.214 | -9.234 | -9.254 | -9.274 | -210                       |  |
| -200  | -8.824 | -8.850                                     | -8.874 | -8.899 | -8.923 | -8.947 | -8.971 | -8.994 | -9.017 | -9.040 | -9.063 | -200                       |  |
| -190  | -8.561 | -8.588                                     | -8.615 | -8.642 | -8.669 | -8.696 | -8.722 | -8.748 | -8.774 | -8.799 | -8.824 | -190                       |  |
| -180  | -8.273 | -8.303                                     | -8.333 | -8.362 | -8.391 | -8.420 | -8.449 | -8.477 | -8.505 | -8.533 | -8.561 | -180                       |  |
| -170  | -7.963 | -7.995                                     | -8.027 | -8.058 | -8.090 | -8.121 | -8.152 | -8.183 | -8.213 | -8.243 | -8.273 | -170                       |  |
| -160  | -7.631 | -7.665                                     | -7.699 | -7.733 | -7.767 | -7.800 | -7.833 | -7.866 | -7.898 | -7.931 | -7.963 | -160                       |  |
| -150  | -7.279 | -7.315                                     | -7.351 | -7.387 | -7.422 | -7.458 | -7.493 | -7.528 | -7.562 | -7.597 | -7.631 | -150                       |  |
| -140  | -6.907 | -6.945                                     | -6.983 | -7.020 | -7.058 | -7.095 | -7.132 | -7.169 | -7.206 | -7.243 | -7.279 | -140                       |  |
| -130  | -6.516 | -6.556                                     | -6.596 | -6.635 | -6.675 | -6.714 | -6.753 | -6.792 | -6.830 | -6.869 | -6.907 | -130                       |  |
| -120  | -6.107 | -6.149                                     | -6.190 | -6.231 | -6.273 | -6.314 | -6.356 | -6.397 | -6.436 | -6.476 | -6.516 | -120                       |  |
| -110  | -5.680 | -5.724                                     | -5.767 | -5.810 | -5.853 | -5.896 | -5.938 | -5.981 | -6.023 | -6.065 | -6.107 | -110                       |  |
| -100  | -5.237 | -5.282                                     | -5.327 | -5.371 | -5.416 | -5.460 | -5.505 | -5.549 | -5.593 | -5.637 | -5.680 | -100                       |  |
| -90   | -4.777 | -4.824                                     | -4.870 | -4.916 | -4.963 | -5.009 | -5.055 | -5.100 | -5.146 | -5.191 | -5.237 | -90                        |  |
| -80   | -4.301 | -4.350                                     | -4.398 | -4.446 | -4.493 | -4.541 | -4.588 | -4.636 | -4.683 | -4.730 | -4.777 | -80                        |  |
| -70   | -3.811 | -3.860                                     | -3.910 | -3.959 | -4.009 | -4.058 | -4.107 | -4.156 | -4.204 | -4.253 | -4.301 | -70                        |  |
| -60   | -3.306 | -3.357                                     | -3.408 | -3.459 | -3.509 | -3.560 | -3.610 | -3.661 | -3.711 | -3.761 | -3.811 | -60                        |  |
| -50   | -2.787 | -2.839                                     | -2.892 | -2.944 | -2.996 | -3.048 | -3.100 | -3.152 | -3.203 | -3.254 | -3.306 | -50                        |  |
| -40   | -2.254 | -2.308                                     | -2.362 | -2.416 | -2.469 | -2.522 | -2.575 | -2.628 | -2.681 | -2.734 | -2.787 | -40                        |  |
| -30   | -1.709 | -1.764                                     | -1.819 | -1.874 | -1.929 | -1.983 | -2.038 | -2.092 | -2.146 | -2.200 | -2.254 | -30                        |  |
| -20   | -1.151 | -1.208                                     | -1.264 | -1.320 | -1.376 | -1.432 | -1.487 | -1.543 | -1.599 | -1.654 | -1.709 | -20                        |  |
| -10   | -0.581 | -0.639                                     | -0.696 | -0.754 | -0.811 | -0.868 | -0.925 | -0.982 | -1.038 | -1.095 | -1.151 | -10                        |  |
| 0   | 0.000  | -0.059                                     | -0.117 | -0.176 | -0.234 | -0.292 | -0.350 | -0.408 | -0.466 | -0.524 | -0.581 | 0                          |  |
| 0   | 0.000  | 0.059                                      | 0.118  | 0.176  | 0.235  | 0.295  | 0.354  | 0.413  | 0.472  | 0.532  | 0.591  | 0                          |  |
| 10  | 0.591  | 0.651                                      | 0.711  | 0.770  | 0.830  | 0.890  | 0.950  | 1.011  | 1.071  | 1.131  | 1.192  | 10                         |  |
| 20  | 1.192  | 1.252                                      | 1.313  | 1.373  | 1.434  | 1.495  | 1.556  | 1.617  | 1.678  | 1.739  | 1.801  | 20                         |  |
| 30  | 1.801  | 1.862                                      | 1.924  | 1.985  | 2.047  | 2.109  | 2.171  | 2.233  | 2.295  | 2.357  | 2.419  | 30                         |  |
| 40  | 2.419  | 2.482                                      | 2.544  | 2.607  | 2.669  | 2.732  | 2.795  | 2.858  | 2.921  | 2.984  | 3.047  | 40                         |  |
| 50  | 3.047  | 3.110                                      | 3.173  | 3.237  | 3.300  | 3.364  | 3.428  | 3.491  | 3.555  | 3.619  | 3.683  | 50                         |  |
| 60  | 3.683  | 3.748                                      | 3.812  | 3.876  | 3.941  | 4.005  | 4.070  | 4.134  | 4.199  | 4.264  | 4.329  | 60                         |  |
| 70  | 4.329  | 4.394                                      | 4.459  | 4.524  | 4.590  | 4.655  | 4.720  | 4.786  | 4.852  | 4.917  | 4.983  | 70                         |  |
| 80  | 4.983  | 5.049                                      | 5.115  | 5.181  | 5.247  | 5.314  | 5.380  | 5.446  | 5.513  | 5.579  | 5.646  | 80                         |  |
| 90  | 5.646  | 5.713                                      | 5.780  | 5.846  | 5.913  | 5.981  | 6.048  | 6.115  | 6.182  | 6.250  | 6.317  | 90                         |  |
| 100   | 6.317  | 6.385                                      | 6.452  | 6.520  | 6.588  | 6.656  | 6.724  | 6.792  | 6.860  | 6.928  | 6.996  | 100                        |  |
| 110   | 6.996  | 7.064                                      | 7.133  | 7.201  | 7.270  | 7.339  | 7.407  | 7.476  | 7.545  | 7.614  | 7.683  | 110                        |  |
| 120   | 7.683  | 7.752                                      | 7.821  | 7.890  | 7.960  | 8.029  | 8.099  | 8.168  | 8.238  | 8.307  | 8.377  | 120                        |  |
| 130   | 8.377  | 8.447                                      | 8.517  | 8.587  | 8.657  | 8.727  | 8.797  | 8.867  | 8.938  | 9.008  | 9.078  | 130                        |  |
| 140   | 9.078  | 9.149                                      | 9.220  | 9.290  | 9.361  | 9.432  | 9.503  | 9.573  | 9.644  | 9.715  | 9.787  | 140                        |  |
| 150   | 9.787  | 9.858                                      | 9.929  | 10.000 | 10.072 | 10.143 | 10.215 | 10.286 | 10.358 | 10.429 | 10.501 | 150                        |  |
| 160   | 10.501 | 10.573                                     | 10.645 | 10.717 | 10.789 | 10.861 | 10.933 | 11.005 | 11.077 | 11.150 | 11.222 | 160                        |  |
| 170   | 11.222 | 11.294                                     | 11.367 | 11.439 | 11.512 | 11.585 | 11.657 | 11.730 | 11.803 | 11.876 | 11.949 | 170                        |  |
| 180   | 11.949 | 12.022                                     | 12.095 | 12.168 | 12.241 | 12.314 | 12.387 | 12.461 | 12.534 | 12.608 | 12.681 | 180                        |  |
| 190   | 12.681 | 12.755                                     | 12.828 | 12.902 | 12.975 | 13.049 | 13.123 | 13.197 | 13.271 | 13.345 | 13.419 | 190                        |  |
| 200   | 13.419 | 13.493                                     | 13.567 | 13.641 | 13.715 | 13.789 | 13.864 | 13.938 | 14.012 | 14.087 | 14.161 | 200                        |  |
| 210   | 14.161 | 14.236                                     | 14.310 | 14.385 | 14.460 | 14.534 | 14.609 | 14.684 | 14.759 | 14.834 | 14.909 | 210                        |  |
| 220   | 14.909 | 14.984                                     | 15.059 | 15.134 | 15.209 | 15.284 | 15.359 | 15.434 | 15.509 | 15.584 | 15.661 | 220                        |  |
| 230   | 15.661 | 15.736                                     | 15.812 | 15.887 | 15.963 | 16.038 | 16.114 | 16.190 | 16.266 | 16.341 | 16.417 | 230                        |  |
| 240   | 16.417 | 16.493                                     | 16.569 | 16.645 | 16.721 | 16.797 | 16.873 | 16.949 | 17.025 | 17.101 | 17.178 | 240                        |  |
| 250   | 17.178 | 17.254                                     | 17.330 | 17.406 | 17.483 | 17.559 | 17.636 | 17.712 | 17.789 | 17.865 | 17.942 | 250                        |  |
| 260   | 17.942 | 18.018                                     | 18.095 | 18.172 | 18.248 | 18.325 | 18.402 | 18.479 | 18.556 | 18.633 | 18.710 | 260                        |  |
| 270   | 18.710 | 18.787                                     | 18.864 | 18.941 | 19.018 | 19.095 | 19.172 | 19.249 | 19.326 | 19.404 | 19.481 | 270                        |  |
| 280   | 19.481 | 19.558                                     | 19.636 | 19.713 | 19.790 | 19.868 | 19.945 | 20.023 | 20.100 | 20.178 | 20.256 | 280                        |  |
| 290   | 20.256 | 20.333                                     | 20.411 | 20.488 | 20.566 | 20.644 | 20.722 | 20.800 | 20.877 | 20.955 | 21.033 | 290                        |  |
| 300   | 21.033 | 21.111                                     | 21.189 | 21.267 | 21.345 | 21.423 | 21.501 | 21.579 | 21.657 | 21.735 | 21.814 | 300                        |  |
| 310   | 21.814 | 21.892                                     | 21.970 | 22.048 | 22.127 | 22.205 | 22.283 | 22.362 | 22.440 | 22.518 | 22.597 | 310                        |  |
| 320   | 22.597 | 22.675                                     | 22.754 | 22.832 | 22.911 | 22.989 | 23.068 | 23.147 | 23.225 | 23.304 | 23.383 | 320                        |  |
| 330   | 23.383 | 23.461                                     | 23.540 | 23.619 | 23.698 | 23.777 | 23.855 | 23.934 | 24.013 | 24.092 | 24.171 | 330                        |  |
| 340   | 24.171 | 24.250                                     | 24.329 | 24.408 | 24.487 | 24.566 | 24.645 | 24.724 | 24.803 | 24.882 | 24.961 | 340                        |  |
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |

TABLE 10.5—Type E thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Celsius (IPTS 1968) |        |        |        |        |        |        |        |        |        | Reference Junctions at 0 C |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------------------------|--|
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                            |  |
| 350   | 24.961 | 25.041                                     | 25.120 | 25.199 | 25.278 | 25.357 | 25.437 | 25.516 | 25.595 | 25.675 | 25.754 | 350                        |  |
| 360   | 25.754 | 25.833                                     | 25.913 | 25.992 | 26.072 | 26.151 | 26.230 | 26.310 | 26.389 | 26.469 | 26.549 | 360                        |  |
| 370   | 26.549 | 26.628                                     | 26.708 | 26.787 | 26.867 | 26.947 | 27.026 | 27.106 | 27.186 | 27.265 | 27.345 | 370                        |  |
| 380   | 27.345 | 27.425                                     | 27.504 | 27.584 | 27.664 | 27.744 | 27.824 | 27.903 | 27.983 | 28.063 | 28.143 | 380                        |  |
| 390   | 28.143 | 28.223                                     | 28.303 | 28.383 | 28.463 | 28.543 | 28.623 | 28.703 | 28.783 | 28.863 | 28.943 | 390                        |  |
| 400   | 28.943 | 29.023                                     | 29.103 | 29.183 | 29.263 | 29.343 | 29.423 | 29.503 | 29.584 | 29.664 | 29.744 | 400                        |  |
| 410   | 29.744 | 29.824                                     | 29.904 | 29.984 | 30.065 | 30.145 | 30.225 | 30.305 | 30.386 | 30.466 | 30.546 | 410                        |  |
| 420   | 30.546 | 30.627                                     | 30.707 | 30.787 | 30.868 | 30.948 | 31.028 | 31.109 | 31.189 | 31.270 | 31.350 | 420                        |  |
| 430   | 31.350 | 31.430                                     | 31.511 | 31.591 | 31.672 | 31.752 | 31.833 | 31.913 | 31.994 | 32.074 | 32.155 | 430                        |  |
| 440   | 32.155 | 32.235                                     | 32.316 | 32.396 | 32.477 | 32.557 | 32.638 | 32.719 | 32.799 | 32.880 | 32.960 | 440                        |  |
| 450   | 32.960 | 33.041                                     | 33.122 | 33.202 | 33.283 | 33.364 | 33.444 | 33.525 | 33.605 | 33.686 | 33.767 | 450                        |  |
| 460   | 33.767 | 33.848                                     | 33.928 | 34.009 | 34.090 | 34.170 | 34.251 | 34.332 | 34.413 | 34.493 | 34.574 | 460                        |  |
| 470   | 34.574 | 34.655                                     | 34.736 | 34.816 | 34.897 | 34.978 | 35.059 | 35.140 | 35.220 | 35.301 | 35.382 | 470                        |  |
| 480   | 35.382 | 35.463                                     | 35.544 | 35.624 | 35.705 | 35.786 | 35.867 | 35.948 | 36.029 | 36.109 | 36.190 | 480                        |  |
| 490   | 36.190 | 36.271                                     | 36.352 | 36.433 | 36.514 | 36.595 | 36.675 | 36.756 | 36.837 | 36.918 | 36.999 | 490                        |  |
| 500   | 36.999 | 37.080                                     | 37.161 | 37.242 | 37.323 | 37.403 | 37.484 | 37.565 | 37.646 | 37.727 | 37.808 | 500                        |  |
| 510   | 37.808 | 37.889                                     | 37.970 | 38.051 | 38.132 | 38.213 | 38.293 | 38.374 | 38.455 | 38.536 | 38.617 | 510                        |  |
| 520   | 38.617 | 38.698                                     | 38.779 | 38.860 | 38.941 | 39.022 | 39.103 | 39.184 | 39.264 | 39.345 | 39.426 | 520                        |  |
| 530   | 39.426 | 39.507                                     | 39.588 | 39.669 | 39.750 | 39.831 | 39.912 | 39.993 | 40.074 | 40.155 | 40.236 | 530                        |  |
| 540   | 40.236 | 40.316                                     | 40.397 | 40.478 | 40.559 | 40.640 | 40.721 | 40.802 | 40.883 | 40.964 | 41.045 | 540                        |  |
| 550   | 41.045 | 41.125                                     | 41.206 | 41.287 | 41.368 | 41.449 | 41.530 | 41.611 | 41.692 | 41.773 | 41.853 | 550                        |  |
| 560   | 41.853 | 41.934                                     | 42.015 | 42.096 | 42.177 | 42.258 | 42.339 | 42.419 | 42.500 | 42.581 | 42.662 | 560                        |  |
| 570   | 42.662 | 42.743                                     | 42.824 | 42.904 | 42.985 | 43.066 | 43.147 | 43.228 | 43.308 | 43.389 | 43.470 | 570                        |  |
| 580   | 43.470 | 43.551                                     | 43.632 | 43.712 | 43.793 | 43.874 | 43.955 | 44.035 | 44.116 | 44.197 | 44.278 | 580                        |  |
| 590   | 44.278 | 44.358                                     | 44.439 | 44.520 | 44.601 | 44.681 | 44.762 | 44.843 | 44.923 | 45.004 | 45.085 | 590                        |  |
| 600   | 45.085 | 45.165                                     | 45.246 | 45.327 | 45.407 | 45.488 | 45.569 | 45.649 | 45.730 | 45.811 | 45.891 | 600                        |  |
| 610   | 45.891 | 45.972                                     | 46.052 | 46.133 | 46.213 | 46.294 | 46.375 | 46.455 | 46.536 | 46.616 | 46.697 | 610                        |  |
| 620   | 46.697 | 46.777                                     | 46.858 | 46.938 | 47.019 | 47.099 | 47.180 | 47.260 | 47.341 | 47.421 | 47.502 | 620                        |  |
| 630   | 47.502 | 47.582                                     | 47.663 | 47.743 | 47.824 | 47.904 | 47.984 | 48.065 | 48.145 | 48.226 | 48.306 | 630                        |  |
| 640   | 48.306 | 48.386                                     | 48.467 | 48.547 | 48.627 | 48.708 | 48.788 | 48.868 | 48.949 | 49.029 | 49.109 | 640                        |  |
| 650   | 49.109 | 49.189                                     | 49.270 | 49.350 | 49.430 | 49.510 | 49.591 | 49.671 | 49.751 | 49.831 | 49.911 | 650                        |  |
| 660   | 49.911 | 49.992                                     | 50.072 | 50.152 | 50.232 | 50.312 | 50.392 | 50.472 | 50.553 | 50.633 | 50.713 | 660                        |  |
| 670   | 50.713 | 50.793                                     | 50.873 | 50.953 | 51.033 | 51.113 | 51.193 | 51.273 | 51.353 | 51.433 | 51.513 | 670                        |  |
| 680   | 51.513 | 51.593                                     | 51.673 | 51.753 | 51.833 | 51.913 | 51.993 | 52.073 | 52.153 | 52.233 | 52.313 | 680                        |  |
| 690   | 52.313 | 52.392                                     | 52.472 | 52.552 | 52.632 | 52.711 | 52.791 | 52.871 | 52.951 | 53.031 | 53.110 | 690                        |  |
| 700   | 53.110 | 53.190                                     | 53.270 | 53.350 | 53.429 | 53.509 | 53.589 | 53.668 | 53.748 | 53.828 | 53.907 | 700                        |  |
| 710   | 53.907 | 53.987                                     | 54.066 | 54.146 | 54.226 | 54.305 | 54.385 | 54.464 | 54.544 | 54.623 | 54.703 | 710                        |  |
| 720   | 54.703 | 54.782                                     | 54.862 | 54.941 | 55.021 | 55.100 | 55.180 | 55.259 | 55.339 | 55.418 | 55.498 | 720                        |  |
| 730   | 55.498 | 55.577                                     | 55.656 | 55.736 | 55.815 | 55.894 | 55.974 | 56.053 | 56.132 | 56.212 | 56.291 | 730                        |  |
| 740   | 56.291 | 56.370                                     | 56.449 | 56.529 | 56.608 | 56.687 | 56.766 | 56.845 | 56.924 | 57.004 | 57.083 | 740                        |  |
| 750   | 57.083 | 57.162                                     | 57.241 | 57.320 | 57.399 | 57.478 | 57.557 | 57.636 | 57.715 | 57.794 | 57.873 | 750                        |  |
| 760   | 57.873 | 57.952                                     | 58.031 | 58.110 | 58.189 | 58.268 | 58.347 | 58.426 | 58.505 | 58.584 | 58.663 | 760                        |  |
| 770   | 58.663 | 58.742                                     | 58.820 | 58.899 | 58.978 | 59.057 | 59.136 | 59.214 | 59.293 | 59.372 | 59.451 | 770                        |  |
| 780   | 59.451 | 59.529                                     | 59.608 | 59.687 | 59.765 | 59.844 | 59.923 | 60.001 | 60.080 | 60.159 | 60.237 | 780                        |  |
| 790   | 60.237 | 60.316                                     | 60.394 | 60.473 | 60.551 | 60.630 | 60.708 | 60.787 | 60.865 | 60.944 | 61.022 | 790                        |  |
| 800   | 61.022 | 61.101                                     | 61.179 | 61.258 | 61.336 | 61.414 | 61.493 | 61.571 | 61.649 | 61.728 | 61.806 | 800                        |  |
| 810   | 61.806 | 61.884                                     | 61.962 | 62.041 | 62.119 | 62.197 | 62.275 | 62.353 | 62.432 | 62.510 | 62.588 | 810                        |  |
| 820   | 62.588 | 62.666                                     | 62.744 | 62.822 | 62.900 | 62.978 | 63.056 | 63.134 | 63.212 | 63.290 | 63.368 | 820                        |  |
| 830   | 63.368 | 63.446                                     | 63.524 | 63.602 | 63.680 | 63.758 | 63.836 | 63.914 | 63.992 | 64.069 | 64.147 | 830                        |  |
| 840   | 64.147 | 64.225                                     | 64.303 | 64.380 | 64.458 | 64.536 | 64.614 | 64.691 | 64.769 | 64.847 | 64.924 | 840                        |  |
| 850   | 64.924 | 65.002                                     | 65.080 | 65.157 | 65.235 | 65.312 | 65.390 | 65.467 | 65.545 | 65.622 | 65.700 | 850                        |  |
| 860   | 65.700 | 65.777                                     | 65.855 | 65.932 | 66.009 | 66.087 | 66.164 | 66.241 | 66.319 | 66.396 | 66.473 | 860                        |  |
| 870   | 66.473 | 66.551                                     | 66.628 | 66.705 | 66.782 | 66.859 | 66.937 | 67.014 | 67.091 | 67.168 | 67.245 | 870                        |  |
| 880   | 67.245 | 67.322                                     | 67.399 | 67.476 | 67.553 | 67.630 | 67.707 | 67.784 | 67.861 | 67.938 | 68.015 | 880                        |  |
| 890   | 68.015 | 68.092                                     | 68.169 | 68.246 | 68.323 | 68.399 | 68.476 | 68.553 | 68.630 | 68.706 | 68.783 | 890                        |  |
| 900   | 68.783 | 68.860                                     | 68.936 | 69.013 | 69.090 | 69.166 | 69.243 | 69.320 | 69.396 | 69.473 | 69.549 | 900                        |  |
| 910   | 69.549 | 69.626                                     | 69.702 | 69.779 | 69.855 | 69.931 | 70.008 | 70.084 | 70.161 | 70.237 | 70.313 | 910                        |  |
| 920   | 70.313 | 70.390                                     | 70.466 | 70.542 | 70.618 | 70.694 | 70.771 | 70.847 | 70.923 | 70.999 | 71.075 | 920                        |  |
| 930   | 71.075 | 71.151                                     | 71.227 | 71.304 | 71.380 | 71.456 | 71.532 | 71.608 | 71.683 | 71.759 | 71.835 | 930                        |  |
| 940   | 71.835 | 71.911                                     | 71.987 | 72.063 | 72.139 | 72.215 | 72.290 | 72.366 | 72.442 | 72.518 | 72.593 | 940                        |  |
| 950   | 72.593 | 72.669                                     | 72.745 | 72.820 | 72.896 | 72.972 | 73.047 | 73.123 | 73.199 | 73.274 | 73.350 | 950                        |  |
| 960   | 73.350 | 73.425                                     | 73.501 | 73.576 | 73.652 | 73.727 | 73.802 | 73.878 | 73.953 | 74.029 | 74.104 | 960                        |  |
| 970   | 74.104 | 74.179                                     | 74.255 | 74.330 | 74.405 | 74.480 | 74.556 | 74.631 | 74.706 | 74.781 | 74.857 | 970                        |  |
| 980   | 74.857 | 74.932                                     | 75.007 | 75.082 | 75.157 | 75.232 | 75.307 | 75.382 | 75.458 | 75.533 | 75.608 | 980                        |  |
| 990   | 75.608 | 75.683                                     | 75.758 | 75.833 | 75.908 | 75.983 | 76.058 | 76.133 | 76.208 | 76.283 | 76.358 | 990                        |  |
| 1-000   | 76.358 |  |        |        |        |        |        |        |        |        |        | 1-000                      |  |
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |

180 THE USE OF THERMOCOUPLES IN TEMPERATURE MEASUREMENT

TABLE 10.6—Type J thermocouples (deg F-millivolts).

NOTE—The maximum recommended temperature limit for Type J thermocouples is 1400 F (760 C) as specified in Table 2. Extension of the Type J tables beyond 1400 F gives temperature-electromotive force data to 2192 F (1200 C). This extension is a mathematical extrapolation based on limited calibration data and caution should be exercised in its use. The basis for the extended curve is discussed in *NBS Monograph 125*.

It should be noted that limits of error for Type J thermocouples (Table 1) do not apply above 1400 F (760 C).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit* |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|------------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
| DEG F   | 0      | 1                                  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |                                    |        |        |        |        |        |        |        |        |        |                             |  |
| -350  | -8.137 |                                    |        |        |        |        |        |        |        |        |        | -350                        |  |
| -340  | -8.030 | -8.041                             | -8.052 | -8.063 | -8.074 | -8.085 | -8.096 | -8.106 | -8.117 | -8.127 | -8.137 | -340                        |  |
| -330  | -7.915 | -7.927                             | -7.938 | -7.950 | -7.962 | -7.973 | -7.985 | -7.996 | -8.008 | -8.019 | -8.030 | -330                        |  |
| -320  | -7.791 | -7.803                             | -7.816 | -7.829 | -7.841 | -7.854 | -7.866 | -7.878 | -7.890 | -7.903 | -7.915 | -320                        |  |
| -310  | -7.659 | -7.672                             | -7.686 | -7.699 | -7.712 | -7.726 | -7.739 | -7.752 | -7.765 | -7.778 | -7.791 | -310                        |  |
| -300  | -7.519 | -7.533                             | -7.548 | -7.562 | -7.576 | -7.590 | -7.604 | -7.618 | -7.631 | -7.645 | -7.659 | -300                        |  |
| -290  | -7.372 | -7.387                             | -7.402 | -7.417 | -7.432 | -7.447 | -7.461 | -7.476 | -7.490 | -7.505 | -7.519 | -290                        |  |
| -280  | -7.218 | -7.234                             | -7.250 | -7.265 | -7.281 | -7.296 | -7.311 | -7.327 | -7.342 | -7.357 | -7.372 | -280                        |  |
| -270  | -7.057 | -7.074                             | -7.090 | -7.106 | -7.122 | -7.139 | -7.155 | -7.171 | -7.187 | -7.202 | -7.218 | -270                        |  |
| -260  | -6.890 | -6.907                             | -6.924 | -6.941 | -6.958 | -6.974 | -6.991 | -7.008 | -7.024 | -7.041 | -7.057 | -260                        |  |
| -250  | -6.716 | -6.734                             | -6.751 | -6.769 | -6.786 | -6.804 | -6.821 | -6.838 | -6.856 | -6.873 | -6.890 | -250                        |  |
| -240  | -6.536 | -6.554                             | -6.572 | -6.591 | -6.609 | -6.627 | -6.645 | -6.663 | -6.680 | -6.698 | -6.716 | -240                        |  |
| -230  | -6.350 | -6.369                             | -6.388 | -6.407 | -6.425 | -6.444 | -6.462 | -6.481 | -6.499 | -6.518 | -6.536 | -230                        |  |
| -220  | -6.159 | -6.178                             | -6.198 | -6.217 | -6.236 | -6.255 | -6.274 | -6.293 | -6.312 | -6.331 | -6.350 | -220                        |  |
| -210  | -5.962 | -5.982                             | -6.002 | -6.022 | -6.041 | -6.061 | -6.081 | -6.100 | -6.120 | -6.139 | -6.159 | -210                        |  |
| -200  | -5.760 | -5.780                             | -5.801 | -5.821 | -5.841 | -5.861 | -5.882 | -5.902 | -5.922 | -5.942 | -5.962 | -200                        |  |
| -190  | -5.553 | -5.574                             | -5.594 | -5.615 | -5.636 | -5.657 | -5.678 | -5.698 | -5.719 | -5.739 | -5.760 | -190                        |  |
| -180  | -5.341 | -5.362                             | -5.383 | -5.405 | -5.426 | -5.447 | -5.468 | -5.490 | -5.511 | -5.532 | -5.553 | -180                        |  |
| -170  | -5.124 | -5.146                             | -5.168 | -5.190 | -5.211 | -5.233 | -5.255 | -5.276 | -5.298 | -5.319 | -5.341 | -170                        |  |
| -160  | -4.903 | -4.925                             | -4.948 | -4.970 | -4.992 | -5.014 | -5.036 | -5.058 | -5.080 | -5.102 | -5.124 | -160                        |  |
| -150  | -4.678 | -4.700                             | -4.723 | -4.746 | -4.768 | -4.791 | -4.813 | -4.836 | -4.858 | -4.881 | -4.903 | -150                        |  |
| -140  | -4.448 | -4.471                             | -4.494 | -4.517 | -4.540 | -4.563 | -4.586 | -4.609 | -4.632 | -4.655 | -4.678 | -140                        |  |
| -130  | -4.215 | -4.238                             | -4.262 | -4.285 | -4.309 | -4.332 | -4.355 | -4.379 | -4.402 | -4.425 | -4.448 | -130                        |  |
| -120  | -3.978 | -4.001                             | -4.025 | -4.049 | -4.073 | -4.097 | -4.120 | -4.144 | -4.168 | -4.191 | -4.215 | -120                        |  |
| -110  | -3.737 | -3.761                             | -3.785 | -3.809 | -3.833 | -3.858 | -3.882 | -3.906 | -3.930 | -3.954 | -3.978 | -110                        |  |
| -100  | -3.492 | -3.517                             | -3.541 | -3.566 | -3.590 | -3.615 | -3.639 | -3.664 | -3.688 | -3.712 | -3.737 | -100                        |  |
| -90   | -3.245 | -3.270                             | -3.294 | -3.319 | -3.344 | -3.369 | -3.394 | -3.418 | -3.443 | -3.468 | -3.492 | -90                         |  |
| -80   | -2.994 | -3.019                             | -3.044 | -3.069 | -3.094 | -3.120 | -3.145 | -3.170 | -3.195 | -3.220 | -3.245 | -80                         |  |
| -70   | -2.740 | -2.765                             | -2.791 | -2.816 | -2.842 | -2.867 | -2.892 | -2.918 | -2.943 | -2.968 | -2.994 | -70                         |  |
| -60   | -2.483 | -2.509                             | -2.534 | -2.560 | -2.586 | -2.612 | -2.637 | -2.663 | -2.689 | -2.714 | -2.740 | -60                         |  |
| -50   | -2.223 | -2.249                             | -2.275 | -2.301 | -2.327 | -2.353 | -2.379 | -2.405 | -2.431 | -2.457 | -2.483 | -50                         |  |
| -40   | -1.960 | -1.987                             | -2.013 | -2.039 | -2.066 | -2.092 | -2.118 | -2.144 | -2.171 | -2.197 | -2.223 | -40                         |  |
| -30   | -1.695 | -1.722                             | -1.748 | -1.775 | -1.802 | -1.828 | -1.855 | -1.881 | -1.908 | -1.934 | -1.960 | -30                         |  |
| -20   | -1.428 | -1.455                             | -1.481 | -1.508 | -1.535 | -1.562 | -1.589 | -1.615 | -1.642 | -1.669 | -1.695 | -20                         |  |
| -10   | -1.158 | -1.185                             | -1.212 | -1.239 | -1.266 | -1.293 | -1.320 | -1.347 | -1.374 | -1.401 | -1.428 | -10                         |  |
| 0   | -0.885 | -0.913                             | -0.940 | -0.967 | -0.995 | -1.022 | -1.049 | -1.076 | -1.103 | -1.131 | -1.158 | 0                           |  |
| 0   | -0.885 | -0.858                             | -0.831 | -0.803 | -0.776 | -0.748 | -0.721 | -0.694 | -0.666 | -0.639 | -0.611 | 0                           |  |
| 10  | -0.611 | -0.583                             | -0.556 | -0.528 | -0.501 | -0.473 | -0.445 | -0.418 | -0.390 | -0.362 | -0.334 | 10                          |  |
| 20  | -0.334 | -0.307                             | -0.279 | -0.251 | -0.223 | -0.195 | -0.168 | -0.140 | -0.112 | -0.084 | -0.056 | 20                          |  |
| 30  | -0.056 | -0.028                             | 0.000  | 0.028  | 0.056  | 0.084  | 0.112  | 0.140  | 0.168  | 0.196  | 0.224  | 30                          |  |
| 40  | 0.224  | 0.253                              | 0.281  | 0.309  | 0.337  | 0.365  | 0.394  | 0.422  | 0.450  | 0.478  | 0.507  | 40                          |  |
| 50  | 0.507  | 0.535                              | 0.563  | 0.592  | 0.620  | 0.648  | 0.677  | 0.705  | 0.734  | 0.762  | 0.791  | 50                          |  |
| 60  | 0.791  | 0.819                              | 0.848  | 0.876  | 0.905  | 0.933  | 0.962  | 0.990  | 1.019  | 1.048  | 1.076  | 60                          |  |
| 70  | 1.076  | 1.105                              | 1.134  | 1.162  | 1.191  | 1.220  | 1.248  | 1.277  | 1.306  | 1.335  | 1.363  | 70                          |  |
| 80  | 1.363  | 1.392                              | 1.421  | 1.450  | 1.479  | 1.507  | 1.536  | 1.565  | 1.594  | 1.623  | 1.652  | 80                          |  |
| 90  | 1.652  | 1.681                              | 1.710  | 1.739  | 1.768  | 1.797  | 1.826  | 1.855  | 1.884  | 1.913  | 1.942  | 90                          |  |
| 100   | 1.942  | 1.971                              | 2.000  | 2.029  | 2.058  | 2.088  | 2.117  | 2.146  | 2.175  | 2.204  | 2.233  | 100                         |  |
| 110   | 2.233  | 2.263                              | 2.292  | 2.321  | 2.350  | 2.380  | 2.409  | 2.438  | 2.467  | 2.497  | 2.526  | 110                         |  |
| 120   | 2.526  | 2.555                              | 2.585  | 2.614  | 2.644  | 2.673  | 2.702  | 2.732  | 2.761  | 2.791  | 2.820  | 120                         |  |
| 130   | 2.820  | 2.849                              | 2.879  | 2.908  | 2.938  | 2.967  | 2.997  | 3.026  | 3.056  | 3.085  | 3.115  | 130                         |  |
| 140   | 3.115  | 3.145                              | 3.174  | 3.204  | 3.233  | 3.263  | 3.293  | 3.322  | 3.352  | 3.381  | 3.411  | 140                         |  |
| 150   | 3.411  | 3.441                              | 3.470  | 3.500  | 3.530  | 3.560  | 3.589  | 3.619  | 3.649  | 3.678  | 3.708  | 150                         |  |
| 160   | 3.708  | 3.738                              | 3.768  | 3.798  | 3.827  | 3.857  | 3.887  | 3.917  | 3.947  | 3.976  | 4.006  | 160                         |  |
| 170   | 4.006  | 4.036                              | 4.066  | 4.096  | 4.126  | 4.156  | 4.186  | 4.216  | 4.245  | 4.275  | 4.305  | 170                         |  |
| 180   | 4.305  | 4.335                              | 4.365  | 4.395  | 4.425  | 4.455  | 4.485  | 4.515  | 4.545  | 4.575  | 4.605  | 180                         |  |
| 190   | 4.605  | 4.635                              | 4.665  | 4.695  | 4.725  | 4.755  | 4.786  | 4.816  | 4.846  | 4.876  | 4.906  | 190                         |  |
| DEG F   | 0      | 1                                  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |

\* Converted from degrees Celsius (IPTS 1968).

TABLE 10.6—Type J thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit <sup>a</sup> |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
| DEG F   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                             |  |
| 200   | 4.906  | 4.936  | 4.966  | 4.996  | 5.026  | 5.057  | 5.087  | 5.117  | 5.147  | 5.177  | 5.207  | 200                         |  |
| 210   | 5.207  | 5.238  | 5.268  | 5.298  | 5.328  | 5.358  | 5.389  | 5.419  | 5.449  | 5.479  | 5.509  | 210                         |  |
| 220   | 5.509  | 5.540  | 5.570  | 5.600  | 5.630  | 5.661  | 5.691  | 5.721  | 5.752  | 5.782  | 5.812  | 220                         |  |
| 230   | 5.812  | 5.843  | 5.873  | 5.903  | 5.934  | 5.964  | 5.994  | 6.025  | 6.055  | 6.085  | 6.116  | 230                         |  |
| 240   | 6.116  | 6.146  | 6.176  | 6.207  | 6.237  | 6.268  | 6.298  | 6.328  | 6.359  | 6.389  | 6.420  | 240                         |  |
| 250   | 6.420  | 6.450  | 6.481  | 6.511  | 6.541  | 6.572  | 6.602  | 6.633  | 6.663  | 6.694  | 6.724  | 250                         |  |
| 260   | 6.724  | 6.755  | 6.785  | 6.816  | 6.846  | 6.877  | 6.907  | 6.938  | 6.968  | 6.999  | 7.029  | 260                         |  |
| 270   | 7.029  | 7.060  | 7.090  | 7.121  | 7.151  | 7.182  | 7.212  | 7.243  | 7.274  | 7.304  | 7.335  | 270                         |  |
| 280   | 7.335  | 7.365  | 7.396  | 7.426  | 7.457  | 7.488  | 7.518  | 7.549  | 7.579  | 7.610  | 7.641  | 280                         |  |
| 290   | 7.641  | 7.671  | 7.702  | 7.732  | 7.763  | 7.794  | 7.824  | 7.855  | 7.885  | 7.916  | 7.947  | 290                         |  |
| 300   | 7.947  | 7.977  | 8.008  | 8.039  | 8.069  | 8.100  | 8.131  | 8.161  | 8.192  | 8.223  | 8.253  | 300                         |  |
| 310   | 8.253  | 8.284  | 8.315  | 8.345  | 8.376  | 8.407  | 8.437  | 8.468  | 8.499  | 8.530  | 8.560  | 310                         |  |
| 320   | 8.560  | 8.591  | 8.622  | 8.652  | 8.683  | 8.714  | 8.745  | 8.775  | 8.806  | 8.837  | 8.867  | 320                         |  |
| 330   | 8.867  | 8.898  | 8.929  | 8.960  | 8.990  | 9.021  | 9.052  | 9.083  | 9.113  | 9.144  | 9.175  | 330                         |  |
| 340   | 9.175  | 9.206  | 9.236  | 9.267  | 9.298  | 9.329  | 9.359  | 9.390  | 9.421  | 9.452  | 9.483  | 340                         |  |
| 350   | 9.483  | 9.513  | 9.544  | 9.575  | 9.606  | 9.636  | 9.667  | 9.698  | 9.729  | 9.760  | 9.790  | 350                         |  |
| 360   | 9.790  | 9.821  | 9.852  | 9.883  | 9.914  | 9.944  | 9.975  | 10.006 | 10.037 | 10.068 | 10.098 | 360                         |  |
| 370   | 10.098 | 10.129   | 10.160 | 10.191 | 10.222 | 10.252 | 10.283 | 10.314 | 10.345 | 10.376 | 10.407 | 370                         |  |
| 380   | 10.407 | 10.437   | 10.468 | 10.499 | 10.530 | 10.561 | 10.592 | 10.622 | 10.653 | 10.684 | 10.715 | 380                         |  |
| 390   | 10.715 | 10.746   | 10.777 | 10.807 | 10.838 | 10.869 | 10.900 | 10.931 | 10.962 | 10.992 | 11.023 | 390                         |  |
| 400   | 11.023 | 11.054   | 11.085 | 11.116 | 11.147 | 11.177 | 11.208 | 11.239 | 11.270 | 11.301 | 11.332 | 400                         |  |
| 410   | 11.332 | 11.363   | 11.393 | 11.424 | 11.455 | 11.486 | 11.517 | 11.548 | 11.578 | 11.609 | 11.640 | 410                         |  |
| 420   | 11.640 | 11.671   | 11.702 | 11.733 | 11.764 | 11.794 | 11.825 | 11.856 | 11.887 | 11.918 | 11.949 | 420                         |  |
| 430   | 11.949 | 11.980   | 12.010 | 12.041 | 12.072 | 12.103 | 12.134 | 12.165 | 12.196 | 12.226 | 12.257 | 430                         |  |
| 440   | 12.257 | 12.288   | 12.319 | 12.350 | 12.381 | 12.411 | 12.442 | 12.473 | 12.504 | 12.535 | 12.566 | 440                         |  |
| 450   | 12.566 | 12.597   | 12.627 | 12.658 | 12.689 | 12.720 | 12.751 | 12.782 | 12.813 | 12.843 | 12.874 | 450                         |  |
| 460   | 12.874 | 12.905   | 12.936 | 12.967 | 12.998 | 13.029 | 13.059 | 13.090 | 13.121 | 13.152 | 13.183 | 460                         |  |
| 470   | 13.183 | 13.214   | 13.244 | 13.275 | 13.306 | 13.337 | 13.368 | 13.399 | 13.430 | 13.460 | 13.491 | 470                         |  |
| 480   | 13.491 | 13.522   | 13.553 | 13.584 | 13.615 | 13.645 | 13.676 | 13.707 | 13.738 | 13.769 | 13.800 | 480                         |  |
| 490   | 13.800 | 13.830   | 13.861 | 13.892 | 13.923 | 13.954 | 13.985 | 14.015 | 14.046 | 14.077 | 14.108 | 490                         |  |
| 500   | 14.108 | 14.139   | 14.170 | 14.200 | 14.231 | 14.262 | 14.293 | 14.324 | 14.355 | 14.385 | 14.416 | 500                         |  |
| 510   | 14.416 | 14.447   | 14.478 | 14.509 | 14.539 | 14.570 | 14.601 | 14.632 | 14.663 | 14.694 | 14.724 | 510                         |  |
| 520   | 14.724 | 14.755   | 14.786 | 14.817 | 14.848 | 14.878 | 14.909 | 14.940 | 14.971 | 15.002 | 15.032 | 520                         |  |
| 530   | 15.032 | 15.063   | 15.094 | 15.125 | 15.156 | 15.186 | 15.217 | 15.248 | 15.279 | 15.310 | 15.340 | 530                         |  |
| 540   | 15.340 | 15.371   | 15.402 | 15.433 | 15.464 | 15.494 | 15.525 | 15.556 | 15.587 | 15.617 | 15.648 | 540                         |  |
| 550   | 15.648 | 15.679   | 15.710 | 15.741 | 15.771 | 15.802 | 15.833 | 15.864 | 15.894 | 15.925 | 15.956 | 550                         |  |
| 560   | 15.956 | 15.987   | 16.018 | 16.048 | 16.079 | 16.110 | 16.141 | 16.171 | 16.202 | 16.233 | 16.264 | 560                         |  |
| 570   | 16.264 | 16.294   | 16.325 | 16.356 | 16.387 | 16.417 | 16.448 | 16.479 | 16.510 | 16.540 | 16.571 | 570                         |  |
| 580   | 16.571 | 16.602   | 16.633 | 16.663 | 16.694 | 16.725 | 16.756 | 16.786 | 16.817 | 16.848 | 16.879 | 580                         |  |
| 590   | 16.879 | 16.909   | 16.940 | 16.971 | 17.001 | 17.032 | 17.063 | 17.094 | 17.124 | 17.155 | 17.186 | 590                         |  |
| 600   | 17.186 | 17.217   | 17.247 | 17.278 | 17.309 | 17.339 | 17.370 | 17.401 | 17.432 | 17.462 | 17.493 | 600                         |  |
| 610   | 17.493 | 17.524   | 17.554 | 17.585 | 17.616 | 17.646 | 17.677 | 17.708 | 17.739 | 17.769 | 17.800 | 610                         |  |
| 620   | 17.800 | 17.831   | 17.861 | 17.892 | 17.923 | 17.953 | 17.984 | 18.015 | 18.046 | 18.076 | 18.107 | 620                         |  |
| 630   | 18.107 | 18.138   | 18.168 | 18.199 | 18.230 | 18.260 | 18.291 | 18.322 | 18.352 | 18.383 | 18.414 | 630                         |  |
| 640   | 18.414 | 18.444   | 18.475 | 18.506 | 18.537 | 18.567 | 18.598 | 18.629 | 18.659 | 18.690 | 18.721 | 640                         |  |
| 650   | 18.721 | 18.751   | 18.782 | 18.813 | 18.843 | 18.874 | 18.905 | 18.935 | 18.966 | 18.997 | 19.027 | 650                         |  |
| 660   | 19.027 | 19.058   | 19.089 | 19.119 | 19.150 | 19.180 | 19.211 | 19.242 | 19.272 | 19.303 | 19.334 | 660                         |  |
| 670   | 19.334 | 19.364   | 19.395 | 19.426 | 19.456 | 19.487 | 19.518 | 19.548 | 19.579 | 19.610 | 19.640 | 670                         |  |
| 680   | 19.640 | 19.671   | 19.702 | 19.732 | 19.763 | 19.793 | 19.824 | 19.855 | 19.885 | 19.916 | 19.947 | 680                         |  |
| 690   | 19.947 | 19.977   | 20.008 | 20.039 | 20.069 | 20.100 | 20.131 | 20.161 | 20.192 | 20.222 | 20.253 | 690                         |  |
| 700   | 20.253 | 20.284   | 20.314 | 20.345 | 20.376 | 20.406 | 20.437 | 20.467 | 20.498 | 20.529 | 20.559 | 700                         |  |
| 710   | 20.559 | 20.590   | 20.621 | 20.651 | 20.682 | 20.713 | 20.743 | 20.774 | 20.804 | 20.835 | 20.866 | 710                         |  |
| 720   | 20.866 | 20.896   | 20.927 | 20.958 | 20.988 | 21.019 | 21.049 | 21.080 | 21.111 | 21.141 | 21.172 | 720                         |  |
| 730   | 21.172 | 21.203   | 21.233 | 21.264 | 21.295 | 21.325 | 21.356 | 21.386 | 21.417 | 21.448 | 21.478 | 730                         |  |
| 740   | 21.478 | 21.509   | 21.540 | 21.570 | 21.601 | 21.631 | 21.662 | 21.693 | 21.723 | 21.754 | 21.785 | 740                         |  |
| 750   | 21.785 | 21.815   | 21.846 | 21.877 | 21.907 | 21.938 | 21.968 | 21.999 | 22.030 | 22.060 | 22.091 | 750                         |  |
| 760   | 22.091 | 22.122   | 22.152 | 22.183 | 22.214 | 22.244 | 22.275 | 22.305 | 22.336 | 22.366 | 22.397 | 760                         |  |
| 770   | 22.397 | 22.428   | 22.459 | 22.489 | 22.520 | 22.551 | 22.581 | 22.612 | 22.643 | 22.673 | 22.704 | 770                         |  |
| 780   | 22.704 | 22.735   | 22.765 | 22.796 | 22.826 | 22.857 | 22.888 | 22.918 | 22.949 | 22.980 | 23.010 | 780                         |  |
| 790   | 23.010 | 23.041   | 23.072 | 23.102 | 23.133 | 23.164 | 23.194 | 23.225 | 23.256 | 23.286 | 23.317 | 790                         |  |
| DEG F   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |

<sup>a</sup> Converted from degrees Celsius (IPTS 1968)



TABLE 10.6—Type J thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit* |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|------------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
|   |        | DEG F                              | 0      | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      |                             |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |                                    |        |        |        |        |        |        |        |        |        |                             |  |
| 800   | 23.317 | 23.348                             | 23.378 | 23.409 | 23.440 | 23.471 | 23.501 | 23.532 | 23.563 | 23.593 | 23.624 | 800                         |  |
| 810   | 23.624 | 23.655                             | 23.685 | 23.716 | 23.747 | 23.777 | 23.808 | 23.839 | 23.870 | 23.900 | 23.931 | 810                         |  |
| 820   | 23.931 | 23.962                             | 23.992 | 24.023 | 24.054 | 24.085 | 24.115 | 24.146 | 24.177 | 24.207 | 24.238 | 820                         |  |
| 830   | 24.238 | 24.269                             | 24.300 | 24.330 | 24.361 | 24.392 | 24.423 | 24.453 | 24.484 | 24.515 | 24.546 | 830                         |  |
| 840   | 24.546 | 24.576                             | 24.607 | 24.638 | 24.669 | 24.699 | 24.730 | 24.761 | 24.792 | 24.822 | 24.853 | 840                         |  |
| 850   | 24.853 | 24.884                             | 24.915 | 24.946 | 24.976 | 25.007 | 25.038 | 25.069 | 25.099 | 25.130 | 25.161 | 850                         |  |
| 860   | 25.161 | 25.192                             | 25.223 | 25.254 | 25.284 | 25.315 | 25.346 | 25.377 | 25.408 | 25.438 | 25.469 | 860                         |  |
| 870   | 25.469 | 25.500                             | 25.531 | 25.562 | 25.593 | 25.623 | 25.654 | 25.685 | 25.716 | 25.747 | 25.778 | 870                         |  |
| 880   | 25.778 | 25.809                             | 25.840 | 25.870 | 25.901 | 25.932 | 25.963 | 25.994 | 26.025 | 26.056 | 26.087 | 880                         |  |
| 890   | 26.087 | 26.118                             | 26.148 | 26.179 | 26.210 | 26.241 | 26.272 | 26.303 | 26.334 | 26.365 | 26.396 | 890                         |  |
| 900   | 26.396 | 26.427                             | 26.458 | 26.489 | 26.520 | 26.551 | 26.582 | 26.613 | 26.644 | 26.675 | 26.705 | 900                         |  |
| 910   | 26.705 | 26.736                             | 26.767 | 26.798 | 26.829 | 26.860 | 26.891 | 26.922 | 26.953 | 26.984 | 27.015 | 910                         |  |
| 920   | 27.016 | 27.047                             | 27.078 | 27.109 | 27.140 | 27.171 | 27.202 | 27.233 | 27.264 | 27.295 | 27.326 | 920                         |  |
| 930   | 27.326 | 27.357                             | 27.388 | 27.419 | 27.450 | 27.482 | 27.513 | 27.544 | 27.575 | 27.606 | 27.637 | 930                         |  |
| 940   | 27.637 | 27.668                             | 27.699 | 27.731 | 27.762 | 27.793 | 27.824 | 27.855 | 27.886 | 27.917 | 27.949 | 940                         |  |
| 950   | 27.949 | 27.980                             | 28.011 | 28.042 | 28.073 | 28.105 | 28.136 | 28.167 | 28.198 | 28.230 | 28.261 | 950                         |  |
| 960   | 28.261 | 28.292                             | 28.323 | 28.355 | 28.386 | 28.417 | 28.448 | 28.480 | 28.511 | 28.542 | 28.573 | 960                         |  |
| 970   | 28.573 | 28.605                             | 28.636 | 28.667 | 28.699 | 28.730 | 28.761 | 28.793 | 28.824 | 28.855 | 28.887 | 970                         |  |
| 980   | 28.887 | 28.918                             | 28.950 | 28.981 | 29.012 | 29.044 | 29.075 | 29.107 | 29.138 | 29.169 | 29.201 | 980                         |  |
| 990   | 29.201 | 29.232                             | 29.264 | 29.295 | 29.327 | 29.358 | 29.390 | 29.421 | 29.452 | 29.484 | 29.515 | 990                         |  |
| 1000  | 29.515 | 29.547                             | 29.578 | 29.610 | 29.642 | 29.673 | 29.705 | 29.736 | 29.768 | 29.799 | 29.831 | 1000                        |  |
| 1010  | 29.831 | 29.862                             | 29.894 | 29.926 | 29.957 | 29.989 | 30.020 | 30.052 | 30.084 | 30.115 | 30.147 | 1010                        |  |
| 1020  | 30.147 | 30.179                             | 30.210 | 30.242 | 30.274 | 30.305 | 30.337 | 30.369 | 30.400 | 30.432 | 30.464 | 1020                        |  |
| 1030  | 30.464 | 30.496                             | 30.527 | 30.559 | 30.591 | 30.623 | 30.654 | 30.686 | 30.718 | 30.750 | 30.782 | 1030                        |  |
| 1040  | 30.782 | 30.813                             | 30.845 | 30.877 | 30.909 | 30.941 | 30.973 | 31.005 | 31.036 | 31.068 | 31.100 | 1040                        |  |
| 1050  | 31.100 | 31.132                             | 31.164 | 31.196 | 31.228 | 31.260 | 31.292 | 31.324 | 31.356 | 31.388 | 31.420 | 1050                        |  |
| 1060  | 31.420 | 31.452                             | 31.484 | 31.516 | 31.548 | 31.580 | 31.612 | 31.644 | 31.676 | 31.708 | 31.740 | 1060                        |  |
| 1070  | 31.740 | 31.772                             | 31.804 | 31.836 | 31.868 | 31.901 | 31.933 | 31.965 | 31.997 | 32.029 | 32.061 | 1070                        |  |
| 1080  | 32.061 | 32.094                             | 32.126 | 32.158 | 32.190 | 32.222 | 32.255 | 32.287 | 32.319 | 32.351 | 32.384 | 1080                        |  |
| 1090  | 32.384 | 32.416                             | 32.448 | 32.480 | 32.513 | 32.545 | 32.577 | 32.610 | 32.642 | 32.674 | 32.707 | 1090                        |  |
| 1100  | 32.707 | 32.739                             | 32.772 | 32.804 | 32.836 | 32.869 | 32.901 | 32.934 | 32.966 | 32.999 | 33.031 | 1100                        |  |
| 1110  | 33.031 | 33.064                             | 33.096 | 33.129 | 33.161 | 33.194 | 33.226 | 33.259 | 33.291 | 33.324 | 33.356 | 1110                        |  |
| 1120  | 33.356 | 33.389                             | 33.422 | 33.454 | 33.487 | 33.519 | 33.552 | 33.585 | 33.617 | 33.650 | 33.683 | 1120                        |  |
| 1130  | 33.683 | 33.715                             | 33.748 | 33.781 | 33.814 | 33.846 | 33.879 | 33.912 | 33.945 | 33.977 | 34.010 | 1130                        |  |
| 1140  | 34.010 | 34.043                             | 34.076 | 34.109 | 34.141 | 34.174 | 34.207 | 34.240 | 34.273 | 34.306 | 34.339 | 1140                        |  |
| 1150  | 34.339 | 34.372                             | 34.405 | 34.437 | 34.470 | 34.503 | 34.536 | 34.569 | 34.602 | 34.635 | 34.668 | 1150                        |  |
| 1160  | 34.668 | 34.701                             | 34.734 | 34.767 | 34.801 | 34.834 | 34.867 | 34.900 | 34.933 | 34.966 | 34.999 | 1160                        |  |
| 1170  | 34.999 | 35.032                             | 35.065 | 35.099 | 35.132 | 35.165 | 35.198 | 35.231 | 35.265 | 35.298 | 35.331 | 1170                        |  |
| 1180  | 35.331 | 35.364                             | 35.398 | 35.431 | 35.464 | 35.498 | 35.531 | 35.564 | 35.598 | 35.631 | 35.664 | 1180                        |  |
| 1190  | 35.664 | 35.698                             | 35.731 | 35.764 | 35.798 | 35.831 | 35.865 | 35.898 | 35.932 | 35.965 | 35.999 | 1190                        |  |
| 1200  | 35.999 | 36.032                             | 36.066 | 36.099 | 36.133 | 36.166 | 36.200 | 36.233 | 36.267 | 36.301 | 36.334 | 1200                        |  |
| 1210  | 36.334 | 36.368                             | 36.401 | 36.435 | 36.469 | 36.502 | 36.536 | 36.570 | 36.603 | 36.637 | 36.671 | 1210                        |  |
| 1220  | 36.671 | 36.705                             | 36.738 | 36.772 | 36.806 | 36.840 | 36.873 | 36.907 | 36.941 | 36.975 | 37.009 | 1220                        |  |
| 1230  | 37.009 | 37.043                             | 37.076 | 37.110 | 37.144 | 37.178 | 37.212 | 37.246 | 37.280 | 37.314 | 37.348 | 1230                        |  |
| 1240  | 37.348 | 37.382                             | 37.416 | 37.450 | 37.484 | 37.518 | 37.552 | 37.586 | 37.620 | 37.654 | 37.688 | 1240                        |  |
| 1250  | 37.688 | 37.722                             | 37.756 | 37.790 | 37.825 | 37.859 | 37.893 | 37.927 | 37.961 | 37.995 | 38.030 | 1250                        |  |
| 1260  | 38.030 | 38.064                             | 38.098 | 38.132 | 38.167 | 38.201 | 38.235 | 38.269 | 38.304 | 38.338 | 38.372 | 1260                        |  |
| 1270  | 38.372 | 38.407                             | 38.441 | 38.475 | 38.510 | 38.544 | 38.578 | 38.613 | 38.647 | 38.682 | 38.716 | 1270                        |  |
| 1280  | 38.716 | 38.751                             | 38.785 | 38.819 | 38.854 | 38.888 | 38.923 | 38.957 | 38.992 | 39.027 | 39.061 | 1280                        |  |
| 1290  | 39.061 | 39.096                             | 39.130 | 39.165 | 39.199 | 39.234 | 39.269 | 39.303 | 39.338 | 39.373 | 39.407 | 1290                        |  |
| 1300  | 39.407 | 39.442                             | 39.477 | 39.511 | 39.546 | 39.581 | 39.615 | 39.650 | 39.685 | 39.720 | 39.754 | 1300                        |  |
| 1310  | 39.754 | 39.789                             | 39.824 | 39.859 | 39.894 | 39.928 | 39.963 | 39.998 | 40.033 | 40.068 | 40.103 | 1310                        |  |
| 1320  | 40.103 | 40.138                             | 40.172 | 40.207 | 40.242 | 40.277 | 40.312 | 40.347 | 40.382 | 40.417 | 40.452 | 1320                        |  |
| 1330  | 40.452 | 40.487                             | 40.522 | 40.557 | 40.592 | 40.627 | 40.662 | 40.697 | 40.732 | 40.767 | 40.802 | 1330                        |  |
| 1340  | 40.802 | 40.837                             | 40.872 | 40.908 | 40.943 | 40.978 | 41.013 | 41.048 | 41.083 | 41.118 | 41.154 | 1340                        |  |
| 1350  | 41.154 | 41.189                             | 41.224 | 41.259 | 41.294 | 41.329 | 41.365 | 41.400 | 41.435 | 41.470 | 41.506 | 1350                        |  |
| 1360  | 41.506 | 41.541                             | 41.576 | 41.611 | 41.647 | 41.682 | 41.717 | 41.753 | 41.788 | 41.823 | 41.859 | 1360                        |  |
| 1370  | 41.859 | 41.894                             | 41.929 | 41.965 | 42.000 | 42.035 | 42.071 | 42.106 | 42.142 | 42.177 | 42.212 | 1370                        |  |
| 1380  | 42.212 | 42.248                             | 42.283 | 42.319 | 42.354 | 42.390 | 42.425 | 42.460 | 42.496 | 42.531 | 42.567 | 1380                        |  |
| 1390  | 42.567 | 42.602                             | 42.638 | 42.673 | 42.709 | 42.744 | 42.780 | 42.815 | 42.851 | 42.886 | 42.922 | 1390                        |  |

\* Converted from degrees Celsius (ITS 1968).

TABLE 10.6—Type J thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit* |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|------------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
| DEG F   | 0      | 1                                  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |                                    |        |        |        |        |        |        |        |        |        |                             |  |
| 1.400   | 42.922 | 42.957                             | 42.993 | 43.029 | 43.064 | 43.100 | 43.135 | 43.171 | 43.207 | 43.242 | 43.278 | 1.400                       |  |
| 1.410   | 43.278 | 43.313                             | 43.349 | 43.385 | 43.420 | 43.456 | 43.492 | 43.527 | 43.563 | 43.599 | 43.635 | 1.410                       |  |
| 1.420   | 43.635 | 43.670                             | 43.706 | 43.742 | 43.777 | 43.813 | 43.849 | 43.885 | 43.921 | 43.956 | 43.992 | 1.420                       |  |
| 1.430   | 43.992 | 44.028                             | 44.064 | 44.099 | 44.135 | 44.171 | 44.207 | 44.243 | 44.279 | 44.314 | 44.350 | 1.430                       |  |
| 1.440   | 44.350 | 44.386                             | 44.422 | 44.458 | 44.494 | 44.530 | 44.565 | 44.601 | 44.637 | 44.673 | 44.709 | 1.440                       |  |
| 1.450   | 44.709 | 44.745                             | 44.780 | 44.816 | 44.852 | 44.888 | 44.924 | 44.960 | 44.996 | 45.032 | 45.067 | 1.450                       |  |
| 1.460   | 45.067 | 45.103                             | 45.139 | 45.175 | 45.211 | 45.247 | 45.283 | 45.319 | 45.355 | 45.391 | 45.426 | 1.460                       |  |
| 1.470   | 45.426 | 45.462                             | 45.498 | 45.534 | 45.570 | 45.606 | 45.642 | 45.678 | 45.714 | 45.749 | 45.785 | 1.470                       |  |
| 1.480   | 45.785 | 45.821                             | 45.857 | 45.893 | 45.929 | 45.965 | 46.001 | 46.037 | 46.072 | 46.108 | 46.144 | 1.480                       |  |
| 1.490   | 46.144 | 46.180                             | 46.216 | 46.252 | 46.288 | 46.324 | 46.359 | 46.395 | 46.431 | 46.467 | 46.503 | 1.490                       |  |
| 1.500   | 46.503 | 46.539                             | 46.575 | 46.610 | 46.646 | 46.682 | 46.718 | 46.754 | 46.790 | 46.825 | 46.861 | 1.500                       |  |
| 1.510   | 46.861 | 46.897                             | 46.933 | 46.969 | 47.005 | 47.040 | 47.076 | 47.112 | 47.148 | 47.183 | 47.219 | 1.510                       |  |
| 1.520   | 47.219 | 47.255                             | 47.291 | 47.327 | 47.362 | 47.398 | 47.434 | 47.470 | 47.505 | 47.541 | 47.577 | 1.520                       |  |
| 1.530   | 47.577 | 47.612                             | 47.648 | 47.684 | 47.720 | 47.755 | 47.791 | 47.827 | 47.862 | 47.898 | 47.934 | 1.530                       |  |
| 1.540   | 47.934 | 47.969                             | 48.005 | 48.041 | 48.076 | 48.112 | 48.147 | 48.183 | 48.219 | 48.254 | 48.290 | 1.540                       |  |
| 1.550   | 48.290 | 48.325                             | 48.361 | 48.397 | 48.432 | 48.468 | 48.503 | 48.539 | 48.574 | 48.610 | 48.645 | 1.550                       |  |
| 1.560   | 48.645 | 48.681                             | 48.716 | 48.752 | 48.787 | 48.823 | 48.858 | 48.894 | 48.929 | 48.965 | 49.000 | 1.560                       |  |
| 1.570   | 49.000 | 49.036                             | 49.071 | 49.107 | 49.142 | 49.177 | 49.213 | 49.248 | 49.283 | 49.319 | 49.354 | 1.570                       |  |
| 1.580   | 49.354 | 49.390                             | 49.425 | 49.460 | 49.496 | 49.531 | 49.566 | 49.601 | 49.637 | 49.672 | 49.707 | 1.580                       |  |
| 1.590   | 49.707 | 49.743                             | 49.778 | 49.813 | 49.848 | 49.883 | 49.919 | 49.954 | 49.989 | 50.024 | 50.059 | 1.590                       |  |
| 1.600   | 50.059 | 50.095                             | 50.130 | 50.165 | 50.200 | 50.235 | 50.270 | 50.305 | 50.340 | 50.376 | 50.411 | 1.600                       |  |
| 1.610   | 50.411 | 50.446                             | 50.481 | 50.516 | 50.551 | 50.586 | 50.621 | 50.656 | 50.691 | 50.726 | 50.761 | 1.610                       |  |
| 1.620   | 50.761 | 50.796                             | 50.831 | 50.866 | 50.901 | 50.936 | 50.970 | 51.005 | 51.040 | 51.075 | 51.110 | 1.620                       |  |
| 1.630   | 51.111 | 51.145                             | 51.180 | 51.215 | 51.249 | 51.284 | 51.319 | 51.354 | 51.389 | 51.423 | 51.458 | 1.630                       |  |
| 1.640   | 51.458 | 51.493                             | 51.528 | 51.562 | 51.597 | 51.632 | 51.667 | 51.701 | 51.736 | 51.771 | 51.805 | 1.640                       |  |
| 1.650   | 51.805 | 51.840                             | 51.875 | 51.909 | 51.944 | 51.978 | 52.013 | 52.048 | 52.082 | 52.117 | 52.151 | 1.650                       |  |
| 1.660   | 52.151 | 52.186                             | 52.220 | 52.255 | 52.289 | 52.324 | 52.358 | 52.393 | 52.427 | 52.462 | 52.496 | 1.660                       |  |
| 1.670   | 52.496 | 52.531                             | 52.565 | 52.600 | 52.634 | 52.668 | 52.703 | 52.737 | 52.772 | 52.806 | 52.840 | 1.670                       |  |
| 1.680   | 52.840 | 52.875                             | 52.909 | 52.943 | 52.977 | 53.011 | 53.046 | 53.080 | 53.115 | 53.149 | 53.183 | 1.680                       |  |
| 1.690   | 53.183 | 53.217                             | 53.251 | 53.286 | 53.320 | 53.354 | 53.388 | 53.423 | 53.457 | 53.491 | 53.525 | 1.690                       |  |
| 1.700   | 53.525 | 53.559                             | 53.593 | 53.627 | 53.661 | 53.695 | 53.729 | 53.763 | 53.797 | 53.831 | 53.865 | 1.700                       |  |
| 1.710   | 53.865 | 53.899                             | 53.933 | 53.967 | 54.001 | 54.035 | 54.069 | 54.103 | 54.137 | 54.171 | 54.205 | 1.710                       |  |
| 1.720   | 54.205 | 54.239                             | 54.273 | 54.307 | 54.341 | 54.374 | 54.408 | 54.442 | 54.476 | 54.510 | 54.544 | 1.720                       |  |
| 1.730   | 54.544 | 54.577                             | 54.611 | 54.645 | 54.679 | 54.712 | 54.746 | 54.780 | 54.814 | 54.847 | 54.881 | 1.730                       |  |
| 1.740   | 54.881 | 54.915                             | 54.948 | 54.982 | 55.016 | 55.049 | 55.083 | 55.117 | 55.150 | 55.184 | 55.218 | 1.740                       |  |
| 1.750   | 55.218 | 55.251                             | 55.285 | 55.318 | 55.352 | 55.385 | 55.419 | 55.453 | 55.486 | 55.520 | 55.553 | 1.750                       |  |
| 1.760   | 55.553 | 55.587                             | 55.620 | 55.654 | 55.687 | 55.720 | 55.754 | 55.787 | 55.821 | 55.854 | 55.888 | 1.760                       |  |
| 1.770   | 55.888 | 55.921                             | 55.954 | 55.988 | 56.021 | 56.055 | 56.088 | 56.121 | 56.155 | 56.188 | 56.221 | 1.770                       |  |
| 1.780   | 56.221 | 56.255                             | 56.288 | 56.321 | 56.354 | 56.388 | 56.421 | 56.454 | 56.487 | 56.521 | 56.554 | 1.780                       |  |
| 1.790   | 56.554 | 56.587                             | 56.620 | 56.654 | 56.687 | 56.720 | 56.753 | 56.786 | 56.819 | 56.853 | 56.886 | 1.790                       |  |
| 1.800   | 56.886 | 56.919                             | 56.952 | 56.985 | 57.018 | 57.051 | 57.084 | 57.118 | 57.151 | 57.184 | 57.217 | 1.800                       |  |
| 1.810   | 57.217 | 57.250                             | 57.283 | 57.316 | 57.349 | 57.382 | 57.415 | 57.448 | 57.481 | 57.514 | 57.547 | 1.810                       |  |
| 1.820   | 57.547 | 57.580                             | 57.613 | 57.646 | 57.679 | 57.712 | 57.745 | 57.778 | 57.810 | 57.843 | 57.876 | 1.820                       |  |
| 1.830   | 57.876 | 57.909                             | 57.942 | 57.975 | 58.008 | 58.041 | 58.074 | 58.106 | 58.139 | 58.172 | 58.205 | 1.830                       |  |
| 1.840   | 58.205 | 58.238                             | 58.271 | 58.303 | 58.336 | 58.369 | 58.402 | 58.435 | 58.467 | 58.500 | 58.533 | 1.840                       |  |
| 1.850   | 58.533 | 58.566                             | 58.598 | 58.631 | 58.664 | 58.697 | 58.729 | 58.762 | 58.795 | 58.827 | 58.860 | 1.850                       |  |
| 1.860   | 58.860 | 58.893                             | 58.926 | 58.958 | 58.991 | 59.024 | 59.056 | 59.089 | 59.121 | 59.154 | 59.187 | 1.860                       |  |
| 1.870   | 59.187 | 59.219                             | 59.252 | 59.285 | 59.317 | 59.350 | 59.382 | 59.415 | 59.448 | 59.480 | 59.513 | 1.870                       |  |
| 1.880   | 59.513 | 59.545                             | 59.578 | 59.610 | 59.643 | 59.676 | 59.708 | 59.741 | 59.773 | 59.806 | 59.838 | 1.880                       |  |
| 1.890   | 59.838 | 59.871                             | 59.903 | 59.936 | 59.968 | 60.001 | 60.033 | 60.066 | 60.098 | 60.131 | 60.163 | 1.890                       |  |
| 1.900   | 60.163 | 60.196                             | 60.228 | 60.261 | 60.293 | 60.326 | 60.358 | 60.390 | 60.423 | 60.455 | 60.488 | 1.900                       |  |
| 1.910   | 60.488 | 60.520                             | 60.553 | 60.585 | 60.617 | 60.650 | 60.682 | 60.715 | 60.747 | 60.779 | 60.812 | 1.910                       |  |
| 1.920   | 60.812 | 60.844                             | 60.876 | 60.909 | 60.941 | 60.974 | 61.006 | 61.038 | 61.071 | 61.103 | 61.135 | 1.920                       |  |
| 1.930   | 61.135 | 61.168                             | 61.200 | 61.232 | 61.265 | 61.297 | 61.329 | 61.362 | 61.394 | 61.426 | 61.459 | 1.930                       |  |
| 1.940   | 61.459 | 61.491                             | 61.523 | 61.555 | 61.588 | 61.620 | 61.652 | 61.685 | 61.717 | 61.749 | 61.781 | 1.940                       |  |
| 1.950   | 61.781 | 61.814                             | 61.846 | 61.878 | 61.910 | 61.943 | 61.975 | 62.007 | 62.039 | 62.072 | 62.104 | 1.950                       |  |
| 1.960   | 62.104 | 62.136                             | 62.168 | 62.201 | 62.233 | 62.265 | 62.297 | 62.330 | 62.362 | 62.394 | 62.426 | 1.960                       |  |
| 1.970   | 62.426 | 62.458                             | 62.491 | 62.523 | 62.555 | 62.587 | 62.619 | 62.652 | 62.684 | 62.716 | 62.748 | 1.970                       |  |
| 1.980   | 62.748 | 62.780                             | 62.812 | 62.845 | 62.877 | 62.909 | 62.941 | 62.974 | 63.006 | 63.038 | 63.070 | 1.980                       |  |
| 1.990   | 63.070 | 63.102                             | 63.134 | 63.167 | 63.199 | 63.231 | 63.263 | 63.295 | 63.327 | 63.359 | 63.392 | 1.990                       |  |

\* Converted from degrees Celsius (IPTS 1968).

TABLE 10.6—Type J thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit <sup>a</sup> |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
| DEG F   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                             |  |
| 2,000   | 63.392 | 63.424   | 63.456 | 63.488 | 63.520 | 63.552 | 63.584 | 63.617 | 63.649 | 63.681 | 63.713 | 2,000                       |  |
| 2,010   | 63.713 | 63.745   | 63.777 | 63.809 | 63.842 | 63.874 | 63.906 | 63.938 | 63.970 | 64.002 | 64.034 | 2,010                       |  |
| 2,020   | 64.034 | 64.066   | 64.098 | 64.131 | 64.163 | 64.195 | 64.227 | 64.259 | 64.291 | 64.323 | 64.355 | 2,020                       |  |
| 2,030   | 64.355 | 64.387   | 64.420 | 64.452 | 64.484 | 64.516 | 64.548 | 64.580 | 64.612 | 64.644 | 64.676 | 2,030                       |  |
| 2,040   | 64.676 | 64.708   | 64.740 | 64.773 | 64.805 | 64.837 | 64.869 | 64.901 | 64.933 | 64.965 | 64.997 | 2,040                       |  |
| 2,050   | 64.997 | 65.029   | 65.061 | 65.093 | 65.125 | 65.158 | 65.190 | 65.222 | 65.254 | 65.286 | 65.318 | 2,050                       |  |
| 2,060   | 65.318 | 65.350   | 65.382 | 65.414 | 65.446 | 65.478 | 65.510 | 65.542 | 65.574 | 65.606 | 65.638 | 2,060                       |  |
| 2,070   | 65.638 | 65.671   | 65.703 | 65.735 | 65.767 | 65.799 | 65.831 | 65.863 | 65.895 | 65.927 | 65.959 | 2,070                       |  |
| 2,080   | 65.959 | 65.991   | 66.023 | 66.055 | 66.087 | 66.119 | 66.151 | 66.183 | 66.215 | 66.247 | 66.279 | 2,080                       |  |
| 2,090   | 66.279 | 66.311   | 66.343 | 66.375 | 66.407 | 66.439 | 66.472 | 66.504 | 66.536 | 66.568 | 66.600 | 2,090                       |  |
| 2,100   | 66.600 | 66.632   | 66.664 | 66.696 | 66.728 | 66.760 | 66.792 | 66.824 | 66.856 | 66.888 | 66.920 | 2,100                       |  |
| 2,110   | 66.920 | 66.952   | 66.984 | 67.016 | 67.048 | 67.080 | 67.112 | 67.144 | 67.176 | 67.208 | 67.240 | 2,110                       |  |
| 2,120   | 67.240 | 67.272   | 67.304 | 67.336 | 67.368 | 67.400 | 67.432 | 67.464 | 67.495 | 67.527 | 67.559 | 2,120                       |  |
| 2,130   | 67.559 | 67.591   | 67.623 | 67.655 | 67.687 | 67.719 | 67.751 | 67.783 | 67.815 | 67.847 | 67.879 | 2,130                       |  |
| 2,140   | 67.879 | 67.911   | 67.943 | 67.975 | 68.007 | 68.039 | 68.071 | 68.103 | 68.134 | 68.166 | 68.198 | 2,140                       |  |
| 2,150   | 68.198 | 68.230   | 68.262 | 68.294 | 68.326 | 68.358 | 68.390 | 68.422 | 68.454 | 68.486 | 68.517 | 2,150                       |  |
| 2,160   | 68.517 | 68.549   | 68.581 | 68.613 | 68.645 | 68.677 | 68.709 | 68.741 | 68.772 | 68.804 | 68.836 | 2,160                       |  |
| 2,170   | 68.836 | 68.868   | 68.900 | 68.932 | 68.964 | 68.995 | 69.027 | 69.059 | 69.091 | 69.123 | 69.155 | 2,170                       |  |
| 2,180   | 69.155 | 69.186   | 69.218 | 69.250 | 69.282 | 69.314 | 69.345 | 69.377 | 69.409 | 69.441 | 69.472 | 2,180                       |  |
| 2,190   | 69.472 | 69.504   | 69.536 |        |        |        |        |        |        |        |        | 2,190                       |  |
| DEG F   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |

<sup>a</sup> Converted from degrees Celsius (IPTS 1968).

TABLE 10.7—Type J thermocouples (deg C-millivolts).

NOTE—The maximum recommended temperature limit for Type J thermocouples is 1400 F (760 C) as specified in Table 2. Extension of the Type J tables beyond 1400 F gives temperature - electromotive force data to 2192 F (1200 C). This extension is a mathematical extrapolation based on limited calibration data and caution should be exercised in its use. The basis for the extended curve is discussed in *NBS Monograph 125*.

It should be noted that limits of error for Type J thermocouples (Table 1) do not apply above 1400 F (760 C)

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Celsius (IPTS 1968) |        |        |        |        |        |        |        |        |        | Reference Junctions at 0 C |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------------------------|--|
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                            |  |
| -210  | -8.096 |  |        |        |        |        |        |        |        |        |        | -210                       |  |
| -200  | -7.890 | -7.912                                     | -7.934 | -7.955 | -7.976 | -7.996 | -8.017 | -8.037 | -8.057 | -8.076 | -8.096 | -200                       |  |
| -190  | -7.659 | -7.683                                     | -7.707 | -7.731 | -7.755 | -7.778 | -7.801 | -7.824 | -7.846 | -7.868 | -7.890 | -190                       |  |
| -180  | -7.402 | -7.429                                     | -7.455 | -7.482 | -7.508 | -7.533 | -7.559 | -7.584 | -7.609 | -7.634 | -7.659 | -180                       |  |
| -170  | -7.122 | -7.151                                     | -7.180 | -7.209 | -7.237 | -7.265 | -7.293 | -7.321 | -7.349 | -7.375 | -7.402 | -170                       |  |
| -160  | -6.821 | -6.852                                     | -6.883 | -6.914 | -6.944 | -6.974 | -7.004 | -7.034 | -7.064 | -7.093 | -7.122 | -160                       |  |
| -150  | -6.499 | -6.532                                     | -6.565 | -6.598 | -6.630 | -6.663 | -6.695 | -6.727 | -6.758 | -6.790 | -6.821 | -150                       |  |
| -140  | -6.159 | -6.194                                     | -6.228 | -6.263 | -6.297 | -6.331 | -6.365 | -6.399 | -6.433 | -6.466 | -6.499 | -140                       |  |
| -130  | -5.801 | -5.837                                     | -5.874 | -5.910 | -5.946 | -5.982 | -6.018 | -6.053 | -6.089 | -6.124 | -6.159 | -130                       |  |
| -120  | -5.426 | -5.464                                     | -5.502 | -5.540 | -5.578 | -5.615 | -5.653 | -5.690 | -5.727 | -5.764 | -5.801 | -120                       |  |
| -110  | -5.036 | -5.076                                     | -5.115 | -5.155 | -5.194 | -5.233 | -5.272 | -5.311 | -5.349 | -5.388 | -5.426 | -110                       |  |
| -100  | -4.632 | -4.673                                     | -4.714 | -4.755 | -4.795 | -4.836 | -4.876 | -4.916 | -4.956 | -4.996 | -5.036 | -100                       |  |
| -90   | -4.215 | -4.257                                     | -4.299 | -4.341 | -4.383 | -4.425 | -4.467 | -4.508 | -4.550 | -4.591 | -4.632 | -90                        |  |
| -80   | -3.785 | -3.829                                     | -3.872 | -3.915 | -3.958 | -4.001 | -4.044 | -4.087 | -4.130 | -4.172 | -4.215 | -80                        |  |
| -70   | -3.344 | -3.389                                     | -3.433 | -3.478 | -3.522 | -3.566 | -3.610 | -3.654 | -3.698 | -3.742 | -3.785 | -70                        |  |
| -60   | -2.892 | -2.938                                     | -2.984 | -3.029 | -3.074 | -3.120 | -3.165 | -3.210 | -3.255 | -3.299 | -3.344 | -60                        |  |
| -50   | -2.431 | -2.478                                     | -2.524 | -2.570 | -2.617 | -2.663 | -2.709 | -2.755 | -2.801 | -2.847 | -2.892 | -50                        |  |
| -40   | -1.960 | -2.008                                     | -2.055 | -2.102 | -2.150 | -2.197 | -2.244 | -2.291 | -2.338 | -2.384 | -2.431 | -40                        |  |
| -30   | -1.481 | -1.530                                     | -1.578 | -1.626 | -1.674 | -1.722 | -1.770 | -1.818 | -1.865 | -1.913 | -1.960 | -30                        |  |
| -20   | -0.995 | -1.044                                     | -1.093 | -1.141 | -1.190 | -1.239 | -1.288 | -1.336 | -1.385 | -1.433 | -1.481 | -20                        |  |
| -10   | -0.501 | -0.550                                     | -0.600 | -0.650 | -0.699 | -0.748 | -0.798 | -0.847 | -0.896 | -0.945 | -0.995 | -10                        |  |
| 0   | 0.000  | -0.050                                     | -0.101 | -0.151 | -0.201 | -0.251 | -0.301 | -0.351 | -0.401 | -0.451 | -0.501 | 0                          |  |
| 0   | 0.000  | 0.050                                      | 0.101  | 0.151  | 0.202  | 0.253  | 0.303  | 0.354  | 0.405  | 0.456  | 0.507  | 0                          |  |
| 10  | 0.507  | 0.558                                      | 0.609  | 0.660  | 0.711  | 0.762  | 0.813  | 0.865  | 0.916  | 0.967  | 1.019  | 10                         |  |
| 20  | 1.019  | 1.070                                      | 1.122  | 1.174  | 1.225  | 1.277  | 1.329  | 1.381  | 1.432  | 1.484  | 1.536  | 20                         |  |
| 30  | 1.536  | 1.588                                      | 1.640  | 1.693  | 1.745  | 1.797  | 1.849  | 1.901  | 1.954  | 2.006  | 2.058  | 30                         |  |
| 40  | 2.058  | 2.111                                      | 2.163  | 2.216  | 2.268  | 2.321  | 2.374  | 2.426  | 2.479  | 2.532  | 2.585  | 40                         |  |
| 50  | 2.585  | 2.638                                      | 2.691  | 2.743  | 2.796  | 2.849  | 2.902  | 2.955  | 3.009  | 3.062  | 3.115  | 50                         |  |
| 60  | 3.115  | 3.168                                      | 3.221  | 3.273  | 3.326  | 3.381  | 3.435  | 3.488  | 3.542  | 3.595  | 3.649  | 60                         |  |
| 70  | 3.649  | 3.702                                      | 3.756  | 3.809  | 3.863  | 3.917  | 3.971  | 4.024  | 4.078  | 4.132  | 4.186  | 70                         |  |
| 80  | 4.186  | 4.239                                      | 4.293  | 4.347  | 4.401  | 4.455  | 4.509  | 4.563  | 4.617  | 4.671  | 4.725  | 80                         |  |
| 90  | 4.725  | 4.780                                      | 4.834  | 4.888  | 4.942  | 4.996  | 5.050  | 5.105  | 5.159  | 5.213  | 5.268  | 90                         |  |
| 100   | 5.268  | 5.322                                      | 5.376  | 5.431  | 5.485  | 5.540  | 5.594  | 5.649  | 5.703  | 5.758  | 5.812  | 100                        |  |
| 110   | 5.812  | 5.867                                      | 5.921  | 5.976  | 6.031  | 6.085  | 6.140  | 6.195  | 6.249  | 6.304  | 6.359  | 110                        |  |
| 120   | 6.359  | 6.414                                      | 6.468  | 6.523  | 6.578  | 6.633  | 6.688  | 6.742  | 6.797  | 6.852  | 6.907  | 120                        |  |
| 130   | 6.907  | 6.962                                      | 7.017  | 7.072  | 7.127  | 7.182  | 7.237  | 7.292  | 7.347  | 7.402  | 7.457  | 130                        |  |
| 140   | 7.457  | 7.512                                      | 7.567  | 7.622  | 7.677  | 7.732  | 7.787  | 7.843  | 7.898  | 7.953  | 8.008  | 140                        |  |
| 150   | 8.008  | 8.063                                      | 8.118  | 8.174  | 8.229  | 8.284  | 8.339  | 8.394  | 8.449  | 8.505  | 8.560  | 150                        |  |
| 160   | 8.560  | 8.616                                      | 8.671  | 8.726  | 8.781  | 8.837  | 8.892  | 8.947  | 9.003  | 9.058  | 9.113  | 160                        |  |
| 170   | 9.113  | 9.169                                      | 9.224  | 9.279  | 9.335  | 9.390  | 9.446  | 9.501  | 9.556  | 9.612  | 9.667  | 170                        |  |
| 180   | 9.667  | 9.723                                      | 9.778  | 9.834  | 9.889  | 9.944  | 10.000 | 10.055 | 10.111 | 10.166 | 10.222 | 180                        |  |
| 190   | 10.222 | 10.277                                     | 10.333 | 10.388 | 10.444 | 10.499 | 10.555 | 10.610 | 10.666 | 10.721 | 10.777 | 190                        |  |
| 200   | 10.777 | 10.832                                     | 10.888 | 10.943 | 10.999 | 11.054 | 11.110 | 11.165 | 11.221 | 11.276 | 11.332 | 200                        |  |
| 210   | 11.332 | 11.387                                     | 11.443 | 11.498 | 11.554 | 11.609 | 11.665 | 11.720 | 11.776 | 11.831 | 11.887 | 210                        |  |
| 220   | 11.887 | 11.943                                     | 11.998 | 12.054 | 12.109 | 12.165 | 12.220 | 12.276 | 12.331 | 12.387 | 12.442 | 220                        |  |
| 230   | 12.442 | 12.498                                     | 12.553 | 12.609 | 12.664 | 12.720 | 12.776 | 12.831 | 12.887 | 12.942 | 12.998 | 230                        |  |
| 240   | 12.998 | 13.053                                     | 13.109 | 13.164 | 13.220 | 13.275 | 13.331 | 13.386 | 13.442 | 13.497 | 13.553 | 240                        |  |
| 250   | 13.553 | 13.608                                     | 13.664 | 13.719 | 13.775 | 13.830 | 13.886 | 13.941 | 13.997 | 14.052 | 14.108 | 250                        |  |
| 260   | 14.108 | 14.163                                     | 14.219 | 14.274 | 14.330 | 14.385 | 14.441 | 14.496 | 14.552 | 14.607 | 14.663 | 260                        |  |
| 270   | 14.663 | 14.718                                     | 14.774 | 14.829 | 14.885 | 14.940 | 14.995 | 15.051 | 15.106 | 15.162 | 15.217 | 270                        |  |
| 280   | 15.217 | 15.273                                     | 15.328 | 15.383 | 15.439 | 15.494 | 15.550 | 15.605 | 15.661 | 15.716 | 15.771 | 280                        |  |
| 290   | 15.771 | 15.827                                     | 15.882 | 15.938 | 15.993 | 16.048 | 16.104 | 16.159 | 16.214 | 16.270 | 16.325 | 290                        |  |
| 300   | 16.325 | 16.380                                     | 16.436 | 16.491 | 16.547 | 16.602 | 16.657 | 16.713 | 16.768 | 16.823 | 16.879 | 300                        |  |
| 310   | 16.879 | 16.934                                     | 16.989 | 17.044 | 17.100 | 17.155 | 17.210 | 17.266 | 17.321 | 17.376 | 17.432 | 310                        |  |
| 320   | 17.432 | 17.487                                     | 17.542 | 17.597 | 17.653 | 17.708 | 17.763 | 17.818 | 17.873 | 17.928 | 17.984 | 320                        |  |
| 330   | 17.984 | 18.039                                     | 18.095 | 18.150 | 18.205 | 18.260 | 18.316 | 18.371 | 18.426 | 18.481 | 18.537 | 330                        |  |
| 340   | 18.537 | 18.592                                     | 18.647 | 18.702 | 18.757 | 18.813 | 18.868 | 18.923 | 18.978 | 19.033 | 19.089 | 340                        |  |

| DEG C | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | DEG C |
|-------|---|---|---|---|---|---|---|---|---|---|----|-------|
|-------|---|---|---|---|---|---|---|---|---|---|----|-------|

TABLE 10.7—Type J thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Celsius (IPTS 1968) |        |        |        |        |        |        |        |        |        | Reference Junctions at 0 C |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------------------------|--|
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                            |  |
| 350   | 19.089 | 19.144                                     | 19.199 | 19.254 | 19.309 | 19.364 | 19.420 | 19.475 | 19.530 | 19.585 | 19.640 | 350                        |  |
| 360   | 19.640 | 19.695                                     | 19.751 | 19.806 | 19.861 | 19.916 | 19.971 | 20.026 | 20.081 | 20.137 | 20.192 | 360                        |  |
| 370   | 20.192 | 20.247                                     | 20.302 | 20.357 | 20.412 | 20.467 | 20.523 | 20.578 | 20.633 | 20.688 | 20.743 | 370                        |  |
| 380   | 20.743 | 20.798                                     | 20.853 | 20.909 | 20.964 | 21.019 | 21.074 | 21.129 | 21.184 | 21.239 | 21.295 | 380                        |  |
| 390   | 21.295 | 21.350                                     | 21.405 | 21.460 | 21.515 | 21.570 | 21.625 | 21.680 | 21.736 | 21.791 | 21.846 | 390                        |  |
| 400   | 21.846 | 21.901                                     | 21.956 | 22.011 | 22.066 | 22.122 | 22.177 | 22.232 | 22.287 | 22.342 | 22.397 | 400                        |  |
| 410   | 22.397 | 22.452                                     | 22.507 | 22.562 | 22.618 | 22.673 | 22.728 | 22.783 | 22.838 | 22.893 | 22.948 | 410                        |  |
| 420   | 22.949 | 23.004                                     | 23.059 | 23.115 | 23.170 | 23.225 | 23.280 | 23.336 | 23.391 | 23.446 | 23.501 | 420                        |  |
| 430   | 23.501 | 23.556                                     | 23.612 | 23.667 | 23.722 | 23.777 | 23.833 | 23.888 | 23.943 | 23.999 | 24.054 | 430                        |  |
| 440   | 24.054 | 24.109                                     | 24.164 | 24.220 | 24.275 | 24.330 | 24.386 | 24.441 | 24.496 | 24.552 | 24.607 | 440                        |  |
| 450   | 24.607 | 24.662                                     | 24.718 | 24.773 | 24.829 | 24.884 | 24.939 | 24.995 | 25.050 | 25.106 | 25.161 | 450                        |  |
| 460   | 25.161 | 25.217                                     | 25.272 | 25.327 | 25.383 | 25.438 | 25.494 | 25.549 | 25.605 | 25.661 | 25.716 | 460                        |  |
| 470   | 25.716 | 25.772                                     | 25.827 | 25.883 | 25.938 | 25.994 | 26.050 | 26.105 | 26.161 | 26.216 | 26.272 | 470                        |  |
| 480   | 26.272 | 26.328                                     | 26.383 | 26.439 | 26.495 | 26.551 | 26.606 | 26.662 | 26.718 | 26.774 | 26.829 | 480                        |  |
| 490   | 26.829 | 26.885                                     | 26.941 | 26.997 | 27.053 | 27.109 | 27.165 | 27.220 | 27.276 | 27.332 | 27.388 | 490                        |  |
| 500   | 27.388 | 27.444                                     | 27.500 | 27.556 | 27.612 | 27.668 | 27.724 | 27.780 | 27.836 | 27.892 | 27.948 | 500                        |  |
| 510   | 27.949 | 28.005                                     | 28.061 | 28.117 | 28.173 | 28.229 | 28.286 | 28.342 | 28.398 | 28.455 | 28.511 | 510                        |  |
| 520   | 28.511 | 28.567                                     | 28.624 | 28.680 | 28.736 | 28.793 | 28.849 | 28.906 | 28.962 | 29.019 | 29.075 | 520                        |  |
| 530   | 29.075 | 29.132                                     | 29.188 | 29.245 | 29.301 | 29.358 | 29.415 | 29.471 | 29.528 | 29.585 | 29.642 | 530                        |  |
| 540   | 29.642 | 29.699                                     | 29.755 | 29.812 | 29.869 | 29.926 | 29.983 | 30.039 | 30.096 | 30.153 | 30.210 | 540                        |  |
| 550   | 30.210 | 30.267                                     | 30.324 | 30.381 | 30.439 | 30.496 | 30.553 | 30.610 | 30.667 | 30.724 | 30.782 | 550                        |  |
| 560   | 30.782 | 30.839                                     | 30.896 | 30.954 | 31.011 | 31.068 | 31.126 | 31.183 | 31.241 | 31.298 | 31.356 | 560                        |  |
| 570   | 31.356 | 31.413                                     | 31.471 | 31.528 | 31.586 | 31.644 | 31.702 | 31.759 | 31.817 | 31.875 | 31.933 | 570                        |  |
| 580   | 31.933 | 31.991                                     | 32.048 | 32.106 | 32.164 | 32.222 | 32.280 | 32.338 | 32.396 | 32.455 | 32.513 | 580                        |  |
| 590   | 32.513 | 32.571                                     | 32.629 | 32.687 | 32.746 | 32.804 | 32.862 | 32.921 | 32.979 | 33.038 | 33.096 | 590                        |  |
| 600   | 33.096 | 33.155                                     | 33.213 | 33.272 | 33.330 | 33.389 | 33.448 | 33.506 | 33.565 | 33.624 | 33.683 | 600                        |  |
| 610   | 33.683 | 33.742                                     | 33.800 | 33.859 | 33.918 | 33.977 | 34.036 | 34.095 | 34.155 | 34.214 | 34.273 | 610                        |  |
| 620   | 34.273 | 34.332                                     | 34.391 | 34.451 | 34.510 | 34.569 | 34.629 | 34.688 | 34.748 | 34.807 | 34.867 | 620                        |  |
| 630   | 34.867 | 34.926                                     | 34.985 | 35.045 | 35.105 | 35.165 | 35.225 | 35.285 | 35.344 | 35.404 | 35.464 | 630                        |  |
| 640   | 35.464 | 35.524                                     | 35.584 | 35.644 | 35.704 | 35.764 | 35.825 | 35.885 | 35.945 | 36.005 | 36.066 | 640                        |  |
| 650   | 36.066 | 36.126                                     | 36.186 | 36.247 | 36.307 | 36.368 | 36.428 | 36.489 | 36.549 | 36.610 | 36.671 | 650                        |  |
| 660   | 36.671 | 36.732                                     | 36.792 | 36.853 | 36.914 | 36.975 | 37.036 | 37.097 | 37.158 | 37.219 | 37.280 | 660                        |  |
| 670   | 37.280 | 37.341                                     | 37.402 | 37.463 | 37.525 | 37.586 | 37.647 | 37.709 | 37.770 | 37.831 | 37.893 | 670                        |  |
| 680   | 37.893 | 37.954                                     | 38.016 | 38.078 | 38.139 | 38.201 | 38.262 | 38.324 | 38.386 | 38.448 | 38.510 | 680                        |  |
| 690   | 38.510 | 38.572                                     | 38.633 | 38.695 | 38.757 | 38.819 | 38.882 | 38.944 | 39.006 | 39.068 | 39.130 | 690                        |  |
| 700   | 39.130 | 39.192                                     | 39.255 | 39.317 | 39.379 | 39.442 | 39.504 | 39.567 | 39.629 | 39.692 | 39.754 | 700                        |  |
| 710   | 39.754 | 39.817                                     | 39.880 | 39.942 | 40.005 | 40.068 | 40.131 | 40.193 | 40.256 | 40.319 | 40.382 | 710                        |  |
| 720   | 40.382 | 40.445                                     | 40.508 | 40.571 | 40.634 | 40.697 | 40.760 | 40.823 | 40.886 | 40.950 | 41.013 | 720                        |  |
| 730   | 41.013 | 41.076                                     | 41.139 | 41.203 | 41.266 | 41.329 | 41.393 | 41.456 | 41.520 | 41.583 | 41.647 | 730                        |  |
| 740   | 41.647 | 41.710                                     | 41.774 | 41.837 | 41.901 | 41.965 | 42.028 | 42.092 | 42.156 | 42.219 | 42.283 | 740                        |  |
| 750   | 42.283 | 42.347                                     | 42.411 | 42.475 | 42.538 | 42.602 | 42.666 | 42.730 | 42.794 | 42.858 | 42.922 | 750                        |  |
| 760   | 42.922 | 42.986                                     | 43.050 | 43.114 | 43.178 | 43.242 | 43.306 | 43.370 | 43.435 | 43.499 | 43.563 | 760                        |  |
| 770   | 43.563 | 43.627                                     | 43.692 | 43.756 | 43.820 | 43.885 | 43.949 | 44.014 | 44.078 | 44.142 | 44.207 | 770                        |  |
| 780   | 44.207 | 44.271                                     | 44.336 | 44.400 | 44.465 | 44.529 | 44.594 | 44.658 | 44.723 | 44.788 | 44.852 | 780                        |  |
| 790   | 44.852 | 44.917                                     | 44.981 | 45.046 | 45.111 | 45.175 | 45.240 | 45.304 | 45.369 | 45.434 | 45.498 | 790                        |  |
| 800   | 45.498 | 45.563                                     | 45.627 | 45.692 | 45.757 | 45.821 | 45.886 | 45.950 | 46.015 | 46.080 | 46.144 | 800                        |  |
| 810   | 46.144 | 46.209                                     | 46.273 | 46.338 | 46.403 | 46.467 | 46.532 | 46.596 | 46.661 | 46.725 | 46.790 | 810                        |  |
| 820   | 46.790 | 46.855                                     | 46.919 | 46.983 | 47.047 | 47.112 | 47.176 | 47.241 | 47.305 | 47.369 | 47.434 | 820                        |  |
| 830   | 47.434 | 47.498                                     | 47.562 | 47.627 | 47.691 | 47.755 | 47.819 | 47.884 | 47.948 | 48.012 | 48.076 | 830                        |  |
| 840   | 48.076 | 48.140                                     | 48.204 | 48.269 | 48.333 | 48.397 | 48.461 | 48.525 | 48.589 | 48.653 | 48.716 | 840                        |  |
| 850   | 48.716 | 48.780                                     | 48.844 | 48.908 | 48.972 | 49.036 | 49.099 | 49.163 | 49.227 | 49.291 | 49.354 | 850                        |  |
| 860   | 49.354 | 49.418                                     | 49.481 | 49.545 | 49.608 | 49.672 | 49.735 | 49.799 | 49.862 | 49.926 | 49.989 | 860                        |  |
| 870   | 49.989 | 50.052                                     | 50.116 | 50.179 | 50.242 | 50.305 | 50.369 | 50.432 | 50.495 | 50.558 | 50.621 | 870                        |  |
| 880   | 50.621 | 50.684                                     | 50.747 | 50.810 | 50.873 | 50.936 | 50.999 | 51.061 | 51.124 | 51.187 | 51.249 | 880                        |  |
| 890   | 51.249 | 51.312                                     | 51.375 | 51.437 | 51.500 | 51.562 | 51.625 | 51.687 | 51.750 | 51.812 | 51.875 | 890                        |  |
| 900   | 51.875 | 51.937                                     | 51.999 | 52.061 | 52.124 | 52.186 | 52.248 | 52.310 | 52.372 | 52.434 | 52.496 | 900                        |  |
| 910   | 52.496 | 52.558                                     | 52.620 | 52.682 | 52.744 | 52.806 | 52.868 | 52.929 | 52.991 | 53.053 | 53.115 | 910                        |  |
| 920   | 53.115 | 53.176                                     | 53.238 | 53.299 | 53.361 | 53.422 | 53.484 | 53.545 | 53.607 | 53.668 | 53.729 | 920                        |  |
| 930   | 53.729 | 53.791                                     | 53.852 | 53.913 | 53.974 | 54.035 | 54.096 | 54.157 | 54.218 | 54.280 | 54.341 | 930                        |  |
| 940   | 54.341 | 54.401                                     | 54.462 | 54.523 | 54.584 | 54.645 | 54.706 | 54.766 | 54.827 | 54.888 | 54.948 | 940                        |  |
| 950   | 54.948 | 55.009                                     | 55.070 | 55.130 | 55.191 | 55.251 | 55.312 | 55.372 | 55.432 | 55.493 | 55.553 | 950                        |  |
| 960   | 55.553 | 55.613                                     | 55.674 | 55.734 | 55.794 | 55.854 | 55.914 | 55.974 | 56.035 | 56.095 | 56.155 | 960                        |  |
| 970   | 56.155 | 56.215                                     | 56.275 | 56.334 | 56.394 | 56.454 | 56.514 | 56.574 | 56.634 | 56.693 | 56.753 | 970                        |  |
| 980   | 56.753 | 56.813                                     | 56.873 | 56.932 | 56.992 | 57.051 | 57.111 | 57.170 | 57.230 | 57.289 | 57.349 | 980                        |  |
| 990   | 57.349 | 57.408                                     | 57.468 | 57.527 | 57.586 | 57.646 | 57.705 | 57.764 | 57.824 | 57.883 | 57.942 | 990                        |  |

DEG C 0 1 2 3 4 5 6 7 8 9 10 DEG C

TABLE 10.7—Type J thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Celsius (IPTS 1968) |        |        |        |        |        |        |        |        |        | Reference Junctions at 0 C |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------------------------|--|
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                            |  |
| 1.000   | 57.942 | 58.001                                     | 58.060 | 58.120 | 58.179 | 58.238 | 58.297 | 58.356 | 58.415 | 58.474 | 58.533 | 1.000                      |  |
| 1.010   | 58.533 | 58.592                                     | 58.651 | 58.710 | 58.769 | 58.827 | 58.886 | 58.945 | 59.004 | 59.063 | 59.121 | 1.010                      |  |
| 1.020   | 59.121 | 59.180                                     | 59.239 | 59.298 | 59.356 | 59.415 | 59.474 | 59.532 | 59.591 | 59.650 | 59.708 | 1.020                      |  |
| 1.030   | 59.708 | 59.767                                     | 59.825 | 59.884 | 59.942 | 60.001 | 60.059 | 60.118 | 60.176 | 60.235 | 60.293 | 1.030                      |  |
| 1.040   | 60.293 | 60.351                                     | 60.410 | 60.468 | 60.527 | 60.585 | 60.643 | 60.702 | 60.760 | 60.818 | 60.876 | 1.040                      |  |
| 1.050   | 60.876 | 60.935                                     | 60.993 | 61.051 | 61.109 | 61.168 | 61.226 | 61.284 | 61.342 | 61.400 | 61.459 | 1.050                      |  |
| 1.060   | 61.459 | 61.517                                     | 61.575 | 61.633 | 61.691 | 61.749 | 61.807 | 61.865 | 61.923 | 61.981 | 62.039 | 1.060                      |  |
| 1.070   | 62.039 | 62.097                                     | 62.156 | 62.214 | 62.272 | 62.330 | 62.388 | 62.446 | 62.504 | 62.562 | 62.619 | 1.070                      |  |
| 1.080   | 62.619 | 62.677                                     | 62.735 | 62.793 | 62.851 | 62.909 | 62.967 | 63.025 | 63.083 | 63.141 | 63.199 | 1.080                      |  |
| 1.090   | 63.199 | 63.257                                     | 63.314 | 63.372 | 63.430 | 63.488 | 63.546 | 63.604 | 63.662 | 63.719 | 63.777 | 1.090                      |  |
| 1.100   | 63.777 | 63.835                                     | 63.893 | 63.951 | 64.009 | 64.066 | 64.124 | 64.182 | 64.240 | 64.298 | 64.355 | 1.100                      |  |
| 1.110   | 64.355 | 64.413                                     | 64.471 | 64.529 | 64.586 | 64.644 | 64.702 | 64.760 | 64.817 | 64.875 | 64.933 | 1.110                      |  |
| 1.120   | 64.933 | 64.991                                     | 65.048 | 65.106 | 65.164 | 65.222 | 65.279 | 65.337 | 65.395 | 65.453 | 65.510 | 1.120                      |  |
| 1.130   | 65.510 | 65.568                                     | 65.626 | 65.683 | 65.741 | 65.799 | 65.856 | 65.914 | 65.972 | 66.029 | 66.087 | 1.130                      |  |
| 1.140   | 66.087 | 66.145                                     | 66.202 | 66.260 | 66.318 | 66.375 | 66.433 | 66.491 | 66.548 | 66.606 | 66.664 | 1.140                      |  |
| 1.150   | 66.664 | 66.721                                     | 66.779 | 66.836 | 66.894 | 66.952 | 67.009 | 67.067 | 67.124 | 67.182 | 67.240 | 1.150                      |  |
| 1.160   | 67.240 | 67.297                                     | 67.355 | 67.412 | 67.470 | 67.527 | 67.585 | 67.643 | 67.700 | 67.758 | 67.815 | 1.160                      |  |
| 1.170   | 67.815 | 67.873                                     | 67.930 | 67.988 | 68.045 | 68.103 | 68.160 | 68.217 | 68.275 | 68.332 | 68.390 | 1.170                      |  |
| 1.180   | 68.390 | 68.447                                     | 68.505 | 68.562 | 68.619 | 68.677 | 68.734 | 68.792 | 68.849 | 68.906 | 68.964 | 1.180                      |  |
| 1.190   | 68.964 | 69.021                                     | 69.078 | 69.135 | 69.193 | 69.250 | 69.307 | 69.364 | 69.422 | 69.479 | 69.536 | 1.190                      |  |
| 1.200   | 69.536 |  |        |        |        |        |        |        |        |        |        | 1.200                      |  |
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |

TABLE 10.8—Type K thermocouples (deg F-millivolts).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit* |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|------------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
| DEG F   | 0      | 1                                  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |                                    |        |        |        |        |        |        |        |        |        |                             |  |
| -450  | -6.456 | -6.456                             | -6.457 | -6.457 | -6.458 |        |        |        |        |        |        | -450                        |  |
| -440  | -6.447 | -6.448                             | -6.449 | -6.450 | -6.451 | -6.452 | -6.453 | -6.454 | -6.454 | -6.455 | -6.456 | -440                        |  |
| -430  | -6.431 | -6.433                             | -6.435 | -6.436 | -6.438 | -6.440 | -6.441 | -6.443 | -6.444 | -6.445 | -6.447 | -430                        |  |
| -420  | -6.409 | -6.411                             | -6.414 | -6.416 | -6.419 | -6.421 | -6.423 | -6.425 | -6.427 | -6.429 | -6.431 | -420                        |  |
| -410  | -6.380 | -6.383                             | -6.386 | -6.389 | -6.392 | -6.395 | -6.398 | -6.401 | -6.404 | -6.406 | -6.409 | -410                        |  |
| -400  | -6.344 | -6.348                             | -6.352 | -6.355 | -6.359 | -6.363 | -6.366 | -6.370 | -6.373 | -6.377 | -6.380 | -400                        |  |
| -390  | -6.301 | -6.306                             | -6.310 | -6.315 | -6.319 | -6.323 | -6.328 | -6.332 | -6.336 | -6.340 | -6.344 | -390                        |  |
| -380  | -6.251 | -6.257                             | -6.262 | -6.267 | -6.272 | -6.277 | -6.282 | -6.287 | -6.292 | -6.296 | -6.301 | -380                        |  |
| -370  | -6.195 | -6.201                             | -6.207 | -6.213 | -6.219 | -6.224 | -6.230 | -6.235 | -6.241 | -6.246 | -6.251 | -370                        |  |
| -360  | -6.133 | -6.139                             | -6.146 | -6.152 | -6.158 | -6.165 | -6.171 | -6.177 | -6.183 | -6.189 | -6.195 | -360                        |  |
| -350  | -6.064 | -6.071                             | -6.078 | -6.085 | -6.092 | -6.099 | -6.106 | -6.113 | -6.119 | -6.126 | -6.133 | -350                        |  |
| -340  | -5.989 | -5.997                             | -6.004 | -6.012 | -6.020 | -6.027 | -6.035 | -6.042 | -6.049 | -6.057 | -6.064 | -340                        |  |
| -330  | -5.908 | -5.917                             | -5.925 | -5.933 | -5.941 | -5.949 | -5.957 | -5.965 | -5.973 | -5.981 | -5.989 | -330                        |  |
| -320  | -5.822 | -5.831                             | -5.839 | -5.848 | -5.857 | -5.866 | -5.874 | -5.883 | -5.891 | -5.900 | -5.908 | -320                        |  |
| -310  | -5.730 | -5.739                             | -5.748 | -5.758 | -5.767 | -5.776 | -5.786 | -5.795 | -5.804 | -5.813 | -5.822 | -310                        |  |
| -300  | -5.632 | -5.642                             | -5.652 | -5.662 | -5.672 | -5.682 | -5.691 | -5.701 | -5.711 | -5.720 | -5.730 | -300                        |  |
| -290  | -5.529 | -5.540                             | -5.550 | -5.561 | -5.571 | -5.581 | -5.592 | -5.602 | -5.612 | -5.622 | -5.632 | -290                        |  |
| -280  | -5.421 | -5.432                             | -5.443 | -5.454 | -5.465 | -5.476 | -5.487 | -5.497 | -5.508 | -5.519 | -5.529 | -280                        |  |
| -270  | -5.308 | -5.319                             | -5.331 | -5.342 | -5.354 | -5.365 | -5.376 | -5.388 | -5.399 | -5.410 | -5.421 | -270                        |  |
| -260  | -5.190 | -5.202                             | -5.214 | -5.226 | -5.238 | -5.249 | -5.261 | -5.273 | -5.285 | -5.296 | -5.308 | -260                        |  |
| -250  | -5.067 | -5.079                             | -5.092 | -5.104 | -5.116 | -5.129 | -5.141 | -5.153 | -5.165 | -5.178 | -5.190 | -250                        |  |
| -240  | -4.939 | -4.952                             | -4.965 | -4.978 | -4.990 | -5.003 | -5.016 | -5.029 | -5.041 | -5.054 | -5.067 | -240                        |  |
| -230  | -4.806 | -4.819                             | -4.833 | -4.846 | -4.860 | -4.873 | -4.886 | -4.899 | -4.912 | -4.926 | -4.939 | -230                        |  |
| -220  | -4.669 | -4.683                             | -4.697 | -4.710 | -4.724 | -4.738 | -4.752 | -4.765 | -4.779 | -4.792 | -4.806 | -220                        |  |
| -210  | -4.527 | -4.541                             | -4.556 | -4.570 | -4.584 | -4.598 | -4.613 | -4.627 | -4.641 | -4.655 | -4.669 | -210                        |  |
| -200  | -4.381 | -4.396                             | -4.410 | -4.425 | -4.440 | -4.454 | -4.469 | -4.484 | -4.498 | -4.512 | -4.527 | -200                        |  |
| -190  | -4.230 | -4.245                             | -4.261 | -4.276 | -4.291 | -4.306 | -4.321 | -4.336 | -4.351 | -4.366 | -4.381 | -190                        |  |
| -180  | -4.075 | -4.091                             | -4.107 | -4.122 | -4.138 | -4.153 | -4.168 | -4.183 | -4.215 | -4.230 | -4.245 | -180                        |  |
| -170  | -3.917 | -3.933                             | -3.949 | -3.965 | -3.981 | -3.997 | -4.012 | -4.028 | -4.044 | -4.060 | -4.075 | -170                        |  |
| -160  | -3.754 | -3.770                             | -3.787 | -3.803 | -3.819 | -3.836 | -3.852 | -3.868 | -3.884 | -3.901 | -3.917 | -160                        |  |
| -150  | -3.587 | -3.604                             | -3.621 | -3.637 | -3.654 | -3.671 | -3.688 | -3.704 | -3.721 | -3.737 | -3.754 | -150                        |  |
| -140  | -3.417 | -3.434                             | -3.451 | -3.468 | -3.485 | -3.502 | -3.519 | -3.536 | -3.553 | -3.570 | -3.587 | -140                        |  |
| -130  | -3.242 | -3.260                             | -3.277 | -3.295 | -3.312 | -3.330 | -3.347 | -3.365 | -3.382 | -3.399 | -3.417 | -130                        |  |
| -120  | -3.065 | -3.082                             | -3.100 | -3.118 | -3.136 | -3.154 | -3.172 | -3.189 | -3.207 | -3.225 | -3.242 | -120                        |  |
| -110  | -2.883 | -2.902                             | -2.920 | -2.938 | -2.956 | -2.974 | -2.992 | -3.010 | -3.029 | -3.047 | -3.065 | -110                        |  |
| -100  | -2.699 | -2.717                             | -2.736 | -2.754 | -2.773 | -2.791 | -2.810 | -2.828 | -2.847 | -2.865 | -2.883 | -100                        |  |
| -90   | -2.511 | -2.530                             | -2.549 | -2.567 | -2.586 | -2.605 | -2.624 | -2.643 | -2.661 | -2.680 | -2.699 | -90                         |  |
| -80   | -2.320 | -2.339                             | -2.358 | -2.377 | -2.397 | -2.416 | -2.435 | -2.454 | -2.473 | -2.492 | -2.511 | -80                         |  |
| -70   | -2.126 | -2.145                             | -2.165 | -2.184 | -2.204 | -2.223 | -2.243 | -2.262 | -2.281 | -2.300 | -2.320 | -70                         |  |
| -60   | -1.929 | -1.949                             | -1.968 | -1.988 | -2.008 | -2.028 | -2.047 | -2.067 | -2.087 | -2.106 | -2.126 | -60                         |  |
| -50   | -1.729 | -1.749                             | -1.769 | -1.789 | -1.809 | -1.829 | -1.849 | -1.869 | -1.889 | -1.909 | -1.929 | -50                         |  |
| -40   | -1.527 | -1.547                             | -1.567 | -1.588 | -1.608 | -1.628 | -1.648 | -1.669 | -1.689 | -1.709 | -1.729 | -40                         |  |
| -30   | -1.322 | -1.342                             | -1.363 | -1.383 | -1.404 | -1.424 | -1.445 | -1.465 | -1.486 | -1.506 | -1.527 | -30                         |  |
| -20   | -1.114 | -1.135                             | -1.156 | -1.177 | -1.197 | -1.218 | -1.239 | -1.260 | -1.280 | -1.301 | -1.322 | -20                         |  |
| -10   | -0.904 | -0.925                             | -0.946 | -0.968 | -0.989 | -1.010 | -1.031 | -1.051 | -1.072 | -1.093 | -1.114 | -10                         |  |
| 0   | -0.692 | -0.714                             | -0.735 | -0.756 | -0.777 | -0.799 | -0.820 | -0.841 | -0.862 | -0.883 | -0.904 | 0                           |  |
| 0   | -0.692 | -0.671                             | -0.650 | -0.628 | -0.607 | -0.585 | -0.564 | -0.543 | -0.521 | -0.500 | -0.478 | 0                           |  |
| 10  | -0.478 | -0.457                             | -0.435 | -0.413 | -0.392 | -0.370 | -0.349 | -0.327 | -0.305 | -0.284 | -0.262 | 10                          |  |
| 20  | -0.262 | -0.240                             | -0.218 | -0.197 | -0.175 | -0.153 | -0.131 | -0.109 | -0.088 | -0.066 | -0.044 | 20                          |  |
| 30  | -0.044 | -0.022                             | 0.000  | 0.022  | 0.044  | 0.066  | 0.088  | 0.110  | 0.132  | 0.154  | 0.176  | 30                          |  |
| 40  | 0.176  | 0.198                              | 0.220  | 0.242  | 0.264  | 0.286  | 0.308  | 0.331  | 0.353  | 0.375  | 0.397  | 40                          |  |
| 50  | 0.397  | 0.419                              | 0.441  | 0.464  | 0.486  | 0.508  | 0.530  | 0.553  | 0.575  | 0.597  | 0.619  | 50                          |  |
| 60  | 0.619  | 0.642                              | 0.664  | 0.686  | 0.709  | 0.731  | 0.753  | 0.776  | 0.798  | 0.821  | 0.843  | 60                          |  |
| 70  | 0.843  | 0.865                              | 0.888  | 0.910  | 0.933  | 0.955  | 0.978  | 1.000  | 1.023  | 1.045  | 1.068  | 70                          |  |
| 80  | 1.068  | 1.090                              | 1.113  | 1.135  | 1.158  | 1.181  | 1.203  | 1.226  | 1.248  | 1.271  | 1.294  | 80                          |  |
| 90  | 1.294  | 1.316                              | 1.339  | 1.362  | 1.384  | 1.407  | 1.430  | 1.452  | 1.475  | 1.498  | 1.520  | 90                          |  |
| 100   | 1.520  | 1.543                              | 1.566  | 1.589  | 1.611  | 1.634  | 1.657  | 1.680  | 1.703  | 1.725  | 1.748  | 100                         |  |
| 110   | 1.748  | 1.771                              | 1.794  | 1.817  | 1.839  | 1.862  | 1.885  | 1.908  | 1.931  | 1.954  | 1.977  | 110                         |  |
| 120   | 1.977  | 2.000                              | 2.022  | 2.045  | 2.068  | 2.091  | 2.114  | 2.137  | 2.160  | 2.183  | 2.206  | 120                         |  |
| 130   | 2.206  | 2.229                              | 2.252  | 2.275  | 2.298  | 2.321  | 2.344  | 2.367  | 2.390  | 2.413  | 2.436  | 130                         |  |
| 140   | 2.436  | 2.459                              | 2.482  | 2.505  | 2.528  | 2.551  | 2.574  | 2.597  | 2.620  | 2.643  | 2.666  | 140                         |  |

\* Converted from degrees Celsius (IPTS 1968).

TABLE 10.8—Type K thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit <sup>a</sup> |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
| DEG F   | °      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                             |  |
| 150   | 2.666  | 2.689  | 2.712  | 2.735  | 2.758  | 2.781  | 2.804  | 2.827  | 2.850  | 2.873  | 2.896  | 150                         |  |
| 160   | 2.896  | 2.920  | 2.943  | 2.966  | 2.989  | 3.012  | 3.035  | 3.058  | 3.081  | 3.104  | 3.127  | 160                         |  |
| 170   | 3.127  | 3.150  | 3.173  | 3.196  | 3.220  | 3.243  | 3.266  | 3.289  | 3.312  | 3.335  | 3.358  | 170                         |  |
| 180   | 3.358  | 3.381  | 3.404  | 3.427  | 3.450  | 3.473  | 3.496  | 3.519  | 3.542  | 3.566  | 3.589  | 180                         |  |
| 190   | 3.589  | 3.612  | 3.635  | 3.658  | 3.681  | 3.704  | 3.727  | 3.750  | 3.773  | 3.796  | 3.819  | 190                         |  |
| 200   | 3.819  | 3.842  | 3.865  | 3.888  | 3.911  | 3.934  | 3.957  | 3.980  | 4.003  | 4.026  | 4.049  | 200                         |  |
| 210   | 4.049  | 4.072  | 4.095  | 4.118  | 4.141  | 4.164  | 4.187  | 4.210  | 4.233  | 4.256  | 4.279  | 210                         |  |
| 220   | 4.279  | 4.302  | 4.325  | 4.348  | 4.371  | 4.394  | 4.417  | 4.439  | 4.462  | 4.485  | 4.508  | 220                         |  |
| 230   | 4.508  | 4.531  | 4.554  | 4.577  | 4.600  | 4.622  | 4.645  | 4.668  | 4.691  | 4.714  | 4.737  | 230                         |  |
| 240   | 4.737  | 4.759  | 4.782  | 4.805  | 4.828  | 4.851  | 4.873  | 4.896  | 4.919  | 4.942  | 4.964  | 240                         |  |
| 250   | 4.964  | 4.987  | 5.010  | 5.033  | 5.055  | 5.078  | 5.101  | 5.124  | 5.146  | 5.169  | 5.192  | 250                         |  |
| 260   | 5.192  | 5.214  | 5.237  | 5.260  | 5.282  | 5.305  | 5.327  | 5.350  | 5.373  | 5.395  | 5.418  | 260                         |  |
| 270   | 5.418  | 5.440  | 5.463  | 5.486  | 5.508  | 5.531  | 5.553  | 5.576  | 5.598  | 5.621  | 5.643  | 270                         |  |
| 280   | 5.643  | 5.666  | 5.688  | 5.711  | 5.733  | 5.756  | 5.778  | 5.801  | 5.823  | 5.846  | 5.868  | 280                         |  |
| 290   | 5.868  | 5.891  | 5.913  | 5.936  | 5.958  | 5.980  | 6.003  | 6.025  | 6.048  | 6.070  | 6.092  | 290                         |  |
| 300   | 6.092  | 6.115  | 6.137  | 6.160  | 6.182  | 6.204  | 6.227  | 6.249  | 6.271  | 6.294  | 6.316  | 300                         |  |
| 310   | 6.316  | 6.338  | 6.361  | 6.383  | 6.405  | 6.428  | 6.450  | 6.472  | 6.494  | 6.517  | 6.539  | 310                         |  |
| 320   | 6.539  | 6.561  | 6.583  | 6.606  | 6.628  | 6.650  | 6.672  | 6.695  | 6.717  | 6.739  | 6.761  | 320                         |  |
| 330   | 6.761  | 6.784  | 6.806  | 6.828  | 6.850  | 6.873  | 6.895  | 6.917  | 6.939  | 6.961  | 6.984  | 330                         |  |
| 340   | 6.984  | 7.006  | 7.028  | 7.050  | 7.072  | 7.094  | 7.117  | 7.139  | 7.161  | 7.183  | 7.205  | 340                         |  |
| 350   | 7.205  | 7.228  | 7.250  | 7.272  | 7.294  | 7.316  | 7.338  | 7.361  | 7.383  | 7.405  | 7.427  | 350                         |  |
| 360   | 7.427  | 7.449  | 7.471  | 7.494  | 7.516  | 7.538  | 7.560  | 7.582  | 7.604  | 7.627  | 7.649  | 360                         |  |
| 370   | 7.649  | 7.671  | 7.693  | 7.715  | 7.737  | 7.760  | 7.782  | 7.804  | 7.826  | 7.848  | 7.870  | 370                         |  |
| 380   | 7.870  | 7.893  | 7.915  | 7.937  | 7.959  | 7.981  | 8.003  | 8.025  | 8.048  | 8.070  | 8.092  | 380                         |  |
| 390   | 8.092  | 8.114  | 8.137  | 8.159  | 8.181  | 8.203  | 8.225  | 8.248  | 8.270  | 8.292  | 8.314  | 390                         |  |
| 400   | 8.314  | 8.336  | 8.359  | 8.381  | 8.403  | 8.425  | 8.448  | 8.470  | 8.492  | 8.514  | 8.537  | 400                         |  |
| 410   | 8.537  | 8.559  | 8.581  | 8.603  | 8.626  | 8.648  | 8.670  | 8.692  | 8.715  | 8.737  | 8.759  | 410                         |  |
| 420   | 8.759  | 8.782  | 8.804  | 8.826  | 8.849  | 8.871  | 8.893  | 8.916  | 8.938  | 8.960  | 8.982  | 420                         |  |
| 430   | 8.983  | 9.005  | 9.027  | 9.050  | 9.072  | 9.094  | 9.117  | 9.139  | 9.161  | 9.184  | 9.206  | 430                         |  |
| 440   | 9.206  | 9.229  | 9.251  | 9.273  | 9.296  | 9.318  | 9.341  | 9.363  | 9.385  | 9.408  | 9.430  | 440                         |  |
| 450   | 9.430  | 9.453  | 9.475  | 9.498  | 9.520  | 9.543  | 9.565  | 9.588  | 9.610  | 9.633  | 9.655  | 450                         |  |
| 460   | 9.655  | 9.678  | 9.700  | 9.723  | 9.745  | 9.768  | 9.790  | 9.813  | 9.835  | 9.858  | 9.880  | 460                         |  |
| 470   | 9.880  | 9.903  | 9.926  | 9.948  | 9.971  | 9.993  | 10.016 | 10.038 | 10.061 | 10.084 | 10.106 | 470                         |  |
| 480   | 10.106 | 10.129   | 10.151 | 10.174 | 10.197 | 10.219 | 10.242 | 10.265 | 10.287 | 10.310 | 10.333 | 480                         |  |
| 490   | 10.333 | 10.355   | 10.378 | 10.401 | 10.423 | 10.446 | 10.469 | 10.491 | 10.514 | 10.537 | 10.560 | 490                         |  |
| 500   | 10.560 | 10.582   | 10.605 | 10.628 | 10.650 | 10.673 | 10.696 | 10.719 | 10.741 | 10.764 | 10.787 | 500                         |  |
| 510   | 10.787 | 10.810   | 10.833 | 10.855 | 10.878 | 10.901 | 10.924 | 10.947 | 10.969 | 10.992 | 11.015 | 510                         |  |
| 520   | 11.015 | 11.038   | 11.061 | 11.083 | 11.106 | 11.129 | 11.152 | 11.175 | 11.198 | 11.221 | 11.243 | 520                         |  |
| 530   | 11.243 | 11.266   | 11.289 | 11.312 | 11.335 | 11.358 | 11.381 | 11.404 | 11.426 | 11.449 | 11.472 | 530                         |  |
| 540   | 11.472 | 11.495   | 11.518 | 11.541 | 11.564 | 11.587 | 11.610 | 11.633 | 11.656 | 11.679 | 11.702 | 540                         |  |
| 550   | 11.702 | 11.725   | 11.748 | 11.770 | 11.793 | 11.816 | 11.839 | 11.862 | 11.885 | 11.908 | 11.931 | 550                         |  |
| 560   | 11.931 | 11.954   | 11.977 | 12.000 | 12.023 | 12.046 | 12.069 | 12.092 | 12.115 | 12.138 | 12.161 | 560                         |  |
| 570   | 12.161 | 12.184   | 12.207 | 12.230 | 12.254 | 12.277 | 12.300 | 12.323 | 12.346 | 12.369 | 12.392 | 570                         |  |
| 580   | 12.392 | 12.415   | 12.438 | 12.461 | 12.484 | 12.507 | 12.530 | 12.553 | 12.576 | 12.599 | 12.623 | 580                         |  |
| 590   | 12.623 | 12.646   | 12.669 | 12.692 | 12.715 | 12.738 | 12.761 | 12.784 | 12.807 | 12.831 | 12.854 | 590                         |  |
| 600   | 12.854 | 12.877   | 12.900 | 12.923 | 12.946 | 12.969 | 12.992 | 13.016 | 13.039 | 13.062 | 13.085 | 600                         |  |
| 610   | 13.085 | 13.108   | 13.131 | 13.154 | 13.178 | 13.201 | 13.224 | 13.247 | 13.270 | 13.293 | 13.317 | 610                         |  |
| 620   | 13.317 | 13.340   | 13.363 | 13.386 | 13.409 | 13.433 | 13.456 | 13.479 | 13.502 | 13.525 | 13.549 | 620                         |  |
| 630   | 13.549 | 13.572   | 13.595 | 13.618 | 13.641 | 13.665 | 13.688 | 13.711 | 13.734 | 13.757 | 13.781 | 630                         |  |
| 640   | 13.781 | 13.804   | 13.827 | 13.850 | 13.874 | 13.897 | 13.920 | 13.943 | 13.966 | 13.990 | 14.013 | 640                         |  |
| 650   | 14.013 | 14.036   | 14.060 | 14.083 | 14.106 | 14.129 | 14.153 | 14.176 | 14.199 | 14.222 | 14.246 | 650                         |  |
| 660   | 14.246 | 14.269   | 14.292 | 14.315 | 14.339 | 14.362 | 14.385 | 14.409 | 14.432 | 14.455 | 14.479 | 660                         |  |
| 670   | 14.479 | 14.502   | 14.525 | 14.548 | 14.572 | 14.595 | 14.618 | 14.642 | 14.665 | 14.688 | 14.712 | 670                         |  |
| 680   | 14.712 | 14.735   | 14.758 | 14.782 | 14.805 | 14.828 | 14.852 | 14.875 | 14.898 | 14.922 | 14.945 | 680                         |  |
| 690   | 14.945 | 14.968   | 14.992 | 15.015 | 15.038 | 15.062 | 15.085 | 15.108 | 15.132 | 15.155 | 15.178 | 690                         |  |
| 700   | 15.178 | 15.202   | 15.225 | 15.248 | 15.272 | 15.295 | 15.318 | 15.342 | 15.365 | 15.389 | 15.412 | 700                         |  |
| 710   | 15.412 | 15.435   | 15.459 | 15.482 | 15.505 | 15.529 | 15.552 | 15.576 | 15.599 | 15.622 | 15.646 | 710                         |  |
| 720   | 15.646 | 15.669   | 15.693 | 15.716 | 15.739 | 15.763 | 15.786 | 15.810 | 15.833 | 15.856 | 15.880 | 720                         |  |
| 730   | 15.880 | 15.903   | 15.927 | 15.950 | 15.974 | 15.997 | 16.020 | 16.044 | 16.067 | 16.091 | 16.114 | 730                         |  |
| 740   | 16.114 | 16.138   | 16.161 | 16.184 | 16.208 | 16.231 | 16.255 | 16.278 | 16.302 | 16.325 | 16.349 | 740                         |  |
| 750   | 16.349 | 16.372   | 16.395 | 16.419 | 16.442 | 16.466 | 16.489 | 16.513 | 16.536 | 16.560 | 16.583 | 750                         |  |
| 760   | 16.583 | 16.607   | 16.630 | 16.654 | 16.677 | 16.700 | 16.724 | 16.747 | 16.771 | 16.794 | 16.818 | 760                         |  |
| 770   | 16.818 | 16.841   | 16.865 | 16.888 | 16.912 | 16.935 | 16.959 | 16.982 | 17.006 | 17.029 | 17.053 | 770                         |  |
| 780   | 17.053 | 17.076   | 17.100 | 17.123 | 17.147 | 17.170 | 17.194 | 17.217 | 17.241 | 17.264 | 17.288 | 780                         |  |
| 790   | 17.288 | 17.311   | 17.335 | 17.358 | 17.382 | 17.406 | 17.429 | 17.453 | 17.476 | 17.500 | 17.523 | 790                         |  |

<sup>a</sup> Converted from degrees Celsius (IPTS 1968).



# 190 THE USE OF THERMOCOUPLES IN TEMPERATURE MEASUREMENT

## TABLE 10.8—Type *K* thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit* |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|------------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
| DEG F   | 0      | 1                                  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |                                    |        |        |        |        |        |        |        |        |        |                             |  |
| 800   | 17.523 | 17.547                             | 17.570 | 17.594 | 17.617 | 17.641 | 17.664 | 17.688 | 17.711 | 17.735 | 17.759 | 800                         |  |
| 810   | 17.759 | 17.782                             | 17.806 | 17.829 | 17.853 | 17.876 | 17.900 | 17.923 | 17.947 | 17.971 | 17.994 | 810                         |  |
| 820   | 17.994 | 18.018                             | 18.041 | 18.065 | 18.088 | 18.112 | 18.136 | 18.159 | 18.183 | 18.206 | 18.230 | 820                         |  |
| 830   | 18.230 | 18.253                             | 18.277 | 18.301 | 18.324 | 18.348 | 18.371 | 18.395 | 18.418 | 18.442 | 18.466 | 830                         |  |
| 840   | 18.466 | 18.489                             | 18.513 | 18.536 | 18.560 | 18.584 | 18.607 | 18.631 | 18.654 | 18.678 | 18.702 | 840                         |  |
| 850   | 18.702 | 18.725                             | 18.749 | 18.772 | 18.796 | 18.820 | 18.843 | 18.867 | 18.890 | 18.914 | 18.938 | 850                         |  |
| 860   | 18.938 | 18.961                             | 18.985 | 19.008 | 19.032 | 19.056 | 19.079 | 19.103 | 19.127 | 19.150 | 19.174 | 860                         |  |
| 870   | 19.174 | 19.197                             | 19.221 | 19.245 | 19.268 | 19.292 | 19.316 | 19.339 | 19.363 | 19.386 | 19.410 | 870                         |  |
| 880   | 19.410 | 19.434                             | 19.457 | 19.481 | 19.505 | 19.528 | 19.552 | 19.576 | 19.599 | 19.623 | 19.646 | 880                         |  |
| 890   | 19.646 | 19.670                             | 19.694 | 19.717 | 19.741 | 19.765 | 19.788 | 19.812 | 19.836 | 19.859 | 19.883 | 890                         |  |
| 900   | 19.883 | 19.907                             | 19.930 | 19.954 | 19.978 | 20.001 | 20.025 | 20.049 | 20.072 | 20.096 | 20.120 | 900                         |  |
| 910   | 20.120 | 20.143                             | 20.167 | 20.190 | 20.214 | 20.238 | 20.261 | 20.285 | 20.309 | 20.332 | 20.356 | 910                         |  |
| 920   | 20.356 | 20.380                             | 20.403 | 20.427 | 20.451 | 20.474 | 20.498 | 20.522 | 20.545 | 20.569 | 20.593 | 920                         |  |
| 930   | 20.593 | 20.616                             | 20.640 | 20.664 | 20.688 | 20.711 | 20.735 | 20.759 | 20.782 | 20.806 | 20.830 | 930                         |  |
| 940   | 20.830 | 20.853                             | 20.877 | 20.901 | 20.924 | 20.948 | 20.972 | 20.995 | 21.019 | 21.043 | 21.066 | 940                         |  |
| 950   | 21.066 | 21.090                             | 21.114 | 21.137 | 21.161 | 21.185 | 21.208 | 21.232 | 21.256 | 21.280 | 21.303 | 950                         |  |
| 960   | 21.303 | 21.327                             | 21.351 | 21.374 | 21.398 | 21.422 | 21.445 | 21.469 | 21.493 | 21.516 | 21.540 | 960                         |  |
| 970   | 21.540 | 21.564                             | 21.587 | 21.611 | 21.635 | 21.659 | 21.682 | 21.706 | 21.730 | 21.753 | 21.777 | 970                         |  |
| 980   | 21.777 | 21.801                             | 21.824 | 21.848 | 21.872 | 21.895 | 21.919 | 21.943 | 21.966 | 21.990 | 22.014 | 980                         |  |
| 990   | 22.014 | 22.038                             | 22.061 | 22.085 | 22.109 | 22.132 | 22.156 | 22.180 | 22.203 | 22.227 | 22.251 | 990                         |  |
| 1000  | 22.251 | 22.274                             | 22.298 | 22.322 | 22.346 | 22.369 | 22.393 | 22.417 | 22.440 | 22.464 | 22.488 | 1000                        |  |
| 1010  | 22.488 | 22.511                             | 22.535 | 22.559 | 22.582 | 22.606 | 22.630 | 22.654 | 22.677 | 22.701 | 22.725 | 1010                        |  |
| 1020  | 22.725 | 22.748                             | 22.772 | 22.796 | 22.819 | 22.843 | 22.867 | 22.890 | 22.914 | 22.938 | 22.961 | 1020                        |  |
| 1030  | 22.961 | 22.985                             | 23.009 | 23.032 | 23.056 | 23.080 | 23.104 | 23.127 | 23.151 | 23.175 | 23.199 | 1030                        |  |
| 1040  | 23.198 | 23.222                             | 23.246 | 23.269 | 23.293 | 23.317 | 23.340 | 23.364 | 23.388 | 23.411 | 23.435 | 1040                        |  |
| 1050  | 23.435 | 23.459                             | 23.482 | 23.506 | 23.530 | 23.553 | 23.577 | 23.601 | 23.624 | 23.648 | 23.672 | 1050                        |  |
| 1060  | 23.672 | 23.695                             | 23.719 | 23.743 | 23.766 | 23.790 | 23.814 | 23.837 | 23.861 | 23.885 | 23.908 | 1060                        |  |
| 1070  | 23.908 | 23.932                             | 23.956 | 23.979 | 24.003 | 24.027 | 24.050 | 24.074 | 24.098 | 24.121 | 24.145 | 1070                        |  |
| 1080  | 24.145 | 24.169                             | 24.192 | 24.216 | 24.240 | 24.263 | 24.287 | 24.311 | 24.334 | 24.358 | 24.382 | 1080                        |  |
| 1090  | 24.382 | 24.405                             | 24.429 | 24.453 | 24.476 | 24.500 | 24.523 | 24.547 | 24.571 | 24.594 | 24.618 | 1090                        |  |
| 1100  | 24.618 | 24.642                             | 24.665 | 24.689 | 24.713 | 24.736 | 24.760 | 24.783 | 24.807 | 24.831 | 24.854 | 1100                        |  |
| 1110  | 24.854 | 24.878                             | 24.902 | 24.925 | 24.949 | 24.972 | 24.996 | 25.020 | 25.043 | 25.067 | 25.091 | 1110                        |  |
| 1120  | 25.091 | 25.114                             | 25.138 | 25.161 | 25.185 | 25.209 | 25.232 | 25.256 | 25.279 | 25.303 | 25.327 | 1120                        |  |
| 1130  | 25.327 | 25.350                             | 25.374 | 25.397 | 25.421 | 25.445 | 25.468 | 25.492 | 25.515 | 25.539 | 25.563 | 1130                        |  |
| 1140  | 25.563 | 25.586                             | 25.610 | 25.633 | 25.657 | 25.681 | 25.704 | 25.728 | 25.751 | 25.775 | 25.799 | 1140                        |  |
| 1150  | 25.799 | 25.822                             | 25.846 | 25.869 | 25.893 | 25.916 | 25.940 | 25.964 | 25.987 | 26.011 | 26.034 | 1150                        |  |
| 1160  | 26.034 | 26.058                             | 26.081 | 26.105 | 26.128 | 26.152 | 26.176 | 26.199 | 26.223 | 26.246 | 26.270 | 1160                        |  |
| 1170  | 26.270 | 26.293                             | 26.317 | 26.340 | 26.364 | 26.387 | 26.411 | 26.435 | 26.458 | 26.482 | 26.505 | 1170                        |  |
| 1180  | 26.505 | 26.529                             | 26.552 | 26.576 | 26.599 | 26.623 | 26.646 | 26.670 | 26.694 | 26.717 | 26.740 | 1180                        |  |
| 1190  | 26.740 | 26.764                             | 26.787 | 26.811 | 26.834 | 26.858 | 26.881 | 26.905 | 26.928 | 26.952 | 26.975 | 1190                        |  |
| 1200  | 26.975 | 26.999                             | 27.022 | 27.046 | 27.069 | 27.093 | 27.116 | 27.140 | 27.163 | 27.187 | 27.210 | 1200                        |  |
| 1210  | 27.210 | 27.234                             | 27.257 | 27.281 | 27.304 | 27.328 | 27.351 | 27.375 | 27.398 | 27.422 | 27.445 | 1210                        |  |
| 1220  | 27.445 | 27.468                             | 27.492 | 27.515 | 27.539 | 27.562 | 27.586 | 27.609 | 27.633 | 27.656 | 27.679 | 1220                        |  |
| 1230  | 27.679 | 27.703                             | 27.726 | 27.750 | 27.773 | 27.797 | 27.820 | 27.844 | 27.867 | 27.890 | 27.914 | 1230                        |  |
| 1240  | 27.914 | 27.937                             | 27.961 | 27.984 | 28.007 | 28.031 | 28.054 | 28.078 | 28.101 | 28.124 | 28.148 | 1240                        |  |
| 1250  | 28.148 | 28.171                             | 28.195 | 28.218 | 28.241 | 28.265 | 28.288 | 28.311 | 28.335 | 28.358 | 28.382 | 1250                        |  |
| 1260  | 28.382 | 28.405                             | 28.428 | 28.452 | 28.475 | 28.498 | 28.522 | 28.545 | 28.569 | 28.592 | 28.615 | 1260                        |  |
| 1270  | 28.615 | 28.639                             | 28.662 | 28.685 | 28.709 | 28.732 | 28.755 | 28.779 | 28.802 | 28.825 | 28.849 | 1270                        |  |
| 1280  | 28.849 | 28.872                             | 28.895 | 28.919 | 28.942 | 28.965 | 28.988 | 29.012 | 29.035 | 29.058 | 29.082 | 1280                        |  |
| 1290  | 29.082 | 29.105                             | 29.128 | 29.152 | 29.175 | 29.198 | 29.221 | 29.245 | 29.268 | 29.291 | 29.315 | 1290                        |  |
| 1300  | 29.315 | 29.338                             | 29.361 | 29.384 | 29.408 | 29.431 | 29.454 | 29.477 | 29.501 | 29.524 | 29.547 | 1300                        |  |
| 1310  | 29.547 | 29.570                             | 29.594 | 29.617 | 29.640 | 29.663 | 29.687 | 29.710 | 29.733 | 29.756 | 29.780 | 1310                        |  |
| 1320  | 29.780 | 29.803                             | 29.826 | 29.849 | 29.872 | 29.896 | 29.919 | 29.942 | 29.965 | 29.989 | 30.012 | 1320                        |  |
| 1330  | 30.012 | 30.035                             | 30.058 | 30.081 | 30.104 | 30.128 | 30.151 | 30.174 | 30.197 | 30.220 | 30.244 | 1330                        |  |
| 1340  | 30.244 | 30.267                             | 30.290 | 30.313 | 30.336 | 30.359 | 30.383 | 30.406 | 30.429 | 30.452 | 30.475 | 1340                        |  |
| 1350  | 30.475 | 30.498                             | 30.521 | 30.545 | 30.568 | 30.591 | 30.614 | 30.637 | 30.660 | 30.683 | 30.706 | 1350                        |  |
| 1360  | 30.706 | 30.730                             | 30.753 | 30.776 | 30.799 | 30.822 | 30.845 | 30.868 | 30.891 | 30.914 | 30.937 | 1360                        |  |
| 1370  | 30.937 | 30.961                             | 30.984 | 31.007 | 31.030 | 31.053 | 31.076 | 31.099 | 31.122 | 31.145 | 31.168 | 1370                        |  |
| 1380  | 31.168 | 31.191                             | 31.214 | 31.237 | 31.260 | 31.283 | 31.306 | 31.329 | 31.352 | 31.375 | 31.399 | 1380                        |  |
| 1390  | 31.399 | 31.422                             | 31.445 | 31.468 | 31.491 | 31.514 | 31.537 | 31.560 | 31.583 | 31.606 | 31.629 | 1390                        |  |
| 1400  | 31.629 | 31.652                             | 31.675 | 31.698 | 31.721 | 31.744 | 31.767 | 31.790 | 31.813 | 31.836 | 31.859 | 1400                        |  |
| 1410  | 31.859 | 31.882                             | 31.905 | 31.927 | 31.950 | 31.973 | 31.996 | 32.019 | 32.042 | 32.065 | 32.088 | 1410                        |  |
| 1420  | 32.088 | 32.111                             | 32.134 | 32.157 | 32.180 | 32.203 | 32.226 | 32.249 | 32.272 | 32.295 | 32.317 | 1420                        |  |
| 1430  | 32.317 | 32.340                             | 32.363 | 32.386 | 32.409 | 32.432 | 32.455 | 32.478 | 32.501 | 32.524 | 32.546 | 1430                        |  |
| 1440  | 32.546 | 32.569                             | 32.592 | 32.615 | 32.638 | 32.661 | 32.683 | 32.706 | 32.729 | 32.752 | 32.775 | 1440                        |  |

\* Converted from degrees Celsius (IPTS 1968).

TABLE 10.8—Type K thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit* |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|------------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
| DEG F   | 0      | 1                                  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |                                    |        |        |        |        |        |        |        |        |        |                             |  |
| 1.450   | 32.775 | 32.798                             | 32.821 | 32.843 | 32.866 | 32.889 | 32.912 | 32.935 | 32.958 | 32.980 | 33.003 | 1.450                       |  |
| 1.460   | 33.003 | 33.026                             | 33.049 | 33.072 | 33.094 | 33.117 | 33.140 | 33.163 | 33.186 | 33.208 | 33.231 | 1.460                       |  |
| 1.470   | 33.231 | 33.254                             | 33.277 | 33.300 | 33.322 | 33.345 | 33.368 | 33.391 | 33.413 | 33.436 | 33.459 | 1.470                       |  |
| 1.480   | 33.459 | 33.482                             | 33.504 | 33.527 | 33.550 | 33.573 | 33.595 | 33.618 | 33.641 | 33.664 | 33.686 | 1.480                       |  |
| 1.490   | 33.686 | 33.709                             | 33.732 | 33.754 | 33.777 | 33.800 | 33.823 | 33.845 | 33.868 | 33.891 | 33.913 | 1.490                       |  |
| 1.500   | 33.913 | 33.936                             | 33.959 | 33.981 | 34.004 | 34.027 | 34.049 | 34.072 | 34.095 | 34.117 | 34.140 | 1.500                       |  |
| 1.510   | 34.140 | 34.163                             | 34.185 | 34.208 | 34.231 | 34.253 | 34.276 | 34.299 | 34.321 | 34.344 | 34.366 | 1.510                       |  |
| 1.520   | 34.366 | 34.389                             | 34.412 | 34.434 | 34.457 | 34.480 | 34.502 | 34.525 | 34.547 | 34.570 | 34.592 | 1.520                       |  |
| 1.530   | 34.593 | 34.615                             | 34.638 | 34.660 | 34.683 | 34.705 | 34.728 | 34.751 | 34.773 | 34.796 | 34.818 | 1.530                       |  |
| 1.540   | 34.818 | 34.841                             | 34.863 | 34.886 | 34.909 | 34.931 | 34.954 | 34.976 | 34.999 | 35.021 | 35.044 | 1.540                       |  |
| 1.550   | 35.044 | 35.066                             | 35.089 | 35.111 | 35.134 | 35.156 | 35.179 | 35.201 | 35.224 | 35.246 | 35.269 | 1.550                       |  |
| 1.560   | 35.269 | 35.291                             | 35.314 | 35.336 | 35.359 | 35.381 | 35.404 | 35.426 | 35.449 | 35.471 | 35.494 | 1.560                       |  |
| 1.570   | 35.494 | 35.516                             | 35.539 | 35.561 | 35.583 | 35.606 | 35.628 | 35.651 | 35.673 | 35.696 | 35.718 | 1.570                       |  |
| 1.580   | 35.718 | 35.741                             | 35.763 | 35.785 | 35.808 | 35.830 | 35.853 | 35.875 | 35.897 | 35.920 | 35.942 | 1.580                       |  |
| 1.590   | 35.942 | 35.965                             | 35.987 | 36.009 | 36.032 | 36.054 | 36.077 | 36.099 | 36.121 | 36.144 | 36.166 | 1.590                       |  |
| 1.600   | 36.166 | 36.188                             | 36.211 | 36.233 | 36.256 | 36.278 | 36.300 | 36.323 | 36.345 | 36.367 | 36.390 | 1.600                       |  |
| 1.610   | 36.390 | 36.412                             | 36.434 | 36.457 | 36.479 | 36.501 | 36.524 | 36.546 | 36.568 | 36.590 | 36.613 | 1.610                       |  |
| 1.620   | 36.613 | 36.635                             | 36.657 | 36.680 | 36.702 | 36.724 | 36.746 | 36.769 | 36.791 | 36.813 | 36.836 | 1.620                       |  |
| 1.630   | 36.836 | 36.858                             | 36.880 | 36.902 | 36.925 | 36.947 | 36.969 | 36.991 | 37.014 | 37.036 | 37.058 | 1.630                       |  |
| 1.640   | 37.058 | 37.080                             | 37.103 | 37.125 | 37.147 | 37.169 | 37.191 | 37.214 | 37.236 | 37.258 | 37.280 | 1.640                       |  |
| 1.650   | 37.280 | 37.303                             | 37.325 | 37.347 | 37.369 | 37.391 | 37.413 | 37.436 | 37.458 | 37.480 | 37.502 | 1.650                       |  |
| 1.660   | 37.502 | 37.524                             | 37.547 | 37.569 | 37.591 | 37.613 | 37.635 | 37.657 | 37.679 | 37.702 | 37.724 | 1.660                       |  |
| 1.670   | 37.724 | 37.746                             | 37.768 | 37.790 | 37.812 | 37.834 | 37.857 | 37.879 | 37.901 | 37.923 | 37.945 | 1.670                       |  |
| 1.680   | 37.945 | 37.967                             | 37.989 | 38.011 | 38.033 | 38.055 | 38.078 | 38.100 | 38.122 | 38.144 | 38.166 | 1.680                       |  |
| 1.690   | 38.166 | 38.188                             | 38.210 | 38.232 | 38.254 | 38.276 | 38.298 | 38.320 | 38.342 | 38.364 | 38.387 | 1.690                       |  |
| 1.700   | 38.387 | 38.409                             | 38.431 | 38.453 | 38.475 | 38.497 | 38.519 | 38.541 | 38.563 | 38.585 | 38.607 | 1.700                       |  |
| 1.710   | 38.607 | 38.629                             | 38.651 | 38.673 | 38.695 | 38.717 | 38.739 | 38.761 | 38.783 | 38.805 | 38.827 | 1.710                       |  |
| 1.720   | 38.827 | 38.849                             | 38.871 | 38.893 | 38.915 | 38.937 | 38.959 | 38.981 | 39.003 | 39.024 | 39.046 | 1.720                       |  |
| 1.730   | 39.046 | 39.068                             | 39.090 | 39.112 | 39.134 | 39.156 | 39.178 | 39.200 | 39.222 | 39.244 | 39.266 | 1.730                       |  |
| 1.740   | 39.266 | 39.288                             | 39.310 | 39.331 | 39.353 | 39.375 | 39.397 | 39.419 | 39.441 | 39.463 | 39.485 | 1.740                       |  |
| 1.750   | 39.485 | 39.507                             | 39.529 | 39.550 | 39.572 | 39.594 | 39.616 | 39.638 | 39.660 | 39.682 | 39.703 | 1.750                       |  |
| 1.760   | 39.703 | 39.725                             | 39.747 | 39.769 | 39.791 | 39.813 | 39.835 | 39.856 | 39.878 | 39.900 | 39.922 | 1.760                       |  |
| 1.770   | 39.922 | 39.944                             | 39.965 | 39.987 | 40.009 | 40.031 | 40.053 | 40.075 | 40.096 | 40.118 | 40.140 | 1.770                       |  |
| 1.780   | 40.140 | 40.162                             | 40.183 | 40.205 | 40.227 | 40.249 | 40.271 | 40.292 | 40.314 | 40.336 | 40.358 | 1.780                       |  |
| 1.790   | 40.358 | 40.379                             | 40.401 | 40.423 | 40.445 | 40.466 | 40.488 | 40.510 | 40.532 | 40.553 | 40.575 | 1.790                       |  |
| 1.800   | 40.575 | 40.597                             | 40.619 | 40.640 | 40.662 | 40.684 | 40.705 | 40.727 | 40.749 | 40.770 | 40.792 | 1.800                       |  |
| 1.810   | 40.792 | 40.814                             | 40.836 | 40.857 | 40.879 | 40.901 | 40.922 | 40.944 | 40.966 | 40.987 | 41.009 | 1.810                       |  |
| 1.820   | 41.009 | 41.031                             | 41.052 | 41.074 | 41.096 | 41.117 | 41.139 | 41.161 | 41.182 | 41.204 | 41.225 | 1.820                       |  |
| 1.830   | 41.225 | 41.247                             | 41.269 | 41.290 | 41.312 | 41.334 | 41.355 | 41.377 | 41.398 | 41.420 | 41.442 | 1.830                       |  |
| 1.840   | 41.442 | 41.463                             | 41.485 | 41.506 | 41.528 | 41.550 | 41.571 | 41.593 | 41.614 | 41.636 | 41.657 | 1.840                       |  |
| 1.850   | 41.657 | 41.679                             | 41.701 | 41.722 | 41.744 | 41.765 | 41.787 | 41.808 | 41.830 | 41.851 | 41.873 | 1.850                       |  |
| 1.860   | 41.873 | 41.895                             | 41.916 | 41.938 | 41.959 | 41.981 | 42.002 | 42.024 | 42.045 | 42.067 | 42.088 | 1.860                       |  |
| 1.870   | 42.088 | 42.110                             | 42.131 | 42.153 | 42.174 | 42.196 | 42.217 | 42.239 | 42.260 | 42.282 | 42.303 | 1.870                       |  |
| 1.880   | 42.303 | 42.325                             | 42.346 | 42.367 | 42.389 | 42.410 | 42.432 | 42.453 | 42.475 | 42.496 | 42.518 | 1.880                       |  |
| 1.890   | 42.518 | 42.539                             | 42.560 | 42.582 | 42.603 | 42.625 | 42.646 | 42.668 | 42.689 | 42.710 | 42.732 | 1.890                       |  |
| 1.900   | 42.732 | 42.753                             | 42.775 | 42.796 | 42.817 | 42.839 | 42.860 | 42.882 | 42.903 | 42.924 | 42.946 | 1.900                       |  |
| 1.910   | 42.946 | 42.967                             | 42.989 | 43.010 | 43.031 | 43.053 | 43.074 | 43.095 | 43.117 | 43.138 | 43.159 | 1.910                       |  |
| 1.920   | 43.159 | 43.181                             | 43.202 | 43.223 | 43.245 | 43.266 | 43.287 | 43.309 | 43.330 | 43.351 | 43.373 | 1.920                       |  |
| 1.930   | 43.373 | 43.394                             | 43.415 | 43.436 | 43.458 | 43.479 | 43.500 | 43.522 | 43.543 | 43.564 | 43.585 | 1.930                       |  |
| 1.940   | 43.585 | 43.607                             | 43.628 | 43.649 | 43.671 | 43.692 | 43.713 | 43.734 | 43.756 | 43.777 | 43.798 | 1.940                       |  |
| 1.950   | 43.798 | 43.819                             | 43.841 | 43.862 | 43.883 | 43.904 | 43.925 | 43.947 | 43.968 | 43.989 | 44.010 | 1.950                       |  |
| 1.960   | 44.010 | 44.031                             | 44.053 | 44.074 | 44.095 | 44.116 | 44.137 | 44.159 | 44.180 | 44.201 | 44.222 | 1.960                       |  |
| 1.970   | 44.222 | 44.243                             | 44.265 | 44.286 | 44.307 | 44.328 | 44.349 | 44.370 | 44.391 | 44.413 | 44.434 | 1.970                       |  |
| 1.980   | 44.434 | 44.455                             | 44.476 | 44.497 | 44.518 | 44.539 | 44.560 | 44.582 | 44.603 | 44.624 | 44.645 | 1.980                       |  |
| 1.990   | 44.645 | 44.666                             | 44.687 | 44.708 | 44.729 | 44.750 | 44.771 | 44.793 | 44.814 | 44.835 | 44.856 | 1.990                       |  |
| 2.000   | 44.856 | 44.877                             | 44.898 | 44.919 | 44.940 | 44.961 | 44.982 | 45.003 | 45.024 | 45.045 | 45.066 | 2.000                       |  |
| 2.010   | 45.066 | 45.087                             | 45.108 | 45.129 | 45.150 | 45.171 | 45.192 | 45.213 | 45.234 | 45.255 | 45.276 | 2.010                       |  |
| 2.020   | 45.276 | 45.297                             | 45.318 | 45.339 | 45.360 | 45.381 | 45.402 | 45.423 | 45.444 | 45.465 | 45.486 | 2.020                       |  |
| 2.030   | 45.486 | 45.507                             | 45.528 | 45.549 | 45.570 | 45.591 | 45.612 | 45.633 | 45.654 | 45.675 | 45.695 | 2.030                       |  |
| 2.040   | 45.695 | 45.716                             | 45.737 | 45.758 | 45.779 | 45.800 | 45.821 | 45.842 | 45.863 | 45.884 | 45.904 | 2.040                       |  |
| 2.050   | 45.904 | 45.925                             | 45.946 | 45.967 | 45.988 | 46.009 | 46.030 | 46.051 | 46.071 | 46.092 | 46.113 | 2.050                       |  |
| 2.060   | 46.113 | 46.134                             | 46.155 | 46.176 | 46.196 | 46.217 | 46.238 | 46.259 | 46.280 | 46.300 | 46.321 | 2.060                       |  |
| 2.070   | 46.321 | 46.342                             | 46.363 | 46.384 | 46.404 | 46.425 | 46.446 | 46.467 | 46.488 | 46.508 | 46.529 | 2.070                       |  |
| 2.080   | 46.529 | 46.550                             | 46.571 | 46.591 | 46.612 | 46.633 | 46.654 | 46.674 | 46.695 | 46.716 | 46.737 | 2.080                       |  |
| 2.090   | 46.737 | 46.757                             | 46.778 | 46.799 | 46.819 | 46.840 | 46.861 | 46.881 | 46.902 | 46.923 | 46.944 | 2.090                       |  |

\* Converted from degrees Celsius (IP15 1968)

TABLE 10.8—Type K thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit <sup>a</sup> |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
| DEG F   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                             |  |
| 2,100   | 46.944 | 46.964   | 46.985 | 47.006 | 47.026 | 47.047 | 47.068 | 47.088 | 47.109 | 47.130 | 47.150 | 2,100                       |  |
| 2,110   | 47.150 | 47.171   | 47.191 | 47.212 | 47.233 | 47.253 | 47.274 | 47.295 | 47.315 | 47.336 | 47.356 | 2,110                       |  |
| 2,120   | 47.356 | 47.377   | 47.398 | 47.418 | 47.439 | 47.459 | 47.480 | 47.500 | 47.521 | 47.542 | 47.562 | 2,120                       |  |
| 2,130   | 47.562 | 47.583   | 47.603 | 47.624 | 47.644 | 47.665 | 47.685 | 47.706 | 47.726 | 47.747 | 47.767 | 2,130                       |  |
| 2,140   | 47.767 | 47.788   | 47.808 | 47.829 | 47.849 | 47.870 | 47.890 | 47.911 | 47.931 | 47.952 | 47.972 | 2,140                       |  |
| 2,150   | 47.972 | 47.993   | 48.013 | 48.034 | 48.054 | 48.075 | 48.095 | 48.116 | 48.136 | 48.156 | 48.177 | 2,150                       |  |
| 2,160   | 48.177 | 48.197   | 48.218 | 48.238 | 48.258 | 48.279 | 48.299 | 48.320 | 48.340 | 48.360 | 48.381 | 2,160                       |  |
| 2,170   | 48.381 | 48.401   | 48.422 | 48.442 | 48.462 | 48.483 | 48.503 | 48.523 | 48.544 | 48.564 | 48.584 | 2,170                       |  |
| 2,180   | 48.584 | 48.605   | 48.625 | 48.645 | 48.666 | 48.686 | 48.706 | 48.727 | 48.747 | 48.767 | 48.787 | 2,180                       |  |
| 2,190   | 48.787 | 48.808   | 48.828 | 48.848 | 48.869 | 48.889 | 48.909 | 48.929 | 48.950 | 48.970 | 48.990 | 2,190                       |  |
| 2,200   | 48.990 | 49.010   | 49.031 | 49.051 | 49.071 | 49.091 | 49.111 | 49.132 | 49.152 | 49.172 | 49.192 | 2,200                       |  |
| 2,210   | 49.192 | 49.212   | 49.233 | 49.253 | 49.273 | 49.293 | 49.313 | 49.333 | 49.354 | 49.374 | 49.394 | 2,210                       |  |
| 2,220   | 49.394 | 49.414   | 49.434 | 49.454 | 49.474 | 49.495 | 49.515 | 49.535 | 49.555 | 49.575 | 49.595 | 2,220                       |  |
| 2,230   | 49.595 | 49.615   | 49.635 | 49.655 | 49.675 | 49.696 | 49.716 | 49.736 | 49.756 | 49.776 | 49.796 | 2,230                       |  |
| 2,240   | 49.796 | 49.816   | 49.836 | 49.856 | 49.876 | 49.896 | 49.916 | 49.936 | 49.956 | 49.976 | 49.996 | 2,240                       |  |
| 2,250   | 49.996 | 50.016   | 50.036 | 50.056 | 50.076 | 50.096 | 50.116 | 50.136 | 50.156 | 50.176 | 50.196 | 2,250                       |  |
| 2,260   | 50.196 | 50.216   | 50.236 | 50.256 | 50.276 | 50.296 | 50.315 | 50.335 | 50.355 | 50.375 | 50.395 | 2,260                       |  |
| 2,270   | 50.395 | 50.415   | 50.435 | 50.455 | 50.475 | 50.494 | 50.514 | 50.534 | 50.554 | 50.574 | 50.594 | 2,270                       |  |
| 2,280   | 50.594 | 50.614   | 50.633 | 50.653 | 50.673 | 50.693 | 50.713 | 50.733 | 50.752 | 50.772 | 50.792 | 2,280                       |  |
| 2,290   | 50.792 | 50.812   | 50.832 | 50.851 | 50.871 | 50.891 | 50.911 | 50.930 | 50.950 | 50.970 | 50.990 | 2,290                       |  |
| 2,300   | 50.990 | 51.009   | 51.029 | 51.049 | 51.069 | 51.088 | 51.108 | 51.128 | 51.148 | 51.167 | 51.187 | 2,300                       |  |
| 2,310   | 51.187 | 51.207   | 51.226 | 51.246 | 51.266 | 51.285 | 51.305 | 51.325 | 51.344 | 51.364 | 51.384 | 2,310                       |  |
| 2,320   | 51.384 | 51.403   | 51.423 | 51.443 | 51.462 | 51.482 | 51.501 | 51.521 | 51.541 | 51.560 | 51.580 | 2,320                       |  |
| 2,330   | 51.580 | 51.599   | 51.619 | 51.639 | 51.658 | 51.678 | 51.697 | 51.717 | 51.736 | 51.756 | 51.776 | 2,330                       |  |
| 2,340   | 51.776 | 51.795   | 51.815 | 51.834 | 51.854 | 51.873 | 51.893 | 51.912 | 51.932 | 51.951 | 51.971 | 2,340                       |  |
| 2,350   | 51.971 | 51.990   | 52.010 | 52.029 | 52.049 | 52.068 | 52.088 | 52.107 | 52.127 | 52.146 | 52.165 | 2,350                       |  |
| 2,360   | 52.165 | 52.185   | 52.204 | 52.224 | 52.243 | 52.263 | 52.282 | 52.301 | 52.321 | 52.340 | 52.360 | 2,360                       |  |
| 2,370   | 52.360 | 52.379   | 52.398 | 52.418 | 52.437 | 52.457 | 52.476 | 52.495 | 52.515 | 52.534 | 52.553 | 2,370                       |  |
| 2,380   | 52.553 | 52.573   | 52.592 | 52.611 | 52.631 | 52.650 | 52.669 | 52.689 | 52.708 | 52.727 | 52.747 | 2,380                       |  |
| 2,390   | 52.747 | 52.766   | 52.785 | 52.805 | 52.824 | 52.843 | 52.862 | 52.882 | 52.901 | 52.920 | 52.939 | 2,390                       |  |
| 2,400   | 52.939 | 52.959   | 52.978 | 52.997 | 53.016 | 53.036 | 53.055 | 53.074 | 53.093 | 53.113 | 53.132 | 2,400                       |  |
| 2,410   | 53.132 | 53.151   | 53.170 | 53.189 | 53.209 | 53.228 | 53.247 | 53.266 | 53.285 | 53.304 | 53.324 | 2,410                       |  |
| 2,420   | 53.324 | 53.343   | 53.362 | 53.381 | 53.400 | 53.419 | 53.439 | 53.458 | 53.477 | 53.496 | 53.515 | 2,420                       |  |
| 2,430   | 53.515 | 53.534   | 53.553 | 53.572 | 53.592 | 53.611 | 53.630 | 53.649 | 53.668 | 53.687 | 53.706 | 2,430                       |  |
| 2,440   | 53.706 | 53.725   | 53.744 | 53.763 | 53.782 | 53.801 | 53.821 | 53.840 | 53.859 | 53.878 | 53.897 | 2,440                       |  |
| 2,450   | 53.897 | 53.916   | 53.935 | 53.954 | 53.973 | 53.992 | 54.011 | 54.030 | 54.049 | 54.068 | 54.087 | 2,450                       |  |
| 2,460   | 54.087 | 54.106   | 54.125 | 54.144 | 54.163 | 54.182 | 54.201 | 54.220 | 54.239 | 54.258 | 54.277 | 2,460                       |  |
| 2,470   | 54.277 | 54.296   | 54.315 | 54.334 | 54.353 | 54.372 | 54.391 | 54.410 | 54.429 | 54.447 | 54.466 | 2,470                       |  |
| 2,480   | 54.466 | 54.485   | 54.504 | 54.523 | 54.542 | 54.561 | 54.580 | 54.599 | 54.618 | 54.637 | 54.656 | 2,480                       |  |
| 2,490   | 54.656 | 54.675   | 54.694 | 54.712 | 54.731 | 54.750 | 54.769 | 54.788 | 54.807 | 54.826 | 54.845 | 2,490                       |  |
| 2,500   | 54.845 |  |        |        |        |        |        |        |        |        |        | 2,500                       |  |
| DEG F   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |

<sup>a</sup>Converted from degrees Celsius (ITS 1968).

TABLE 10.9—Type K thermocouples (deg C-millivolts).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Celsius (IPTS 1968) |        |        |        |        |        |        |        |        |        | Reference Junctions at 0 C |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------------------------|--|
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                            |  |
| -270  | -6.458 |  |        |        |        |        |        |        |        |        |        | -270                       |  |
| -260  | -6.441 | -6.444                                     | -6.446 | -6.448 | -6.450 | -6.452 | -6.453 | -6.455 | -6.456 | -6.457 | -6.458 | -260                       |  |
| -250  | -6.404 | -6.408                                     | -6.413 | -6.417 | -6.421 | -6.425 | -6.429 | -6.432 | -6.435 | -6.438 | -6.441 | -250                       |  |
| -240  | -6.344 | -6.351                                     | -6.358 | -6.364 | -6.371 | -6.377 | -6.382 | -6.388 | -6.394 | -6.399 | -6.404 | -240                       |  |
| -230  | -6.262 | -6.271                                     | -6.280 | -6.289 | -6.297 | -6.306 | -6.314 | -6.322 | -6.329 | -6.337 | -6.344 | -230                       |  |
| -220  | -6.158 | -6.170                                     | -6.181 | -6.192 | -6.202 | -6.213 | -6.223 | -6.233 | -6.243 | -6.253 | -6.262 | -220                       |  |
| -210  | -6.035 | -6.048                                     | -6.061 | -6.074 | -6.087 | -6.099 | -6.111 | -6.123 | -6.135 | -6.147 | -6.158 | -210                       |  |
| -200  | -5.891 | -5.907                                     | -5.922 | -5.936 | -5.951 | -5.965 | -5.980 | -5.994 | -6.007 | -6.021 | -6.035 | -200                       |  |
| -190  | -5.730 | -5.747                                     | -5.763 | -5.780 | -5.796 | -5.813 | -5.829 | -5.845 | -5.860 | -5.876 | -5.891 | -190                       |  |
| -180  | -5.550 | -5.569                                     | -5.587 | -5.606 | -5.624 | -5.642 | -5.660 | -5.678 | -5.695 | -5.712 | -5.730 | -180                       |  |
| -170  | -5.354 | -5.374                                     | -5.394 | -5.414 | -5.434 | -5.454 | -5.474 | -5.493 | -5.512 | -5.531 | -5.550 | -170                       |  |
| -160  | -5.141 | -5.163                                     | -5.185 | -5.207 | -5.228 | -5.249 | -5.271 | -5.292 | -5.313 | -5.333 | -5.354 | -160                       |  |
| -150  | -4.912 | -4.936                                     | -4.959 | -4.983 | -5.006 | -5.029 | -5.051 | -5.074 | -5.097 | -5.119 | -5.141 | -150                       |  |
| -140  | -4.669 | -4.694                                     | -4.719 | -4.743 | -4.768 | -4.792 | -4.817 | -4.841 | -4.865 | -4.889 | -4.912 | -140                       |  |
| -130  | -4.410 | -4.437                                     | -4.463 | -4.489 | -4.515 | -4.541 | -4.567 | -4.593 | -4.618 | -4.644 | -4.669 | -130                       |  |
| -120  | -4.138 | -4.166                                     | -4.193 | -4.221 | -4.248 | -4.276 | -4.303 | -4.330 | -4.357 | -4.384 | -4.410 | -120                       |  |
| -110  | -3.852 | -3.881                                     | -3.910 | -3.939 | -3.968 | -3.997 | -4.025 | -4.053 | -4.082 | -4.110 | -4.138 | -110                       |  |
| -100  | -3.553 | -3.584                                     | -3.614 | -3.644 | -3.674 | -3.704 | -3.734 | -3.764 | -3.793 | -3.823 | -3.852 | -100                       |  |
| -90   | -3.242 | -3.274                                     | -3.305 | -3.337 | -3.368 | -3.399 | -3.430 | -3.461 | -3.492 | -3.523 | -3.553 | -90                        |  |
| -80   | -2.920 | -2.953                                     | -2.985 | -3.018 | -3.050 | -3.082 | -3.115 | -3.147 | -3.179 | -3.211 | -3.242 | -80                        |  |
| -70   | -2.586 | -2.620                                     | -2.654 | -2.687 | -2.721 | -2.754 | -2.788 | -2.821 | -2.854 | -2.887 | -2.920 | -70                        |  |
| -60   | -2.243 | -2.277                                     | -2.312 | -2.347 | -2.381 | -2.414 | -2.448 | -2.484 | -2.518 | -2.552 | -2.586 | -60                        |  |
| -50   | -1.889 | -1.925                                     | -1.961 | -1.996 | -2.032 | -2.067 | -2.102 | -2.137 | -2.173 | -2.208 | -2.243 | -50                        |  |
| -40   | -1.527 | -1.563                                     | -1.600 | -1.636 | -1.673 | -1.709 | -1.745 | -1.781 | -1.817 | -1.853 | -1.889 | -40                        |  |
| -30   | -1.156 | -1.193                                     | -1.231 | -1.268 | -1.305 | -1.342 | -1.379 | -1.416 | -1.453 | -1.490 | -1.527 | -30                        |  |
| -20   | -0.777 | -0.816                                     | -0.854 | -0.892 | -0.930 | -0.968 | -1.005 | -1.043 | -1.081 | -1.118 | -1.156 | -20                        |  |
| -10   | -0.392 | -0.431                                     | -0.469 | -0.508 | -0.547 | -0.585 | -0.624 | -0.662 | -0.701 | -0.739 | -0.777 | -10                        |  |
| 0   | 0.000  | -0.039                                     | -0.079 | -0.118 | -0.157 | -0.197 | -0.236 | -0.275 | -0.314 | -0.353 | -0.392 | 0                          |  |
| 0   | 0.000  | 0.039                                      | 0.079  | 0.119  | 0.158  | 0.198  | 0.238  | 0.277  | 0.317  | 0.357  | 0.397  | 0                          |  |
| 10  | 0.397  | 0.437                                      | 0.477  | 0.517  | 0.557  | 0.597  | 0.637  | 0.677  | 0.718  | 0.758  | 0.798  | 10                         |  |
| 20  | 0.798  | 0.838                                      | 0.879  | 0.919  | 0.960  | 1.000  | 1.041  | 1.081  | 1.122  | 1.162  | 1.203  | 20                         |  |
| 30  | 1.203  | 1.244                                      | 1.285  | 1.325  | 1.366  | 1.407  | 1.448  | 1.489  | 1.529  | 1.570  | 1.611  | 30                         |  |
| 40  | 1.611  | 1.652                                      | 1.693  | 1.734  | 1.776  | 1.817  | 1.858  | 1.899  | 1.940  | 1.981  | 2.022  | 40                         |  |
| 50  | 2.022  | 2.064                                      | 2.105  | 2.146  | 2.188  | 2.229  | 2.270  | 2.312  | 2.353  | 2.394  | 2.436  | 50                         |  |
| 60  | 2.436  | 2.477                                      | 2.519  | 2.560  | 2.601  | 2.643  | 2.684  | 2.726  | 2.767  | 2.809  | 2.850  | 60                         |  |
| 70  | 2.850  | 2.892                                      | 2.933  | 2.975  | 3.016  | 3.058  | 3.100  | 3.141  | 3.183  | 3.224  | 3.266  | 70                         |  |
| 80  | 3.266  | 3.307                                      | 3.349  | 3.390  | 3.432  | 3.473  | 3.515  | 3.556  | 3.598  | 3.640  | 3.681  | 80                         |  |
| 90  | 3.681  | 3.722                                      | 3.764  | 3.805  | 3.847  | 3.888  | 3.930  | 3.971  | 4.012  | 4.054  | 4.095  | 90                         |  |
| 100   | 4.095  | 4.137                                      | 4.178  | 4.219  | 4.261  | 4.302  | 4.343  | 4.384  | 4.426  | 4.467  | 4.508  | 100                        |  |
| 110   | 4.508  | 4.549                                      | 4.590  | 4.632  | 4.673  | 4.714  | 4.755  | 4.796  | 4.837  | 4.878  | 4.919  | 110                        |  |
| 120   | 4.919  | 4.960                                      | 5.001  | 5.042  | 5.083  | 5.124  | 5.164  | 5.205  | 5.246  | 5.287  | 5.327  | 120                        |  |
| 130   | 5.327  | 5.368                                      | 5.409  | 5.450  | 5.490  | 5.531  | 5.571  | 5.612  | 5.652  | 5.693  | 5.733  | 130                        |  |
| 140   | 5.733  | 5.774                                      | 5.814  | 5.855  | 5.895  | 5.936  | 5.976  | 6.016  | 6.057  | 6.097  | 6.137  | 140                        |  |
| 150   | 6.137  | 6.177                                      | 6.218  | 6.258  | 6.298  | 6.338  | 6.378  | 6.419  | 6.459  | 6.499  | 6.539  | 150                        |  |
| 160   | 6.539  | 6.579                                      | 6.619  | 6.659  | 6.699  | 6.739  | 6.779  | 6.819  | 6.859  | 6.899  | 6.939  | 160                        |  |
| 170   | 6.939  | 6.979                                      | 7.019  | 7.059  | 7.099  | 7.139  | 7.179  | 7.219  | 7.259  | 7.299  | 7.338  | 170                        |  |
| 180   | 7.338  | 7.378                                      | 7.418  | 7.458  | 7.498  | 7.538  | 7.578  | 7.618  | 7.658  | 7.697  | 7.737  | 180                        |  |
| 190   | 7.737  | 7.777                                      | 7.817  | 7.857  | 7.897  | 7.937  | 7.977  | 8.017  | 8.057  | 8.097  | 8.137  | 190                        |  |
| 200   | 8.137  | 8.177                                      | 8.216  | 8.256  | 8.296  | 8.336  | 8.376  | 8.416  | 8.456  | 8.497  | 8.537  | 200                        |  |
| 210   | 8.537  | 8.577                                      | 8.617  | 8.657  | 8.697  | 8.737  | 8.777  | 8.817  | 8.857  | 8.898  | 8.938  | 210                        |  |
| 220   | 8.938  | 8.978                                      | 9.018  | 9.058  | 9.099  | 9.139  | 9.179  | 9.220  | 9.260  | 9.300  | 9.341  | 220                        |  |
| 230   | 9.341  | 9.381                                      | 9.421  | 9.462  | 9.502  | 9.543  | 9.583  | 9.624  | 9.664  | 9.705  | 9.745  | 230                        |  |
| 240   | 9.745  | 9.786                                      | 9.826  | 9.867  | 9.907  | 9.948  | 9.989  | 10.029 | 10.070 | 10.111 | 10.151 | 240                        |  |
| 250   | 10.151 | 10.192                                     | 10.233 | 10.274 | 10.315 | 10.355 | 10.396 | 10.437 | 10.478 | 10.519 | 10.560 | 250                        |  |
| 260   | 10.560 | 10.600                                     | 10.641 | 10.682 | 10.723 | 10.764 | 10.805 | 10.846 | 10.887 | 10.928 | 10.969 | 260                        |  |
| 270   | 10.969 | 11.010                                     | 11.051 | 11.093 | 11.134 | 11.175 | 11.216 | 11.257 | 11.299 | 11.339 | 11.381 | 270                        |  |
| 280   | 11.381 | 11.422                                     | 11.463 | 11.504 | 11.546 | 11.587 | 11.628 | 11.669 | 11.711 | 11.752 | 11.793 | 280                        |  |
| 290   | 11.793 | 11.835                                     | 11.876 | 11.918 | 11.959 | 12.000 | 12.042 | 12.083 | 12.125 | 12.166 | 12.207 | 290                        |  |
| 300   | 12.207 | 12.249                                     | 12.290 | 12.332 | 12.373 | 12.415 | 12.456 | 12.498 | 12.539 | 12.581 | 12.623 | 300                        |  |
| 310   | 12.623 | 12.664                                     | 12.706 | 12.747 | 12.789 | 12.831 | 12.872 | 12.914 | 12.955 | 12.997 | 13.039 | 310                        |  |
| 320   | 13.039 | 13.080                                     | 13.122 | 13.164 | 13.205 | 13.247 | 13.289 | 13.331 | 13.372 | 13.414 | 13.456 | 320                        |  |
| 330   | 13.456 | 13.497                                     | 13.539 | 13.581 | 13.623 | 13.665 | 13.706 | 13.748 | 13.790 | 13.832 | 13.874 | 330                        |  |
| 340   | 13.874 | 13.915                                     | 13.957 | 13.999 | 14.041 | 14.083 | 14.125 | 14.167 | 14.208 | 14.250 | 14.292 | 340                        |  |
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |

194 THE USE OF THERMOCOUPLES IN TEMPERATURE MEASUREMENT

TABLE 10.9—Type K thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Celsius (IPTS 1968) |        |        |        |        |        |        |        |        |        | Reference Junctions at 0 C |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------------------------|--|
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                            |  |
| * 350   | 14.292 | 14.334                                     | 14.376 | 14.418 | 14.460 | 14.502 | 14.544 | 14.586 | 14.628 | 14.670 | 14.712 | 350                        |  |
| 360   | 14.712 | 14.754                                     | 14.796 | 14.838 | 14.880 | 14.922 | 14.964 | 15.006 | 15.048 | 15.090 | 15.132 | 360                        |  |
| 370   | 15.132 | 15.174                                     | 15.216 | 15.258 | 15.300 | 15.342 | 15.384 | 15.426 | 15.468 | 15.510 | 15.552 | 370                        |  |
| 380   | 15.552 | 15.594                                     | 15.636 | 15.679 | 15.721 | 15.763 | 15.805 | 15.847 | 15.889 | 15.931 | 15.974 | 380                        |  |
| 390   | 15.974 | 16.016                                     | 16.058 | 16.100 | 16.142 | 16.184 | 16.227 | 16.269 | 16.311 | 16.353 | 16.395 | 390                        |  |
| 400   | 16.395 | 16.438                                     | 16.480 | 16.522 | 16.564 | 16.607 | 16.649 | 16.691 | 16.733 | 16.776 | 16.818 | 400                        |  |
| 410   | 16.818 | 16.860                                     | 16.902 | 16.945 | 16.987 | 17.029 | 17.072 | 17.114 | 17.156 | 17.199 | 17.241 | 410                        |  |
| 420   | 17.241 | 17.283                                     | 17.326 | 17.368 | 17.410 | 17.453 | 17.495 | 17.537 | 17.580 | 17.622 | 17.664 | 420                        |  |
| 430   | 17.664 | 17.707                                     | 17.749 | 17.792 | 17.834 | 17.876 | 17.919 | 17.961 | 18.004 | 18.046 | 18.088 | 430                        |  |
| 440   | 18.088 | 18.131                                     | 18.173 | 18.216 | 18.258 | 18.301 | 18.343 | 18.385 | 18.428 | 18.470 | 18.513 | 440                        |  |
| 450   | 18.513 | 18.555                                     | 18.598 | 18.640 | 18.683 | 18.725 | 18.768 | 18.810 | 18.853 | 18.895 | 18.938 | 450                        |  |
| 460   | 18.938 | 18.980                                     | 19.023 | 19.065 | 19.108 | 19.150 | 19.193 | 19.235 | 19.278 | 19.320 | 19.363 | 460                        |  |
| 470   | 19.363 | 19.405                                     | 19.448 | 19.490 | 19.533 | 19.576 | 19.618 | 19.661 | 19.703 | 19.746 | 19.788 | 470                        |  |
| 480   | 19.788 | 19.831                                     | 19.873 | 19.916 | 19.959 | 20.001 | 20.044 | 20.086 | 20.129 | 20.172 | 20.214 | 480                        |  |
| 490   | 20.214 | 20.257                                     | 20.299 | 20.342 | 20.385 | 20.427 | 20.470 | 20.512 | 20.555 | 20.598 | 20.640 | 490                        |  |
| 500   | 20.640 | 20.683                                     | 20.725 | 20.768 | 20.811 | 20.853 | 20.896 | 20.938 | 20.981 | 21.024 | 21.066 | 500                        |  |
| 510   | 21.066 | 21.109                                     | 21.152 | 21.194 | 21.237 | 21.280 | 21.322 | 21.365 | 21.407 | 21.450 | 21.493 | 510                        |  |
| 520   | 21.493 | 21.535                                     | 21.578 | 21.621 | 21.663 | 21.706 | 21.749 | 21.791 | 21.834 | 21.876 | 21.919 | 520                        |  |
| 530   | 21.919 | 21.962                                     | 22.004 | 22.047 | 22.090 | 22.132 | 22.175 | 22.218 | 22.260 | 22.303 | 22.346 | 530                        |  |
| 540   | 22.346 | 22.388                                     | 22.431 | 22.473 | 22.516 | 22.559 | 22.601 | 22.644 | 22.687 | 22.729 | 22.772 | 540                        |  |
| 550   | 22.772 | 22.815                                     | 22.857 | 22.900 | 22.942 | 22.985 | 23.028 | 23.070 | 23.113 | 23.156 | 23.198 | 550                        |  |
| 560   | 23.198 | 23.241                                     | 23.284 | 23.326 | 23.369 | 23.411 | 23.454 | 23.497 | 23.539 | 23.582 | 23.624 | 560                        |  |
| 570   | 23.624 | 23.667                                     | 23.710 | 23.752 | 23.795 | 23.837 | 23.880 | 23.923 | 23.965 | 24.008 | 24.050 | 570                        |  |
| 580   | 24.050 | 24.093                                     | 24.136 | 24.178 | 24.221 | 24.263 | 24.306 | 24.348 | 24.391 | 24.434 | 24.476 | 580                        |  |
| 590   | 24.476 | 24.519                                     | 24.561 | 24.604 | 24.646 | 24.689 | 24.731 | 24.774 | 24.817 | 24.859 | 24.902 | 590                        |  |
| 600   | 24.902 | 24.944                                     | 24.987 | 25.029 | 25.072 | 25.114 | 25.157 | 25.199 | 25.242 | 25.284 | 25.327 | 600                        |  |
| 610   | 25.327 | 25.369                                     | 25.412 | 25.454 | 25.497 | 25.539 | 25.582 | 25.624 | 25.666 | 25.709 | 25.751 | 610                        |  |
| 620   | 25.751 | 25.794                                     | 25.836 | 25.879 | 25.921 | 25.964 | 26.006 | 26.048 | 26.091 | 26.133 | 26.176 | 620                        |  |
| 630   | 26.176 | 26.218                                     | 26.260 | 26.303 | 26.345 | 26.387 | 26.430 | 26.472 | 26.515 | 26.557 | 26.599 | 630                        |  |
| 640   | 26.599 | 26.642                                     | 26.684 | 26.726 | 26.769 | 26.811 | 26.853 | 26.896 | 26.938 | 26.980 | 27.022 | 640                        |  |
| 650   | 27.022 | 27.065                                     | 27.107 | 27.149 | 27.192 | 27.234 | 27.276 | 27.318 | 27.361 | 27.403 | 27.445 | 650                        |  |
| 660   | 27.445 | 27.487                                     | 27.529 | 27.572 | 27.614 | 27.656 | 27.698 | 27.740 | 27.783 | 27.825 | 27.867 | 660                        |  |
| 670   | 27.867 | 27.909                                     | 27.951 | 27.993 | 28.035 | 28.078 | 28.120 | 28.162 | 28.204 | 28.246 | 28.288 | 670                        |  |
| 680   | 28.288 | 28.330                                     | 28.372 | 28.414 | 28.456 | 28.498 | 28.540 | 28.583 | 28.625 | 28.667 | 28.709 | 680                        |  |
| 690   | 28.709 | 28.751                                     | 28.793 | 28.835 | 28.877 | 28.919 | 28.961 | 29.002 | 29.044 | 29.086 | 29.128 | 690                        |  |
| 700   | 29.128 | 29.170                                     | 29.212 | 29.254 | 29.296 | 29.338 | 29.380 | 29.422 | 29.464 | 29.506 | 29.547 | 700                        |  |
| 710   | 29.547 | 29.589                                     | 29.631 | 29.673 | 29.715 | 29.756 | 29.798 | 29.840 | 29.882 | 29.924 | 29.965 | 710                        |  |
| 720   | 29.965 | 30.007                                     | 30.049 | 30.091 | 30.132 | 30.174 | 30.216 | 30.257 | 30.299 | 30.341 | 30.383 | 720                        |  |
| 730   | 30.383 | 30.424                                     | 30.466 | 30.508 | 30.549 | 30.591 | 30.632 | 30.674 | 30.716 | 30.757 | 30.799 | 730                        |  |
| 740   | 30.799 | 30.840                                     | 30.882 | 30.924 | 30.965 | 31.007 | 31.048 | 31.090 | 31.131 | 31.173 | 31.214 | 740                        |  |
| 750   | 31.214 | 31.256                                     | 31.297 | 31.339 | 31.380 | 31.422 | 31.463 | 31.504 | 31.546 | 31.587 | 31.629 | 750                        |  |
| 760   | 31.629 | 31.670                                     | 31.712 | 31.753 | 31.794 | 31.836 | 31.877 | 31.918 | 31.960 | 32.001 | 32.042 | 760                        |  |
| 770   | 32.042 | 32.084                                     | 32.125 | 32.166 | 32.207 | 32.249 | 32.290 | 32.331 | 32.372 | 32.414 | 32.455 | 770                        |  |
| 780   | 32.455 | 32.496                                     | 32.537 | 32.578 | 32.619 | 32.661 | 32.702 | 32.743 | 32.784 | 32.825 | 32.866 | 780                        |  |
| 790   | 32.866 | 32.907                                     | 32.948 | 32.990 | 33.031 | 33.072 | 33.113 | 33.154 | 33.195 | 33.236 | 33.277 | 790                        |  |
| 800   | 33.277 | 33.318                                     | 33.359 | 33.400 | 33.441 | 33.482 | 33.523 | 33.564 | 33.604 | 33.645 | 33.686 | 800                        |  |
| 810   | 33.686 | 33.727                                     | 33.768 | 33.809 | 33.850 | 33.891 | 33.931 | 33.972 | 34.013 | 34.054 | 34.095 | 810                        |  |
| 820   | 34.095 | 34.136                                     | 34.176 | 34.217 | 34.258 | 34.299 | 34.339 | 34.380 | 34.421 | 34.461 | 34.502 | 820                        |  |
| 830   | 34.502 | 34.543                                     | 34.583 | 34.624 | 34.665 | 34.705 | 34.746 | 34.787 | 34.827 | 34.868 | 34.909 | 830                        |  |
| 840   | 34.909 | 34.949                                     | 34.990 | 35.030 | 35.071 | 35.111 | 35.152 | 35.192 | 35.233 | 35.273 | 35.314 | 840                        |  |
| 850   | 35.314 | 35.354                                     | 35.395 | 35.435 | 35.476 | 35.516 | 35.557 | 35.597 | 35.637 | 35.678 | 35.718 | 850                        |  |
| 860   | 35.718 | 35.758                                     | 35.799 | 35.839 | 35.880 | 35.920 | 35.960 | 36.000 | 36.041 | 36.081 | 36.121 | 860                        |  |
| 870   | 36.121 | 36.162                                     | 36.202 | 36.242 | 36.282 | 36.323 | 36.363 | 36.403 | 36.443 | 36.483 | 36.524 | 870                        |  |
| 880   | 36.524 | 36.564                                     | 36.604 | 36.644 | 36.684 | 36.724 | 36.764 | 36.804 | 36.844 | 36.885 | 36.925 | 880                        |  |
| 890   | 36.925 | 36.965                                     | 37.005 | 37.045 | 37.085 | 37.125 | 37.165 | 37.205 | 37.245 | 37.285 | 37.325 | 890                        |  |
| 900   | 37.325 | 37.365                                     | 37.405 | 37.445 | 37.484 | 37.524 | 37.564 | 37.604 | 37.644 | 37.684 | 37.724 | 900                        |  |
| 910   | 37.724 | 37.764                                     | 37.803 | 37.843 | 37.883 | 37.923 | 37.963 | 38.002 | 38.042 | 38.082 | 38.122 | 910                        |  |
| 920   | 38.122 | 38.162                                     | 38.201 | 38.241 | 38.281 | 38.320 | 38.360 | 38.400 | 38.439 | 38.479 | 38.519 | 920                        |  |
| 930   | 38.519 | 38.558                                     | 38.598 | 38.638 | 38.677 | 38.717 | 38.756 | 38.796 | 38.836 | 38.875 | 38.915 | 930                        |  |
| 940   | 38.915 | 38.954                                     | 38.994 | 39.033 | 39.073 | 39.112 | 39.152 | 39.191 | 39.231 | 39.270 | 39.310 | 940                        |  |
| 950   | 39.310 | 39.349                                     | 39.388 | 39.428 | 39.467 | 39.507 | 39.546 | 39.585 | 39.625 | 39.664 | 39.703 | 950                        |  |
| 960   | 39.703 | 39.743                                     | 39.782 | 39.821 | 39.861 | 39.900 | 39.939 | 39.979 | 40.018 | 40.057 | 40.096 | 960                        |  |
| 970   | 40.096 | 40.136                                     | 40.175 | 40.214 | 40.253 | 40.292 | 40.332 | 40.371 | 40.410 | 40.449 | 40.488 | 970                        |  |
| 980   | 40.488 | 40.527                                     | 40.566 | 40.605 | 40.645 | 40.684 | 40.723 | 40.762 | 40.801 | 40.840 | 40.879 | 980                        |  |
| 990   | 40.879 | 40.918                                     | 40.957 | 40.996 | 41.035 | 41.074 | 41.113 | 41.152 | 41.191 | 41.230 | 41.269 | 990                        |  |
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |

TABLE 10.9—Type K thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Celsius (IPTS 1968) |        |        |        |        |        |        |        |        |        | Reference Junctions at 0 C |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------------------------|--|
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                            |  |
| 1.000   | 41.269 | 41.308                                     | 41.347 | 41.385 | 41.424 | 41.463 | 41.502 | 41.541 | 41.580 | 41.619 | 41.657 | 1.000                      |  |
| 1.010   | 41.657 | 41.696                                     | 41.735 | 41.774 | 41.813 | 41.851 | 41.890 | 41.929 | 41.968 | 42.006 | 42.045 | 1.010                      |  |
| 1.020   | 42.045 | 42.084                                     | 42.123 | 42.161 | 42.200 | 42.239 | 42.277 | 42.316 | 42.355 | 42.393 | 42.432 | 1.020                      |  |
| 1.030   | 42.432 | 42.470                                     | 42.509 | 42.548 | 42.586 | 42.625 | 42.663 | 42.702 | 42.740 | 42.779 | 42.817 | 1.030                      |  |
| 1.040   | 42.817 | 42.856                                     | 42.894 | 42.933 | 42.971 | 43.010 | 43.048 | 43.087 | 43.125 | 43.164 | 43.202 | 1.040                      |  |
| 1.050   | 43.202 | 43.240                                     | 43.279 | 43.317 | 43.356 | 43.394 | 43.432 | 43.471 | 43.509 | 43.547 | 43.585 | 1.050                      |  |
| 1.060   | 43.585 | 43.624                                     | 43.662 | 43.700 | 43.739 | 43.777 | 43.815 | 43.853 | 43.891 | 43.930 | 43.968 | 1.060                      |  |
| 1.070   | 43.968 | 44.006                                     | 44.044 | 44.082 | 44.121 | 44.159 | 44.197 | 44.235 | 44.273 | 44.311 | 44.349 | 1.070                      |  |
| 1.080   | 44.349 | 44.387                                     | 44.425 | 44.463 | 44.501 | 44.539 | 44.577 | 44.615 | 44.653 | 44.691 | 44.729 | 1.080                      |  |
| 1.090   | 44.729 | 44.767                                     | 44.805 | 44.843 | 44.881 | 44.919 | 44.957 | 44.995 | 45.033 | 45.070 | 45.108 | 1.090                      |  |
| 1.100   | 45.108 | 45.146                                     | 45.184 | 45.222 | 45.260 | 45.297 | 45.335 | 45.373 | 45.411 | 45.448 | 45.486 | 1.100                      |  |
| 1.110   | 45.486 | 45.524                                     | 45.561 | 45.599 | 45.637 | 45.675 | 45.712 | 45.750 | 45.787 | 45.825 | 45.863 | 1.110                      |  |
| 1.120   | 45.863 | 45.900                                     | 45.938 | 45.975 | 46.013 | 46.051 | 46.088 | 46.126 | 46.163 | 46.201 | 46.238 | 1.120                      |  |
| 1.130   | 46.238 | 46.275                                     | 46.313 | 46.350 | 46.388 | 46.425 | 46.463 | 46.500 | 46.537 | 46.575 | 46.612 | 1.130                      |  |
| 1.140   | 46.612 | 46.649                                     | 46.687 | 46.724 | 46.761 | 46.799 | 46.836 | 46.873 | 46.910 | 46.948 | 46.985 | 1.140                      |  |
| 1.150   | 46.985 | 47.022                                     | 47.059 | 47.096 | 47.134 | 47.171 | 47.208 | 47.245 | 47.282 | 47.319 | 47.356 | 1.150                      |  |
| 1.160   | 47.356 | 47.393                                     | 47.430 | 47.468 | 47.505 | 47.542 | 47.579 | 47.616 | 47.653 | 47.689 | 47.726 | 1.160                      |  |
| 1.170   | 47.726 | 47.763                                     | 47.800 | 47.837 | 47.874 | 47.911 | 47.948 | 47.985 | 48.021 | 48.058 | 48.095 | 1.170                      |  |
| 1.180   | 48.095 | 48.132                                     | 48.169 | 48.205 | 48.242 | 48.279 | 48.316 | 48.352 | 48.389 | 48.426 | 48.462 | 1.180                      |  |
| 1.190   | 48.462 | 48.499                                     | 48.536 | 48.572 | 48.609 | 48.645 | 48.682 | 48.718 | 48.755 | 48.792 | 48.828 | 1.190                      |  |
| 1.200   | 48.828 | 48.865                                     | 48.901 | 48.937 | 48.974 | 49.010 | 49.047 | 49.083 | 49.120 | 49.156 | 49.192 | 1.200                      |  |
| 1.210   | 49.192 | 49.229                                     | 49.265 | 49.301 | 49.338 | 49.374 | 49.410 | 49.446 | 49.483 | 49.519 | 49.555 | 1.210                      |  |
| 1.220   | 49.555 | 49.591                                     | 49.627 | 49.663 | 49.700 | 49.736 | 49.772 | 49.808 | 49.844 | 49.880 | 49.916 | 1.220                      |  |
| 1.230   | 49.916 | 49.952                                     | 49.988 | 50.024 | 50.060 | 50.096 | 50.132 | 50.168 | 50.204 | 50.240 | 50.276 | 1.230                      |  |
| 1.240   | 50.276 | 50.311                                     | 50.347 | 50.383 | 50.419 | 50.455 | 50.491 | 50.526 | 50.562 | 50.598 | 50.633 | 1.240                      |  |
| 1.250   | 50.633 | 50.669                                     | 50.705 | 50.741 | 50.776 | 50.812 | 50.847 | 50.883 | 50.919 | 50.954 | 50.990 | 1.250                      |  |
| 1.260   | 50.990 | 51.025                                     | 51.061 | 51.096 | 51.132 | 51.167 | 51.203 | 51.238 | 51.274 | 51.309 | 51.344 | 1.260                      |  |
| 1.270   | 51.344 | 51.380                                     | 51.415 | 51.450 | 51.486 | 51.521 | 51.556 | 51.592 | 51.627 | 51.662 | 51.697 | 1.270                      |  |
| 1.280   | 51.697 | 51.733                                     | 51.768 | 51.803 | 51.838 | 51.873 | 51.908 | 51.943 | 51.979 | 52.014 | 52.049 | 1.280                      |  |
| 1.290   | 52.049 | 52.084                                     | 52.119 | 52.154 | 52.189 | 52.224 | 52.259 | 52.294 | 52.329 | 52.364 | 52.398 | 1.290                      |  |
| 1.300   | 52.398 | 52.433                                     | 52.468 | 52.503 | 52.538 | 52.573 | 52.608 | 52.642 | 52.677 | 52.712 | 52.747 | 1.300                      |  |
| 1.310   | 52.747 | 52.781                                     | 52.816 | 52.851 | 52.886 | 52.920 | 52.955 | 52.989 | 53.024 | 53.059 | 53.093 | 1.310                      |  |
| 1.320   | 53.093 | 53.128                                     | 53.162 | 53.197 | 53.232 | 53.266 | 53.301 | 53.335 | 53.370 | 53.404 | 53.439 | 1.320                      |  |
| 1.330   | 53.439 | 53.473                                     | 53.507 | 53.542 | 53.576 | 53.611 | 53.645 | 53.679 | 53.714 | 53.748 | 53.782 | 1.330                      |  |
| 1.340   | 53.782 | 53.817                                     | 53.851 | 53.885 | 53.920 | 53.954 | 53.988 | 54.022 | 54.057 | 54.091 | 54.125 | 1.340                      |  |
| 1.350   | 54.125 | 54.159                                     | 54.193 | 54.228 | 54.262 | 54.296 | 54.330 | 54.364 | 54.398 | 54.432 | 54.466 | 1.350                      |  |
| 1.360   | 54.466 | 54.501                                     | 54.535 | 54.569 | 54.603 | 54.637 | 54.671 | 54.705 | 54.739 | 54.773 | 54.807 | 1.360                      |  |
| 1.370   | 54.807 | 54.841                                     | 54.875 |        |        |        |        |        |        |        |        | 1.370                      |  |
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |

TABLE 10.10—Type R thermocouples (deg F-millivolts).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit* |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |    |       |
|---|--------|------------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|----|-------|
|   |        | 0                                  | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      |                             |  | 10 |       |
| DEG F   |        |                                    |        |        |        |        |        |        |        |        |        |                             |  |    | DEG F |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |                                    |        |        |        |        |        |        |        |        |        |                             |  |    |       |
| -50   | -0.210 | -0.212                             | -0.214 | -0.216 | -0.218 | -0.220 | -0.222 | -0.224 | -0.226 |        |        |                             |  |    | -50   |
| -40   | -0.188 | -0.190                             | -0.192 | -0.194 | -0.197 | -0.199 | -0.201 | -0.203 | -0.205 | -0.207 | -0.210 |                             |  |    | -40   |
| -30   | -0.165 | -0.167                             | -0.169 | -0.172 | -0.174 | -0.176 | -0.179 | -0.181 | -0.183 | -0.185 | -0.188 |                             |  |    | -30   |
| -20   | -0.141 | -0.143                             | -0.145 | -0.148 | -0.150 | -0.153 | -0.155 | -0.158 | -0.160 | -0.162 | -0.165 |                             |  |    | -20   |
| -10   | -0.116 | -0.118                             | -0.121 | -0.123 | -0.126 | -0.128 | -0.131 | -0.133 | -0.136 | -0.138 | -0.141 |                             |  |    | -10   |
| 0   | -0.089 | -0.092                             | -0.095 | -0.097 | -0.100 | -0.103 | -0.105 | -0.108 | -0.110 | -0.113 | -0.116 |                             |  |    | 0     |
| 0   | -0.089 | -0.087                             | -0.084 | -0.082 | -0.079 | -0.076 | -0.073 | -0.071 | -0.068 | -0.065 | -0.063 |                             |  |    | 0     |
| 10  | -0.063 | -0.060                             | -0.057 | -0.054 | -0.051 | -0.049 | -0.046 | -0.043 | -0.040 | -0.037 | -0.035 |                             |  |    | 10    |
| 20  | -0.035 | -0.032                             | -0.029 | -0.026 | -0.023 | -0.020 | -0.017 | -0.015 | -0.012 | -0.009 | -0.006 |                             |  |    | 20    |
| 30  | -0.006 | -0.003                             | 0.000  | 0.003  | 0.006  | 0.009  | 0.012  | 0.015  | 0.018  | 0.021  | 0.024  |                             |  |    | 30    |
| 40  | 0.024  | 0.027                              | 0.030  | 0.033  | 0.036  | 0.039  | 0.042  | 0.045  | 0.048  | 0.051  | 0.054  |                             |  |    | 40    |
| 50  | 0.054  | 0.057                              | 0.060  | 0.064  | 0.067  | 0.070  | 0.073  | 0.076  | 0.079  | 0.082  | 0.086  |                             |  |    | 50    |
| 60  | 0.086  | 0.089                              | 0.092  | 0.095  | 0.098  | 0.101  | 0.105  | 0.108  | 0.111  | 0.114  | 0.118  |                             |  |    | 60    |
| 70  | 0.118  | 0.121                              | 0.124  | 0.127  | 0.131  | 0.134  | 0.137  | 0.141  | 0.144  | 0.147  | 0.150  |                             |  |    | 70    |
| 80  | 0.150  | 0.154                              | 0.157  | 0.161  | 0.164  | 0.167  | 0.171  | 0.174  | 0.177  | 0.181  | 0.184  |                             |  |    | 80    |
| 90  | 0.184  | 0.188                              | 0.191  | 0.194  | 0.198  | 0.201  | 0.205  | 0.208  | 0.212  | 0.215  | 0.218  |                             |  |    | 90    |
| 100   | 0.218  | 0.222                              | 0.225  | 0.229  | 0.232  | 0.236  | 0.239  | 0.243  | 0.246  | 0.250  | 0.253  |                             |  |    | 100   |
| 110   | 0.253  | 0.257                              | 0.261  | 0.264  | 0.268  | 0.271  | 0.275  | 0.278  | 0.282  | 0.286  | 0.289  |                             |  |    | 110   |
| 120   | 0.289  | 0.293                              | 0.296  | 0.300  | 0.304  | 0.307  | 0.311  | 0.315  | 0.318  | 0.322  | 0.326  |                             |  |    | 120   |
| 130   | 0.326  | 0.329                              | 0.333  | 0.337  | 0.340  | 0.344  | 0.348  | 0.351  | 0.355  | 0.359  | 0.363  |                             |  |    | 130   |
| 140   | 0.363  | 0.366                              | 0.370  | 0.374  | 0.378  | 0.381  | 0.385  | 0.389  | 0.393  | 0.397  | 0.400  |                             |  |    | 140   |
| 150   | 0.400  | 0.404                              | 0.408  | 0.412  | 0.416  | 0.419  | 0.423  | 0.427  | 0.431  | 0.435  | 0.439  |                             |  |    | 150   |
| 160   | 0.439  | 0.443                              | 0.446  | 0.450  | 0.454  | 0.458  | 0.462  | 0.466  | 0.470  | 0.474  | 0.478  |                             |  |    | 160   |
| 170   | 0.478  | 0.482                              | 0.485  | 0.489  | 0.493  | 0.497  | 0.501  | 0.505  | 0.509  | 0.513  | 0.517  |                             |  |    | 170   |
| 180   | 0.517  | 0.521                              | 0.525  | 0.529  | 0.533  | 0.537  | 0.541  | 0.545  | 0.549  | 0.553  | 0.557  |                             |  |    | 180   |
| 190   | 0.557  | 0.561                              | 0.565  | 0.569  | 0.573  | 0.577  | 0.581  | 0.586  | 0.590  | 0.594  | 0.598  |                             |  |    | 190   |
| 200   | 0.598  | 0.602                              | 0.606  | 0.610  | 0.614  | 0.618  | 0.622  | 0.627  | 0.631  | 0.635  | 0.639  |                             |  |    | 200   |
| 210   | 0.639  | 0.643                              | 0.647  | 0.651  | 0.656  | 0.660  | 0.664  | 0.668  | 0.672  | 0.676  | 0.681  |                             |  |    | 210   |
| 220   | 0.681  | 0.685                              | 0.689  | 0.693  | 0.697  | 0.702  | 0.706  | 0.710  | 0.714  | 0.719  | 0.723  |                             |  |    | 220   |
| 230   | 0.723  | 0.727                              | 0.731  | 0.736  | 0.740  | 0.744  | 0.748  | 0.753  | 0.757  | 0.761  | 0.766  |                             |  |    | 230   |
| 240   | 0.766  | 0.770                              | 0.774  | 0.778  | 0.783  | 0.787  | 0.791  | 0.796  | 0.800  | 0.804  | 0.809  |                             |  |    | 240   |
| 250   | 0.809  | 0.813                              | 0.817  | 0.822  | 0.826  | 0.830  | 0.835  | 0.839  | 0.844  | 0.848  | 0.852  |                             |  |    | 250   |
| 260   | 0.852  | 0.857                              | 0.861  | 0.866  | 0.870  | 0.874  | 0.879  | 0.883  | 0.888  | 0.892  | 0.897  |                             |  |    | 260   |
| 270   | 0.897  | 0.901                              | 0.905  | 0.910  | 0.914  | 0.919  | 0.923  | 0.928  | 0.932  | 0.937  | 0.941  |                             |  |    | 270   |
| 280   | 0.941  | 0.946                              | 0.950  | 0.955  | 0.959  | 0.964  | 0.968  | 0.973  | 0.977  | 0.982  | 0.986  |                             |  |    | 280   |
| 290   | 0.986  | 0.991                              | 0.995  | 1.000  | 1.004  | 1.009  | 1.013  | 1.018  | 1.022  | 1.027  | 1.032  |                             |  |    | 290   |
| 300   | 1.032  | 1.036                              | 1.041  | 1.045  | 1.050  | 1.054  | 1.059  | 1.064  | 1.068  | 1.073  | 1.077  |                             |  |    | 300   |
| 310   | 1.077  | 1.082                              | 1.087  | 1.091  | 1.096  | 1.101  | 1.105  | 1.110  | 1.114  | 1.119  | 1.124  |                             |  |    | 310   |
| 320   | 1.124  | 1.128                              | 1.133  | 1.138  | 1.142  | 1.147  | 1.152  | 1.156  | 1.161  | 1.166  | 1.170  |                             |  |    | 320   |
| 330   | 1.170  | 1.175                              | 1.180  | 1.184  | 1.189  | 1.194  | 1.199  | 1.203  | 1.208  | 1.213  | 1.217  |                             |  |    | 330   |
| 340   | 1.217  | 1.222                              | 1.227  | 1.232  | 1.236  | 1.241  | 1.246  | 1.251  | 1.255  | 1.260  | 1.265  |                             |  |    | 340   |
| 350   | 1.265  | 1.270                              | 1.274  | 1.279  | 1.284  | 1.289  | 1.294  | 1.298  | 1.303  | 1.308  | 1.313  |                             |  |    | 350   |
| 360   | 1.313  | 1.318                              | 1.322  | 1.327  | 1.332  | 1.337  | 1.342  | 1.346  | 1.351  | 1.356  | 1.361  |                             |  |    | 360   |
| 370   | 1.361  | 1.366                              | 1.371  | 1.375  | 1.380  | 1.385  | 1.390  | 1.395  | 1.400  | 1.405  | 1.409  |                             |  |    | 370   |
| 380   | 1.409  | 1.414                              | 1.419  | 1.424  | 1.429  | 1.434  | 1.439  | 1.444  | 1.449  | 1.453  | 1.458  |                             |  |    | 380   |
| 390   | 1.458  | 1.463                              | 1.468  | 1.473  | 1.478  | 1.483  | 1.488  | 1.493  | 1.498  | 1.503  | 1.508  |                             |  |    | 390   |
| 400   | 1.508  | 1.512                              | 1.517  | 1.522  | 1.527  | 1.532  | 1.537  | 1.542  | 1.547  | 1.552  | 1.557  |                             |  |    | 400   |
| 410   | 1.557  | 1.562                              | 1.567  | 1.572  | 1.577  | 1.582  | 1.587  | 1.592  | 1.597  | 1.602  | 1.607  |                             |  |    | 410   |
| 420   | 1.607  | 1.612                              | 1.617  | 1.622  | 1.627  | 1.632  | 1.637  | 1.642  | 1.647  | 1.652  | 1.657  |                             |  |    | 420   |
| 430   | 1.657  | 1.662                              | 1.667  | 1.672  | 1.677  | 1.682  | 1.687  | 1.692  | 1.698  | 1.703  | 1.708  |                             |  |    | 430   |
| 440   | 1.708  | 1.713                              | 1.718  | 1.723  | 1.728  | 1.733  | 1.738  | 1.743  | 1.748  | 1.753  | 1.758  |                             |  |    | 440   |
| 450   | 1.758  | 1.764                              | 1.769  | 1.774  | 1.779  | 1.784  | 1.789  | 1.794  | 1.799  | 1.804  | 1.810  |                             |  |    | 450   |
| 460   | 1.810  | 1.815                              | 1.820  | 1.825  | 1.830  | 1.835  | 1.840  | 1.845  | 1.851  | 1.856  | 1.861  |                             |  |    | 460   |
| 470   | 1.861  | 1.866                              | 1.871  | 1.876  | 1.882  | 1.887  | 1.892  | 1.897  | 1.902  | 1.907  | 1.913  |                             |  |    | 470   |
| 480   | 1.913  | 1.918                              | 1.923  | 1.928  | 1.933  | 1.938  | 1.944  | 1.949  | 1.954  | 1.959  | 1.964  |                             |  |    | 480   |
| 490   | 1.964  | 1.970                              | 1.975  | 1.980  | 1.985  | 1.991  | 1.996  | 2.001  | 2.006  | 2.011  | 2.017  |                             |  |    | 490   |
| 500   | 2.017  | 2.022                              | 2.027  | 2.032  | 2.038  | 2.043  | 2.048  | 2.053  | 2.059  | 2.064  | 2.069  |                             |  |    | 500   |
| 510   | 2.069  | 2.074                              | 2.080  | 2.085  | 2.090  | 2.095  | 2.101  | 2.106  | 2.111  | 2.117  | 2.122  |                             |  |    | 510   |
| 520   | 2.122  | 2.127                              | 2.132  | 2.138  | 2.143  | 2.148  | 2.154  | 2.159  | 2.164  | 2.170  | 2.175  |                             |  |    | 520   |
| 530   | 2.175  | 2.180                              | 2.186  | 2.191  | 2.196  | 2.201  | 2.207  | 2.212  | 2.217  | 2.223  | 2.228  |                             |  |    | 530   |
| 540   | 2.228  | 2.233                              | 2.239  | 2.244  | 2.249  | 2.255  | 2.260  | 2.266  | 2.271  | 2.276  | 2.282  |                             |  |    | 540   |
| DEG F   | 0      | 1                                  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     |                             |  |    | DEG F |

\* Converted from degrees Celsius (IPTS 1968).

TABLE 10.10—Type R thermocouples (continued).

| EMF in Absolute Millivolts                    |       | Temperature in Degrees Fahrenheit* |       |       |       |       |       |       |       |       |       | Reference Junctions at 32 F |  |    |  |       |
|---|-------|------------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-----------------------------|--|----|--|-------|
|   |       | 0                                  | 1     | 2     | 3     | 4     | 5     | 6     | 7     | 8     | 9     |                             |  | 10 |  |       |
| DEG F   |       |                                    |       |       |       |       |       |       |       |       |       |                             |  |    |  | DEG F |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |       |                                    |       |       |       |       |       |       |       |       |       |                             |  |    |  |       |
| 550   | 2.282 | 2.287                              | 2.292 | 2.298 | 2.303 | 2.308 | 2.314 | 2.319 | 2.325 | 2.330 | 2.335 | 550                         |  |    |  |       |
| 560   | 2.335 | 2.341                              | 2.346 | 2.351 | 2.357 | 2.362 | 2.368 | 2.373 | 2.378 | 2.384 | 2.389 | 560                         |  |    |  |       |
| 570   | 2.389 | 2.395                              | 2.400 | 2.405 | 2.411 | 2.416 | 2.422 | 2.427 | 2.433 | 2.438 | 2.443 | 570                         |  |    |  |       |
| 580   | 2.443 | 2.449                              | 2.454 | 2.460 | 2.465 | 2.471 | 2.476 | 2.481 | 2.487 | 2.492 | 2.498 | 580                         |  |    |  |       |
| 590   | 2.498 | 2.503                              | 2.509 | 2.514 | 2.520 | 2.525 | 2.531 | 2.536 | 2.541 | 2.547 | 2.552 | 590                         |  |    |  |       |
| 600   | 2.552 | 2.558                              | 2.563 | 2.569 | 2.574 | 2.580 | 2.585 | 2.591 | 2.596 | 2.602 | 2.607 | 600                         |  |    |  |       |
| 610   | 2.607 | 2.613                              | 2.618 | 2.624 | 2.629 | 2.635 | 2.640 | 2.646 | 2.651 | 2.657 | 2.662 | 610                         |  |    |  |       |
| 620   | 2.662 | 2.668                              | 2.673 | 2.679 | 2.684 | 2.690 | 2.695 | 2.701 | 2.706 | 2.712 | 2.718 | 620                         |  |    |  |       |
| 630   | 2.718 | 2.723                              | 2.729 | 2.734 | 2.740 | 2.745 | 2.751 | 2.756 | 2.762 | 2.767 | 2.773 | 630                         |  |    |  |       |
| 640   | 2.773 | 2.779                              | 2.784 | 2.790 | 2.795 | 2.801 | 2.806 | 2.812 | 2.818 | 2.823 | 2.829 | 640                         |  |    |  |       |
| 650   | 2.829 | 2.834                              | 2.840 | 2.845 | 2.851 | 2.857 | 2.862 | 2.868 | 2.873 | 2.879 | 2.885 | 650                         |  |    |  |       |
| 660   | 2.885 | 2.890                              | 2.896 | 2.901 | 2.907 | 2.913 | 2.918 | 2.924 | 2.929 | 2.935 | 2.941 | 660                         |  |    |  |       |
| 670   | 2.941 | 2.946                              | 2.952 | 2.957 | 2.963 | 2.969 | 2.974 | 2.980 | 2.986 | 2.991 | 2.997 | 670                         |  |    |  |       |
| 680   | 2.997 | 3.002                              | 3.008 | 3.014 | 3.019 | 3.025 | 3.031 | 3.036 | 3.042 | 3.048 | 3.053 | 680                         |  |    |  |       |
| 690   | 3.053 | 3.059                              | 3.065 | 3.070 | 3.076 | 3.082 | 3.087 | 3.093 | 3.099 | 3.104 | 3.110 | 690                         |  |    |  |       |
| 700   | 3.110 | 3.116                              | 3.121 | 3.127 | 3.133 | 3.138 | 3.144 | 3.150 | 3.155 | 3.161 | 3.167 | 700                         |  |    |  |       |
| 710   | 3.167 | 3.172                              | 3.178 | 3.184 | 3.189 | 3.195 | 3.201 | 3.207 | 3.212 | 3.218 | 3.224 | 710                         |  |    |  |       |
| 720   | 3.224 | 3.229                              | 3.235 | 3.241 | 3.247 | 3.252 | 3.258 | 3.264 | 3.269 | 3.275 | 3.281 | 720                         |  |    |  |       |
| 730   | 3.281 | 3.287                              | 3.292 | 3.298 | 3.304 | 3.309 | 3.315 | 3.321 | 3.327 | 3.332 | 3.338 | 730                         |  |    |  |       |
| 740   | 3.338 | 3.344                              | 3.350 | 3.355 | 3.361 | 3.367 | 3.373 | 3.378 | 3.384 | 3.390 | 3.396 | 740                         |  |    |  |       |
| 750   | 3.396 | 3.401                              | 3.407 | 3.413 | 3.419 | 3.424 | 3.430 | 3.436 | 3.442 | 3.448 | 3.453 | 750                         |  |    |  |       |
| 760   | 3.453 | 3.459                              | 3.465 | 3.471 | 3.476 | 3.482 | 3.488 | 3.494 | 3.500 | 3.505 | 3.511 | 760                         |  |    |  |       |
| 770   | 3.511 | 3.517                              | 3.523 | 3.529 | 3.534 | 3.540 | 3.546 | 3.552 | 3.558 | 3.563 | 3.569 | 770                         |  |    |  |       |
| 780   | 3.569 | 3.575                              | 3.581 | 3.587 | 3.592 | 3.598 | 3.604 | 3.610 | 3.616 | 3.622 | 3.627 | 780                         |  |    |  |       |
| 790   | 3.627 | 3.633                              | 3.639 | 3.645 | 3.651 | 3.657 | 3.662 | 3.668 | 3.674 | 3.680 | 3.686 | 790                         |  |    |  |       |
| 800   | 3.686 | 3.692                              | 3.697 | 3.703 | 3.709 | 3.715 | 3.721 | 3.727 | 3.733 | 3.738 | 3.744 | 800                         |  |    |  |       |
| 810   | 3.744 | 3.750                              | 3.756 | 3.762 | 3.768 | 3.774 | 3.779 | 3.785 | 3.791 | 3.797 | 3.803 | 810                         |  |    |  |       |
| 820   | 3.803 | 3.809                              | 3.815 | 3.821 | 3.826 | 3.832 | 3.838 | 3.844 | 3.850 | 3.856 | 3.862 | 820                         |  |    |  |       |
| 830   | 3.862 | 3.868                              | 3.874 | 3.879 | 3.885 | 3.891 | 3.897 | 3.903 | 3.909 | 3.915 | 3.921 | 830                         |  |    |  |       |
| 840   | 3.921 | 3.927                              | 3.933 | 3.938 | 3.944 | 3.950 | 3.956 | 3.962 | 3.968 | 3.974 | 3.980 | 840                         |  |    |  |       |
| 850   | 3.980 | 3.986                              | 3.992 | 3.998 | 4.004 | 4.009 | 4.015 | 4.021 | 4.027 | 4.033 | 4.039 | 850                         |  |    |  |       |
| 860   | 4.039 | 4.045                              | 4.051 | 4.057 | 4.063 | 4.069 | 4.075 | 4.081 | 4.087 | 4.093 | 4.099 | 860                         |  |    |  |       |
| 870   | 4.099 | 4.105                              | 4.110 | 4.116 | 4.122 | 4.128 | 4.134 | 4.140 | 4.146 | 4.152 | 4.158 | 870                         |  |    |  |       |
| 880   | 4.158 | 4.164                              | 4.170 | 4.176 | 4.182 | 4.188 | 4.194 | 4.200 | 4.206 | 4.212 | 4.218 | 880                         |  |    |  |       |
| 890   | 4.218 | 4.224                              | 4.230 | 4.236 | 4.242 | 4.248 | 4.254 | 4.260 | 4.266 | 4.272 | 4.278 | 890                         |  |    |  |       |
| 900   | 4.278 | 4.284                              | 4.290 | 4.296 | 4.302 | 4.308 | 4.314 | 4.320 | 4.326 | 4.332 | 4.338 | 900                         |  |    |  |       |
| 910   | 4.338 | 4.344                              | 4.350 | 4.356 | 4.362 | 4.368 | 4.374 | 4.380 | 4.386 | 4.392 | 4.398 | 910                         |  |    |  |       |
| 920   | 4.398 | 4.404                              | 4.410 | 4.416 | 4.422 | 4.428 | 4.434 | 4.440 | 4.446 | 4.452 | 4.458 | 920                         |  |    |  |       |
| 930   | 4.458 | 4.464                              | 4.471 | 4.477 | 4.483 | 4.489 | 4.495 | 4.501 | 4.507 | 4.513 | 4.519 | 930                         |  |    |  |       |
| 940   | 4.519 | 4.525                              | 4.531 | 4.537 | 4.543 | 4.549 | 4.555 | 4.561 | 4.567 | 4.574 | 4.580 | 940                         |  |    |  |       |
| 950   | 4.580 | 4.586                              | 4.592 | 4.598 | 4.604 | 4.610 | 4.616 | 4.622 | 4.628 | 4.634 | 4.640 | 950                         |  |    |  |       |
| 960   | 4.640 | 4.647                              | 4.653 | 4.659 | 4.665 | 4.671 | 4.677 | 4.683 | 4.689 | 4.695 | 4.701 | 960                         |  |    |  |       |
| 970   | 4.701 | 4.707                              | 4.714 | 4.720 | 4.726 | 4.732 | 4.738 | 4.744 | 4.750 | 4.756 | 4.762 | 970                         |  |    |  |       |
| 980   | 4.762 | 4.769                              | 4.775 | 4.781 | 4.787 | 4.793 | 4.799 | 4.805 | 4.811 | 4.818 | 4.824 | 980                         |  |    |  |       |
| 990   | 4.824 | 4.830                              | 4.836 | 4.842 | 4.848 | 4.854 | 4.860 | 4.867 | 4.873 | 4.879 | 4.885 | 990                         |  |    |  |       |
| 1.000   | 4.885 | 4.891                              | 4.897 | 4.904 | 4.910 | 4.916 | 4.922 | 4.928 | 4.934 | 4.940 | 4.947 | 1.000                       |  |    |  |       |
| 1.010   | 4.947 | 4.953                              | 4.959 | 4.965 | 4.971 | 4.977 | 4.984 | 4.990 | 4.996 | 5.002 | 5.008 | 1.010                       |  |    |  |       |
| 1.020   | 5.008 | 5.014                              | 5.021 | 5.027 | 5.033 | 5.039 | 5.045 | 5.052 | 5.058 | 5.064 | 5.070 | 1.020                       |  |    |  |       |
| 1.030   | 5.070 | 5.076                              | 5.082 | 5.088 | 5.095 | 5.101 | 5.107 | 5.113 | 5.120 | 5.126 | 5.132 | 1.030                       |  |    |  |       |
| 1.040   | 5.132 | 5.138                              | 5.144 | 5.151 | 5.157 | 5.163 | 5.169 | 5.175 | 5.182 | 5.188 | 5.194 | 1.040                       |  |    |  |       |
| 1.050   | 5.194 | 5.200                              | 5.207 | 5.213 | 5.219 | 5.225 | 5.231 | 5.238 | 5.244 | 5.250 | 5.256 | 1.050                       |  |    |  |       |
| 1.060   | 5.256 | 5.263                              | 5.269 | 5.275 | 5.281 | 5.288 | 5.294 | 5.300 | 5.306 | 5.313 | 5.319 | 1.060                       |  |    |  |       |
| 1.070   | 5.319 | 5.325                              | 5.331 | 5.337 | 5.344 | 5.350 | 5.356 | 5.362 | 5.369 | 5.375 | 5.381 | 1.070                       |  |    |  |       |
| 1.080   | 5.381 | 5.388                              | 5.394 | 5.400 | 5.406 | 5.413 | 5.419 | 5.425 | 5.431 | 5.438 | 5.444 | 1.080                       |  |    |  |       |
| 1.090   | 5.444 | 5.450                              | 5.456 | 5.463 | 5.469 | 5.475 | 5.482 | 5.488 | 5.494 | 5.500 | 5.507 | 1.090                       |  |    |  |       |
| 1.100   | 5.507 | 5.513                              | 5.519 | 5.526 | 5.532 | 5.538 | 5.544 | 5.551 | 5.557 | 5.563 | 5.570 | 1.100                       |  |    |  |       |
| 1.110   | 5.570 | 5.576                              | 5.582 | 5.589 | 5.595 | 5.601 | 5.607 | 5.614 | 5.620 | 5.626 | 5.633 | 1.110                       |  |    |  |       |
| 1.120   | 5.633 | 5.639                              | 5.645 | 5.652 | 5.658 | 5.664 | 5.671 | 5.677 | 5.683 | 5.690 | 5.696 | 1.120                       |  |    |  |       |
| 1.130   | 5.696 | 5.702                              | 5.709 | 5.715 | 5.721 | 5.728 | 5.734 | 5.740 | 5.747 | 5.753 | 5.759 | 1.130                       |  |    |  |       |
| 1.140   | 5.759 | 5.766                              | 5.772 | 5.778 | 5.785 | 5.791 | 5.797 | 5.804 | 5.810 | 5.816 | 5.823 | 1.140                       |  |    |  |       |
| 1.150   | 5.823 | 5.829                              | 5.835 | 5.842 | 5.848 | 5.855 | 5.861 | 5.867 | 5.874 | 5.880 | 5.886 | 1.150                       |  |    |  |       |
| 1.160   | 5.886 | 5.893                              | 5.899 | 5.905 | 5.912 | 5.918 | 5.925 | 5.931 | 5.937 | 5.944 | 5.950 | 1.160                       |  |    |  |       |
| 1.170   | 5.950 | 5.957                              | 5.963 | 5.969 | 5.976 | 5.982 | 5.988 | 5.995 | 6.001 | 6.008 | 6.014 | 1.170                       |  |    |  |       |
| 1.180   | 6.014 | 6.021                              | 6.027 | 6.033 | 6.040 | 6.046 | 6.053 | 6.059 | 6.065 | 6.072 | 6.078 | 1.180                       |  |    |  |       |
| 1.190   | 6.078 | 6.085                              | 6.091 | 6.098 | 6.104 | 6.110 | 6.117 | 6.123 | 6.130 | 6.136 | 6.143 | 1.190                       |  |    |  |       |
| DEG F   | 0     | 1                                  | 2     | 3     | 4     | 5     | 6     | 7     | 8     | 9     | 10    | DEG F                       |  |    |  |       |

\* Converted from degrees Celsius (IPTS 1968).



# 198 THE USE OF THERMOCOUPLES IN TEMPERATURE MEASUREMENT

## TABLE 10.10—Type R thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit* |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|------------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
|   |        | DEG F                              | 0      | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      |                             |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |                                    |        |        |        |        |        |        |        |        |        |                             |  |
| 1200  | 6.143  | 6.149                              | 6.155  | 6.162  | 6.168  | 6.175  | 6.181  | 6.188  | 6.194  | 6.201  | 6.207  | 1200                        |  |
| 1210  | 6.207  | 6.213                              | 6.220  | 6.226  | 6.233  | 6.239  | 6.246  | 6.252  | 6.259  | 6.265  | 6.272  | 1210                        |  |
| 1220  | 6.272  | 6.278                              | 6.285  | 6.291  | 6.297  | 6.304  | 6.311  | 6.317  | 6.323  | 6.330  | 6.336  | 1220                        |  |
| 1230  | 6.336  | 6.343                              | 6.349  | 6.356  | 6.362  | 6.369  | 6.375  | 6.382  | 6.388  | 6.395  | 6.401  | 1230                        |  |
| 1240  | 6.401  | 6.408                              | 6.414  | 6.421  | 6.427  | 6.434  | 6.440  | 6.447  | 6.453  | 6.460  | 6.466  | 1240                        |  |
| 1250  | 6.466  | 6.473                              | 6.479  | 6.486  | 6.492  | 6.499  | 6.505  | 6.512  | 6.518  | 6.525  | 6.532  | 1250                        |  |
| 1260  | 6.532  | 6.538                              | 6.545  | 6.551  | 6.558  | 6.564  | 6.571  | 6.577  | 6.584  | 6.590  | 6.597  | 1260                        |  |
| 1270  | 6.597  | 6.603                              | 6.610  | 6.616  | 6.623  | 6.630  | 6.636  | 6.643  | 6.649  | 6.656  | 6.662  | 1270                        |  |
| 1280  | 6.662  | 6.669                              | 6.675  | 6.682  | 6.689  | 6.695  | 6.702  | 6.708  | 6.715  | 6.721  | 6.728  | 1280                        |  |
| 1290  | 6.728  | 6.735                              | 6.741  | 6.748  | 6.754  | 6.761  | 6.767  | 6.774  | 6.781  | 6.787  | 6.794  | 1290                        |  |
| 1300  | 6.794  | 6.800                              | 6.807  | 6.814  | 6.820  | 6.827  | 6.833  | 6.840  | 6.847  | 6.853  | 6.860  | 1300                        |  |
| 1310  | 6.860  | 6.866                              | 6.873  | 6.880  | 6.886  | 6.893  | 6.899  | 6.906  | 6.913  | 6.919  | 6.926  | 1310                        |  |
| 1320  | 6.926  | 6.932                              | 6.939  | 6.946  | 6.952  | 6.959  | 6.966  | 6.972  | 6.979  | 6.985  | 6.992  | 1320                        |  |
| 1330  | 6.992  | 6.999                              | 7.005  | 7.012  | 7.019  | 7.025  | 7.032  | 7.039  | 7.045  | 7.052  | 7.059  | 1330                        |  |
| 1340  | 7.059  | 7.065                              | 7.072  | 7.078  | 7.085  | 7.092  | 7.098  | 7.105  | 7.112  | 7.118  | 7.125  | 1340                        |  |
| 1350  | 7.125  | 7.132                              | 7.138  | 7.145  | 7.152  | 7.158  | 7.165  | 7.172  | 7.178  | 7.185  | 7.192  | 1350                        |  |
| 1360  | 7.192  | 7.198                              | 7.205  | 7.212  | 7.218  | 7.225  | 7.232  | 7.239  | 7.245  | 7.252  | 7.259  | 1360                        |  |
| 1370  | 7.259  | 7.265                              | 7.272  | 7.279  | 7.285  | 7.292  | 7.299  | 7.305  | 7.312  | 7.319  | 7.326  | 1370                        |  |
| 1380  | 7.326  | 7.332                              | 7.339  | 7.346  | 7.352  | 7.359  | 7.366  | 7.373  | 7.379  | 7.386  | 7.393  | 1380                        |  |
| 1390  | 7.393  | 7.399                              | 7.406  | 7.413  | 7.420  | 7.426  | 7.433  | 7.440  | 7.447  | 7.453  | 7.460  | 1390                        |  |
| 1400  | 7.460  | 7.467                              | 7.474  | 7.480  | 7.487  | 7.494  | 7.500  | 7.507  | 7.514  | 7.521  | 7.527  | 1400                        |  |
| 1410  | 7.527  | 7.534                              | 7.541  | 7.548  | 7.554  | 7.561  | 7.568  | 7.575  | 7.582  | 7.588  | 7.595  | 1410                        |  |
| 1420  | 7.595  | 7.602                              | 7.609  | 7.615  | 7.622  | 7.629  | 7.636  | 7.642  | 7.649  | 7.656  | 7.663  | 1420                        |  |
| 1430  | 7.663  | 7.670                              | 7.676  | 7.683  | 7.690  | 7.697  | 7.703  | 7.710  | 7.717  | 7.724  | 7.731  | 1430                        |  |
| 1440  | 7.731  | 7.737                              | 7.744  | 7.751  | 7.758  | 7.765  | 7.771  | 7.778  | 7.785  | 7.792  | 7.799  | 1440                        |  |
| 1450  | 7.799  | 7.805                              | 7.812  | 7.819  | 7.826  | 7.833  | 7.840  | 7.846  | 7.853  | 7.860  | 7.867  | 1450                        |  |
| 1460  | 7.867  | 7.874                              | 7.880  | 7.887  | 7.894  | 7.901  | 7.908  | 7.915  | 7.921  | 7.928  | 7.935  | 1460                        |  |
| 1470  | 7.935  | 7.942                              | 7.949  | 7.956  | 7.963  | 7.969  | 7.976  | 7.983  | 7.990  | 7.997  | 8.004  | 1470                        |  |
| 1480  | 8.004  | 8.010                              | 8.017  | 8.024  | 8.031  | 8.038  | 8.045  | 8.052  | 8.058  | 8.065  | 8.072  | 1480                        |  |
| 1490  | 8.072  | 8.079                              | 8.086  | 8.093  | 8.100  | 8.107  | 8.113  | 8.120  | 8.127  | 8.134  | 8.141  | 1490                        |  |
| 1500  | 8.141  | 8.148                              | 8.155  | 8.162  | 8.168  | 8.175  | 8.182  | 8.189  | 8.196  | 8.203  | 8.210  | 1500                        |  |
| 1510  | 8.210  | 8.217                              | 8.224  | 8.231  | 8.237  | 8.244  | 8.251  | 8.258  | 8.265  | 8.272  | 8.279  | 1510                        |  |
| 1520  | 8.275  | 8.286                              | 8.293  | 8.300  | 8.306  | 8.313  | 8.320  | 8.327  | 8.334  | 8.341  | 8.348  | 1520                        |  |
| 1530  | 8.348  | 8.355                              | 8.362  | 8.369  | 8.376  | 8.383  | 8.390  | 8.397  | 8.403  | 8.410  | 8.417  | 1530                        |  |
| 1540  | 8.417  | 8.424                              | 8.431  | 8.438  | 8.445  | 8.452  | 8.459  | 8.466  | 8.473  | 8.480  | 8.487  | 1540                        |  |
| 1550  | 8.487  | 8.494                              | 8.501  | 8.508  | 8.515  | 8.522  | 8.529  | 8.535  | 8.542  | 8.549  | 8.556  | 1550                        |  |
| 1560  | 8.556  | 8.563                              | 8.570  | 8.577  | 8.584  | 8.591  | 8.598  | 8.605  | 8.612  | 8.619  | 8.626  | 1560                        |  |
| 1570  | 8.626  | 8.633                              | 8.640  | 8.647  | 8.654  | 8.661  | 8.668  | 8.675  | 8.682  | 8.689  | 8.696  | 1570                        |  |
| 1580  | 8.696  | 8.703                              | 8.710  | 8.717  | 8.724  | 8.731  | 8.738  | 8.745  | 8.752  | 8.759  | 8.766  | 1580                        |  |
| 1590  | 8.766  | 8.773                              | 8.780  | 8.787  | 8.794  | 8.801  | 8.808  | 8.815  | 8.822  | 8.829  | 8.836  | 1590                        |  |
| 1600  | 8.836  | 8.843                              | 8.850  | 8.857  | 8.864  | 8.871  | 8.878  | 8.885  | 8.892  | 8.899  | 8.907  | 1600                        |  |
| 1610  | 8.907  | 8.914                              | 8.921  | 8.928  | 8.935  | 8.942  | 8.949  | 8.956  | 8.963  | 8.970  | 8.977  | 1610                        |  |
| 1620  | 8.977  | 8.984                              | 8.991  | 8.998  | 9.005  | 9.012  | 9.019  | 9.026  | 9.033  | 9.040  | 9.048  | 1620                        |  |
| 1630  | 9.048  | 9.055                              | 9.062  | 9.069  | 9.076  | 9.083  | 9.090  | 9.097  | 9.104  | 9.111  | 9.118  | 1630                        |  |
| 1640  | 9.118  | 9.125                              | 9.132  | 9.140  | 9.147  | 9.154  | 9.161  | 9.168  | 9.175  | 9.182  | 9.189  | 1640                        |  |
| 1650  | 9.189  | 9.196                              | 9.203  | 9.210  | 9.218  | 9.225  | 9.232  | 9.239  | 9.246  | 9.253  | 9.260  | 1650                        |  |
| 1660  | 9.260  | 9.267                              | 9.274  | 9.282  | 9.289  | 9.296  | 9.303  | 9.310  | 9.317  | 9.324  | 9.331  | 1660                        |  |
| 1670  | 9.331  | 9.338                              | 9.346  | 9.353  | 9.360  | 9.367  | 9.374  | 9.381  | 9.388  | 9.395  | 9.403  | 1670                        |  |
| 1680  | 9.403  | 9.410                              | 9.417  | 9.424  | 9.431  | 9.438  | 9.445  | 9.453  | 9.460  | 9.467  | 9.474  | 1680                        |  |
| 1690  | 9.474  | 9.481                              | 9.488  | 9.495  | 9.503  | 9.510  | 9.517  | 9.524  | 9.531  | 9.538  | 9.546  | 1690                        |  |
| 1700  | 9.546  | 9.553                              | 9.560  | 9.567  | 9.574  | 9.581  | 9.589  | 9.596  | 9.603  | 9.610  | 9.617  | 1700                        |  |
| 1710  | 9.617  | 9.624                              | 9.632  | 9.639  | 9.646  | 9.653  | 9.660  | 9.668  | 9.675  | 9.682  | 9.689  | 1710                        |  |
| 1720  | 9.689  | 9.696                              | 9.704  | 9.711  | 9.718  | 9.725  | 9.732  | 9.740  | 9.747  | 9.754  | 9.761  | 1720                        |  |
| 1730  | 9.761  | 9.768                              | 9.776  | 9.783  | 9.790  | 9.797  | 9.804  | 9.812  | 9.819  | 9.826  | 9.833  | 1730                        |  |
| 1740  | 9.833  | 9.840                              | 9.848  | 9.855  | 9.862  | 9.869  | 9.877  | 9.884  | 9.891  | 9.898  | 9.906  | 1740                        |  |
| 1750  | 9.906  | 9.913                              | 9.920  | 9.927  | 9.934  | 9.942  | 9.949  | 9.956  | 9.963  | 9.971  | 9.978  | 1750                        |  |
| 1760  | 9.978  | 9.985                              | 9.992  | 10.000 | 10.007 | 10.014 | 10.021 | 10.029 | 10.036 | 10.043 | 10.050 | 1760                        |  |
| 1770  | 10.050 | 10.058                             | 10.065 | 10.072 | 10.079 | 10.087 | 10.094 | 10.101 | 10.109 | 10.116 | 10.123 | 1770                        |  |
| 1780  | 10.123 | 10.130                             | 10.138 | 10.145 | 10.152 | 10.159 | 10.167 | 10.174 | 10.181 | 10.189 | 10.196 | 1780                        |  |
| 1790  | 10.196 | 10.203                             | 10.210 | 10.218 | 10.225 | 10.232 | 10.240 | 10.247 | 10.254 | 10.262 | 10.269 | 1790                        |  |
| 1800  | 10.269 | 10.276                             | 10.283 | 10.291 | 10.298 | 10.305 | 10.313 | 10.320 | 10.327 | 10.335 | 10.342 | 1800                        |  |
| 1810  | 10.342 | 10.349                             | 10.357 | 10.364 | 10.371 | 10.379 | 10.386 | 10.393 | 10.400 | 10.408 | 10.415 | 1810                        |  |
| 1820  | 10.415 | 10.422                             | 10.430 | 10.437 | 10.444 | 10.452 | 10.459 | 10.466 | 10.474 | 10.481 | 10.488 | 1820                        |  |
| 1830  | 10.488 | 10.496                             | 10.503 | 10.511 | 10.518 | 10.525 | 10.533 | 10.540 | 10.547 | 10.555 | 10.562 | 1830                        |  |
| 1840  | 10.562 | 10.569                             | 10.577 | 10.584 | 10.591 | 10.599 | 10.606 | 10.613 | 10.621 | 10.628 | 10.636 | 1840                        |  |

\* Converted from degrees Celsius (IPTS 1968).

TABLE 10.10—Type R thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit* |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|------------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
| DEG F   | 0      | 1                                  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |                                    |        |        |        |        |        |        |        |        |        |                             |  |
| 1,850   | 10.636 | 10.643                             | 10.650 | 10.658 | 10.665 | 10.672 | 10.680 | 10.687 | 10.695 | 10.702 | 10.709 | 1,850                       |  |
| 1,860   | 10.709 | 10.717                             | 10.724 | 10.731 | 10.739 | 10.746 | 10.754 | 10.761 | 10.768 | 10.776 | 10.783 | 1,860                       |  |
| 1,870   | 10.783 | 10.791                             | 10.798 | 10.805 | 10.813 | 10.820 | 10.828 | 10.835 | 10.842 | 10.850 | 10.857 | 1,870                       |  |
| 1,880   | 10.857 | 10.865                             | 10.872 | 10.879 | 10.887 | 10.894 | 10.902 | 10.909 | 10.917 | 10.924 | 10.931 | 1,880                       |  |
| 1,890   | 10.931 | 10.939                             | 10.946 | 10.954 | 10.961 | 10.968 | 10.976 | 10.983 | 10.991 | 10.998 | 11.006 | 1,890                       |  |
| 1,900   | 11.006 | 11.013                             | 11.021 | 11.028 | 11.035 | 11.043 | 11.050 | 11.058 | 11.065 | 11.073 | 11.080 | 1,900                       |  |
| 1,910   | 11.080 | 11.088                             | 11.095 | 11.102 | 11.110 | 11.117 | 11.125 | 11.132 | 11.140 | 11.147 | 11.155 | 1,910                       |  |
| 1,920   | 11.155 | 11.162                             | 11.170 | 11.177 | 11.184 | 11.192 | 11.199 | 11.207 | 11.214 | 11.222 | 11.229 | 1,920                       |  |
| 1,930   | 11.229 | 11.237                             | 11.244 | 11.252 | 11.259 | 11.267 | 11.274 | 11.282 | 11.289 | 11.297 | 11.304 | 1,930                       |  |
| 1,940   | 11.304 | 11.312                             | 11.319 | 11.327 | 11.334 | 11.342 | 11.349 | 11.357 | 11.364 | 11.372 | 11.379 | 1,940                       |  |
| 1,950   | 11.379 | 11.387                             | 11.394 | 11.402 | 11.409 | 11.417 | 11.424 | 11.432 | 11.439 | 11.447 | 11.454 | 1,950                       |  |
| 1,960   | 11.454 | 11.462                             | 11.469 | 11.477 | 11.484 | 11.492 | 11.500 | 11.507 | 11.514 | 11.522 | 11.529 | 1,960                       |  |
| 1,970   | 11.529 | 11.537                             | 11.544 | 11.552 | 11.559 | 11.567 | 11.574 | 11.582 | 11.590 | 11.597 | 11.605 | 1,970                       |  |
| 1,980   | 11.605 | 11.612                             | 11.620 | 11.627 | 11.635 | 11.642 | 11.650 | 11.657 | 11.665 | 11.672 | 11.680 | 1,980                       |  |
| 1,990   | 11.680 | 11.688                             | 11.695 | 11.703 | 11.710 | 11.718 | 11.725 | 11.733 | 11.740 | 11.748 | 11.756 | 1,990                       |  |
| 2,000   | 11.756 | 11.763                             | 11.771 | 11.778 | 11.786 | 11.793 | 11.801 | 11.808 | 11.816 | 11.824 | 11.831 | 2,000                       |  |
| 2,010   | 11.831 | 11.839                             | 11.846 | 11.854 | 11.861 | 11.869 | 11.877 | 11.884 | 11.892 | 11.899 | 11.907 | 2,010                       |  |
| 2,020   | 11.907 | 11.914                             | 11.922 | 11.930 | 11.937 | 11.945 | 11.952 | 11.960 | 11.968 | 11.975 | 11.983 | 2,020                       |  |
| 2,030   | 11.983 | 11.990                             | 11.998 | 12.005 | 12.013 | 12.021 | 12.028 | 12.036 | 12.043 | 12.051 | 12.059 | 2,030                       |  |
| 2,040   | 12.059 | 12.066                             | 12.074 | 12.081 | 12.089 | 12.097 | 12.104 | 12.112 | 12.119 | 12.127 | 12.135 | 2,040                       |  |
| 2,050   | 12.135 | 12.142                             | 12.150 | 12.157 | 12.165 | 12.173 | 12.180 | 12.188 | 12.196 | 12.203 | 12.211 | 2,050                       |  |
| 2,060   | 12.211 | 12.218                             | 12.226 | 12.234 | 12.241 | 12.249 | 12.257 | 12.264 | 12.272 | 12.279 | 12.287 | 2,060                       |  |
| 2,070   | 12.287 | 12.295                             | 12.302 | 12.310 | 12.318 | 12.325 | 12.333 | 12.340 | 12.348 | 12.356 | 12.363 | 2,070                       |  |
| 2,080   | 12.363 | 12.371                             | 12.379 | 12.386 | 12.394 | 12.402 | 12.409 | 12.417 | 12.424 | 12.432 | 12.440 | 2,080                       |  |
| 2,090   | 12.440 | 12.447                             | 12.455 | 12.463 | 12.470 | 12.478 | 12.486 | 12.493 | 12.501 | 12.509 | 12.516 | 2,090                       |  |
| 2,100   | 12.516 | 12.524                             | 12.532 | 12.539 | 12.547 | 12.555 | 12.562 | 12.570 | 12.577 | 12.585 | 12.593 | 2,100                       |  |
| 2,110   | 12.593 | 12.600                             | 12.608 | 12.616 | 12.623 | 12.631 | 12.639 | 12.646 | 12.654 | 12.662 | 12.669 | 2,110                       |  |
| 2,120   | 12.669 | 12.677                             | 12.685 | 12.693 | 12.700 | 12.708 | 12.716 | 12.723 | 12.731 | 12.739 | 12.746 | 2,120                       |  |
| 2,130   | 12.746 | 12.754                             | 12.762 | 12.769 | 12.777 | 12.785 | 12.792 | 12.800 | 12.808 | 12.815 | 12.823 | 2,130                       |  |
| 2,140   | 12.823 | 12.831                             | 12.838 | 12.846 | 12.854 | 12.862 | 12.869 | 12.877 | 12.885 | 12.892 | 12.900 | 2,140                       |  |
| 2,150   | 12.900 | 12.908                             | 12.915 | 12.923 | 12.931 | 12.938 | 12.946 | 12.954 | 12.962 | 12.969 | 12.977 | 2,150                       |  |
| 2,160   | 12.977 | 12.985                             | 12.992 | 13.000 | 13.008 | 13.016 | 13.023 | 13.031 | 13.039 | 13.046 | 13.054 | 2,160                       |  |
| 2,170   | 13.054 | 13.062                             | 13.069 | 13.077 | 13.085 | 13.093 | 13.100 | 13.108 | 13.116 | 13.123 | 13.131 | 2,170                       |  |
| 2,180   | 13.131 | 13.139                             | 13.147 | 13.154 | 13.162 | 13.170 | 13.178 | 13.185 | 13.193 | 13.201 | 13.208 | 2,180                       |  |
| 2,190   | 13.208 | 13.216                             | 13.224 | 13.232 | 13.239 | 13.247 | 13.255 | 13.263 | 13.270 | 13.278 | 13.286 | 2,190                       |  |
| 2,200   | 13.286 | 13.293                             | 13.301 | 13.309 | 13.317 | 13.324 | 13.332 | 13.340 | 13.348 | 13.355 | 13.363 | 2,200                       |  |
| 2,210   | 13.363 | 13.371                             | 13.379 | 13.386 | 13.394 | 13.402 | 13.410 | 13.417 | 13.425 | 13.433 | 13.440 | 2,210                       |  |
| 2,220   | 13.440 | 13.448                             | 13.456 | 13.464 | 13.471 | 13.479 | 13.487 | 13.495 | 13.502 | 13.510 | 13.518 | 2,220                       |  |
| 2,230   | 13.518 | 13.526                             | 13.533 | 13.541 | 13.549 | 13.557 | 13.564 | 13.572 | 13.580 | 13.588 | 13.595 | 2,230                       |  |
| 2,240   | 13.595 | 13.603                             | 13.611 | 13.619 | 13.627 | 13.634 | 13.642 | 13.650 | 13.658 | 13.665 | 13.673 | 2,240                       |  |
| 2,250   | 13.673 | 13.681                             | 13.689 | 13.696 | 13.704 | 13.712 | 13.720 | 13.727 | 13.735 | 13.743 | 13.751 | 2,250                       |  |
| 2,260   | 13.751 | 13.759                             | 13.766 | 13.774 | 13.782 | 13.790 | 13.797 | 13.805 | 13.813 | 13.821 | 13.828 | 2,260                       |  |
| 2,270   | 13.828 | 13.836                             | 13.844 | 13.852 | 13.860 | 13.867 | 13.875 | 13.883 | 13.891 | 13.898 | 13.906 | 2,270                       |  |
| 2,280   | 13.906 | 13.914                             | 13.922 | 13.930 | 13.937 | 13.945 | 13.953 | 13.961 | 13.968 | 13.976 | 13.984 | 2,280                       |  |
| 2,290   | 13.984 | 13.992                             | 14.000 | 14.007 | 14.015 | 14.023 | 14.031 | 14.039 | 14.046 | 14.054 | 14.062 | 2,290                       |  |
| 2,300   | 14.062 | 14.070                             | 14.078 | 14.085 | 14.093 | 14.101 | 14.109 | 14.116 | 14.124 | 14.132 | 14.140 | 2,300                       |  |
| 2,310   | 14.140 | 14.148                             | 14.155 | 14.163 | 14.171 | 14.179 | 14.187 | 14.194 | 14.202 | 14.210 | 14.218 | 2,310                       |  |
| 2,320   | 14.218 | 14.226                             | 14.233 | 14.241 | 14.249 | 14.257 | 14.265 | 14.272 | 14.280 | 14.288 | 14.296 | 2,320                       |  |
| 2,330   | 14.296 | 14.304                             | 14.311 | 14.319 | 14.327 | 14.335 | 14.343 | 14.350 | 14.358 | 14.366 | 14.374 | 2,330                       |  |
| 2,340   | 14.374 | 14.382                             | 14.389 | 14.397 | 14.405 | 14.413 | 14.421 | 14.429 | 14.436 | 14.444 | 14.452 | 2,340                       |  |
| 2,350   | 14.452 | 14.460                             | 14.468 | 14.475 | 14.483 | 14.491 | 14.499 | 14.507 | 14.514 | 14.522 | 14.530 | 2,350                       |  |
| 2,360   | 14.530 | 14.538                             | 14.546 | 14.554 | 14.561 | 14.569 | 14.577 | 14.585 | 14.593 | 14.600 | 14.608 | 2,360                       |  |
| 2,370   | 14.608 | 14.616                             | 14.624 | 14.632 | 14.640 | 14.647 | 14.655 | 14.663 | 14.671 | 14.679 | 14.686 | 2,370                       |  |
| 2,380   | 14.686 | 14.694                             | 14.702 | 14.710 | 14.718 | 14.726 | 14.733 | 14.741 | 14.749 | 14.757 | 14.765 | 2,380                       |  |
| 2,390   | 14.765 | 14.772                             | 14.780 | 14.788 | 14.796 | 14.804 | 14.812 | 14.819 | 14.827 | 14.835 | 14.843 | 2,390                       |  |
| 2,400   | 14.843 | 14.851                             | 14.859 | 14.866 | 14.874 | 14.882 | 14.890 | 14.898 | 14.906 | 14.913 | 14.921 | 2,400                       |  |
| 2,410   | 14.921 | 14.929                             | 14.937 | 14.945 | 14.953 | 14.961 | 14.968 | 14.976 | 14.984 | 14.992 | 15.000 | 2,410                       |  |
| 2,420   | 15.000 | 15.007                             | 15.015 | 15.023 | 15.031 | 15.039 | 15.047 | 15.054 | 15.062 | 15.070 | 15.078 | 2,420                       |  |
| 2,430   | 15.078 | 15.086                             | 15.094 | 15.101 | 15.109 | 15.117 | 15.125 | 15.133 | 15.141 | 15.148 | 15.156 | 2,430                       |  |
| 2,440   | 15.156 | 15.164                             | 15.172 | 15.180 | 15.188 | 15.195 | 15.203 | 15.211 | 15.219 | 15.227 | 15.235 | 2,440                       |  |
| 2,450   | 15.235 | 15.242                             | 15.250 | 15.258 | 15.266 | 15.274 | 15.282 | 15.289 | 15.297 | 15.305 | 15.313 | 2,450                       |  |
| 2,460   | 15.313 | 15.321                             | 15.329 | 15.337 | 15.344 | 15.352 | 15.360 | 15.368 | 15.376 | 15.384 | 15.391 | 2,460                       |  |
| 2,470   | 15.391 | 15.399                             | 15.407 | 15.415 | 15.423 | 15.431 | 15.438 | 15.446 | 15.454 | 15.462 | 15.470 | 2,470                       |  |
| 2,480   | 15.470 | 15.478                             | 15.486 | 15.493 | 15.501 | 15.509 | 15.517 | 15.525 | 15.533 | 15.540 | 15.548 | 2,480                       |  |
| 2,490   | 15.548 | 15.556                             | 15.564 | 15.572 | 15.580 | 15.587 | 15.595 | 15.603 | 15.611 | 15.619 | 15.627 | 2,490                       |  |

\* Converted from degrees Celsius (IPTS 1968).

TABLE 10.10—Type R thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit* |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|------------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
| DEG F   | 0      | 1                                  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |                                    |        |        |        |        |        |        |        |        |        |                             |  |
| 2500  | 15.627 | 15.635                             | 15.642 | 15.650 | 15.658 | 15.666 | 15.674 | 15.682 | 15.689 | 15.697 | 15.705 | 2500                        |  |
| 2510  | 15.705 | 15.713                             | 15.721 | 15.729 | 15.737 | 15.744 | 15.752 | 15.760 | 15.768 | 15.776 | 15.784 | 2510                        |  |
| 2520  | 15.784 | 15.791                             | 15.799 | 15.807 | 15.815 | 15.823 | 15.831 | 15.839 | 15.846 | 15.854 | 15.862 | 2520                        |  |
| 2530  | 15.862 | 15.870                             | 15.878 | 15.886 | 15.893 | 15.901 | 15.909 | 15.917 | 15.925 | 15.933 | 15.941 | 2530                        |  |
| 2540  | 15.941 | 15.948                             | 15.956 | 15.964 | 15.972 | 15.980 | 15.988 | 15.995 | 16.003 | 16.011 | 16.019 | 2540                        |  |
| 2550  | 16.019 | 16.027                             | 16.035 | 16.043 | 16.050 | 16.058 | 16.066 | 16.074 | 16.082 | 16.090 | 16.097 | 2550                        |  |
| 2560  | 16.097 | 16.105                             | 16.113 | 16.121 | 16.129 | 16.137 | 16.145 | 16.152 | 16.160 | 16.168 | 16.176 | 2560                        |  |
| 2570  | 16.176 | 16.184                             | 16.192 | 16.199 | 16.207 | 16.215 | 16.223 | 16.231 | 16.239 | 16.247 | 16.254 | 2570                        |  |
| 2580  | 16.254 | 16.262                             | 16.270 | 16.278 | 16.286 | 16.294 | 16.301 | 16.309 | 16.317 | 16.325 | 16.333 | 2580                        |  |
| 2590  | 16.333 | 16.341                             | 16.349 | 16.356 | 16.364 | 16.372 | 16.380 | 16.388 | 16.396 | 16.403 | 16.411 | 2590                        |  |
| 2600  | 16.411 | 16.419                             | 16.427 | 16.435 | 16.443 | 16.450 | 16.458 | 16.466 | 16.474 | 16.482 | 16.490 | 2600                        |  |
| 2610  | 16.490 | 16.498                             | 16.505 | 16.513 | 16.521 | 16.529 | 16.537 | 16.545 | 16.552 | 16.560 | 16.568 | 2610                        |  |
| 2620  | 16.568 | 16.576                             | 16.584 | 16.592 | 16.600 | 16.607 | 16.615 | 16.623 | 16.631 | 16.639 | 16.646 | 2620                        |  |
| 2630  | 16.646 | 16.654                             | 16.662 | 16.670 | 16.678 | 16.686 | 16.694 | 16.701 | 16.709 | 16.717 | 16.725 | 2630                        |  |
| 2640  | 16.725 | 16.733                             | 16.741 | 16.748 | 16.756 | 16.764 | 16.772 | 16.780 | 16.788 | 16.795 | 16.803 | 2640                        |  |
| 2650  | 16.803 | 16.811                             | 16.819 | 16.827 | 16.835 | 16.842 | 16.850 | 16.858 | 16.866 | 16.874 | 16.882 | 2650                        |  |
| 2660  | 16.882 | 16.889                             | 16.897 | 16.905 | 16.913 | 16.921 | 16.929 | 16.936 | 16.944 | 16.952 | 16.960 | 2660                        |  |
| 2670  | 16.960 | 16.968                             | 16.976 | 16.983 | 16.991 | 16.999 | 17.007 | 17.015 | 17.022 | 17.030 | 17.038 | 2670                        |  |
| 2680  | 17.038 | 17.046                             | 17.054 | 17.062 | 17.069 | 17.077 | 17.085 | 17.093 | 17.101 | 17.109 | 17.116 | 2680                        |  |
| 2690  | 17.116 | 17.124                             | 17.132 | 17.140 | 17.148 | 17.156 | 17.163 | 17.171 | 17.179 | 17.187 | 17.195 | 2690                        |  |
| 2700  | 17.195 | 17.202                             | 17.210 | 17.218 | 17.226 | 17.234 | 17.242 | 17.249 | 17.257 | 17.265 | 17.273 | 2700                        |  |
| 2710  | 17.273 | 17.281                             | 17.288 | 17.296 | 17.304 | 17.312 | 17.320 | 17.328 | 17.335 | 17.343 | 17.351 | 2710                        |  |
| 2720  | 17.351 | 17.359                             | 17.367 | 17.374 | 17.382 | 17.390 | 17.398 | 17.406 | 17.413 | 17.421 | 17.429 | 2720                        |  |
| 2730  | 17.429 | 17.437                             | 17.445 | 17.453 | 17.460 | 17.468 | 17.476 | 17.484 | 17.492 | 17.499 | 17.507 | 2730                        |  |
| 2740  | 17.507 | 17.515                             | 17.523 | 17.531 | 17.538 | 17.546 | 17.554 | 17.562 | 17.570 | 17.577 | 17.585 | 2740                        |  |
| 2750  | 17.585 | 17.593                             | 17.601 | 17.609 | 17.616 | 17.624 | 17.632 | 17.640 | 17.648 | 17.655 | 17.663 | 2750                        |  |
| 2760  | 17.663 | 17.671                             | 17.679 | 17.687 | 17.694 | 17.702 | 17.710 | 17.718 | 17.726 | 17.733 | 17.741 | 2760                        |  |
| 2770  | 17.741 | 17.749                             | 17.757 | 17.765 | 17.772 | 17.780 | 17.788 | 17.796 | 17.804 | 17.811 | 17.819 | 2770                        |  |
| 2780  | 17.819 | 17.827                             | 17.835 | 17.842 | 17.850 | 17.858 | 17.866 | 17.874 | 17.881 | 17.889 | 17.897 | 2780                        |  |
| 2790  | 17.897 | 17.905                             | 17.913 | 17.920 | 17.928 | 17.936 | 17.944 | 17.951 | 17.959 | 17.967 | 17.975 | 2790                        |  |
| 2800  | 17.975 | 17.983                             | 17.990 | 17.998 | 18.006 | 18.014 | 18.021 | 18.029 | 18.037 | 18.045 | 18.053 | 2800                        |  |
| 2810  | 18.053 | 18.060                             | 18.068 | 18.076 | 18.084 | 18.091 | 18.099 | 18.107 | 18.115 | 18.123 | 18.130 | 2810                        |  |
| 2820  | 18.130 | 18.138                             | 18.146 | 18.154 | 18.161 | 18.169 | 18.177 | 18.185 | 18.192 | 18.200 | 18.208 | 2820                        |  |
| 2830  | 18.208 | 18.216                             | 18.223 | 18.231 | 18.239 | 18.247 | 18.255 | 18.262 | 18.270 | 18.278 | 18.286 | 2830                        |  |
| 2840  | 18.286 | 18.293                             | 18.301 | 18.309 | 18.317 | 18.324 | 18.332 | 18.340 | 18.348 | 18.355 | 18.363 | 2840                        |  |
| 2850  | 18.363 | 18.371                             | 18.379 | 18.386 | 18.394 | 18.402 | 18.410 | 18.417 | 18.425 | 18.433 | 18.441 | 2850                        |  |
| 2860  | 18.441 | 18.448                             | 18.456 | 18.464 | 18.472 | 18.479 | 18.487 | 18.495 | 18.502 | 18.510 | 18.518 | 2860                        |  |
| 2870  | 18.518 | 18.526                             | 18.533 | 18.541 | 18.549 | 18.557 | 18.564 | 18.572 | 18.580 | 18.588 | 18.595 | 2870                        |  |
| 2880  | 18.595 | 18.603                             | 18.611 | 18.619 | 18.626 | 18.634 | 18.642 | 18.649 | 18.657 | 18.665 | 18.673 | 2880                        |  |
| 2890  | 18.673 | 18.680                             | 18.688 | 18.696 | 18.703 | 18.711 | 18.719 | 18.727 | 18.734 | 18.742 | 18.750 | 2890                        |  |
| 2900  | 18.750 | 18.758                             | 18.765 | 18.773 | 18.781 | 18.788 | 18.796 | 18.804 | 18.812 | 18.819 | 18.827 | 2900                        |  |
| 2910  | 18.827 | 18.835                             | 18.842 | 18.850 | 18.858 | 18.865 | 18.873 | 18.881 | 18.889 | 18.896 | 18.904 | 2910                        |  |
| 2920  | 18.904 | 18.912                             | 18.919 | 18.927 | 18.935 | 18.943 | 18.950 | 18.958 | 18.966 | 18.973 | 18.981 | 2920                        |  |
| 2930  | 18.981 | 18.989                             | 18.996 | 19.004 | 19.012 | 19.019 | 19.027 | 19.035 | 19.043 | 19.050 | 19.058 | 2930                        |  |
| 2940  | 19.058 | 19.066                             | 19.073 | 19.081 | 19.089 | 19.096 | 19.104 | 19.112 | 19.119 | 19.127 | 19.135 | 2940                        |  |
| 2950  | 19.135 | 19.142                             | 19.150 | 19.158 | 19.165 | 19.173 | 19.181 | 19.188 | 19.196 | 19.204 | 19.211 | 2950                        |  |
| 2960  | 19.211 | 19.219                             | 19.227 | 19.234 | 19.242 | 19.250 | 19.257 | 19.265 | 19.273 | 19.280 | 19.288 | 2960                        |  |
| 2970  | 19.288 | 19.296                             | 19.303 | 19.311 | 19.319 | 19.326 | 19.334 | 19.342 | 19.349 | 19.357 | 19.365 | 2970                        |  |
| 2980  | 19.365 | 19.372                             | 19.380 | 19.388 | 19.395 | 19.403 | 19.411 | 19.418 | 19.426 | 19.434 | 19.441 | 2980                        |  |
| 2990  | 19.441 | 19.449                             | 19.457 | 19.464 | 19.472 | 19.479 | 19.487 | 19.495 | 19.502 | 19.510 | 19.518 | 2990                        |  |
| 3000  | 19.518 | 19.525                             | 19.533 | 19.541 | 19.548 | 19.556 | 19.563 | 19.571 | 19.579 | 19.586 | 19.594 | 3000                        |  |
| 3010  | 19.594 | 19.602                             | 19.609 | 19.617 | 19.624 | 19.632 | 19.640 | 19.647 | 19.655 | 19.663 | 19.670 | 3010                        |  |
| 3020  | 19.670 | 19.678                             | 19.685 | 19.693 | 19.701 | 19.708 | 19.716 | 19.723 | 19.731 | 19.739 | 19.746 | 3020                        |  |
| 3030  | 19.746 | 19.754                             | 19.761 | 19.769 | 19.777 | 19.784 | 19.792 | 19.800 | 19.807 | 19.815 | 19.822 | 3030                        |  |
| 3040  | 19.822 | 19.830                             | 19.837 | 19.845 | 19.853 | 19.860 | 19.868 | 19.875 | 19.883 | 19.891 | 19.898 | 3040                        |  |
| 3050  | 19.898 | 19.906                             | 19.913 | 19.921 | 19.929 | 19.936 | 19.944 | 19.951 | 19.959 | 19.966 | 19.974 | 3050                        |  |
| 3060  | 19.974 | 19.982                             | 19.989 | 19.997 | 20.004 | 20.012 | 20.019 | 20.027 | 20.034 | 20.042 | 20.050 | 3060                        |  |
| 3070  | 20.050 | 20.057                             | 20.065 | 20.072 | 20.080 | 20.087 | 20.095 | 20.102 | 20.110 | 20.117 | 20.125 | 3070                        |  |
| 3080  | 20.125 | 20.132                             | 20.140 | 20.148 | 20.155 | 20.163 | 20.170 | 20.178 | 20.185 | 20.193 | 20.200 | 3080                        |  |
| 3090  | 20.200 | 20.208                             | 20.215 | 20.223 | 20.230 | 20.238 | 20.245 | 20.253 | 20.260 | 20.268 | 20.275 | 3090                        |  |
| 3100  | 20.275 | 20.283                             | 20.290 | 20.297 | 20.305 | 20.312 | 20.320 | 20.327 | 20.335 | 20.342 | 20.350 | 3100                        |  |
| 3110  | 20.350 | 20.357                             | 20.365 | 20.372 | 20.380 | 20.387 | 20.394 | 20.402 | 20.409 | 20.417 | 20.424 | 3110                        |  |
| 3120  | 20.424 | 20.432                             | 20.439 | 20.446 | 20.454 | 20.461 | 20.469 | 20.476 | 20.483 | 20.491 | 20.498 | 3120                        |  |
| 3130  | 20.498 | 20.506                             | 20.513 | 20.520 | 20.528 | 20.535 | 20.543 | 20.550 | 20.557 | 20.565 | 20.572 | 3130                        |  |
| 3140  | 20.572 | 20.579                             | 20.587 | 20.594 | 20.601 | 20.609 | 20.616 | 20.623 | 20.631 | 20.638 | 20.645 | 3140                        |  |
| DEG F   | 0      | 1                                  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |

\* Converted from degrees Celsius (IPTS 1968).

TABLE 10.10—Type R thermocouples (continued).

| EMF in Absolute Millivolts |        | Temperature in Degrees Fahrenheit <sup>a</sup> |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |       |
|----------------------------|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|-------|
|                            |        | 0  | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      |                             |       |
| DEG F                      |        | THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS  |        |        |        |        |        |        |        |        |        |                             | DEG F |
| 3.150                      | 20.645 | 20.653   | 20.660 | 20.667 | 20.675 | 20.682 | 20.689 | 20.697 | 20.704 | 20.711 | 20.718 | 3.150                       |       |
| 3.160                      | 20.718 | 20.726   | 20.733 | 20.740 | 20.748 | 20.755 | 20.762 | 20.769 | 20.777 | 20.784 | 20.791 | 3.160                       |       |
| 3.170                      | 20.791 | 20.798   | 20.806 | 20.813 | 20.820 | 20.827 | 20.834 | 20.842 | 20.849 | 20.856 | 20.863 | 3.170                       |       |
| 3.180                      | 20.863 | 20.870   | 20.878 | 20.885 | 20.892 | 20.899 | 20.906 | 20.914 | 20.921 | 20.928 | 20.935 | 3.180                       |       |
| 3.190                      | 20.935 | 20.942   | 20.949 | 20.956 | 20.964 | 20.971 | 20.978 | 20.985 | 20.992 | 20.999 | 21.006 | 3.190                       |       |
| 3.200                      | 21.006 | 21.013   | 21.021 | 21.028 | 21.035 | 21.042 | 21.049 | 21.056 | 21.063 | 21.070 | 21.077 | 3.200                       |       |
| 3.210                      | 21.077 | 21.084   | 21.091 | 21.098 | 21.105 |        |        |        |        |        |        | 3.210                       |       |
| DEG F                      | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |       |

<sup>a</sup> Converted from degrees Celsius (ITS 1968).

202 THE USE OF THERMOCOUPLES IN TEMPERATURE MEASUREMENT

TABLE 10.11—Type R thermocouples (deg C-millivolts).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Celsius (IPTS 1968) |        |        |        |        |        |        |        |        |        | Reference Junctions at 0 C |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------------------------|--|
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                            |  |
| -50   | -0.226 |  |        |        |        |        |        |        |        |        |        | -50                        |  |
| -40   | -0.188 | -0.192                                     | -0.196 | -0.200 | -0.204 | -0.207 | -0.211 | -0.215 | -0.219 | -0.223 | -0.226 | -40                        |  |
| -30   | -0.145 | -0.150                                     | -0.154 | -0.158 | -0.163 | -0.167 | -0.171 | -0.175 | -0.180 | -0.184 | -0.188 | -30                        |  |
| -20   | -0.100 | -0.105                                     | -0.109 | -0.114 | -0.119 | -0.123 | -0.128 | -0.132 | -0.137 | -0.141 | -0.145 | -20                        |  |
| -10   | -0.051 | -0.056                                     | -0.061 | -0.066 | -0.071 | -0.076 | -0.081 | -0.086 | -0.091 | -0.095 | -0.100 | -10                        |  |
| 0   | 0.000  | -0.005                                     | -0.011 | -0.016 | -0.021 | -0.026 | -0.031 | -0.036 | -0.041 | -0.046 | -0.051 | 0                          |  |
| 0   | 0.000  | 0.005                                      | 0.011  | 0.016  | 0.021  | 0.027  | 0.032  | 0.038  | 0.043  | 0.049  | 0.054  | 0                          |  |
| 10  | 0.054  | 0.060                                      | 0.065  | 0.071  | 0.077  | 0.082  | 0.088  | 0.094  | 0.100  | 0.105  | 0.111  | 10                         |  |
| 20  | 0.111  | 0.117                                      | 0.123  | 0.129  | 0.135  | 0.141  | 0.147  | 0.152  | 0.158  | 0.165  | 0.171  | 20                         |  |
| 30  | 0.171  | 0.177                                      | 0.183  | 0.189  | 0.195  | 0.201  | 0.207  | 0.214  | 0.220  | 0.226  | 0.232  | 30                         |  |
| 40  | 0.232  | 0.239                                      | 0.245  | 0.251  | 0.258  | 0.264  | 0.271  | 0.277  | 0.283  | 0.290  | 0.296  | 40                         |  |
| 50  | 0.296  | 0.303                                      | 0.310  | 0.316  | 0.323  | 0.329  | 0.336  | 0.343  | 0.349  | 0.356  | 0.363  | 50                         |  |
| 60  | 0.363  | 0.369                                      | 0.376  | 0.383  | 0.390  | 0.397  | 0.403  | 0.410  | 0.417  | 0.424  | 0.431  | 60                         |  |
| 70  | 0.431  | 0.438                                      | 0.445  | 0.452  | 0.459  | 0.466  | 0.473  | 0.480  | 0.487  | 0.494  | 0.501  | 70                         |  |
| 80  | 0.501  | 0.508                                      | 0.515  | 0.523  | 0.530  | 0.537  | 0.544  | 0.552  | 0.559  | 0.566  | 0.573  | 80                         |  |
| 90  | 0.573  | 0.581                                      | 0.588  | 0.595  | 0.603  | 0.610  | 0.617  | 0.625  | 0.632  | 0.640  | 0.647  | 90                         |  |
| 100   | 0.647  | 0.655                                      | 0.662  | 0.670  | 0.677  | 0.685  | 0.692  | 0.700  | 0.708  | 0.715  | 0.723  | 100                        |  |
| 110   | 0.723  | 0.730                                      | 0.738  | 0.746  | 0.754  | 0.761  | 0.769  | 0.777  | 0.784  | 0.792  | 0.800  | 110                        |  |
| 120   | 0.800  | 0.808                                      | 0.816  | 0.824  | 0.831  | 0.839  | 0.847  | 0.855  | 0.863  | 0.871  | 0.879  | 120                        |  |
| 130   | 0.879  | 0.887                                      | 0.895  | 0.903  | 0.911  | 0.919  | 0.927  | 0.935  | 0.943  | 0.951  | 0.959  | 130                        |  |
| 140   | 0.959  | 0.967                                      | 0.975  | 0.983  | 0.992  | 1.000  | 1.008  | 1.016  | 1.024  | 1.032  | 1.041  | 140                        |  |
| 150   | 1.041  | 1.049                                      | 1.057  | 1.065  | 1.074  | 1.082  | 1.090  | 1.099  | 1.107  | 1.115  | 1.124  | 150                        |  |
| 160   | 1.124  | 1.132                                      | 1.140  | 1.149  | 1.157  | 1.166  | 1.174  | 1.183  | 1.191  | 1.200  | 1.208  | 160                        |  |
| 170   | 1.208  | 1.217                                      | 1.225  | 1.234  | 1.242  | 1.251  | 1.259  | 1.268  | 1.276  | 1.285  | 1.294  | 170                        |  |
| 180   | 1.294  | 1.302                                      | 1.311  | 1.319  | 1.328  | 1.337  | 1.345  | 1.354  | 1.363  | 1.372  | 1.380  | 180                        |  |
| 190   | 1.380  | 1.389                                      | 1.398  | 1.407  | 1.415  | 1.424  | 1.433  | 1.442  | 1.450  | 1.459  | 1.468  | 190                        |  |
| 200   | 1.468  | 1.477                                      | 1.486  | 1.495  | 1.504  | 1.512  | 1.521  | 1.530  | 1.539  | 1.548  | 1.557  | 200                        |  |
| 210   | 1.557  | 1.566                                      | 1.575  | 1.584  | 1.593  | 1.602  | 1.611  | 1.620  | 1.629  | 1.638  | 1.647  | 210                        |  |
| 220   | 1.647  | 1.656                                      | 1.665  | 1.674  | 1.683  | 1.692  | 1.702  | 1.711  | 1.720  | 1.729  | 1.738  | 220                        |  |
| 230   | 1.738  | 1.747                                      | 1.756  | 1.766  | 1.775  | 1.784  | 1.793  | 1.802  | 1.812  | 1.821  | 1.830  | 230                        |  |
| 240   | 1.830  | 1.839                                      | 1.849  | 1.858  | 1.867  | 1.876  | 1.886  | 1.895  | 1.904  | 1.914  | 1.923  | 240                        |  |
| 250   | 1.923  | 1.932                                      | 1.942  | 1.951  | 1.960  | 1.970  | 1.979  | 1.988  | 1.998  | 2.007  | 2.017  | 250                        |  |
| 260   | 2.017  | 2.026                                      | 2.036  | 2.045  | 2.054  | 2.064  | 2.073  | 2.083  | 2.092  | 2.102  | 2.111  | 260                        |  |
| 270   | 2.111  | 2.121                                      | 2.130  | 2.140  | 2.149  | 2.159  | 2.169  | 2.178  | 2.188  | 2.197  | 2.207  | 270                        |  |
| 280   | 2.207  | 2.216                                      | 2.226  | 2.236  | 2.245  | 2.255  | 2.264  | 2.274  | 2.284  | 2.293  | 2.303  | 280                        |  |
| 290   | 2.303  | 2.313                                      | 2.322  | 2.332  | 2.342  | 2.351  | 2.361  | 2.371  | 2.381  | 2.390  | 2.400  | 290                        |  |
| 300   | 2.400  | 2.410                                      | 2.420  | 2.429  | 2.439  | 2.449  | 2.459  | 2.468  | 2.478  | 2.488  | 2.498  | 300                        |  |
| 310   | 2.498  | 2.508                                      | 2.517  | 2.527  | 2.537  | 2.547  | 2.557  | 2.567  | 2.576  | 2.586  | 2.596  | 310                        |  |
| 320   | 2.596  | 2.606                                      | 2.616  | 2.626  | 2.636  | 2.646  | 2.656  | 2.666  | 2.676  | 2.685  | 2.695  | 320                        |  |
| 330   | 2.695  | 2.705                                      | 2.715  | 2.725  | 2.735  | 2.745  | 2.755  | 2.765  | 2.775  | 2.785  | 2.795  | 330                        |  |
| 340   | 2.795  | 2.805                                      | 2.815  | 2.825  | 2.835  | 2.845  | 2.855  | 2.866  | 2.876  | 2.886  | 2.896  | 340                        |  |
| 350   | 2.896  | 2.906                                      | 2.916  | 2.926  | 2.936  | 2.946  | 2.956  | 2.966  | 2.977  | 2.987  | 2.997  | 350                        |  |
| 360   | 2.997  | 3.007                                      | 3.017  | 3.027  | 3.037  | 3.048  | 3.058  | 3.068  | 3.078  | 3.088  | 3.099  | 360                        |  |
| 370   | 3.099  | 3.109                                      | 3.119  | 3.129  | 3.139  | 3.150  | 3.160  | 3.170  | 3.180  | 3.191  | 3.201  | 370                        |  |
| 380   | 3.201  | 3.211                                      | 3.221  | 3.232  | 3.242  | 3.252  | 3.263  | 3.273  | 3.283  | 3.293  | 3.304  | 380                        |  |
| 390   | 3.304  | 3.314                                      | 3.324  | 3.335  | 3.345  | 3.355  | 3.366  | 3.376  | 3.386  | 3.397  | 3.407  | 390                        |  |
| 400   | 3.407  | 3.418                                      | 3.428  | 3.438  | 3.449  | 3.459  | 3.470  | 3.480  | 3.490  | 3.501  | 3.511  | 400                        |  |
| 410   | 3.511  | 3.522                                      | 3.532  | 3.543  | 3.553  | 3.563  | 3.574  | 3.584  | 3.595  | 3.605  | 3.616  | 410                        |  |
| 420   | 3.616  | 3.626                                      | 3.637  | 3.647  | 3.658  | 3.668  | 3.679  | 3.689  | 3.700  | 3.710  | 3.721  | 420                        |  |
| 430   | 3.721  | 3.731                                      | 3.742  | 3.752  | 3.763  | 3.774  | 3.784  | 3.795  | 3.805  | 3.816  | 3.826  | 430                        |  |
| 440   | 3.826  | 3.837                                      | 3.848  | 3.858  | 3.869  | 3.879  | 3.890  | 3.901  | 3.911  | 3.922  | 3.933  | 440                        |  |
| 450   | 3.933  | 3.943                                      | 3.954  | 3.964  | 3.975  | 3.986  | 3.996  | 4.007  | 4.018  | 4.028  | 4.039  | 450                        |  |
| 460   | 4.039  | 4.050                                      | 4.061  | 4.071  | 4.082  | 4.093  | 4.103  | 4.114  | 4.125  | 4.136  | 4.146  | 460                        |  |
| 470   | 4.146  | 4.157                                      | 4.168  | 4.178  | 4.189  | 4.200  | 4.211  | 4.222  | 4.232  | 4.243  | 4.254  | 470                        |  |
| 480   | 4.254  | 4.265                                      | 4.275  | 4.286  | 4.297  | 4.308  | 4.319  | 4.329  | 4.340  | 4.351  | 4.362  | 480                        |  |
| 490   | 4.362  | 4.373                                      | 4.384  | 4.394  | 4.405  | 4.416  | 4.427  | 4.438  | 4.449  | 4.460  | 4.471  | 490                        |  |
| 500   | 4.471  | 4.481                                      | 4.492  | 4.503  | 4.514  | 4.525  | 4.536  | 4.547  | 4.558  | 4.569  | 4.580  | 500                        |  |
| 510   | 4.580  | 4.591                                      | 4.601  | 4.612  | 4.623  | 4.634  | 4.645  | 4.656  | 4.667  | 4.678  | 4.689  | 510                        |  |
| 520   | 4.689  | 4.700                                      | 4.711  | 4.722  | 4.733  | 4.744  | 4.755  | 4.766  | 4.777  | 4.788  | 4.799  | 520                        |  |
| 530   | 4.799  | 4.810                                      | 4.821  | 4.832  | 4.843  | 4.854  | 4.865  | 4.876  | 4.888  | 4.899  | 4.910  | 530                        |  |
| 540   | 4.910  | 4.921                                      | 4.932  | 4.943  | 4.954  | 4.965  | 4.976  | 4.987  | 4.998  | 5.009  | 5.021  | 540                        |  |
| 550   | 5.021  | 5.032                                      | 5.043  | 5.054  | 5.065  | 5.076  | 5.087  | 5.099  | 5.110  | 5.121  | 5.132  | 550                        |  |
| 560   | 5.132  | 5.143                                      | 5.154  | 5.166  | 5.177  | 5.188  | 5.199  | 5.210  | 5.221  | 5.233  | 5.244  | 560                        |  |
| 570   | 5.244  | 5.255                                      | 5.266  | 5.278  | 5.289  | 5.300  | 5.311  | 5.322  | 5.334  | 5.345  | 5.356  | 570                        |  |
| 580   | 5.356  | 5.368                                      | 5.379  | 5.390  | 5.401  | 5.413  | 5.424  | 5.435  | 5.446  | 5.458  | 5.469  | 580                        |  |
| 590   | 5.469  | 5.480                                      | 5.492  | 5.503  | 5.514  | 5.526  | 5.537  | 5.548  | 5.560  | 5.571  | 5.582  | 590                        |  |
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |

TABLE 10.11—Type R thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Celsius (IPTS 1968) |        |        |        |        |        |        |        |        |        | Reference Junctions at 0 C |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------------------------|--|
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                            |  |
| 600   | 5.582  | 5.594                                      | 5.605  | 5.616  | 5.628  | 5.639  | 5.650  | 5.662  | 5.673  | 5.685  | 5.696  | 600                        |  |
| 610   | 5.696  | 5.707                                      | 5.719  | 5.730  | 5.742  | 5.753  | 5.764  | 5.776  | 5.787  | 5.799  | 5.810  | 610                        |  |
| 620   | 5.810  | 5.821                                      | 5.833  | 5.844  | 5.856  | 5.867  | 5.879  | 5.890  | 5.902  | 5.913  | 5.925  | 620                        |  |
| 630   | 5.925  | 5.936                                      | 5.948  | 5.959  | 5.971  | 5.982  | 5.994  | 6.005  | 6.017  | 6.028  | 6.040  | 630                        |  |
| 640   | 6.040  | 6.051                                      | 6.063  | 6.074  | 6.086  | 6.098  | 6.109  | 6.121  | 6.132  | 6.144  | 6.155  | 640                        |  |
| 650   | 6.155  | 6.167                                      | 6.179  | 6.190  | 6.202  | 6.213  | 6.225  | 6.237  | 6.248  | 6.260  | 6.272  | 650                        |  |
| 660   | 6.272  | 6.283                                      | 6.295  | 6.307  | 6.318  | 6.330  | 6.342  | 6.353  | 6.365  | 6.377  | 6.388  | 660                        |  |
| 670   | 6.388  | 6.400                                      | 6.412  | 6.423  | 6.435  | 6.447  | 6.458  | 6.470  | 6.482  | 6.494  | 6.505  | 670                        |  |
| 680   | 6.505  | 6.517                                      | 6.529  | 6.541  | 6.552  | 6.564  | 6.576  | 6.588  | 6.599  | 6.611  | 6.623  | 680                        |  |
| 690   | 6.623  | 6.635                                      | 6.647  | 6.658  | 6.670  | 6.682  | 6.694  | 6.706  | 6.718  | 6.729  | 6.741  | 690                        |  |
| 700   | 6.741  | 6.753                                      | 6.765  | 6.777  | 6.789  | 6.800  | 6.812  | 6.824  | 6.836  | 6.848  | 6.860  | 700                        |  |
| 710   | 6.860  | 6.872                                      | 6.884  | 6.895  | 6.907  | 6.919  | 6.931  | 6.943  | 6.955  | 6.967  | 6.979  | 710                        |  |
| 720   | 6.979  | 6.991                                      | 7.003  | 7.015  | 7.027  | 7.039  | 7.051  | 7.063  | 7.074  | 7.086  | 7.098  | 720                        |  |
| 730   | 7.098  | 7.110                                      | 7.122  | 7.134  | 7.146  | 7.158  | 7.170  | 7.182  | 7.194  | 7.206  | 7.218  | 730                        |  |
| 740   | 7.218  | 7.231                                      | 7.243  | 7.255  | 7.267  | 7.279  | 7.291  | 7.303  | 7.315  | 7.327  | 7.339  | 740                        |  |
| 750   | 7.339  | 7.351                                      | 7.363  | 7.375  | 7.387  | 7.399  | 7.412  | 7.424  | 7.436  | 7.448  | 7.460  | 750                        |  |
| 760   | 7.460  | 7.472                                      | 7.484  | 7.496  | 7.509  | 7.521  | 7.533  | 7.545  | 7.557  | 7.569  | 7.582  | 760                        |  |
| 770   | 7.582  | 7.594                                      | 7.606  | 7.618  | 7.630  | 7.642  | 7.655  | 7.667  | 7.679  | 7.691  | 7.703  | 770                        |  |
| 780   | 7.703  | 7.716                                      | 7.728  | 7.740  | 7.752  | 7.765  | 7.777  | 7.789  | 7.801  | 7.814  | 7.826  | 780                        |  |
| 790   | 7.826  | 7.838                                      | 7.850  | 7.863  | 7.875  | 7.887  | 7.900  | 7.912  | 7.924  | 7.937  | 7.949  | 790                        |  |
| 800   | 7.949  | 7.961                                      | 7.973  | 7.986  | 7.998  | 8.010  | 8.023  | 8.035  | 8.047  | 8.060  | 8.072  | 800                        |  |
| 810   | 8.072  | 8.085                                      | 8.097  | 8.109  | 8.122  | 8.134  | 8.146  | 8.159  | 8.171  | 8.184  | 8.196  | 810                        |  |
| 820   | 8.196  | 8.208                                      | 8.221  | 8.233  | 8.246  | 8.258  | 8.271  | 8.283  | 8.295  | 8.308  | 8.320  | 820                        |  |
| 830   | 8.320  | 8.333                                      | 8.345  | 8.358  | 8.370  | 8.383  | 8.395  | 8.408  | 8.420  | 8.433  | 8.445  | 830                        |  |
| 840   | 8.445  | 8.458                                      | 8.470  | 8.483  | 8.495  | 8.508  | 8.520  | 8.533  | 8.545  | 8.558  | 8.570  | 840                        |  |
| 850   | 8.570  | 8.583                                      | 8.595  | 8.608  | 8.621  | 8.633  | 8.646  | 8.658  | 8.671  | 8.683  | 8.696  | 850                        |  |
| 860   | 8.696  | 8.709                                      | 8.721  | 8.734  | 8.746  | 8.759  | 8.772  | 8.784  | 8.797  | 8.810  | 8.822  | 860                        |  |
| 870   | 8.822  | 8.835                                      | 8.847  | 8.860  | 8.873  | 8.885  | 8.898  | 8.911  | 8.923  | 8.936  | 8.949  | 870                        |  |
| 880   | 8.949  | 8.961                                      | 8.974  | 8.987  | 9.000  | 9.012  | 9.025  | 9.038  | 9.050  | 9.063  | 9.076  | 880                        |  |
| 890   | 9.076  | 9.089                                      | 9.101  | 9.114  | 9.127  | 9.140  | 9.152  | 9.165  | 9.178  | 9.191  | 9.203  | 890                        |  |
| 900   | 9.203  | 9.216                                      | 9.229  | 9.242  | 9.254  | 9.267  | 9.280  | 9.293  | 9.306  | 9.319  | 9.331  | 900                        |  |
| 910   | 9.331  | 9.344                                      | 9.357  | 9.370  | 9.383  | 9.395  | 9.408  | 9.421  | 9.434  | 9.447  | 9.460  | 910                        |  |
| 920   | 9.460  | 9.473                                      | 9.485  | 9.498  | 9.511  | 9.524  | 9.537  | 9.550  | 9.563  | 9.576  | 9.589  | 920                        |  |
| 930   | 9.589  | 9.602                                      | 9.614  | 9.627  | 9.640  | 9.653  | 9.666  | 9.679  | 9.692  | 9.705  | 9.718  | 930                        |  |
| 940   | 9.718  | 9.731                                      | 9.744  | 9.757  | 9.770  | 9.783  | 9.796  | 9.809  | 9.822  | 9.835  | 9.848  | 940                        |  |
| 950   | 9.848  | 9.861                                      | 9.874  | 9.887  | 9.900  | 9.913  | 9.926  | 9.939  | 9.952  | 9.965  | 9.978  | 950                        |  |
| 960   | 9.978  | 9.991                                      | 10.004 | 10.017 | 10.030 | 10.043 | 10.056 | 10.069 | 10.082 | 10.095 | 10.109 | 960                        |  |
| 970   | 10.109 | 10.122                                     | 10.135 | 10.148 | 10.161 | 10.174 | 10.187 | 10.200 | 10.213 | 10.227 | 10.240 | 970                        |  |
| 980   | 10.240 | 10.253                                     | 10.266 | 10.279 | 10.292 | 10.305 | 10.319 | 10.332 | 10.345 | 10.358 | 10.371 | 980                        |  |
| 990   | 10.371 | 10.384                                     | 10.398 | 10.411 | 10.424 | 10.437 | 10.450 | 10.464 | 10.477 | 10.490 | 10.503 | 990                        |  |
| 1.000   | 10.503 | 10.516                                     | 10.530 | 10.543 | 10.556 | 10.569 | 10.583 | 10.596 | 10.609 | 10.622 | 10.636 | 1.000                      |  |
| 1.010   | 10.636 | 10.649                                     | 10.662 | 10.675 | 10.689 | 10.702 | 10.715 | 10.729 | 10.742 | 10.755 | 10.768 | 1.010                      |  |
| 1.020   | 10.768 | 10.782                                     | 10.795 | 10.808 | 10.822 | 10.835 | 10.848 | 10.862 | 10.875 | 10.888 | 10.902 | 1.020                      |  |
| 1.030   | 10.902 | 10.915                                     | 10.928 | 10.942 | 10.955 | 10.968 | 10.982 | 10.995 | 1.009  | 1.022  | 1.035  | 1.030                      |  |
| 1.040   | 1.035  | 1.049                                      | 1.062  | 1.076  | 1.089  | 1.102  | 1.116  | 1.129  | 1.143  | 1.156  | 1.170  | 1.040                      |  |
| 1.050   | 1.170  | 1.183                                      | 1.196  | 1.210  | 1.223  | 1.237  | 1.250  | 1.264  | 1.277  | 1.291  | 1.304  | 1.050                      |  |
| 1.060   | 1.304  | 1.318                                      | 1.331  | 1.345  | 1.358  | 1.372  | 1.385  | 1.399  | 1.412  | 1.426  | 1.439  | 1.060                      |  |
| 1.070   | 1.439  | 1.453                                      | 1.466  | 1.480  | 1.493  | 1.507  | 1.520  | 1.534  | 1.547  | 1.561  | 1.574  | 1.070                      |  |
| 1.080   | 1.574  | 1.588                                      | 1.602  | 1.615  | 1.629  | 1.642  | 1.656  | 1.669  | 1.683  | 1.697  | 1.710  | 1.080                      |  |
| 1.090   | 1.710  | 1.724                                      | 1.737  | 1.751  | 1.765  | 1.778  | 1.792  | 1.805  | 1.819  | 1.833  | 1.846  | 1.090                      |  |
| 1.100   | 1.846  | 1.860                                      | 1.874  | 1.888  | 1.901  | 1.914  | 1.928  | 1.942  | 1.955  | 1.969  | 1.983  | 1.100                      |  |
| 1.110   | 1.983  | 1.996                                      | 2.010  | 2.024  | 2.037  | 2.051  | 2.065  | 2.078  | 2.092  | 2.106  | 2.119  | 1.110                      |  |
| 1.120   | 2.119  | 2.133                                      | 2.147  | 2.161  | 2.174  | 2.188  | 2.202  | 2.215  | 2.229  | 2.243  | 2.257  | 1.120                      |  |
| 1.130   | 2.257  | 2.270                                      | 2.284  | 2.298  | 2.311  | 2.325  | 2.339  | 2.353  | 2.366  | 2.380  | 2.394  | 1.130                      |  |
| 1.140   | 2.394  | 2.408                                      | 2.422  | 2.435  | 2.449  | 2.463  | 2.476  | 2.490  | 2.504  | 2.518  | 2.532  | 1.140                      |  |
| 1.150   | 2.532  | 2.545                                      | 2.559  | 2.573  | 2.587  | 2.600  | 2.614  | 2.628  | 2.642  | 2.656  | 2.669  | 1.150                      |  |
| 1.160   | 2.669  | 2.683                                      | 2.697  | 2.711  | 2.725  | 2.739  | 2.752  | 2.766  | 2.780  | 2.794  | 2.808  | 1.160                      |  |
| 1.170   | 2.808  | 2.822                                      | 2.835  | 2.849  | 2.863  | 2.877  | 2.891  | 2.905  | 2.919  | 2.932  | 2.946  | 1.170                      |  |
| 1.180   | 2.946  | 2.960                                      | 2.974  | 2.988  | 2.998  | 3.008  | 3.016  | 3.029  | 3.043  | 3.057  | 3.071  | 1.180                      |  |
| 1.190   | 3.071  | 3.085                                      | 3.099  | 3.113  | 3.127  | 3.140  | 3.154  | 3.168  | 3.182  | 3.196  | 3.210  | 1.190                      |  |
| 1.200   | 3.210  | 3.224                                      | 3.238  | 3.252  | 3.266  | 3.280  | 3.293  | 3.307  | 3.321  | 3.335  | 3.349  | 1.200                      |  |
| 1.210   | 3.349  | 3.363                                      | 3.377  | 3.391  | 3.405  | 3.419  | 3.433  | 3.447  | 3.461  | 3.475  | 3.489  | 1.210                      |  |
| 1.220   | 3.489  | 3.503                                      | 3.517  | 3.531  | 3.545  | 3.559  | 3.573  | 3.587  | 3.601  | 3.615  | 3.629  | 1.220                      |  |
| 1.230   | 3.629  | 3.643                                      | 3.657  | 3.671  | 3.685  | 3.699  | 3.713  | 3.727  | 3.741  | 3.755  | 3.769  | 1.230                      |  |
| 1.240   | 3.769  | 3.783                                      | 3.797  | 3.811  | 3.825  | 3.839  | 3.853  | 3.867  | 3.881  | 3.895  | 3.909  | 1.240                      |  |

TABLE 10.11—Type R thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Celsius (IPTS 1968) |        |        |        |        |        |        |        |        |        | Reference Junctions at 0 C |        |        |       |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------------------------|--------|--------|-------|
|   |        | 0  | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      |                            |        | 10     |       |
| DEG C   |        |  |        |        |        |        |        |        |        |        |        |                            |        |        | DEG C |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                            |        |        |       |
| 1,250   | 13.922 | 13.936                                     | 13.950 | 13.964 | 13.978 | 13.992 | 14.006 | 14.020 | 14.034 | 14.048 | 14.062 | 14.076                     | 14.090 | 14.104 | 1,250 |
| 1,260   | 14.062 | 14.076                                     | 14.090 | 14.104 | 14.118 | 14.132 | 14.146 | 14.160 | 14.174 | 14.188 | 14.202 | 14.216                     | 14.230 | 14.244 | 1,260 |
| 1,270   | 14.202 | 14.216                                     | 14.230 | 14.244 | 14.258 | 14.272 | 14.286 | 14.300 | 14.314 | 14.328 | 14.342 | 14.356                     | 14.370 | 14.384 | 1,270 |
| 1,280   | 14.343 | 14.357                                     | 14.371 | 14.385 | 14.399 | 14.413 | 14.427 | 14.441 | 14.455 | 14.469 | 14.483 | 14.497                     | 14.511 | 14.525 | 1,280 |
| 1,290   | 14.483 | 14.497                                     | 14.511 | 14.525 | 14.539 | 14.553 | 14.567 | 14.581 | 14.595 | 14.609 | 14.623 | 14.637                     | 14.651 | 14.665 | 1,290 |
| 1,300   | 14.624 | 14.638                                     | 14.652 | 14.666 | 14.680 | 14.694 | 14.708 | 14.722 | 14.736 | 14.750 | 14.764 | 14.778                     | 14.792 | 14.806 | 1,300 |
| 1,310   | 14.765 | 14.779                                     | 14.793 | 14.807 | 14.821 | 14.835 | 14.849 | 14.863 | 14.877 | 14.891 | 14.905 | 14.919                     | 14.933 | 14.947 | 1,310 |
| 1,320   | 14.906 | 14.920                                     | 14.934 | 14.948 | 14.962 | 14.976 | 14.990 | 15.004 | 15.018 | 15.032 | 15.046 | 15.060                     | 15.074 | 15.088 | 1,320 |
| 1,330   | 15.047 | 15.061                                     | 15.075 | 15.089 | 15.103 | 15.117 | 15.131 | 15.145 | 15.159 | 15.173 | 15.187 | 15.201                     | 15.215 | 15.229 | 1,330 |
| 1,340   | 15.188 | 15.202                                     | 15.216 | 15.230 | 15.244 | 15.258 | 15.272 | 15.286 | 15.300 | 15.314 | 15.328 | 15.342                     | 15.356 | 15.370 | 1,340 |
| 1,350   | 15.329 | 15.343                                     | 15.357 | 15.371 | 15.385 | 15.399 | 15.413 | 15.427 | 15.441 | 15.455 | 15.469 | 15.483                     | 15.497 | 15.511 | 1,350 |
| 1,360   | 15.472 | 15.486                                     | 15.500 | 15.514 | 15.528 | 15.542 | 15.556 | 15.570 | 15.584 | 15.598 | 15.612 | 15.626                     | 15.640 | 15.654 | 1,360 |
| 1,370   | 15.611 | 15.625                                     | 15.639 | 15.653 | 15.667 | 15.681 | 15.695 | 15.709 | 15.723 | 15.737 | 15.751 | 15.765                     | 15.779 | 15.793 | 1,370 |
| 1,380   | 15.752 | 15.766                                     | 15.780 | 15.794 | 15.808 | 15.822 | 15.836 | 15.850 | 15.864 | 15.878 | 15.892 | 15.906                     | 15.920 | 15.934 | 1,380 |
| 1,390   | 15.893 | 15.907                                     | 15.921 | 15.935 | 15.949 | 15.963 | 15.977 | 15.991 | 16.005 | 16.019 | 16.033 | 16.047                     | 16.061 | 16.075 | 1,390 |
| 1,400   | 16.033 | 16.047                                     | 16.061 | 16.075 | 16.089 | 16.103 | 16.117 | 16.131 | 16.145 | 16.159 | 16.173 | 16.187                     | 16.201 | 16.215 | 1,400 |
| 1,410   | 16.176 | 16.190                                     | 16.204 | 16.218 | 16.232 | 16.246 | 16.260 | 16.274 | 16.288 | 16.302 | 16.316 | 16.330                     | 16.344 | 16.358 | 1,410 |
| 1,420   | 16.317 | 16.331                                     | 16.345 | 16.359 | 16.373 | 16.387 | 16.401 | 16.415 | 16.429 | 16.443 | 16.457 | 16.471                     | 16.485 | 16.499 | 1,420 |
| 1,430   | 16.458 | 16.472                                     | 16.486 | 16.500 | 16.514 | 16.528 | 16.542 | 16.556 | 16.570 | 16.584 | 16.598 | 16.612                     | 16.626 | 16.640 | 1,430 |
| 1,440   | 16.599 | 16.613                                     | 16.627 | 16.641 | 16.655 | 16.669 | 16.683 | 16.697 | 16.711 | 16.725 | 16.739 | 16.753                     | 16.767 | 16.781 | 1,440 |
| 1,450   | 16.741 | 16.755                                     | 16.769 | 16.783 | 16.797 | 16.811 | 16.825 | 16.839 | 16.853 | 16.867 | 16.881 | 16.895                     | 16.909 | 16.923 | 1,450 |
| 1,460   | 16.882 | 16.896                                     | 16.910 | 16.924 | 16.938 | 16.952 | 16.966 | 16.980 | 16.994 | 17.008 | 17.022 | 17.036                     | 17.050 | 17.064 | 1,460 |
| 1,470   | 17.022 | 17.036                                     | 17.050 | 17.064 | 17.078 | 17.092 | 17.106 | 17.120 | 17.134 | 17.148 | 17.162 | 17.176                     | 17.190 | 17.204 | 1,470 |
| 1,480   | 17.163 | 17.177                                     | 17.191 | 17.205 | 17.219 | 17.233 | 17.247 | 17.261 | 17.275 | 17.289 | 17.303 | 17.317                     | 17.331 | 17.345 | 1,480 |
| 1,490   | 17.304 | 17.318                                     | 17.332 | 17.346 | 17.360 | 17.374 | 17.388 | 17.402 | 17.416 | 17.430 | 17.444 | 17.458                     | 17.472 | 17.486 | 1,490 |
| 1,500   | 17.445 | 17.459                                     | 17.473 | 17.487 | 17.501 | 17.515 | 17.529 | 17.543 | 17.557 | 17.571 | 17.585 | 17.599                     | 17.613 | 17.627 | 1,500 |
| 1,510   | 17.585 | 17.599                                     | 17.613 | 17.627 | 17.641 | 17.655 | 17.669 | 17.683 | 17.697 | 17.711 | 17.725 | 17.739                     | 17.753 | 17.767 | 1,510 |
| 1,520   | 17.726 | 17.740                                     | 17.754 | 17.768 | 17.782 | 17.796 | 17.810 | 17.824 | 17.838 | 17.852 | 17.866 | 17.880                     | 17.894 | 17.908 | 1,520 |
| 1,530   | 17.866 | 17.880                                     | 17.894 | 17.908 | 17.922 | 17.936 | 17.950 | 17.964 | 17.978 | 17.992 | 18.006 | 18.020                     | 18.034 | 18.048 | 1,530 |
| 1,540   | 18.006 | 18.020                                     | 18.034 | 18.048 | 18.062 | 18.076 | 18.090 | 18.104 | 18.118 | 18.132 | 18.146 | 18.160                     | 18.174 | 18.188 | 1,540 |
| 1,550   | 18.146 | 18.160                                     | 18.174 | 18.188 | 18.202 | 18.216 | 18.230 | 18.244 | 18.258 | 18.272 | 18.286 | 18.300                     | 18.314 | 18.328 | 1,550 |
| 1,560   | 18.286 | 18.300                                     | 18.314 | 18.328 | 18.342 | 18.356 | 18.370 | 18.384 | 18.398 | 18.412 | 18.426 | 18.440                     | 18.454 | 18.468 | 1,560 |
| 1,570   | 18.425 | 18.439                                     | 18.453 | 18.467 | 18.481 | 18.495 | 18.509 | 18.523 | 18.537 | 18.551 | 18.565 | 18.579                     | 18.593 | 18.607 | 1,570 |
| 1,580   | 18.564 | 18.578                                     | 18.592 | 18.606 | 18.620 | 18.634 | 18.648 | 18.662 | 18.676 | 18.690 | 18.704 | 18.718                     | 18.732 | 18.746 | 1,580 |
| 1,590   | 18.703 | 18.717                                     | 18.731 | 18.745 | 18.759 | 18.773 | 18.787 | 18.801 | 18.815 | 18.829 | 18.843 | 18.857                     | 18.871 | 18.885 | 1,590 |
| 1,600   | 18.842 | 18.856                                     | 18.870 | 18.884 | 18.898 | 18.912 | 18.926 | 18.939 | 18.953 | 18.967 | 18.981 | 18.995                     | 19.009 | 19.023 | 1,600 |
| 1,610   | 18.981 | 18.995                                     | 19.009 | 19.023 | 19.037 | 19.051 | 19.065 | 19.079 | 19.093 | 19.107 | 19.121 | 19.135                     | 19.149 | 19.163 | 1,610 |
| 1,620   | 19.119 | 19.133                                     | 19.147 | 19.161 | 19.175 | 19.189 | 19.203 | 19.217 | 19.231 | 19.245 | 19.259 | 19.273                     | 19.287 | 19.301 | 1,620 |
| 1,630   | 19.257 | 19.271                                     | 19.285 | 19.299 | 19.313 | 19.327 | 19.341 | 19.355 | 19.369 | 19.383 | 19.397 | 19.411                     | 19.425 | 19.439 | 1,630 |
| 1,640   | 19.395 | 19.409                                     | 19.423 | 19.437 | 19.451 | 19.465 | 19.479 | 19.493 | 19.507 | 19.521 | 19.535 | 19.549                     | 19.563 | 19.577 | 1,640 |
| 1,650   | 19.533 | 19.547                                     | 19.561 | 19.575 | 19.589 | 19.603 | 19.617 | 19.631 | 19.645 | 19.659 | 19.673 | 19.687                     | 19.701 | 19.715 | 1,650 |
| 1,660   | 19.670 | 19.684                                     | 19.698 | 19.712 | 19.726 | 19.740 | 19.754 | 19.768 | 19.782 | 19.796 | 19.810 | 19.824                     | 19.838 | 19.852 | 1,660 |
| 1,670   | 19.807 | 19.821                                     | 19.835 | 19.849 | 19.863 | 19.877 | 19.891 | 19.905 | 19.919 | 19.933 | 19.947 | 19.961                     | 19.975 | 19.989 | 1,670 |
| 1,680   | 19.944 | 19.958                                     | 19.972 | 19.986 | 19.999 | 20.013 | 20.027 | 20.041 | 20.055 | 20.069 | 20.083 | 20.097                     | 20.111 | 20.125 | 1,680 |
| 1,690   | 20.080 | 20.094                                     | 20.108 | 20.122 | 20.136 | 20.150 | 20.164 | 20.178 | 20.192 | 20.206 | 20.220 | 20.234                     | 20.248 | 20.262 | 1,690 |
| 1,700   | 20.215 | 20.229                                     | 20.243 | 20.257 | 20.271 | 20.285 | 20.299 | 20.313 | 20.327 | 20.341 | 20.355 | 20.369                     | 20.383 | 20.397 | 1,700 |
| 1,710   | 20.350 | 20.364                                     | 20.378 | 20.392 | 20.406 | 20.420 | 20.434 | 20.448 | 20.462 | 20.476 | 20.490 | 20.504                     | 20.518 | 20.532 | 1,710 |
| 1,720   | 20.483 | 20.497                                     | 20.511 | 20.525 | 20.539 | 20.553 | 20.567 | 20.581 | 20.595 | 20.609 | 20.623 | 20.637                     | 20.651 | 20.665 | 1,720 |
| 1,730   | 20.616 | 20.630                                     | 20.644 | 20.658 | 20.672 | 20.686 | 20.700 | 20.714 | 20.728 | 20.742 | 20.756 | 20.770                     | 20.784 | 20.798 | 1,730 |
| 1,740   | 20.748 | 20.762                                     | 20.776 | 20.790 | 20.804 | 20.818 | 20.832 | 20.846 | 20.860 | 20.874 | 20.888 | 20.902                     | 20.916 | 20.930 | 1,740 |
| 1,750   | 20.878 | 20.892                                     | 20.906 | 20.920 | 20.934 | 20.948 | 20.962 | 20.976 | 20.990 | 20.999 | 21.008 | 21.017                     | 21.026 | 21.035 | 1,750 |
| 1,760   | 21.006 | 21.019                                     | 21.032 | 21.045 | 21.057 | 21.070 | 21.083 | 21.096 | 21.108 | 21.121 | 21.134 | 21.147                     | 21.160 | 21.173 | 1,760 |
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     |                            |        |        | DEG C |

TABLE 10.12—Type S thermocouples (deg F-millivolts).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit* |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|------------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
| DEG F   | 0      | 1                                  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |                                    |        |        |        |        |        |        |        |        |        |                             |  |
| -50   | -0.210 | -0.220                             | -0.222 | -0.225 | -0.227 | -0.229 | -0.231 | -0.233 | -0.236 |        |        | -50                         |  |
| -40   | -0.194 | -0.197                             | -0.199 | -0.202 | -0.204 | -0.206 | -0.209 | -0.211 | -0.213 | -0.215 | -0.218 | -40                         |  |
| -30   | -0.170 | -0.173                             | -0.175 | -0.178 | -0.180 | -0.182 | -0.185 | -0.187 | -0.190 | -0.192 | -0.194 | -30                         |  |
| -20   | -0.145 | -0.148                             | -0.150 | -0.153 | -0.155 | -0.158 | -0.160 | -0.163 | -0.165 | -0.168 | -0.170 | -20                         |  |
| -10   | -0.119 | -0.122                             | -0.124 | -0.127 | -0.129 | -0.132 | -0.135 | -0.137 | -0.140 | -0.142 | -0.145 | -10                         |  |
| 0   | -0.092 | -0.095                             | -0.097 | -0.100 | -0.103 | -0.106 | -0.108 | -0.111 | -0.114 | -0.116 | -0.119 | 0                           |  |
| 0   | -0.092 | -0.089                             | -0.086 | -0.084 | -0.081 | -0.078 | -0.075 | -0.073 | -0.070 | -0.067 | -0.064 | 0                           |  |
| 10  | -0.064 | -0.061                             | -0.058 | -0.056 | -0.052 | -0.050 | -0.047 | -0.044 | -0.041 | -0.038 | -0.035 | 10                          |  |
| 20  | -0.035 | -0.033                             | -0.030 | -0.027 | -0.024 | -0.021 | -0.018 | -0.015 | -0.012 | -0.009 | -0.006 | 20                          |  |
| 30  | -0.006 | -0.003                             | 0.000  | 0.003  | 0.006  | 0.009  | 0.012  | 0.015  | 0.016  | 0.021  | 0.024  | 30                          |  |
| 40  | 0.024  | 0.027                              | 0.030  | 0.033  | 0.037  | 0.040  | 0.043  | 0.046  | 0.049  | 0.052  | 0.055  | 40                          |  |
| 50  | 0.055  | 0.058                              | 0.062  | 0.065  | 0.068  | 0.071  | 0.074  | 0.077  | 0.081  | 0.084  | 0.087  | 50                          |  |
| 60  | 0.087  | 0.090                              | 0.093  | 0.097  | 0.100  | 0.103  | 0.106  | 0.110  | 0.113  | 0.116  | 0.119  | 60                          |  |
| 70  | 0.119  | 0.123                              | 0.126  | 0.129  | 0.133  | 0.136  | 0.139  | 0.142  | 0.146  | 0.149  | 0.152  | 70                          |  |
| 80  | 0.152  | 0.156                              | 0.159  | 0.163  | 0.166  | 0.169  | 0.173  | 0.176  | 0.179  | 0.183  | 0.186  | 80                          |  |
| 90  | 0.186  | 0.190                              | 0.193  | 0.197  | 0.200  | 0.203  | 0.207  | 0.210  | 0.214  | 0.217  | 0.221  | 90                          |  |
| 100   | 0.221  | 0.224                              | 0.228  | 0.231  | 0.235  | 0.238  | 0.242  | 0.245  | 0.249  | 0.252  | 0.256  | 100                         |  |
| 110   | 0.256  | 0.259                              | 0.263  | 0.266  | 0.270  | 0.274  | 0.277  | 0.281  | 0.284  | 0.288  | 0.291  | 110                         |  |
| 120   | 0.291  | 0.295                              | 0.299  | 0.302  | 0.306  | 0.309  | 0.313  | 0.317  | 0.320  | 0.324  | 0.328  | 120                         |  |
| 130   | 0.328  | 0.331                              | 0.335  | 0.339  | 0.342  | 0.346  | 0.350  | 0.353  | 0.357  | 0.361  | 0.365  | 130                         |  |
| 140   | 0.365  | 0.368                              | 0.372  | 0.376  | 0.379  | 0.383  | 0.387  | 0.391  | 0.394  | 0.398  | 0.402  | 140                         |  |
| 150   | 0.402  | 0.406                              | 0.409  | 0.413  | 0.417  | 0.421  | 0.425  | 0.428  | 0.432  | 0.436  | 0.440  | 150                         |  |
| 160   | 0.440  | 0.444                              | 0.448  | 0.451  | 0.455  | 0.459  | 0.463  | 0.467  | 0.471  | 0.474  | 0.478  | 160                         |  |
| 170   | 0.478  | 0.482                              | 0.486  | 0.490  | 0.494  | 0.498  | 0.502  | 0.506  | 0.510  | 0.513  | 0.517  | 170                         |  |
| 180   | 0.517  | 0.521                              | 0.525  | 0.529  | 0.533  | 0.537  | 0.541  | 0.545  | 0.549  | 0.553  | 0.557  | 180                         |  |
| 190   | 0.557  | 0.561                              | 0.565  | 0.569  | 0.573  | 0.577  | 0.581  | 0.585  | 0.589  | 0.593  | 0.597  | 190                         |  |
| 200   | 0.597  | 0.601                              | 0.605  | 0.609  | 0.613  | 0.617  | 0.621  | 0.625  | 0.629  | 0.633  | 0.637  | 200                         |  |
| 210   | 0.637  | 0.641                              | 0.645  | 0.649  | 0.653  | 0.658  | 0.662  | 0.666  | 0.670  | 0.674  | 0.678  | 210                         |  |
| 220   | 0.678  | 0.682                              | 0.686  | 0.690  | 0.695  | 0.699  | 0.703  | 0.707  | 0.711  | 0.715  | 0.719  | 220                         |  |
| 230   | 0.719  | 0.724                              | 0.728  | 0.732  | 0.736  | 0.740  | 0.744  | 0.749  | 0.753  | 0.757  | 0.761  | 230                         |  |
| 240   | 0.761  | 0.765                              | 0.770  | 0.774  | 0.778  | 0.782  | 0.786  | 0.791  | 0.795  | 0.799  | 0.803  | 240                         |  |
| 250   | 0.803  | 0.808                              | 0.812  | 0.816  | 0.820  | 0.824  | 0.829  | 0.833  | 0.837  | 0.842  | 0.846  | 250                         |  |
| 260   | 0.846  | 0.850                              | 0.854  | 0.859  | 0.863  | 0.867  | 0.872  | 0.876  | 0.880  | 0.884  | 0.889  | 260                         |  |
| 270   | 0.889  | 0.893                              | 0.897  | 0.902  | 0.906  | 0.910  | 0.915  | 0.919  | 0.923  | 0.928  | 0.932  | 270                         |  |
| 280   | 0.932  | 0.936                              | 0.941  | 0.945  | 0.950  | 0.954  | 0.958  | 0.963  | 0.967  | 0.971  | 0.976  | 280                         |  |
| 290   | 0.976  | 0.980                              | 0.985  | 0.989  | 0.993  | 0.998  | 1.002  | 1.007  | 1.011  | 1.015  | 1.020  | 290                         |  |
| 300   | 1.020  | 1.024                              | 1.029  | 1.033  | 1.037  | 1.042  | 1.046  | 1.051  | 1.055  | 1.060  | 1.064  | 300                         |  |
| 310   | 1.064  | 1.069                              | 1.073  | 1.078  | 1.082  | 1.087  | 1.091  | 1.095  | 1.100  | 1.104  | 1.109  | 310                         |  |
| 320   | 1.109  | 1.113                              | 1.118  | 1.122  | 1.127  | 1.131  | 1.136  | 1.140  | 1.145  | 1.149  | 1.154  | 320                         |  |
| 330   | 1.154  | 1.158                              | 1.163  | 1.168  | 1.172  | 1.177  | 1.181  | 1.186  | 1.190  | 1.195  | 1.199  | 330                         |  |
| 340   | 1.199  | 1.204                              | 1.208  | 1.213  | 1.218  | 1.222  | 1.227  | 1.231  | 1.236  | 1.240  | 1.245  | 340                         |  |
| 350   | 1.245  | 1.250                              | 1.254  | 1.259  | 1.263  | 1.268  | 1.273  | 1.277  | 1.282  | 1.286  | 1.291  | 350                         |  |
| 360   | 1.291  | 1.296                              | 1.300  | 1.305  | 1.309  | 1.314  | 1.319  | 1.323  | 1.328  | 1.333  | 1.337  | 360                         |  |
| 370   | 1.337  | 1.342                              | 1.347  | 1.351  | 1.356  | 1.360  | 1.365  | 1.370  | 1.374  | 1.379  | 1.384  | 370                         |  |
| 380   | 1.384  | 1.388                              | 1.393  | 1.398  | 1.402  | 1.407  | 1.412  | 1.417  | 1.421  | 1.426  | 1.431  | 380                         |  |
| 390   | 1.431  | 1.435                              | 1.440  | 1.445  | 1.449  | 1.454  | 1.459  | 1.464  | 1.468  | 1.473  | 1.478  | 390                         |  |
| 400   | 1.478  | 1.482                              | 1.487  | 1.492  | 1.497  | 1.501  | 1.506  | 1.511  | 1.516  | 1.520  | 1.525  | 400                         |  |
| 410   | 1.525  | 1.530                              | 1.535  | 1.539  | 1.544  | 1.549  | 1.554  | 1.558  | 1.563  | 1.568  | 1.573  | 410                         |  |
| 420   | 1.573  | 1.577                              | 1.582  | 1.587  | 1.592  | 1.597  | 1.601  | 1.606  | 1.611  | 1.616  | 1.620  | 420                         |  |
| 430   | 1.620  | 1.625                              | 1.630  | 1.635  | 1.640  | 1.644  | 1.649  | 1.654  | 1.659  | 1.664  | 1.669  | 430                         |  |
| 440   | 1.669  | 1.673                              | 1.678  | 1.683  | 1.688  | 1.693  | 1.698  | 1.702  | 1.707  | 1.712  | 1.717  | 440                         |  |
| 450   | 1.717  | 1.722                              | 1.727  | 1.731  | 1.736  | 1.741  | 1.746  | 1.751  | 1.756  | 1.761  | 1.765  | 450                         |  |
| 460   | 1.765  | 1.770                              | 1.775  | 1.780  | 1.785  | 1.790  | 1.795  | 1.799  | 1.804  | 1.809  | 1.814  | 460                         |  |
| 470   | 1.814  | 1.819                              | 1.824  | 1.829  | 1.834  | 1.839  | 1.843  | 1.848  | 1.853  | 1.858  | 1.863  | 470                         |  |
| 480   | 1.863  | 1.868                              | 1.873  | 1.878  | 1.883  | 1.888  | 1.893  | 1.898  | 1.902  | 1.907  | 1.912  | 480                         |  |
| 490   | 1.912  | 1.917                              | 1.922  | 1.927  | 1.932  | 1.937  | 1.942  | 1.947  | 1.952  | 1.957  | 1.962  | 490                         |  |
| 500   | 1.962  | 1.967                              | 1.972  | 1.977  | 1.981  | 1.986  | 1.991  | 1.996  | 2.001  | 2.006  | 2.011  | 500                         |  |
| 510   | 2.011  | 2.016                              | 2.021  | 2.026  | 2.031  | 2.036  | 2.041  | 2.046  | 2.051  | 2.056  | 2.061  | 510                         |  |
| 520   | 2.061  | 2.066                              | 2.071  | 2.076  | 2.081  | 2.086  | 2.091  | 2.096  | 2.101  | 2.106  | 2.111  | 520                         |  |
| 530   | 2.111  | 2.116                              | 2.121  | 2.126  | 2.131  | 2.136  | 2.141  | 2.146  | 2.151  | 2.156  | 2.161  | 530                         |  |
| 540   | 2.161  | 2.166                              | 2.171  | 2.176  | 2.181  | 2.186  | 2.191  | 2.196  | 2.201  | 2.206  | 2.211  | 540                         |  |

\* Converted from degrees Celsius (IP15 1968)



TABLE 10.12—Type S thermocouples (continued).

| DEG F   | Temperature in Degrees Fahrenheit* |       |       |       |       |       |       |       |       |       | DEG F |                             |
|---|------------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-----------------------------|
|   | EMF in Absolute Millivolts         |       |       |       |       |       |       |       |       |       |       | Reference Junctions at 32 F |
|   | 0                                  | 1     | 2     | 3     | 4     | 5     | 6     | 7     | 8     | 9     |       | 10                          |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |                                    |       |       |       |       |       |       |       |       |       |       |                             |
| 590   | 2.211                              | 2.216 | 2.221 | 2.227 | 2.232 | 2.237 | 2.242 | 2.247 | 2.252 | 2.257 | 2.262 | 590                         |
| 560   | 2.262                              | 2.267 | 2.272 | 2.277 | 2.282 | 2.287 | 2.292 | 2.297 | 2.302 | 2.307 | 2.313 | 560                         |
| 570   | 2.313                              | 2.318 | 2.323 | 2.328 | 2.333 | 2.338 | 2.343 | 2.348 | 2.353 | 2.358 | 2.363 | 570                         |
| 580   | 2.363                              | 2.368 | 2.374 | 2.379 | 2.384 | 2.389 | 2.394 | 2.399 | 2.404 | 2.409 | 2.414 | 580                         |
| 590   | 2.414                              | 2.419 | 2.425 | 2.430 | 2.435 | 2.440 | 2.445 | 2.450 | 2.455 | 2.460 | 2.465 | 590                         |
| 600   | 2.465                              | 2.471 | 2.476 | 2.481 | 2.486 | 2.491 | 2.496 | 2.501 | 2.506 | 2.512 | 2.517 | 600                         |
| 610   | 2.517                              | 2.522 | 2.527 | 2.532 | 2.537 | 2.542 | 2.548 | 2.553 | 2.558 | 2.563 | 2.568 | 610                         |
| 620   | 2.568                              | 2.573 | 2.578 | 2.584 | 2.589 | 2.594 | 2.599 | 2.604 | 2.609 | 2.615 | 2.620 | 620                         |
| 630   | 2.620                              | 2.625 | 2.630 | 2.635 | 2.640 | 2.646 | 2.651 | 2.656 | 2.661 | 2.666 | 2.672 | 630                         |
| 640   | 2.672                              | 2.677 | 2.682 | 2.687 | 2.692 | 2.697 | 2.703 | 2.708 | 2.713 | 2.718 | 2.723 | 640                         |
| 650   | 2.723                              | 2.729 | 2.734 | 2.739 | 2.744 | 2.749 | 2.755 | 2.760 | 2.765 | 2.770 | 2.775 | 650                         |
| 660   | 2.775                              | 2.781 | 2.786 | 2.791 | 2.796 | 2.801 | 2.807 | 2.812 | 2.817 | 2.822 | 2.828 | 660                         |
| 670   | 2.828                              | 2.833 | 2.838 | 2.843 | 2.848 | 2.854 | 2.859 | 2.864 | 2.869 | 2.875 | 2.880 | 670                         |
| 680   | 2.880                              | 2.885 | 2.890 | 2.895 | 2.901 | 2.906 | 2.911 | 2.916 | 2.922 | 2.927 | 2.932 | 680                         |
| 690   | 2.932                              | 2.937 | 2.943 | 2.948 | 2.953 | 2.958 | 2.964 | 2.969 | 2.974 | 2.979 | 2.985 | 690                         |
| 700   | 2.985                              | 2.990 | 2.995 | 3.000 | 3.006 | 3.011 | 3.016 | 3.022 | 3.027 | 3.032 | 3.037 | 700                         |
| 710   | 3.037                              | 3.043 | 3.048 | 3.053 | 3.058 | 3.064 | 3.069 | 3.074 | 3.080 | 3.085 | 3.090 | 710                         |
| 720   | 3.090                              | 3.095 | 3.101 | 3.106 | 3.111 | 3.117 | 3.122 | 3.127 | 3.132 | 3.138 | 3.143 | 720                         |
| 730   | 3.143                              | 3.148 | 3.154 | 3.159 | 3.164 | 3.169 | 3.175 | 3.180 | 3.185 | 3.191 | 3.196 | 730                         |
| 740   | 3.196                              | 3.201 | 3.207 | 3.212 | 3.217 | 3.223 | 3.228 | 3.233 | 3.238 | 3.244 | 3.249 | 740                         |
| 750   | 3.249                              | 3.254 | 3.260 | 3.265 | 3.270 | 3.276 | 3.281 | 3.286 | 3.292 | 3.297 | 3.302 | 750                         |
| 760   | 3.302                              | 3.308 | 3.313 | 3.318 | 3.324 | 3.329 | 3.334 | 3.340 | 3.345 | 3.350 | 3.356 | 760                         |
| 770   | 3.356                              | 3.361 | 3.366 | 3.372 | 3.377 | 3.382 | 3.388 | 3.393 | 3.398 | 3.404 | 3.409 | 770                         |
| 780   | 3.409                              | 3.414 | 3.420 | 3.425 | 3.430 | 3.436 | 3.441 | 3.447 | 3.452 | 3.457 | 3.463 | 780                         |
| 790   | 3.463                              | 3.468 | 3.473 | 3.479 | 3.484 | 3.489 | 3.495 | 3.500 | 3.506 | 3.511 | 3.516 | 790                         |
| 800   | 3.516                              | 3.522 | 3.527 | 3.532 | 3.538 | 3.543 | 3.549 | 3.554 | 3.559 | 3.565 | 3.570 | 800                         |
| 810   | 3.570                              | 3.575 | 3.581 | 3.586 | 3.592 | 3.597 | 3.602 | 3.608 | 3.613 | 3.619 | 3.624 | 810                         |
| 820   | 3.624                              | 3.629 | 3.635 | 3.640 | 3.645 | 3.651 | 3.656 | 3.662 | 3.667 | 3.672 | 3.678 | 820                         |
| 830   | 3.678                              | 3.683 | 3.689 | 3.694 | 3.699 | 3.705 | 3.710 | 3.716 | 3.721 | 3.726 | 3.732 | 830                         |
| 840   | 3.732                              | 3.737 | 3.743 | 3.748 | 3.754 | 3.759 | 3.764 | 3.770 | 3.775 | 3.781 | 3.786 | 840                         |
| 850   | 3.786                              | 3.791 | 3.797 | 3.802 | 3.808 | 3.813 | 3.819 | 3.824 | 3.829 | 3.835 | 3.840 | 850                         |
| 860   | 3.840                              | 3.846 | 3.851 | 3.857 | 3.862 | 3.867 | 3.873 | 3.878 | 3.884 | 3.889 | 3.895 | 860                         |
| 870   | 3.895                              | 3.900 | 3.906 | 3.911 | 3.916 | 3.922 | 3.927 | 3.933 | 3.938 | 3.944 | 3.949 | 870                         |
| 880   | 3.949                              | 3.955 | 3.960 | 3.965 | 3.971 | 3.976 | 3.982 | 3.987 | 3.993 | 3.998 | 4.004 | 880                         |
| 890   | 4.004                              | 4.009 | 4.015 | 4.020 | 4.025 | 4.031 | 4.036 | 4.042 | 4.047 | 4.053 | 4.058 | 890                         |
| 900   | 4.058                              | 4.064 | 4.069 | 4.075 | 4.080 | 4.086 | 4.091 | 4.096 | 4.102 | 4.107 | 4.113 | 900                         |
| 910   | 4.113                              | 4.118 | 4.124 | 4.129 | 4.135 | 4.140 | 4.146 | 4.151 | 4.157 | 4.162 | 4.168 | 910                         |
| 920   | 4.168                              | 4.173 | 4.179 | 4.184 | 4.190 | 4.195 | 4.201 | 4.206 | 4.212 | 4.217 | 4.223 | 920                         |
| 930   | 4.223                              | 4.228 | 4.234 | 4.239 | 4.245 | 4.250 | 4.256 | 4.261 | 4.267 | 4.272 | 4.278 | 930                         |
| 940   | 4.278                              | 4.283 | 4.289 | 4.294 | 4.300 | 4.305 | 4.311 | 4.316 | 4.322 | 4.327 | 4.333 | 940                         |
| 950   | 4.333                              | 4.338 | 4.344 | 4.349 | 4.355 | 4.360 | 4.366 | 4.371 | 4.377 | 4.382 | 4.388 | 950                         |
| 960   | 4.388                              | 4.393 | 4.399 | 4.404 | 4.410 | 4.415 | 4.421 | 4.426 | 4.432 | 4.438 | 4.443 | 960                         |
| 970   | 4.443                              | 4.449 | 4.454 | 4.460 | 4.465 | 4.471 | 4.476 | 4.482 | 4.487 | 4.493 | 4.498 | 970                         |
| 980   | 4.498                              | 4.504 | 4.509 | 4.515 | 4.521 | 4.526 | 4.532 | 4.537 | 4.543 | 4.548 | 4.554 | 980                         |
| 990   | 4.554                              | 4.559 | 4.565 | 4.570 | 4.576 | 4.582 | 4.587 | 4.593 | 4.598 | 4.604 | 4.609 | 990                         |
| 1.000   | 4.609                              | 4.615 | 4.620 | 4.626 | 4.632 | 4.637 | 4.643 | 4.648 | 4.654 | 4.659 | 4.665 | 1.000                       |
| 1.010   | 4.665                              | 4.670 | 4.676 | 4.682 | 4.687 | 4.693 | 4.698 | 4.704 | 4.709 | 4.715 | 4.721 | 1.010                       |
| 1.020   | 4.721                              | 4.726 | 4.732 | 4.737 | 4.743 | 4.748 | 4.754 | 4.760 | 4.765 | 4.771 | 4.776 | 1.020                       |
| 1.030   | 4.776                              | 4.782 | 4.788 | 4.793 | 4.799 | 4.804 | 4.810 | 4.815 | 4.821 | 4.827 | 4.832 | 1.030                       |
| 1.040   | 4.832                              | 4.838 | 4.843 | 4.849 | 4.855 | 4.860 | 4.866 | 4.871 | 4.877 | 4.883 | 4.888 | 1.040                       |
| 1.050   | 4.888                              | 4.894 | 4.899 | 4.905 | 4.911 | 4.916 | 4.922 | 4.927 | 4.933 | 4.939 | 4.944 | 1.050                       |
| 1.060   | 4.944                              | 4.950 | 4.956 | 4.961 | 4.967 | 4.972 | 4.978 | 4.984 | 4.989 | 4.995 | 5.000 | 1.060                       |
| 1.070   | 5.000                              | 5.006 | 5.012 | 5.017 | 5.023 | 5.029 | 5.034 | 5.040 | 5.045 | 5.051 | 5.057 | 1.070                       |
| 1.080   | 5.057                              | 5.062 | 5.068 | 5.074 | 5.079 | 5.085 | 5.090 | 5.096 | 5.102 | 5.107 | 5.113 | 1.080                       |
| 1.090   | 5.113                              | 5.119 | 5.124 | 5.130 | 5.136 | 5.141 | 5.147 | 5.153 | 5.158 | 5.164 | 5.169 | 1.090                       |
| 1.100   | 5.169                              | 5.175 | 5.181 | 5.186 | 5.192 | 5.198 | 5.203 | 5.209 | 5.215 | 5.220 | 5.226 | 1.100                       |
| 1.110   | 5.226                              | 5.232 | 5.237 | 5.243 | 5.249 | 5.254 | 5.260 | 5.265 | 5.271 | 5.277 | 5.283 | 1.110                       |
| 1.120   | 5.283                              | 5.288 | 5.294 | 5.300 | 5.305 | 5.311 | 5.317 | 5.322 | 5.328 | 5.334 | 5.339 | 1.120                       |
| 1.130   | 5.339                              | 5.345 | 5.351 | 5.356 | 5.362 | 5.368 | 5.373 | 5.379 | 5.385 | 5.391 | 5.396 | 1.130                       |
| 1.140   | 5.396                              | 5.402 | 5.408 | 5.413 | 5.419 | 5.425 | 5.430 | 5.436 | 5.442 | 5.447 | 5.453 | 1.140                       |
| 1.150   | 5.453                              | 5.459 | 5.465 | 5.470 | 5.476 | 5.482 | 5.487 | 5.493 | 5.499 | 5.504 | 5.510 | 1.150                       |
| 1.160   | 5.510                              | 5.516 | 5.522 | 5.527 | 5.533 | 5.539 | 5.544 | 5.550 | 5.556 | 5.562 | 5.567 | 1.160                       |
| 1.170   | 5.567                              | 5.573 | 5.579 | 5.585 | 5.590 | 5.596 | 5.602 | 5.608 | 5.613 | 5.619 | 5.625 | 1.170                       |
| 1.180   | 5.625                              | 5.631 | 5.636 | 5.642 | 5.648 | 5.653 | 5.659 | 5.665 | 5.671 | 5.676 | 5.682 | 1.180                       |
| 1.190   | 5.682                              | 5.688 | 5.694 | 5.700 | 5.705 | 5.711 | 5.717 | 5.723 | 5.728 | 5.734 | 5.740 | 1.190                       |
| DEG F   | 0                                  | 1     | 2     | 3     | 4     | 5     | 6     | 7     | 8     | 9     | 10    | DEG F                       |

\* Converted from degrees Celsius (IPTS 1968).

TABLE 10.12—Type S thermocouples (continued).

| EMF in Absolute Millivolts                    |       | Temperature in Degrees Fahrenheit* |       |       |       |       |       |       |       |       |       | Reference Junctions at 32 F |  |
|---|-------|------------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-----------------------------|--|
| DEG F   | 0     | 1                                  | 2     | 3     | 4     | 5     | 6     | 7     | 8     | 9     | 10    | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |       |                                    |       |       |       |       |       |       |       |       |       |                             |  |
| 1,200   | 5.740 | 5.746                              | 5.751 | 5.757 | 5.763 | 5.769 | 5.774 | 5.780 | 5.786 | 5.792 | 5.797 | 1,200                       |  |
| 1,210   | 5.797 | 5.803                              | 5.809 | 5.815 | 5.821 | 5.826 | 5.832 | 5.838 | 5.844 | 5.849 | 5.855 | 1,210                       |  |
| 1,220   | 5.855 | 5.861                              | 5.867 | 5.873 | 5.878 | 5.884 | 5.890 | 5.896 | 5.902 | 5.907 | 5.913 | 1,220                       |  |
| 1,230   | 5.913 | 5.919                              | 5.925 | 5.931 | 5.936 | 5.942 | 5.948 | 5.954 | 5.960 | 5.965 | 5.971 | 1,230                       |  |
| 1,240   | 5.971 | 5.977                              | 5.983 | 5.989 | 5.994 | 6.000 | 6.006 | 6.012 | 6.018 | 6.023 | 6.029 | 1,240                       |  |
| 1,250   | 6.029 | 6.035                              | 6.041 | 6.047 | 6.052 | 6.058 | 6.064 | 6.070 | 6.076 | 6.082 | 6.087 | 1,250                       |  |
| 1,260   | 6.087 | 6.093                              | 6.099 | 6.105 | 6.111 | 6.117 | 6.122 | 6.128 | 6.134 | 6.140 | 6.146 | 1,260                       |  |
| 1,270   | 6.146 | 6.152                              | 6.157 | 6.163 | 6.169 | 6.175 | 6.181 | 6.187 | 6.192 | 6.198 | 6.204 | 1,270                       |  |
| 1,280   | 6.204 | 6.210                              | 6.216 | 6.222 | 6.227 | 6.233 | 6.239 | 6.245 | 6.251 | 6.257 | 6.263 | 1,280                       |  |
| 1,290   | 6.263 | 6.268                              | 6.274 | 6.280 | 6.286 | 6.292 | 6.298 | 6.304 | 6.309 | 6.315 | 6.321 | 1,290                       |  |
| 1,300   | 6.321 | 6.327                              | 6.333 | 6.339 | 6.345 | 6.350 | 6.356 | 6.362 | 6.368 | 6.374 | 6.380 | 1,300                       |  |
| 1,310   | 6.380 | 6.386                              | 6.392 | 6.397 | 6.403 | 6.409 | 6.415 | 6.421 | 6.427 | 6.433 | 6.439 | 1,310                       |  |
| 1,320   | 6.439 | 6.445                              | 6.450 | 6.456 | 6.462 | 6.468 | 6.474 | 6.480 | 6.486 | 6.492 | 6.498 | 1,320                       |  |
| 1,330   | 6.498 | 6.503                              | 6.509 | 6.515 | 6.521 | 6.527 | 6.533 | 6.539 | 6.545 | 6.551 | 6.557 | 1,330                       |  |
| 1,340   | 6.557 | 6.562                              | 6.568 | 6.574 | 6.580 | 6.586 | 6.592 | 6.598 | 6.604 | 6.610 | 6.616 | 1,340                       |  |
| 1,350   | 6.616 | 6.622                              | 6.627 | 6.633 | 6.639 | 6.645 | 6.651 | 6.657 | 6.663 | 6.669 | 6.675 | 1,350                       |  |
| 1,360   | 6.675 | 6.681                              | 6.687 | 6.693 | 6.699 | 6.704 | 6.710 | 6.716 | 6.722 | 6.728 | 6.734 | 1,360                       |  |
| 1,370   | 6.734 | 6.740                              | 6.746 | 6.752 | 6.758 | 6.764 | 6.770 | 6.776 | 6.782 | 6.788 | 6.794 | 1,370                       |  |
| 1,380   | 6.794 | 6.800                              | 6.805 | 6.811 | 6.817 | 6.823 | 6.829 | 6.835 | 6.841 | 6.847 | 6.853 | 1,380                       |  |
| 1,390   | 6.853 | 6.859                              | 6.865 | 6.871 | 6.877 | 6.883 | 6.889 | 6.895 | 6.901 | 6.907 | 6.913 | 1,390                       |  |
| 1,400   | 6.913 | 6.919                              | 6.925 | 6.931 | 6.937 | 6.943 | 6.948 | 6.954 | 6.960 | 6.966 | 6.972 | 1,400                       |  |
| 1,410   | 6.972 | 6.978                              | 6.984 | 6.990 | 6.996 | 7.002 | 7.008 | 7.014 | 7.020 | 7.026 | 7.032 | 1,410                       |  |
| 1,420   | 7.032 | 7.038                              | 7.044 | 7.050 | 7.056 | 7.062 | 7.068 | 7.074 | 7.080 | 7.086 | 7.092 | 1,420                       |  |
| 1,430   | 7.092 | 7.098                              | 7.104 | 7.110 | 7.116 | 7.122 | 7.128 | 7.134 | 7.140 | 7.146 | 7.152 | 1,430                       |  |
| 1,440   | 7.152 | 7.158                              | 7.164 | 7.170 | 7.176 | 7.182 | 7.188 | 7.194 | 7.200 | 7.206 | 7.212 | 1,440                       |  |
| 1,450   | 7.212 | 7.218                              | 7.224 | 7.230 | 7.236 | 7.242 | 7.248 | 7.254 | 7.260 | 7.266 | 7.272 | 1,450                       |  |
| 1,460   | 7.272 | 7.278                              | 7.285 | 7.291 | 7.297 | 7.303 | 7.309 | 7.315 | 7.321 | 7.327 | 7.333 | 1,460                       |  |
| 1,470   | 7.333 | 7.339                              | 7.345 | 7.351 | 7.357 | 7.363 | 7.369 | 7.375 | 7.381 | 7.387 | 7.393 | 1,470                       |  |
| 1,480   | 7.393 | 7.399                              | 7.405 | 7.411 | 7.417 | 7.423 | 7.429 | 7.436 | 7.442 | 7.448 | 7.454 | 1,480                       |  |
| 1,490   | 7.454 | 7.460                              | 7.466 | 7.472 | 7.478 | 7.484 | 7.490 | 7.496 | 7.502 | 7.508 | 7.514 | 1,490                       |  |
| 1,500   | 7.514 | 7.520                              | 7.526 | 7.533 | 7.539 | 7.545 | 7.551 | 7.557 | 7.563 | 7.569 | 7.575 | 1,500                       |  |
| 1,510   | 7.575 | 7.581                              | 7.587 | 7.593 | 7.599 | 7.605 | 7.612 | 7.618 | 7.624 | 7.630 | 7.636 | 1,510                       |  |
| 1,520   | 7.636 | 7.642                              | 7.648 | 7.654 | 7.660 | 7.666 | 7.672 | 7.679 | 7.685 | 7.691 | 7.697 | 1,520                       |  |
| 1,530   | 7.697 | 7.703                              | 7.709 | 7.715 | 7.721 | 7.727 | 7.733 | 7.740 | 7.746 | 7.752 | 7.758 | 1,530                       |  |
| 1,540   | 7.758 | 7.764                              | 7.770 | 7.776 | 7.782 | 7.788 | 7.795 | 7.801 | 7.807 | 7.813 | 7.819 | 1,540                       |  |
| 1,550   | 7.819 | 7.825                              | 7.831 | 7.837 | 7.843 | 7.850 | 7.856 | 7.862 | 7.868 | 7.874 | 7.880 | 1,550                       |  |
| 1,560   | 7.880 | 7.886                              | 7.892 | 7.899 | 7.905 | 7.911 | 7.917 | 7.923 | 7.929 | 7.935 | 7.942 | 1,560                       |  |
| 1,570   | 7.942 | 7.948                              | 7.954 | 7.960 | 7.966 | 7.972 | 7.978 | 7.985 | 7.991 | 7.997 | 8.003 | 1,570                       |  |
| 1,580   | 8.003 | 8.009                              | 8.015 | 8.021 | 8.028 | 8.034 | 8.040 | 8.046 | 8.052 | 8.058 | 8.065 | 1,580                       |  |
| 1,590   | 8.065 | 8.071                              | 8.077 | 8.083 | 8.089 | 8.095 | 8.101 | 8.108 | 8.114 | 8.120 | 8.126 | 1,590                       |  |
| 1,600   | 8.126 | 8.132                              | 8.138 | 8.145 | 8.151 | 8.157 | 8.163 | 8.169 | 8.176 | 8.182 | 8.188 | 1,600                       |  |
| 1,610   | 8.188 | 8.194                              | 8.200 | 8.206 | 8.213 | 8.219 | 8.225 | 8.231 | 8.237 | 8.244 | 8.250 | 1,610                       |  |
| 1,620   | 8.250 | 8.256                              | 8.262 | 8.268 | 8.275 | 8.281 | 8.287 | 8.293 | 8.299 | 8.305 | 8.312 | 1,620                       |  |
| 1,630   | 8.312 | 8.318                              | 8.324 | 8.330 | 8.336 | 8.343 | 8.349 | 8.355 | 8.361 | 8.368 | 8.374 | 1,630                       |  |
| 1,640   | 8.374 | 8.380                              | 8.386 | 8.392 | 8.399 | 8.405 | 8.411 | 8.417 | 8.423 | 8.430 | 8.436 | 1,640                       |  |
| 1,650   | 8.436 | 8.442                              | 8.448 | 8.455 | 8.461 | 8.467 | 8.473 | 8.479 | 8.486 | 8.492 | 8.498 | 1,650                       |  |
| 1,660   | 8.498 | 8.504                              | 8.511 | 8.517 | 8.523 | 8.529 | 8.536 | 8.542 | 8.548 | 8.554 | 8.560 | 1,660                       |  |
| 1,670   | 8.560 | 8.567                              | 8.573 | 8.579 | 8.585 | 8.592 | 8.598 | 8.604 | 8.610 | 8.617 | 8.623 | 1,670                       |  |
| 1,680   | 8.623 | 8.629                              | 8.635 | 8.642 | 8.648 | 8.654 | 8.660 | 8.667 | 8.673 | 8.679 | 8.685 | 1,680                       |  |
| 1,690   | 8.685 | 8.692                              | 8.698 | 8.704 | 8.711 | 8.717 | 8.723 | 8.729 | 8.736 | 8.742 | 8.748 | 1,690                       |  |
| 1,700   | 8.748 | 8.754                              | 8.761 | 8.767 | 8.773 | 8.780 | 8.786 | 8.792 | 8.798 | 8.805 | 8.811 | 1,700                       |  |
| 1,710   | 8.811 | 8.817                              | 8.823 | 8.830 | 8.836 | 8.842 | 8.849 | 8.855 | 8.861 | 8.867 | 8.874 | 1,710                       |  |
| 1,720   | 8.874 | 8.880                              | 8.886 | 8.893 | 8.899 | 8.905 | 8.912 | 8.918 | 8.924 | 8.930 | 8.937 | 1,720                       |  |
| 1,730   | 8.937 | 8.943                              | 8.949 | 8.956 | 8.962 | 8.968 | 8.975 | 8.981 | 8.987 | 8.993 | 9.000 | 1,730                       |  |
| 1,740   | 9.000 | 9.006                              | 9.012 | 9.019 | 9.025 | 9.031 | 9.038 | 9.044 | 9.050 | 9.057 | 9.063 | 1,740                       |  |
| 1,750   | 9.063 | 9.069                              | 9.076 | 9.082 | 9.088 | 9.095 | 9.101 | 9.107 | 9.114 | 9.120 | 9.126 | 1,750                       |  |
| 1,760   | 9.126 | 9.133                              | 9.139 | 9.145 | 9.152 | 9.158 | 9.164 | 9.171 | 9.177 | 9.183 | 9.189 | 1,760                       |  |
| 1,770   | 9.190 | 9.196                              | 9.202 | 9.209 | 9.215 | 9.221 | 9.228 | 9.234 | 9.240 | 9.247 | 9.253 | 1,770                       |  |
| 1,780   | 9.253 | 9.259                              | 9.266 | 9.272 | 9.278 | 9.285 | 9.291 | 9.298 | 9.304 | 9.310 | 9.317 | 1,780                       |  |
| 1,790   | 9.317 | 9.323                              | 9.329 | 9.336 | 9.342 | 9.348 | 9.355 | 9.361 | 9.368 | 9.374 | 9.380 | 1,790                       |  |
| 1,800   | 9.380 | 9.387                              | 9.393 | 9.399 | 9.406 | 9.412 | 9.419 | 9.425 | 9.431 | 9.438 | 9.444 | 1,800                       |  |
| 1,810   | 9.444 | 9.450                              | 9.457 | 9.463 | 9.470 | 9.476 | 9.482 | 9.489 | 9.495 | 9.502 | 9.508 | 1,810                       |  |
| 1,820   | 9.508 | 9.514                              | 9.521 | 9.527 | 9.533 | 9.540 | 9.546 | 9.553 | 9.559 | 9.565 | 9.572 | 1,820                       |  |
| 1,830   | 9.572 | 9.578                              | 9.585 | 9.591 | 9.598 | 9.604 | 9.610 | 9.617 | 9.623 | 9.630 | 9.636 | 1,830                       |  |
| 1,840   | 9.636 | 9.642                              | 9.649 | 9.655 | 9.662 | 9.668 | 9.674 | 9.681 | 9.687 | 9.694 | 9.700 | 1,840                       |  |

\*Converted from degrees Celsius (IPTS 1968).

TABLE 10.12—Type S thermocouples (continued).

| Temperature in Degrees Fahrenheit*            |        |                             |        |        |        |        |        |        |        |        |        |       |
|---|--------|-----------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|
| EMF in Absolute Millivolts                    |        | Reference Junctions at 32 F |        |        |        |        |        |        |        |        |        |       |
| DEG F   | 0      | 1                           | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |                             |        |        |        |        |        |        |        |        |        |       |
| 1.850   | 9.700  | 9.707                       | 9.713  | 9.719  | 9.726  | 9.732  | 9.739  | 9.745  | 9.752  | 9.758  | 9.764  | 1.850 |
| 1.860   | 9.764  | 9.771                       | 9.777  | 9.784  | 9.790  | 9.797  | 9.803  | 9.809  | 9.816  | 9.822  | 9.829  | 1.860 |
| 1.870   | 9.829  | 9.835                       | 9.842  | 9.848  | 9.855  | 9.861  | 9.867  | 9.874  | 9.880  | 9.887  | 9.893  | 1.870 |
| 1.880   | 9.893  | 9.900                       | 9.906  | 9.913  | 9.919  | 9.926  | 9.932  | 9.938  | 9.945  | 9.951  | 9.958  | 1.880 |
| 1.890   | 9.958  | 9.964                       | 9.971  | 9.977  | 9.984  | 9.990  | 9.997  | 10.003 | 10.010 | 10.016 | 10.023 | 1.890 |
| 1.900   | 10.023 | 10.029                      | 10.036 | 10.042 | 10.048 | 10.055 | 10.061 | 10.068 | 10.074 | 10.081 | 10.087 | 1.900 |
| 1.910   | 10.087 | 10.094                      | 10.100 | 10.107 | 10.113 | 10.120 | 10.126 | 10.133 | 10.139 | 10.146 | 10.152 | 1.910 |
| 1.920   | 10.152 | 10.159                      | 10.165 | 10.172 | 10.178 | 10.185 | 10.191 | 10.198 | 10.204 | 10.211 | 10.217 | 1.920 |
| 1.930   | 10.217 | 10.224                      | 10.230 | 10.237 | 10.243 | 10.250 | 10.256 | 10.263 | 10.269 | 10.276 | 10.282 | 1.930 |
| 1.940   | 10.282 | 10.289                      | 10.295 | 10.302 | 10.308 | 10.315 | 10.321 | 10.328 | 10.334 | 10.341 | 10.348 | 1.940 |
| 1.950   | 10.348 | 10.354                      | 10.361 | 10.367 | 10.374 | 10.380 | 10.387 | 10.393 | 10.400 | 10.406 | 10.413 | 1.950 |
| 1.960   | 10.413 | 10.419                      | 10.426 | 10.432 | 10.439 | 10.445 | 10.452 | 10.459 | 10.465 | 10.472 | 10.478 | 1.960 |
| 1.970   | 10.478 | 10.485                      | 10.491 | 10.498 | 10.504 | 10.511 | 10.517 | 10.524 | 10.531 | 10.537 | 10.544 | 1.970 |
| 1.980   | 10.544 | 10.550                      | 10.557 | 10.563 | 10.570 | 10.576 | 10.583 | 10.589 | 10.596 | 10.603 | 10.609 | 1.980 |
| 1.990   | 10.609 | 10.616                      | 10.622 | 10.629 | 10.635 | 10.642 | 10.648 | 10.655 | 10.662 | 10.668 | 10.675 | 1.990 |
| 2.000   | 10.675 | 10.681                      | 10.688 | 10.694 | 10.701 | 10.708 | 10.714 | 10.721 | 10.727 | 10.734 | 10.740 | 2.000 |
| 2.010   | 10.740 | 10.747                      | 10.754 | 10.760 | 10.767 | 10.773 | 10.780 | 10.786 | 10.793 | 10.800 | 10.806 | 2.010 |
| 2.020   | 10.806 | 10.813                      | 10.819 | 10.826 | 10.832 | 10.839 | 10.846 | 10.852 | 10.859 | 10.865 | 10.872 | 2.020 |
| 2.030   | 10.872 | 10.879                      | 10.885 | 10.892 | 10.898 | 10.905 | 10.912 | 10.918 | 10.925 | 10.931 | 10.938 | 2.030 |
| 2.040   | 10.938 | 10.944                      | 10.951 | 10.958 | 10.964 | 10.971 | 10.977 | 10.984 | 10.991 | 10.997 | 11.004 | 2.040 |
| 2.050   | 11.004 | 11.010                      | 11.017 | 11.024 | 11.030 | 11.037 | 11.043 | 11.050 | 11.057 | 11.063 | 11.070 | 2.050 |
| 2.060   | 11.070 | 11.076                      | 11.083 | 11.090 | 11.096 | 11.103 | 11.110 | 11.116 | 11.123 | 11.129 | 11.136 | 2.060 |
| 2.070   | 11.136 | 11.143                      | 11.149 | 11.156 | 11.162 | 11.169 | 11.176 | 11.182 | 11.189 | 11.196 | 11.202 | 2.070 |
| 2.080   | 11.202 | 11.209                      | 11.215 | 11.222 | 11.229 | 11.235 | 11.242 | 11.248 | 11.255 | 11.262 | 11.268 | 2.080 |
| 2.090   | 11.268 | 11.275                      | 11.282 | 11.288 | 11.295 | 11.301 | 11.308 | 11.315 | 11.321 | 11.328 | 11.335 | 2.090 |
| 2.100   | 11.335 | 11.341                      | 11.348 | 11.355 | 11.361 | 11.368 | 11.374 | 11.381 | 11.388 | 11.394 | 11.401 | 2.100 |
| 2.110   | 11.401 | 11.408                      | 11.414 | 11.421 | 11.428 | 11.434 | 11.441 | 11.447 | 11.454 | 11.461 | 11.467 | 2.110 |
| 2.120   | 11.467 | 11.474                      | 11.481 | 11.487 | 11.494 | 11.501 | 11.507 | 11.514 | 11.521 | 11.527 | 11.534 | 2.120 |
| 2.130   | 11.534 | 11.541                      | 11.547 | 11.554 | 11.560 | 11.567 | 11.574 | 11.580 | 11.587 | 11.594 | 11.600 | 2.130 |
| 2.140   | 11.600 | 11.607                      | 11.614 | 11.620 | 11.627 | 11.634 | 11.640 | 11.647 | 11.654 | 11.660 | 11.667 | 2.140 |
| 2.150   | 11.667 | 11.674                      | 11.680 | 11.687 | 11.694 | 11.700 | 11.707 | 11.714 | 11.720 | 11.727 | 11.734 | 2.150 |
| 2.160   | 11.734 | 11.740                      | 11.747 | 11.754 | 11.760 | 11.767 | 11.774 | 11.780 | 11.787 | 11.794 | 11.800 | 2.160 |
| 2.170   | 11.800 | 11.807                      | 11.814 | 11.820 | 11.827 | 11.834 | 11.840 | 11.847 | 11.854 | 11.860 | 11.867 | 2.170 |
| 2.180   | 11.867 | 11.874                      | 11.880 | 11.887 | 11.894 | 11.900 | 11.907 | 11.914 | 11.920 | 11.927 | 11.934 | 2.180 |
| 2.190   | 11.934 | 11.940                      | 11.947 | 11.954 | 11.960 | 11.967 | 11.974 | 11.980 | 11.987 | 11.994 | 12.001 | 2.190 |
| 2.200   | 12.001 | 12.007                      | 12.014 | 12.021 | 12.027 | 12.034 | 12.041 | 12.047 | 12.054 | 12.061 | 12.067 | 2.200 |
| 2.210   | 12.067 | 12.074                      | 12.081 | 12.087 | 12.094 | 12.101 | 12.107 | 12.114 | 12.121 | 12.128 | 12.134 | 2.210 |
| 2.220   | 12.134 | 12.141                      | 12.148 | 12.154 | 12.161 | 12.168 | 12.174 | 12.181 | 12.188 | 12.194 | 12.201 | 2.220 |
| 2.230   | 12.201 | 12.208                      | 12.215 | 12.221 | 12.228 | 12.235 | 12.241 | 12.248 | 12.255 | 12.261 | 12.268 | 2.230 |
| 2.240   | 12.268 | 12.275                      | 12.282 | 12.288 | 12.295 | 12.302 | 12.308 | 12.315 | 12.322 | 12.328 | 12.335 | 2.240 |
| 2.250   | 12.335 | 12.342                      | 12.349 | 12.355 | 12.362 | 12.369 | 12.375 | 12.382 | 12.389 | 12.395 | 12.402 | 2.250 |
| 2.260   | 12.402 | 12.409                      | 12.416 | 12.422 | 12.429 | 12.436 | 12.442 | 12.449 | 12.456 | 12.463 | 12.469 | 2.260 |
| 2.270   | 12.469 | 12.476                      | 12.483 | 12.489 | 12.496 | 12.503 | 12.510 | 12.516 | 12.523 | 12.530 | 12.536 | 2.270 |
| 2.280   | 12.536 | 12.543                      | 12.550 | 12.557 | 12.563 | 12.570 | 12.577 | 12.583 | 12.590 | 12.597 | 12.604 | 2.280 |
| 2.290   | 12.604 | 12.610                      | 12.617 | 12.624 | 12.630 | 12.637 | 12.644 | 12.651 | 12.657 | 12.664 | 12.671 | 2.290 |
| 2.300   | 12.671 | 12.677                      | 12.684 | 12.691 | 12.698 | 12.704 | 12.711 | 12.718 | 12.724 | 12.731 | 12.738 | 2.300 |
| 2.310   | 12.738 | 12.745                      | 12.751 | 12.758 | 12.765 | 12.771 | 12.778 | 12.785 | 12.792 | 12.798 | 12.805 | 2.310 |
| 2.320   | 12.805 | 12.812                      | 12.819 | 12.825 | 12.832 | 12.839 | 12.845 | 12.852 | 12.859 | 12.866 | 12.872 | 2.320 |
| 2.330   | 12.872 | 12.879                      | 12.886 | 12.893 | 12.899 | 12.906 | 12.913 | 12.919 | 12.926 | 12.933 | 12.940 | 2.330 |
| 2.340   | 12.940 | 12.946                      | 12.953 | 12.960 | 12.967 | 12.973 | 12.980 | 12.987 | 12.993 | 13.000 | 13.007 | 2.340 |
| 2.350   | 13.007 | 13.014                      | 13.020 | 13.027 | 13.034 | 13.041 | 13.047 | 13.054 | 13.061 | 13.067 | 13.074 | 2.350 |
| 2.360   | 13.074 | 13.081                      | 13.088 | 13.094 | 13.101 | 13.108 | 13.115 | 13.121 | 13.128 | 13.135 | 13.142 | 2.360 |
| 2.370   | 13.142 | 13.148                      | 13.155 | 13.162 | 13.168 | 13.175 | 13.182 | 13.189 | 13.195 | 13.202 | 13.209 | 2.370 |
| 2.380   | 13.209 | 13.216                      | 13.222 | 13.229 | 13.236 | 13.243 | 13.249 | 13.256 | 13.263 | 13.269 | 13.276 | 2.380 |
| 2.390   | 13.276 | 13.283                      | 13.290 | 13.296 | 13.303 | 13.310 | 13.317 | 13.323 | 13.330 | 13.337 | 13.344 | 2.390 |
| 2.400   | 13.344 | 13.350                      | 13.357 | 13.364 | 13.371 | 13.377 | 13.384 | 13.391 | 13.397 | 13.404 | 13.411 | 2.400 |
| 2.410   | 13.411 | 13.418                      | 13.424 | 13.431 | 13.438 | 13.445 | 13.451 | 13.458 | 13.465 | 13.472 | 13.478 | 2.410 |
| 2.420   | 13.478 | 13.485                      | 13.492 | 13.499 | 13.505 | 13.512 | 13.519 | 13.526 | 13.532 | 13.539 | 13.546 | 2.420 |
| 2.430   | 13.546 | 13.552                      | 13.559 | 13.566 | 13.573 | 13.579 | 13.586 | 13.592 | 13.600 | 13.606 | 13.613 | 2.430 |
| 2.440   | 13.613 | 13.620                      | 13.627 | 13.633 | 13.640 | 13.647 | 13.654 | 13.660 | 13.667 | 13.674 | 13.681 | 2.440 |
| 2.450   | 13.681 | 13.687                      | 13.694 | 13.701 | 13.708 | 13.714 | 13.721 | 13.728 | 13.734 | 13.741 | 13.748 | 2.450 |
| 2.460   | 13.748 | 13.755                      | 13.761 | 13.768 | 13.775 | 13.782 | 13.788 | 13.795 | 13.802 | 13.809 | 13.815 | 2.460 |
| 2.470   | 13.815 | 13.822                      | 13.829 | 13.836 | 13.842 | 13.849 | 13.856 | 13.863 | 13.870 | 13.876 | 13.883 | 2.470 |
| 2.480   | 13.883 | 13.890                      | 13.896 | 13.903 | 13.910 | 13.916 | 13.923 | 13.930 | 13.937 | 13.943 | 13.950 | 2.480 |
| 2.490   | 13.950 | 13.957                      | 13.964 | 13.970 | 13.977 | 13.984 | 13.991 | 13.997 | 14.004 | 14.011 | 14.018 | 2.490 |

\* Converted from degrees Celsius (IPTS 1968).

TABLE 10.12—Type S thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit* |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|------------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
| DEG F   | 0      | 1                                  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |                                    |        |        |        |        |        |        |        |        |        |                             |  |
| 2500  | 14.018 | 14.024                             | 14.031 | 14.038 | 14.045 | 14.051 | 14.058 | 14.065 | 14.072 | 14.078 | 14.085 | 2500                        |  |
| 2510  | 14.085 | 14.092                             | 14.098 | 14.105 | 14.112 | 14.119 | 14.125 | 14.132 | 14.139 | 14.146 | 14.152 | 2510                        |  |
| 2520  | 14.152 | 14.159                             | 14.166 | 14.173 | 14.179 | 14.186 | 14.193 | 14.200 | 14.206 | 14.213 | 14.220 | 2520                        |  |
| 2530  | 14.220 | 14.226                             | 14.233 | 14.240 | 14.247 | 14.253 | 14.260 | 14.267 | 14.274 | 14.280 | 14.287 | 2530                        |  |
| 2540  | 14.287 | 14.294                             | 14.301 | 14.307 | 14.314 | 14.321 | 14.328 | 14.334 | 14.341 | 14.348 | 14.354 | 2540                        |  |
| 2550  | 14.354 | 14.361                             | 14.368 | 14.375 | 14.381 | 14.388 | 14.395 | 14.402 | 14.408 | 14.415 | 14.422 | 2550                        |  |
| 2560  | 14.422 | 14.429                             | 14.435 | 14.442 | 14.449 | 14.455 | 14.462 | 14.469 | 14.476 | 14.482 | 14.489 | 2560                        |  |
| 2570  | 14.489 | 14.496                             | 14.503 | 14.509 | 14.516 | 14.523 | 14.530 | 14.536 | 14.543 | 14.550 | 14.556 | 2570                        |  |
| 2580  | 14.556 | 14.563                             | 14.570 | 14.577 | 14.583 | 14.590 | 14.597 | 14.604 | 14.610 | 14.617 | 14.624 | 2580                        |  |
| 2590  | 14.624 | 14.631                             | 14.637 | 14.644 | 14.651 | 14.657 | 14.664 | 14.671 | 14.678 | 14.684 | 14.691 | 2590                        |  |
| 2600  | 14.691 | 14.698                             | 14.705 | 14.711 | 14.718 | 14.725 | 14.731 | 14.738 | 14.745 | 14.752 | 14.758 | 2600                        |  |
| 2610  | 14.758 | 14.765                             | 14.772 | 14.778 | 14.785 | 14.792 | 14.799 | 14.805 | 14.812 | 14.819 | 14.826 | 2610                        |  |
| 2620  | 14.826 | 14.832                             | 14.839 | 14.846 | 14.852 | 14.859 | 14.866 | 14.873 | 14.879 | 14.886 | 14.893 | 2620                        |  |
| 2630  | 14.893 | 14.899                             | 14.906 | 14.913 | 14.920 | 14.926 | 14.933 | 14.940 | 14.946 | 14.953 | 14.960 | 2630                        |  |
| 2640  | 14.960 | 14.967                             | 14.973 | 14.980 | 14.987 | 14.994 | 15.000 | 15.007 | 15.014 | 15.020 | 15.027 | 2640                        |  |
| 2650  | 15.027 | 15.034                             | 15.041 | 15.047 | 15.054 | 15.061 | 15.067 | 15.074 | 15.081 | 15.088 | 15.094 | 2650                        |  |
| 2660  | 15.094 | 15.101                             | 15.108 | 15.114 | 15.121 | 15.128 | 15.134 | 15.141 | 15.148 | 15.155 | 15.161 | 2660                        |  |
| 2670  | 15.161 | 15.168                             | 15.175 | 15.181 | 15.188 | 15.195 | 15.202 | 15.208 | 15.215 | 15.222 | 15.228 | 2670                        |  |
| 2680  | 15.228 | 15.235                             | 15.242 | 15.248 | 15.255 | 15.262 | 15.269 | 15.275 | 15.282 | 15.289 | 15.295 | 2680                        |  |
| 2690  | 15.295 | 15.302                             | 15.309 | 15.315 | 15.322 | 15.329 | 15.336 | 15.342 | 15.349 | 15.356 | 15.362 | 2690                        |  |
| 2700  | 15.362 | 15.369                             | 15.376 | 15.382 | 15.389 | 15.396 | 15.403 | 15.409 | 15.416 | 15.423 | 15.429 | 2700                        |  |
| 2710  | 15.429 | 15.436                             | 15.443 | 15.449 | 15.456 | 15.463 | 15.469 | 15.476 | 15.483 | 15.490 | 15.496 | 2710                        |  |
| 2720  | 15.496 | 15.503                             | 15.510 | 15.516 | 15.523 | 15.530 | 15.536 | 15.543 | 15.550 | 15.556 | 15.563 | 2720                        |  |
| 2730  | 15.563 | 15.570                             | 15.576 | 15.583 | 15.590 | 15.597 | 15.603 | 15.610 | 15.617 | 15.623 | 15.630 | 2730                        |  |
| 2740  | 15.630 | 15.637                             | 15.643 | 15.650 | 15.657 | 15.663 | 15.670 | 15.677 | 15.683 | 15.690 | 15.697 | 2740                        |  |
| 2750  | 15.697 | 15.703                             | 15.710 | 15.717 | 15.723 | 15.730 | 15.737 | 15.743 | 15.750 | 15.757 | 15.763 | 2750                        |  |
| 2760  | 15.763 | 15.770                             | 15.777 | 15.783 | 15.790 | 15.797 | 15.804 | 15.810 | 15.817 | 15.824 | 15.830 | 2760                        |  |
| 2770  | 15.830 | 15.837                             | 15.844 | 15.850 | 15.857 | 15.864 | 15.870 | 15.877 | 15.883 | 15.890 | 15.897 | 2770                        |  |
| 2780  | 15.897 | 15.903                             | 15.910 | 15.917 | 15.923 | 15.930 | 15.937 | 15.943 | 15.950 | 15.957 | 15.963 | 2780                        |  |
| 2790  | 15.963 | 15.970                             | 15.977 | 15.983 | 15.990 | 15.997 | 16.003 | 16.010 | 16.017 | 16.023 | 16.030 | 2790                        |  |
| 2800  | 16.030 | 16.037                             | 16.043 | 16.050 | 16.057 | 16.063 | 16.070 | 16.077 | 16.083 | 16.090 | 16.096 | 2800                        |  |
| 2810  | 16.096 | 16.103                             | 16.110 | 16.116 | 16.123 | 16.130 | 16.136 | 16.143 | 16.150 | 16.156 | 16.163 | 2810                        |  |
| 2820  | 16.163 | 16.170                             | 16.176 | 16.183 | 16.189 | 16.196 | 16.203 | 16.209 | 16.216 | 16.223 | 16.229 | 2820                        |  |
| 2830  | 16.229 | 16.236                             | 16.243 | 16.249 | 16.256 | 16.262 | 16.269 | 16.276 | 16.282 | 16.289 | 16.296 | 2830                        |  |
| 2840  | 16.296 | 16.302                             | 16.309 | 16.315 | 16.322 | 16.329 | 16.335 | 16.342 | 16.349 | 16.355 | 16.362 | 2840                        |  |
| 2850  | 16.362 | 16.368                             | 16.375 | 16.382 | 16.388 | 16.395 | 16.402 | 16.408 | 16.415 | 16.421 | 16.428 | 2850                        |  |
| 2860  | 16.428 | 16.435                             | 16.441 | 16.448 | 16.454 | 16.461 | 16.468 | 16.474 | 16.481 | 16.488 | 16.494 | 2860                        |  |
| 2870  | 16.494 | 16.501                             | 16.507 | 16.514 | 16.521 | 16.527 | 16.534 | 16.540 | 16.547 | 16.554 | 16.560 | 2870                        |  |
| 2880  | 16.560 | 16.567                             | 16.573 | 16.580 | 16.587 | 16.593 | 16.600 | 16.606 | 16.613 | 16.620 | 16.626 | 2880                        |  |
| 2890  | 16.626 | 16.633                             | 16.639 | 16.646 | 16.653 | 16.659 | 16.666 | 16.672 | 16.679 | 16.686 | 16.692 | 2890                        |  |
| 2900  | 16.692 | 16.699                             | 16.705 | 16.712 | 16.719 | 16.725 | 16.732 | 16.738 | 16.745 | 16.751 | 16.758 | 2900                        |  |
| 2910  | 16.758 | 16.765                             | 16.771 | 16.778 | 16.784 | 16.791 | 16.797 | 16.804 | 16.811 | 16.817 | 16.824 | 2910                        |  |
| 2920  | 16.824 | 16.830                             | 16.837 | 16.844 | 16.850 | 16.857 | 16.863 | 16.870 | 16.876 | 16.883 | 16.890 | 2920                        |  |
| 2930  | 16.890 | 16.896                             | 16.903 | 16.909 | 16.916 | 16.922 | 16.929 | 16.935 | 16.942 | 16.949 | 16.955 | 2930                        |  |
| 2940  | 16.955 | 16.962                             | 16.968 | 16.975 | 16.981 | 16.988 | 16.995 | 17.001 | 17.008 | 17.014 | 17.021 | 2940                        |  |
| 2950  | 17.021 | 17.027                             | 17.034 | 17.040 | 17.047 | 17.053 | 17.060 | 17.067 | 17.073 | 17.080 | 17.086 | 2950                        |  |
| 2960  | 17.086 | 17.093                             | 17.099 | 17.106 | 17.112 | 17.119 | 17.125 | 17.132 | 17.139 | 17.145 | 17.152 | 2960                        |  |
| 2970  | 17.152 | 17.158                             | 17.165 | 17.171 | 17.178 | 17.184 | 17.191 | 17.197 | 17.204 | 17.210 | 17.217 | 2970                        |  |
| 2980  | 17.217 | 17.223                             | 17.230 | 17.237 | 17.243 | 17.250 | 17.256 | 17.263 | 17.269 | 17.276 | 17.282 | 2980                        |  |
| 2990  | 17.282 | 17.289                             | 17.295 | 17.302 | 17.308 | 17.315 | 17.321 | 17.328 | 17.334 | 17.341 | 17.347 | 2990                        |  |
| 3000  | 17.347 | 17.354                             | 17.360 | 17.367 | 17.373 | 17.380 | 17.386 | 17.393 | 17.399 | 17.406 | 17.412 | 3000                        |  |
| 3010  | 17.412 | 17.419                             | 17.425 | 17.432 | 17.438 | 17.445 | 17.451 | 17.458 | 17.464 | 17.471 | 17.477 | 3010                        |  |
| 3020  | 17.477 | 17.484                             | 17.490 | 17.497 | 17.503 | 17.510 | 17.516 | 17.523 | 17.529 | 17.536 | 17.542 | 3020                        |  |
| 3030  | 17.542 | 17.549                             | 17.555 | 17.562 | 17.568 | 17.575 | 17.581 | 17.588 | 17.594 | 17.601 | 17.607 | 3030                        |  |
| 3040  | 17.607 | 17.614                             | 17.620 | 17.627 | 17.633 | 17.639 | 17.646 | 17.652 | 17.659 | 17.665 | 17.672 | 3040                        |  |
| 3050  | 17.672 | 17.678                             | 17.685 | 17.691 | 17.698 | 17.704 | 17.711 | 17.717 | 17.723 | 17.730 | 17.736 | 3050                        |  |
| 3060  | 17.736 | 17.743                             | 17.749 | 17.756 | 17.762 | 17.769 | 17.775 | 17.781 | 17.788 | 17.794 | 17.801 | 3060                        |  |
| 3070  | 17.801 | 17.807                             | 17.814 | 17.820 | 17.826 | 17.833 | 17.839 | 17.846 | 17.852 | 17.859 | 17.865 | 3070                        |  |
| 3080  | 17.865 | 17.871                             | 17.878 | 17.884 | 17.891 | 17.897 | 17.903 | 17.910 | 17.916 | 17.923 | 17.929 | 3080                        |  |
| 3090  | 17.929 | 17.935                             | 17.942 | 17.948 | 17.954 | 17.961 | 17.967 | 17.974 | 17.980 | 17.986 | 17.993 | 3090                        |  |
| 3100  | 17.993 | 17.999                             | 18.005 | 18.012 | 18.018 | 18.024 | 18.031 | 18.037 | 18.043 | 18.050 | 18.056 | 3100                        |  |
| 3110  | 18.056 | 18.063                             | 18.069 | 18.075 | 18.081 | 18.088 | 18.094 | 18.100 | 18.107 | 18.113 | 18.119 | 3110                        |  |
| 3120  | 18.119 | 18.126                             | 18.132 | 18.138 | 18.145 | 18.151 | 18.157 | 18.163 | 18.170 | 18.176 | 18.182 | 3120                        |  |
| 3130  | 18.182 | 18.189                             | 18.195 | 18.201 | 18.207 | 18.214 | 18.220 | 18.226 | 18.232 | 18.239 | 18.245 | 3130                        |  |
| 3140  | 18.245 | 18.251                             | 18.257 | 18.264 | 18.270 | 18.276 | 18.282 | 18.289 | 18.295 | 18.301 | 18.307 | 3140                        |  |

DEG F 0 1 2 3 4 5 6 7 8 9 10 DEG F

Converted from degrees Celsius (1PTS 1968).

TABLE 10.12—Type S thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit <sup>a</sup> |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
|   |        | DEG F  | 0      | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      |                             |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                             |  |
| 3,150   | 18.307 | 18.313   | 18.320 | 18.326 | 18.332 | 18.338 | 18.344 | 18.351 | 18.357 | 18.363 | 18.369 | 3,150                       |  |
| 3,160   | 18.369 | 18.375   | 18.381 | 18.388 | 18.394 | 18.400 | 18.406 | 18.412 | 18.418 | 18.424 | 18.431 | 3,160                       |  |
| 3,170   | 18.431 | 18.437   | 18.443 | 18.449 | 18.455 | 18.461 | 18.467 | 18.473 | 18.479 | 18.486 | 18.492 | 3,170                       |  |
| 3,180   | 18.492 | 18.498   | 18.504 | 18.510 | 18.516 | 18.522 | 18.528 | 18.534 | 18.540 | 18.546 | 18.552 | 3,180                       |  |
| 3,190   | 18.552 | 18.558   | 18.564 | 18.570 | 18.576 | 18.582 | 18.588 | 18.594 | 18.600 | 18.606 | 18.612 | 3,190                       |  |
| 3,200   | 18.612 | 18.618   | 18.624 | 18.630 | 18.636 | 18.642 | 18.648 | 18.654 | 18.660 | 18.666 | 18.672 | 3,200                       |  |
| 3,210   | 18.672 | 18.678   | 18.684 | 18.690 | 18.696 |        |        |        |        |        |        | 3,210                       |  |
| DEG F   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |

<sup>a</sup> Converted from degrees Celsius (IPTS 1968).

TABLE 10.13—Type S thermocouples (deg C-millivolts).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Celsius (IPTS 1968) |        |        |        |        |        |        |        |        |        | Reference Junctions at 0 C |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------------------------|--|
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                            |  |
| -50   | -0.236 |  |        |        |        |        |        |        |        |        |        | -50                        |  |
| -40   | -0.194 | -0.199                                     | -0.203 | -0.207 | -0.211 | -0.215 | -0.220 | -0.224 | -0.228 | -0.232 | -0.236 | -40                        |  |
| -30   | -0.150 | -0.155                                     | -0.159 | -0.164 | -0.168 | -0.173 | -0.177 | -0.181 | -0.186 | -0.190 | -0.194 | -30                        |  |
| -20   | -0.103 | -0.108                                     | -0.112 | -0.117 | -0.122 | -0.127 | -0.132 | -0.136 | -0.141 | -0.145 | -0.150 | -20                        |  |
| -10   | -0.053 | -0.058                                     | -0.063 | -0.068 | -0.073 | -0.078 | -0.083 | -0.088 | -0.093 | -0.098 | -0.103 | -10                        |  |
| 0   | 0.000  | -0.005                                     | -0.011 | -0.016 | -0.021 | -0.027 | -0.032 | -0.037 | -0.042 | -0.048 | -0.053 | 0                          |  |
| 0   | 0.000  | 0.005                                      | 0.011  | 0.016  | 0.022  | 0.027  | 0.033  | 0.038  | 0.044  | 0.050  | 0.055  | 0                          |  |
| 10  | 0.055  | 0.061                                      | 0.067  | 0.072  | 0.078  | 0.084  | 0.090  | 0.095  | 0.101  | 0.107  | 0.113  | 10                         |  |
| 20  | 0.113  | 0.119                                      | 0.125  | 0.131  | 0.137  | 0.142  | 0.148  | 0.154  | 0.161  | 0.167  | 0.173  | 20                         |  |
| 30  | 0.173  | 0.179                                      | 0.185  | 0.191  | 0.197  | 0.203  | 0.210  | 0.216  | 0.222  | 0.228  | 0.235  | 30                         |  |
| 40  | 0.235  | 0.241                                      | 0.247  | 0.254  | 0.260  | 0.266  | 0.273  | 0.279  | 0.286  | 0.292  | 0.299  | 40                         |  |
| 50  | 0.299  | 0.305                                      | 0.312  | 0.318  | 0.325  | 0.331  | 0.338  | 0.345  | 0.351  | 0.358  | 0.365  | 50                         |  |
| 60  | 0.365  | 0.371                                      | 0.378  | 0.385  | 0.391  | 0.398  | 0.405  | 0.412  | 0.419  | 0.425  | 0.432  | 60                         |  |
| 70  | 0.432  | 0.439                                      | 0.446  | 0.453  | 0.460  | 0.467  | 0.474  | 0.481  | 0.488  | 0.495  | 0.502  | 70                         |  |
| 80  | 0.502  | 0.509                                      | 0.516  | 0.523  | 0.530  | 0.537  | 0.544  | 0.551  | 0.558  | 0.566  | 0.573  | 80                         |  |
| 90  | 0.573  | 0.580                                      | 0.587  | 0.594  | 0.602  | 0.609  | 0.616  | 0.623  | 0.631  | 0.638  | 0.645  | 90                         |  |
| 100   | 0.645  | 0.653                                      | 0.660  | 0.667  | 0.675  | 0.682  | 0.690  | 0.697  | 0.704  | 0.712  | 0.719  | 100                        |  |
| 110   | 0.719  | 0.727                                      | 0.734  | 0.742  | 0.749  | 0.757  | 0.764  | 0.772  | 0.780  | 0.787  | 0.795  | 110                        |  |
| 120   | 0.795  | 0.802                                      | 0.810  | 0.818  | 0.825  | 0.833  | 0.841  | 0.848  | 0.856  | 0.864  | 0.872  | 120                        |  |
| 130   | 0.872  | 0.879                                      | 0.887  | 0.895  | 0.903  | 0.910  | 0.918  | 0.926  | 0.934  | 0.942  | 0.950  | 130                        |  |
| 140   | 0.950  | 0.957                                      | 0.965  | 0.973  | 0.981  | 0.989  | 0.997  | 1.005  | 1.013  | 1.021  | 1.029  | 140                        |  |
| 150   | 1.029  | 1.037                                      | 1.045  | 1.053  | 1.061  | 1.069  | 1.077  | 1.085  | 1.093  | 1.101  | 1.109  | 150                        |  |
| 160   | 1.109  | 1.117                                      | 1.125  | 1.133  | 1.141  | 1.149  | 1.158  | 1.166  | 1.174  | 1.182  | 1.190  | 160                        |  |
| 170   | 1.190  | 1.198                                      | 1.207  | 1.215  | 1.223  | 1.231  | 1.240  | 1.248  | 1.256  | 1.264  | 1.273  | 170                        |  |
| 180   | 1.273  | 1.281                                      | 1.289  | 1.297  | 1.306  | 1.314  | 1.322  | 1.331  | 1.339  | 1.347  | 1.356  | 180                        |  |
| 190   | 1.356  | 1.364                                      | 1.373  | 1.381  | 1.389  | 1.398  | 1.406  | 1.415  | 1.423  | 1.432  | 1.440  | 190                        |  |
| 200   | 1.440  | 1.448                                      | 1.457  | 1.465  | 1.474  | 1.482  | 1.491  | 1.499  | 1.508  | 1.516  | 1.525  | 200                        |  |
| 210   | 1.525  | 1.534                                      | 1.542  | 1.551  | 1.559  | 1.568  | 1.576  | 1.585  | 1.594  | 1.602  | 1.611  | 210                        |  |
| 220   | 1.611  | 1.620                                      | 1.628  | 1.637  | 1.645  | 1.654  | 1.663  | 1.671  | 1.680  | 1.689  | 1.698  | 220                        |  |
| 230   | 1.698  | 1.706                                      | 1.715  | 1.724  | 1.732  | 1.741  | 1.750  | 1.759  | 1.767  | 1.776  | 1.785  | 230                        |  |
| 240   | 1.785  | 1.794                                      | 1.802  | 1.811  | 1.820  | 1.829  | 1.838  | 1.846  | 1.855  | 1.864  | 1.873  | 240                        |  |
| 250   | 1.873  | 1.882                                      | 1.891  | 1.899  | 1.908  | 1.917  | 1.926  | 1.935  | 1.944  | 1.953  | 1.962  | 250                        |  |
| 260   | 1.962  | 1.971                                      | 1.979  | 1.988  | 1.997  | 2.006  | 2.015  | 2.024  | 2.033  | 2.042  | 2.051  | 260                        |  |
| 270   | 2.051  | 2.060                                      | 2.069  | 2.078  | 2.087  | 2.096  | 2.105  | 2.114  | 2.123  | 2.132  | 2.141  | 270                        |  |
| 280   | 2.141  | 2.150                                      | 2.159  | 2.168  | 2.177  | 2.186  | 2.195  | 2.204  | 2.213  | 2.222  | 2.232  | 280                        |  |
| 290   | 2.232  | 2.241                                      | 2.250  | 2.259  | 2.268  | 2.277  | 2.286  | 2.295  | 2.304  | 2.314  | 2.323  | 290                        |  |
| 300   | 2.323  | 2.332                                      | 2.341  | 2.350  | 2.359  | 2.368  | 2.378  | 2.387  | 2.396  | 2.405  | 2.414  | 300                        |  |
| 310   | 2.414  | 2.424                                      | 2.433  | 2.442  | 2.451  | 2.460  | 2.470  | 2.479  | 2.488  | 2.497  | 2.506  | 310                        |  |
| 320   | 2.506  | 2.516                                      | 2.525  | 2.534  | 2.543  | 2.553  | 2.562  | 2.571  | 2.581  | 2.590  | 2.599  | 320                        |  |
| 330   | 2.599  | 2.608                                      | 2.618  | 2.627  | 2.636  | 2.646  | 2.655  | 2.664  | 2.674  | 2.683  | 2.692  | 330                        |  |
| 340   | 2.692  | 2.702                                      | 2.711  | 2.720  | 2.730  | 2.739  | 2.748  | 2.758  | 2.767  | 2.776  | 2.786  | 340                        |  |
| 350   | 2.786  | 2.795                                      | 2.805  | 2.814  | 2.823  | 2.833  | 2.842  | 2.852  | 2.861  | 2.870  | 2.880  | 350                        |  |
| 360   | 2.880  | 2.889                                      | 2.899  | 2.908  | 2.917  | 2.927  | 2.936  | 2.946  | 2.955  | 2.965  | 2.974  | 360                        |  |
| 370   | 2.974  | 2.984                                      | 2.993  | 3.003  | 3.012  | 3.022  | 3.031  | 3.041  | 3.050  | 3.059  | 3.069  | 370                        |  |
| 380   | 3.069  | 3.078                                      | 3.088  | 3.097  | 3.107  | 3.117  | 3.126  | 3.136  | 3.145  | 3.155  | 3.164  | 380                        |  |
| 390   | 3.164  | 3.174                                      | 3.183  | 3.193  | 3.202  | 3.212  | 3.221  | 3.231  | 3.241  | 3.250  | 3.260  | 390                        |  |
| 400   | 3.260  | 3.269                                      | 3.279  | 3.288  | 3.298  | 3.308  | 3.317  | 3.327  | 3.336  | 3.346  | 3.356  | 400                        |  |
| 410   | 3.356  | 3.365                                      | 3.375  | 3.384  | 3.394  | 3.404  | 3.413  | 3.423  | 3.433  | 3.442  | 3.452  | 410                        |  |
| 420   | 3.452  | 3.462                                      | 3.471  | 3.481  | 3.491  | 3.500  | 3.510  | 3.520  | 3.529  | 3.539  | 3.549  | 420                        |  |
| 430   | 3.549  | 3.558                                      | 3.568  | 3.578  | 3.587  | 3.597  | 3.607  | 3.616  | 3.626  | 3.636  | 3.645  | 430                        |  |
| 440   | 3.645  | 3.655                                      | 3.665  | 3.675  | 3.684  | 3.694  | 3.704  | 3.714  | 3.723  | 3.733  | 3.743  | 440                        |  |
| 450   | 3.743  | 3.752                                      | 3.762  | 3.772  | 3.782  | 3.791  | 3.801  | 3.811  | 3.821  | 3.831  | 3.840  | 450                        |  |
| 460   | 3.840  | 3.850                                      | 3.860  | 3.870  | 3.879  | 3.889  | 3.899  | 3.909  | 3.919  | 3.928  | 3.938  | 460                        |  |
| 470   | 3.938  | 3.948                                      | 3.958  | 3.968  | 3.977  | 3.987  | 3.997  | 4.007  | 4.017  | 4.027  | 4.036  | 470                        |  |
| 480   | 4.036  | 4.046                                      | 4.056  | 4.066  | 4.076  | 4.086  | 4.096  | 4.105  | 4.115  | 4.125  | 4.135  | 480                        |  |
| 490   | 4.135  | 4.145                                      | 4.155  | 4.164  | 4.174  | 4.184  | 4.194  | 4.204  | 4.214  | 4.224  | 4.234  | 490                        |  |
| 500   | 4.234  | 4.243                                      | 4.253  | 4.263  | 4.273  | 4.283  | 4.293  | 4.303  | 4.313  | 4.323  | 4.333  | 500                        |  |
| 510   | 4.333  | 4.343                                      | 4.352  | 4.362  | 4.372  | 4.382  | 4.392  | 4.402  | 4.412  | 4.422  | 4.432  | 510                        |  |
| 520   | 4.432  | 4.442                                      | 4.452  | 4.462  | 4.472  | 4.482  | 4.492  | 4.502  | 4.512  | 4.522  | 4.532  | 520                        |  |
| 530   | 4.532  | 4.542                                      | 4.552  | 4.562  | 4.572  | 4.582  | 4.592  | 4.602  | 4.612  | 4.622  | 4.632  | 530                        |  |
| 540   | 4.632  | 4.642                                      | 4.652  | 4.662  | 4.672  | 4.682  | 4.692  | 4.702  | 4.712  | 4.722  | 4.732  | 540                        |  |
| 550   | 4.732  | 4.742                                      | 4.752  | 4.762  | 4.772  | 4.782  | 4.792  | 4.802  | 4.812  | 4.822  | 4.832  | 550                        |  |
| 560   | 4.832  | 4.842                                      | 4.852  | 4.862  | 4.873  | 4.883  | 4.893  | 4.903  | 4.913  | 4.923  | 4.933  | 560                        |  |
| 570   | 4.933  | 4.943                                      | 4.953  | 4.963  | 4.973  | 4.984  | 4.994  | 5.004  | 5.014  | 5.024  | 5.034  | 570                        |  |
| 580   | 5.034  | 5.044                                      | 5.054  | 5.065  | 5.075  | 5.085  | 5.095  | 5.105  | 5.115  | 5.125  | 5.136  | 580                        |  |
| 590   | 5.136  | 5.146                                      | 5.156  | 5.166  | 5.176  | 5.186  | 5.197  | 5.207  | 5.217  | 5.227  | 5.237  | 590                        |  |

212 THE USE OF THERMOCOUPLES IN TEMPERATURE MEASUREMENT

TABLE 10.13—Type S thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Celsius (IPTS 1968) |        |        |        |        |        |        |        |        |        | Reference Junctions at 0 C |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------------------------|--|
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                            |  |
| 600   | 5.237  | 5.247                                      | 5.258  | 5.268  | 5.278  | 5.288  | 5.298  | 5.309  | 5.319  | 5.329  | 5.339  | 600                        |  |
| 610   | 5.339  | 5.350                                      | 5.360  | 5.370  | 5.380  | 5.391  | 5.401  | 5.411  | 5.421  | 5.431  | 5.442  | 610                        |  |
| 620   | 5.442  | 5.452                                      | 5.462  | 5.473  | 5.483  | 5.493  | 5.503  | 5.514  | 5.524  | 5.534  | 5.544  | 620                        |  |
| 630   | 5.544  | 5.555                                      | 5.565  | 5.575  | 5.586  | 5.596  | 5.606  | 5.617  | 5.627  | 5.637  | 5.648  | 630                        |  |
| 640   | 5.648  | 5.658                                      | 5.668  | 5.679  | 5.689  | 5.700  | 5.710  | 5.720  | 5.731  | 5.741  | 5.751  | 640                        |  |
| 650   | 5.751  | 5.762                                      | 5.772  | 5.782  | 5.793  | 5.803  | 5.814  | 5.824  | 5.834  | 5.845  | 5.855  | 650                        |  |
| 660   | 5.855  | 5.866                                      | 5.876  | 5.887  | 5.897  | 5.907  | 5.918  | 5.928  | 5.939  | 5.949  | 5.960  | 660                        |  |
| 670   | 5.960  | 5.970                                      | 5.980  | 5.991  | 6.001  | 6.012  | 6.022  | 6.033  | 6.043  | 6.054  | 6.064  | 670                        |  |
| 680   | 6.064  | 6.075                                      | 6.085  | 6.096  | 6.106  | 6.117  | 6.127  | 6.138  | 6.148  | 6.159  | 6.169  | 680                        |  |
| 690   | 6.169  | 6.180                                      | 6.190  | 6.201  | 6.211  | 6.222  | 6.232  | 6.243  | 6.253  | 6.264  | 6.274  | 690                        |  |
| 700   | 6.274  | 6.285                                      | 6.295  | 6.306  | 6.316  | 6.327  | 6.338  | 6.348  | 6.359  | 6.369  | 6.380  | 700                        |  |
| 710   | 6.380  | 6.390                                      | 6.401  | 6.412  | 6.422  | 6.433  | 6.443  | 6.454  | 6.465  | 6.475  | 6.486  | 710                        |  |
| 720   | 6.486  | 6.496                                      | 6.507  | 6.518  | 6.528  | 6.539  | 6.549  | 6.560  | 6.571  | 6.581  | 6.592  | 720                        |  |
| 730   | 6.592  | 6.603                                      | 6.613  | 6.624  | 6.635  | 6.645  | 6.656  | 6.667  | 6.677  | 6.688  | 6.699  | 730                        |  |
| 740   | 6.699  | 6.709                                      | 6.720  | 6.731  | 6.741  | 6.752  | 6.763  | 6.773  | 6.784  | 6.795  | 6.805  | 740                        |  |
| 750   | 6.805  | 6.816                                      | 6.827  | 6.838  | 6.848  | 6.859  | 6.870  | 6.880  | 6.891  | 6.902  | 6.913  | 750                        |  |
| 760   | 6.913  | 6.923                                      | 6.934  | 6.945  | 6.956  | 6.966  | 6.977  | 6.988  | 6.999  | 7.009  | 7.020  | 760                        |  |
| 770   | 7.020  | 7.031                                      | 7.042  | 7.053  | 7.063  | 7.074  | 7.085  | 7.096  | 7.107  | 7.117  | 7.128  | 770                        |  |
| 780   | 7.128  | 7.139                                      | 7.150  | 7.161  | 7.171  | 7.182  | 7.193  | 7.204  | 7.215  | 7.225  | 7.236  | 780                        |  |
| 790   | 7.236  | 7.247                                      | 7.258  | 7.269  | 7.280  | 7.291  | 7.301  | 7.312  | 7.323  | 7.334  | 7.345  | 790                        |  |
| 800   | 7.345  | 7.356                                      | 7.367  | 7.377  | 7.388  | 7.399  | 7.410  | 7.421  | 7.432  | 7.443  | 7.454  | 800                        |  |
| 810   | 7.454  | 7.465                                      | 7.476  | 7.486  | 7.497  | 7.508  | 7.519  | 7.530  | 7.541  | 7.552  | 7.563  | 810                        |  |
| 820   | 7.563  | 7.574                                      | 7.585  | 7.596  | 7.607  | 7.618  | 7.629  | 7.640  | 7.651  | 7.661  | 7.672  | 820                        |  |
| 830   | 7.672  | 7.683                                      | 7.694  | 7.705  | 7.716  | 7.727  | 7.738  | 7.749  | 7.760  | 7.771  | 7.782  | 830                        |  |
| 840   | 7.782  | 7.793                                      | 7.804  | 7.815  | 7.826  | 7.837  | 7.848  | 7.859  | 7.870  | 7.881  | 7.892  | 840                        |  |
| 850   | 7.892  | 7.904                                      | 7.915  | 7.926  | 7.937  | 7.948  | 7.959  | 7.970  | 7.981  | 7.992  | 8.003  | 850                        |  |
| 860   | 8.003  | 8.014                                      | 8.025  | 8.036  | 8.047  | 8.058  | 8.069  | 8.081  | 8.092  | 8.103  | 8.114  | 860                        |  |
| 870   | 8.114  | 8.125                                      | 8.136  | 8.147  | 8.158  | 8.169  | 8.180  | 8.192  | 8.203  | 8.214  | 8.225  | 870                        |  |
| 880   | 8.225  | 8.236                                      | 8.247  | 8.258  | 8.270  | 8.281  | 8.292  | 8.303  | 8.314  | 8.325  | 8.336  | 880                        |  |
| 890   | 8.336  | 8.348                                      | 8.359  | 8.370  | 8.381  | 8.392  | 8.404  | 8.415  | 8.426  | 8.437  | 8.448  | 890                        |  |
| 900   | 8.448  | 8.460                                      | 8.471  | 8.482  | 8.493  | 8.504  | 8.516  | 8.527  | 8.538  | 8.549  | 8.560  | 900                        |  |
| 910   | 8.560  | 8.572                                      | 8.583  | 8.594  | 8.605  | 8.617  | 8.628  | 8.639  | 8.650  | 8.662  | 8.673  | 910                        |  |
| 920   | 8.673  | 8.684                                      | 8.695  | 8.707  | 8.718  | 8.729  | 8.741  | 8.752  | 8.763  | 8.774  | 8.786  | 920                        |  |
| 930   | 8.786  | 8.797                                      | 8.808  | 8.820  | 8.831  | 8.842  | 8.854  | 8.865  | 8.876  | 8.888  | 8.899  | 930                        |  |
| 940   | 8.899  | 8.910                                      | 8.922  | 8.933  | 8.944  | 8.956  | 8.967  | 8.978  | 8.990  | 9.001  | 9.012  | 940                        |  |
| 950   | 9.012  | 9.024                                      | 9.035  | 9.047  | 9.058  | 9.069  | 9.081  | 9.092  | 9.103  | 9.115  | 9.126  | 950                        |  |
| 960   | 9.126  | 9.138                                      | 9.149  | 9.160  | 9.172  | 9.183  | 9.195  | 9.206  | 9.217  | 9.229  | 9.240  | 960                        |  |
| 970   | 9.240  | 9.252                                      | 9.263  | 9.275  | 9.286  | 9.298  | 9.309  | 9.320  | 9.332  | 9.343  | 9.355  | 970                        |  |
| 980   | 9.355  | 9.366                                      | 9.378  | 9.389  | 9.401  | 9.412  | 9.424  | 9.435  | 9.447  | 9.458  | 9.470  | 980                        |  |
| 990   | 9.470  | 9.481                                      | 9.493  | 9.504  | 9.516  | 9.527  | 9.539  | 9.550  | 9.562  | 9.573  | 9.585  | 990                        |  |
| 1.000   | 9.585  | 9.596                                      | 9.608  | 9.619  | 9.631  | 9.642  | 9.654  | 9.665  | 9.677  | 9.689  | 9.700  | 1.000                      |  |
| 1.010   | 9.700  | 9.712                                      | 9.723  | 9.735  | 9.746  | 9.758  | 9.770  | 9.781  | 9.793  | 9.804  | 9.816  | 1.010                      |  |
| 1.020   | 9.816  | 9.828                                      | 9.839  | 9.851  | 9.862  | 9.874  | 9.886  | 9.897  | 9.909  | 9.920  | 9.932  | 1.020                      |  |
| 1.030   | 9.932  | 9.944                                      | 9.955  | 9.967  | 9.979  | 9.990  | 10.002 | 10.013 | 10.025 | 10.037 | 10.048 | 1.030                      |  |
| 1.040   | 10.048 | 10.060                                     | 10.072 | 10.083 | 10.095 | 10.107 | 10.118 | 10.130 | 10.142 | 10.154 | 10.165 | 1.040                      |  |
| 1.050   | 10.165 | 10.177                                     | 10.189 | 10.200 | 10.212 | 10.224 | 10.235 | 10.247 | 10.259 | 10.271 | 10.282 | 1.050                      |  |
| 1.060   | 10.282 | 10.294                                     | 10.306 | 10.318 | 10.329 | 10.341 | 10.353 | 10.364 | 10.376 | 10.388 | 10.400 | 1.060                      |  |
| 1.070   | 10.400 | 10.411                                     | 10.423 | 10.435 | 10.447 | 10.459 | 10.470 | 10.482 | 10.494 | 10.506 | 10.517 | 1.070                      |  |
| 1.080   | 10.517 | 10.529                                     | 10.541 | 10.553 | 10.565 | 10.576 | 10.588 | 10.600 | 10.612 | 10.624 | 10.635 | 1.080                      |  |
| 1.090   | 10.635 | 10.647                                     | 10.659 | 10.671 | 10.683 | 10.694 | 10.706 | 10.718 | 10.730 | 10.742 | 10.754 | 1.090                      |  |
| 1.100   | 10.754 | 10.765                                     | 10.777 | 10.789 | 10.801 | 10.813 | 10.825 | 10.836 | 10.848 | 10.860 | 10.872 | 1.100                      |  |
| 1.110   | 10.872 | 10.884                                     | 10.896 | 10.908 | 10.919 | 10.931 | 10.943 | 10.955 | 10.967 | 10.979 | 10.991 | 1.110                      |  |
| 1.120   | 10.991 | 11.003                                     | 11.014 | 11.026 | 11.038 | 11.050 | 11.062 | 11.074 | 11.086 | 11.098 | 11.110 | 1.120                      |  |
| 1.130   | 11.110 | 11.121                                     | 11.133 | 11.145 | 11.157 | 11.169 | 11.181 | 11.193 | 11.205 | 11.217 | 11.229 | 1.130                      |  |
| 1.140   | 11.229 | 11.241                                     | 11.252 | 11.264 | 11.276 | 11.288 | 11.300 | 11.312 | 11.324 | 11.336 | 11.348 | 1.140                      |  |
| 1.150   | 11.348 | 11.360                                     | 11.372 | 11.384 | 11.396 | 11.408 | 11.420 | 11.432 | 11.444 | 11.455 | 11.467 | 1.150                      |  |
| 1.160   | 11.467 | 11.479                                     | 11.491 | 11.503 | 11.515 | 11.527 | 11.539 | 11.551 | 11.563 | 11.575 | 11.587 | 1.160                      |  |
| 1.170   | 11.587 | 11.599                                     | 11.611 | 11.623 | 11.635 | 11.647 | 11.659 | 11.671 | 11.683 | 11.695 | 11.707 | 1.170                      |  |
| 1.180   | 11.707 | 11.719                                     | 11.731 | 11.743 | 11.755 | 11.767 | 11.779 | 11.791 | 11.803 | 11.815 | 11.827 | 1.180                      |  |
| 1.190   | 11.827 | 11.839                                     | 11.851 | 11.863 | 11.875 | 11.887 | 11.899 | 11.911 | 11.923 | 11.935 | 11.947 | 1.190                      |  |
| 1.200   | 11.947 | 11.959                                     | 11.971 | 11.983 | 11.995 | 12.007 | 12.019 | 12.031 | 12.043 | 12.055 | 12.067 | 1.200                      |  |
| 1.210   | 12.067 | 12.079                                     | 12.091 | 12.103 | 12.115 | 12.127 | 12.140 | 12.152 | 12.164 | 12.176 | 12.188 | 1.210                      |  |
| 1.220   | 12.188 | 12.200                                     | 12.212 | 12.224 | 12.236 | 12.248 | 12.260 | 12.272 | 12.284 | 12.296 | 12.308 | 1.220                      |  |
| 1.230   | 12.308 | 12.320                                     | 12.332 | 12.345 | 12.357 | 12.369 | 12.381 | 12.393 | 12.405 | 12.417 | 12.429 | 1.230                      |  |
| 1.240   | 12.429 | 12.441                                     | 12.453 | 12.465 | 12.477 | 12.489 | 12.501 | 12.514 | 12.526 | 12.538 | 12.550 | 1.240                      |  |
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |

TABLE 10.13—Type S thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Celsius (IPTS 1968) |        |        |        |        |        |        |        |        |        | Reference Junctions at 0 C |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------------------------|--|
|   |        | 0  | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      |                            |  |
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                            |  |
| 1.250   | 12.550 | 12.562                                     | 12.574 | 12.586 | 12.598 | 12.610 | 12.622 | 12.634 | 12.647 | 12.659 | 12.671 | 1.250                      |  |
| 1.260   | 12.671 | 12.683                                     | 12.695 | 12.707 | 12.719 | 12.731 | 12.743 | 12.755 | 12.767 | 12.780 | 12.792 | 1.260                      |  |
| 1.270   | 12.792 | 12.804                                     | 12.816 | 12.828 | 12.840 | 12.852 | 12.864 | 12.876 | 12.888 | 12.901 | 12.913 | 1.270                      |  |
| 1.280   | 12.913 | 12.925                                     | 12.937 | 12.949 | 12.961 | 12.973 | 12.985 | 12.997 | 13.010 | 13.022 | 13.034 | 1.280                      |  |
| 1.290   | 13.034 | 13.046                                     | 13.058 | 13.070 | 13.082 | 13.094 | 13.107 | 13.119 | 13.131 | 13.143 | 13.155 | 1.290                      |  |
| 1.300   | 13.155 | 13.167                                     | 13.179 | 13.191 | 13.203 | 13.216 | 13.228 | 13.240 | 13.252 | 13.264 | 13.276 | 1.300                      |  |
| 1.310   | 13.276 | 13.288                                     | 13.300 | 13.313 | 13.325 | 13.337 | 13.349 | 13.361 | 13.373 | 13.385 | 13.397 | 1.310                      |  |
| 1.320   | 13.397 | 13.410                                     | 13.422 | 13.434 | 13.446 | 13.458 | 13.470 | 13.482 | 13.495 | 13.507 | 13.519 | 1.320                      |  |
| 1.330   | 13.519 | 13.531                                     | 13.543 | 13.555 | 13.567 | 13.579 | 13.592 | 13.604 | 13.616 | 13.628 | 13.640 | 1.330                      |  |
| 1.340   | 13.640 | 13.652                                     | 13.664 | 13.677 | 13.689 | 13.701 | 13.713 | 13.725 | 13.737 | 13.749 | 13.761 | 1.340                      |  |
| 1.350   | 13.761 | 13.774                                     | 13.786 | 13.798 | 13.810 | 13.822 | 13.834 | 13.846 | 13.859 | 13.871 | 13.883 | 1.350                      |  |
| 1.360   | 13.883 | 13.895                                     | 13.907 | 13.919 | 13.931 | 13.943 | 13.956 | 13.968 | 13.980 | 13.992 | 14.004 | 1.360                      |  |
| 1.370   | 14.004 | 14.016                                     | 14.028 | 14.040 | 14.053 | 14.065 | 14.077 | 14.089 | 14.101 | 14.113 | 14.125 | 1.370                      |  |
| 1.380   | 14.125 | 14.138                                     | 14.150 | 14.162 | 14.174 | 14.186 | 14.198 | 14.210 | 14.222 | 14.235 | 14.247 | 1.380                      |  |
| 1.390   | 14.247 | 14.259                                     | 14.271 | 14.283 | 14.295 | 14.307 | 14.319 | 14.332 | 14.344 | 14.356 | 14.368 | 1.390                      |  |
| 1.400   | 14.368 | 14.380                                     | 14.392 | 14.404 | 14.416 | 14.429 | 14.441 | 14.453 | 14.465 | 14.477 | 14.489 | 1.400                      |  |
| 1.410   | 14.489 | 14.501                                     | 14.513 | 14.526 | 14.538 | 14.550 | 14.562 | 14.574 | 14.586 | 14.598 | 14.610 | 1.410                      |  |
| 1.420   | 14.610 | 14.622                                     | 14.635 | 14.647 | 14.659 | 14.671 | 14.683 | 14.695 | 14.707 | 14.719 | 14.731 | 1.420                      |  |
| 1.430   | 14.731 | 14.744                                     | 14.756 | 14.768 | 14.780 | 14.792 | 14.804 | 14.816 | 14.828 | 14.840 | 14.852 | 1.430                      |  |
| 1.440   | 14.852 | 14.865                                     | 14.877 | 14.889 | 14.901 | 14.913 | 14.925 | 14.937 | 14.949 | 14.961 | 14.973 | 1.440                      |  |
| 1.450   | 14.973 | 14.985                                     | 14.998 | 15.010 | 15.022 | 15.034 | 15.046 | 15.058 | 15.070 | 15.082 | 15.094 | 1.450                      |  |
| 1.460   | 15.094 | 15.106                                     | 15.118 | 15.130 | 15.143 | 15.155 | 15.167 | 15.179 | 15.191 | 15.203 | 15.215 | 1.460                      |  |
| 1.470   | 15.215 | 15.227                                     | 15.239 | 15.251 | 15.263 | 15.275 | 15.287 | 15.299 | 15.311 | 15.323 | 15.336 | 1.470                      |  |
| 1.480   | 15.336 | 15.348                                     | 15.360 | 15.372 | 15.384 | 15.396 | 15.408 | 15.420 | 15.432 | 15.444 | 15.456 | 1.480                      |  |
| 1.490   | 15.456 | 15.468                                     | 15.480 | 15.492 | 15.504 | 15.516 | 15.528 | 15.540 | 15.552 | 15.564 | 15.576 | 1.490                      |  |
| 1.500   | 15.576 | 15.589                                     | 15.601 | 15.613 | 15.625 | 15.637 | 15.649 | 15.661 | 15.673 | 15.685 | 15.697 | 1.500                      |  |
| 1.510   | 15.697 | 15.709                                     | 15.721 | 15.733 | 15.745 | 15.757 | 15.769 | 15.781 | 15.793 | 15.805 | 15.817 | 1.510                      |  |
| 1.520   | 15.817 | 15.829                                     | 15.841 | 15.853 | 15.865 | 15.877 | 15.889 | 15.901 | 15.913 | 15.925 | 15.937 | 1.520                      |  |
| 1.530   | 15.937 | 15.949                                     | 15.961 | 15.973 | 15.985 | 15.997 | 16.009 | 16.021 | 16.033 | 16.045 | 16.057 | 1.530                      |  |
| 1.540   | 16.057 | 16.069                                     | 16.080 | 16.092 | 16.104 | 16.116 | 16.128 | 16.140 | 16.152 | 16.164 | 16.176 | 1.540                      |  |
| 1.550   | 16.176 | 16.188                                     | 16.200 | 16.212 | 16.224 | 16.236 | 16.248 | 16.260 | 16.272 | 16.284 | 16.296 | 1.550                      |  |
| 1.560   | 16.296 | 16.308                                     | 16.319 | 16.331 | 16.343 | 16.355 | 16.367 | 16.379 | 16.391 | 16.403 | 16.415 | 1.560                      |  |
| 1.570   | 16.415 | 16.427                                     | 16.439 | 16.451 | 16.462 | 16.474 | 16.486 | 16.498 | 16.510 | 16.522 | 16.534 | 1.570                      |  |
| 1.580   | 16.534 | 16.546                                     | 16.558 | 16.569 | 16.581 | 16.593 | 16.605 | 16.617 | 16.629 | 16.641 | 16.653 | 1.580                      |  |
| 1.590   | 16.653 | 16.664                                     | 16.676 | 16.688 | 16.700 | 16.712 | 16.724 | 16.736 | 16.747 | 16.759 | 16.771 | 1.590                      |  |
| 1.600   | 16.771 | 16.783                                     | 16.795 | 16.807 | 16.819 | 16.830 | 16.842 | 16.854 | 16.866 | 16.878 | 16.890 | 1.600                      |  |
| 1.610   | 16.890 | 16.901                                     | 16.913 | 16.925 | 16.937 | 16.949 | 16.960 | 16.972 | 16.984 | 16.996 | 17.008 | 1.610                      |  |
| 1.620   | 17.008 | 17.019                                     | 17.031 | 17.043 | 17.055 | 17.067 | 17.078 | 17.090 | 17.102 | 17.114 | 17.125 | 1.620                      |  |
| 1.630   | 17.125 | 17.137                                     | 17.149 | 17.161 | 17.173 | 17.184 | 17.196 | 17.208 | 17.220 | 17.231 | 17.243 | 1.630                      |  |
| 1.640   | 17.243 | 17.255                                     | 17.267 | 17.278 | 17.290 | 17.302 | 17.313 | 17.325 | 17.337 | 17.349 | 17.360 | 1.640                      |  |
| 1.650   | 17.360 | 17.372                                     | 17.384 | 17.396 | 17.407 | 17.419 | 17.431 | 17.442 | 17.454 | 17.466 | 17.477 | 1.650                      |  |
| 1.660   | 17.477 | 17.489                                     | 17.501 | 17.512 | 17.524 | 17.536 | 17.548 | 17.559 | 17.571 | 17.583 | 17.594 | 1.660                      |  |
| 1.670   | 17.594 | 17.606                                     | 17.617 | 17.629 | 17.641 | 17.652 | 17.664 | 17.676 | 17.687 | 17.699 | 17.711 | 1.670                      |  |
| 1.680   | 17.711 | 17.722                                     | 17.734 | 17.745 | 17.757 | 17.769 | 17.780 | 17.792 | 17.803 | 17.815 | 17.826 | 1.680                      |  |
| 1.690   | 17.826 | 17.838                                     | 17.850 | 17.861 | 17.873 | 17.884 | 17.896 | 17.907 | 17.919 | 17.930 | 17.942 | 1.690                      |  |
| 1.700   | 17.942 | 17.953                                     | 17.965 | 17.976 | 17.988 | 17.999 | 18.010 | 18.022 | 18.033 | 18.045 | 18.056 | 1.700                      |  |
| 1.710   | 18.056 | 18.068                                     | 18.079 | 18.090 | 18.102 | 18.113 | 18.124 | 18.136 | 18.147 | 18.158 | 18.170 | 1.710                      |  |
| 1.720   | 18.170 | 18.181                                     | 18.192 | 18.204 | 18.215 | 18.226 | 18.237 | 18.249 | 18.260 | 18.271 | 18.282 | 1.720                      |  |
| 1.730   | 18.282 | 18.293                                     | 18.305 | 18.316 | 18.327 | 18.338 | 18.349 | 18.360 | 18.372 | 18.383 | 18.394 | 1.730                      |  |
| 1.740   | 18.394 | 18.405                                     | 18.416 | 18.427 | 18.438 | 18.449 | 18.460 | 18.471 | 18.482 | 18.493 | 18.504 | 1.740                      |  |
| 1.750   | 18.504 | 18.515                                     | 18.526 | 18.536 | 18.547 | 18.558 | 18.569 | 18.580 | 18.591 | 18.602 | 18.612 | 1.750                      |  |
| 1.760   | 18.612 | 18.623                                     | 18.634 | 18.645 | 18.655 | 18.666 | 18.677 | 18.687 | 18.698 |        |        | 1.760                      |  |
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |



214 THE USE OF THERMOCOUPLES IN TEMPERATURE MEASUREMENT

TABLE 10.14—Type T thermocouples (deg F-millivolts).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit* |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|------------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
| DEG F   | 0      | 1                                  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |                                    |        |        |        |        |        |        |        |        |        |                             |  |
| -450  | -6.254 | -6.255                             | -6.256 | -6.257 | -6.258 |        |        |        |        |        |        | -450                        |  |
| -440  | -6.240 | -6.242                             | -6.243 | -6.245 | -6.247 | -6.248 | -6.250 | -6.251 | -6.252 | -6.253 | -6.254 | -440                        |  |
| -430  | -6.217 | -6.220                             | -6.223 | -6.225 | -6.227 | -6.230 | -6.232 | -6.234 | -6.236 | -6.238 | -6.240 | -430                        |  |
| -420  | -6.187 | -6.191                             | -6.194 | -6.197 | -6.200 | -6.203 | -6.206 | -6.209 | -6.212 | -6.215 | -6.217 | -420                        |  |
| -410  | -6.150 | -6.154                             | -6.158 | -6.162 | -6.166 | -6.170 | -6.173 | -6.177 | -6.181 | -6.184 | -6.187 | -410                        |  |
| -400  | -6.105 | -6.110                             | -6.115 | -6.119 | -6.124 | -6.128 | -6.133 | -6.137 | -6.142 | -6.146 | -6.150 | -400                        |  |
| -390  | -6.053 | -6.059                             | -6.064 | -6.069 | -6.075 | -6.080 | -6.085 | -6.090 | -6.095 | -6.100 | -6.105 | -390                        |  |
| -380  | -5.995 | -6.001                             | -6.007 | -6.013 | -6.019 | -6.025 | -6.030 | -6.036 | -6.042 | -6.048 | -6.053 | -380                        |  |
| -370  | -5.930 | -5.937                             | -5.943 | -5.950 | -5.957 | -5.963 | -5.969 | -5.976 | -5.982 | -5.988 | -5.995 | -370                        |  |
| -360  | -5.860 | -5.867                             | -5.874 | -5.881 | -5.889 | -5.896 | -5.903 | -5.910 | -5.916 | -5.923 | -5.930 | -360                        |  |
| -350  | -5.785 | -5.792                             | -5.800 | -5.808 | -5.815 | -5.823 | -5.830 | -5.838 | -5.845 | -5.853 | -5.860 | -350                        |  |
| -340  | -5.705 | -5.713                             | -5.721 | -5.729 | -5.737 | -5.745 | -5.753 | -5.761 | -5.769 | -5.777 | -5.785 | -340                        |  |
| -330  | -5.620 | -5.629                             | -5.638 | -5.646 | -5.655 | -5.663 | -5.672 | -5.680 | -5.688 | -5.697 | -5.705 | -330                        |  |
| -320  | -5.532 | -5.541                             | -5.550 | -5.559 | -5.568 | -5.576 | -5.585 | -5.594 | -5.603 | -5.612 | -5.620 | -320                        |  |
| -310  | -5.439 | -5.448                             | -5.457 | -5.467 | -5.476 | -5.486 | -5.495 | -5.504 | -5.513 | -5.522 | -5.532 | -310                        |  |
| -300  | -5.341 | -5.351                             | -5.361 | -5.371 | -5.381 | -5.390 | -5.400 | -5.410 | -5.419 | -5.429 | -5.439 | -300                        |  |
| -290  | -5.240 | -5.250                             | -5.261 | -5.271 | -5.281 | -5.291 | -5.301 | -5.311 | -5.321 | -5.331 | -5.341 | -290                        |  |
| -280  | -5.135 | -5.145                             | -5.156 | -5.167 | -5.177 | -5.188 | -5.198 | -5.209 | -5.219 | -5.230 | -5.240 | -280                        |  |
| -270  | -5.025 | -5.036                             | -5.047 | -5.058 | -5.069 | -5.080 | -5.091 | -5.102 | -5.113 | -5.124 | -5.135 | -270                        |  |
| -260  | -4.912 | -4.923                             | -4.935 | -4.946 | -4.958 | -4.969 | -4.980 | -4.992 | -5.003 | -5.014 | -5.025 | -260                        |  |
| -250  | -4.794 | -4.806                             | -4.818 | -4.830 | -4.842 | -4.853 | -4.865 | -4.877 | -4.889 | -4.900 | -4.912 | -250                        |  |
| -240  | -4.673 | -4.685                             | -4.698 | -4.710 | -4.722 | -4.734 | -4.746 | -4.758 | -4.770 | -4.782 | -4.794 | -240                        |  |
| -230  | -4.548 | -4.560                             | -4.573 | -4.586 | -4.598 | -4.611 | -4.623 | -4.636 | -4.648 | -4.661 | -4.673 | -230                        |  |
| -220  | -4.419 | -4.432                             | -4.445 | -4.458 | -4.471 | -4.484 | -4.497 | -4.509 | -4.522 | -4.535 | -4.548 | -220                        |  |
| -210  | -4.286 | -4.299                             | -4.313 | -4.326 | -4.339 | -4.353 | -4.366 | -4.379 | -4.392 | -4.406 | -4.419 | -210                        |  |
| -200  | -4.149 | -4.163                             | -4.177 | -4.191 | -4.204 | -4.218 | -4.232 | -4.245 | -4.259 | -4.272 | -4.286 | -200                        |  |
| -190  | -4.009 | -4.023                             | -4.037 | -4.051 | -4.065 | -4.079 | -4.093 | -4.107 | -4.121 | -4.135 | -4.149 | -190                        |  |
| -180  | -3.864 | -3.879                             | -3.894 | -3.908 | -3.923 | -3.937 | -3.951 | -3.966 | -3.980 | -3.994 | -4.009 | -180                        |  |
| -170  | -3.717 | -3.732                             | -3.746 | -3.761 | -3.776 | -3.791 | -3.806 | -3.820 | -3.835 | -3.850 | -3.864 | -170                        |  |
| -160  | -3.565 | -3.580                             | -3.596 | -3.611 | -3.626 | -3.641 | -3.656 | -3.671 | -3.687 | -3.702 | -3.717 | -160                        |  |
| -150  | -3.410 | -3.425                             | -3.441 | -3.457 | -3.472 | -3.488 | -3.503 | -3.519 | -3.534 | -3.550 | -3.565 | -150                        |  |
| -140  | -3.251 | -3.267                             | -3.283 | -3.299 | -3.315 | -3.331 | -3.347 | -3.362 | -3.378 | -3.394 | -3.410 | -140                        |  |
| -130  | -3.089 | -3.105                             | -3.121 | -3.138 | -3.154 | -3.170 | -3.186 | -3.203 | -3.219 | -3.235 | -3.251 | -130                        |  |
| -120  | -2.923 | -2.939                             | -2.956 | -2.973 | -2.989 | -3.006 | -3.023 | -3.039 | -3.056 | -3.072 | -3.089 | -120                        |  |
| -110  | -2.753 | -2.771                             | -2.788 | -2.805 | -2.822 | -2.838 | -2.855 | -2.872 | -2.889 | -2.906 | -2.923 | -110                        |  |
| -100  | -2.581 | -2.598                             | -2.616 | -2.633 | -2.650 | -2.667 | -2.685 | -2.702 | -2.719 | -2.736 | -2.753 | -100                        |  |
| -90   | -2.405 | -2.422                             | -2.440 | -2.458 | -2.475 | -2.493 | -2.511 | -2.528 | -2.546 | -2.563 | -2.581 | -90                         |  |
| -80   | -2.225 | -2.243                             | -2.261 | -2.279 | -2.297 | -2.315 | -2.333 | -2.351 | -2.369 | -2.387 | -2.405 | -80                         |  |
| -70   | -2.042 | -2.061                             | -2.077 | -2.098 | -2.116 | -2.134 | -2.152 | -2.171 | -2.189 | -2.207 | -2.225 | -70                         |  |
| -60   | -1.856 | -1.875                             | -1.894 | -1.912 | -1.931 | -1.950 | -1.968 | -1.987 | -2.005 | -2.024 | -2.042 | -60                         |  |
| -50   | -1.667 | -1.686                             | -1.705 | -1.724 | -1.743 | -1.762 | -1.781 | -1.800 | -1.819 | -1.838 | -1.856 | -50                         |  |
| -40   | -1.475 | -1.494                             | -1.513 | -1.533 | -1.552 | -1.571 | -1.591 | -1.610 | -1.629 | -1.648 | -1.667 | -40                         |  |
| -30   | -1.279 | -1.299                             | -1.319 | -1.338 | -1.358 | -1.377 | -1.397 | -1.416 | -1.436 | -1.455 | -1.475 | -30                         |  |
| -20   | -1.081 | -1.101                             | -1.121 | -1.141 | -1.160 | -1.180 | -1.200 | -1.220 | -1.240 | -1.260 | -1.277 | -20                         |  |
| -10   | -0.877 | -0.899                             | -0.920 | -0.940 | -0.960 | -0.980 | -1.000 | -1.021 | -1.041 | -1.061 | -1.081 | -10                         |  |
| 0   | -0.674 | -0.695                             | -0.716 | -0.736 | -0.757 | -0.777 | -0.798 | -0.818 | -0.838 | -0.859 | -0.879 | 0                           |  |
| 0   | -0.674 | -0.654                             | -0.633 | -0.613 | -0.592 | -0.571 | -0.550 | -0.529 | -0.509 | -0.488 | -0.467 | 0                           |  |
| 10  | -0.467 | -0.446                             | -0.425 | -0.404 | -0.383 | -0.362 | -0.341 | -0.320 | -0.299 | -0.277 | -0.256 | 10                          |  |
| 20  | -0.256 | -0.235                             | -0.214 | -0.193 | -0.171 | -0.150 | -0.129 | -0.107 | -0.086 | -0.064 | -0.043 | 20                          |  |
| 30  | -0.043 | -0.022                             | 0.000  | 0.022  | 0.043  | 0.065  | 0.086  | 0.108  | 0.130  | 0.151  | 0.173  | 30                          |  |
| 40  | 0.173  | 0.195                              | 0.216  | 0.238  | 0.260  | 0.282  | 0.303  | 0.325  | 0.347  | 0.369  | 0.391  | 40                          |  |
| 50  | 0.391  | 0.413                              | 0.435  | 0.457  | 0.479  | 0.501  | 0.523  | 0.545  | 0.567  | 0.589  | 0.611  | 50                          |  |
| 60  | 0.611  | 0.634                              | 0.656  | 0.678  | 0.700  | 0.722  | 0.745  | 0.767  | 0.789  | 0.812  | 0.834  | 60                          |  |
| 70  | 0.834  | 0.857                              | 0.879  | 0.902  | 0.924  | 0.947  | 0.969  | 0.992  | 1.014  | 1.037  | 1.060  | 70                          |  |
| 80  | 1.060  | 1.082                              | 1.105  | 1.128  | 1.151  | 1.173  | 1.196  | 1.219  | 1.242  | 1.265  | 1.288  | 80                          |  |
| 90  | 1.288  | 1.311                              | 1.334  | 1.357  | 1.380  | 1.403  | 1.426  | 1.449  | 1.472  | 1.495  | 1.518  | 90                          |  |
| 100   | 1.518  | 1.542                              | 1.565  | 1.588  | 1.611  | 1.635  | 1.658  | 1.681  | 1.705  | 1.728  | 1.752  | 100                         |  |
| 110   | 1.752  | 1.775                              | 1.799  | 1.822  | 1.846  | 1.869  | 1.893  | 1.917  | 1.940  | 1.964  | 1.988  | 110                         |  |
| 120   | 1.988  | 2.011                              | 2.035  | 2.059  | 2.083  | 2.107  | 2.131  | 2.154  | 2.178  | 2.202  | 2.226  | 120                         |  |
| 130   | 2.226  | 2.250                              | 2.274  | 2.298  | 2.322  | 2.347  | 2.371  | 2.395  | 2.419  | 2.443  | 2.467  | 130                         |  |
| 140   | 2.467  | 2.492                              | 2.516  | 2.540  | 2.565  | 2.589  | 2.613  | 2.638  | 2.662  | 2.687  | 2.711  | 140                         |  |

\* Converted from degrees Celsius (1PTS 1968).

TABLE 10.14—Type T thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Fahrenheit* |        |        |        |        |        |        |        |        |        | Reference Junctions at 32 F |  |
|---|--------|------------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-----------------------------|--|
| DEG F   | 0      | 1                                  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG F                       |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |                                    |        |        |        |        |        |        |        |        |        |                             |  |
| 150   | 2.711  | 2.736                              | 2.760  | 2.785  | 2.809  | 2.834  | 2.859  | 2.883  | 2.908  | 2.933  | 2.958  | 150                         |  |
| 160   | 2.958  | 2.982                              | 3.007  | 3.032  | 3.057  | 3.082  | 3.107  | 3.131  | 3.156  | 3.181  | 3.206  | 160                         |  |
| 170   | 3.206  | 3.231                              | 3.256  | 3.281  | 3.307  | 3.332  | 3.357  | 3.382  | 3.407  | 3.432  | 3.458  | 170                         |  |
| 180   | 3.458  | 3.483                              | 3.508  | 3.533  | 3.559  | 3.584  | 3.609  | 3.635  | 3.660  | 3.686  | 3.711  | 180                         |  |
| 190   | 3.711  | 3.737                              | 3.762  | 3.788  | 3.813  | 3.839  | 3.864  | 3.890  | 3.916  | 3.941  | 3.967  | 190                         |  |
| 200   | 3.967  | 3.993                              | 4.019  | 4.044  | 4.070  | 4.096  | 4.122  | 4.148  | 4.174  | 4.199  | 4.225  | 200                         |  |
| 210   | 4.225  | 4.251                              | 4.277  | 4.303  | 4.329  | 4.355  | 4.381  | 4.408  | 4.434  | 4.460  | 4.486  | 210                         |  |
| 220   | 4.486  | 4.512                              | 4.538  | 4.565  | 4.591  | 4.617  | 4.643  | 4.670  | 4.696  | 4.722  | 4.749  | 220                         |  |
| 230   | 4.749  | 4.775                              | 4.801  | 4.828  | 4.854  | 4.881  | 4.907  | 4.934  | 4.960  | 4.987  | 5.014  | 230                         |  |
| 240   | 5.014  | 5.040                              | 5.067  | 5.093  | 5.120  | 5.147  | 5.174  | 5.200  | 5.227  | 5.254  | 5.281  | 240                         |  |
| 250   | 5.281  | 5.307                              | 5.334  | 5.361  | 5.388  | 5.415  | 5.442  | 5.469  | 5.496  | 5.523  | 5.550  | 250                         |  |
| 260   | 5.550  | 5.577                              | 5.604  | 5.631  | 5.658  | 5.685  | 5.712  | 5.739  | 5.767  | 5.794  | 5.821  | 260                         |  |
| 270   | 5.821  | 5.848                              | 5.875  | 5.903  | 5.930  | 5.957  | 5.985  | 6.012  | 6.039  | 6.067  | 6.094  | 270                         |  |
| 280   | 6.094  | 6.122                              | 6.149  | 6.177  | 6.204  | 6.232  | 6.259  | 6.287  | 6.314  | 6.342  | 6.369  | 280                         |  |
| 290   | 6.369  | 6.397                              | 6.425  | 6.452  | 6.480  | 6.508  | 6.536  | 6.563  | 6.591  | 6.619  | 6.647  | 290                         |  |
| 300   | 6.647  | 6.675                              | 6.702  | 6.730  | 6.758  | 6.786  | 6.814  | 6.842  | 6.870  | 6.898  | 6.926  | 300                         |  |
| 310   | 6.926  | 6.954                              | 6.982  | 7.010  | 7.038  | 7.066  | 7.094  | 7.122  | 7.151  | 7.179  | 7.207  | 310                         |  |
| 320   | 7.207  | 7.235                              | 7.263  | 7.292  | 7.320  | 7.348  | 7.377  | 7.405  | 7.433  | 7.462  | 7.490  | 320                         |  |
| 330   | 7.490  | 7.518                              | 7.547  | 7.575  | 7.604  | 7.632  | 7.661  | 7.689  | 7.718  | 7.746  | 7.775  | 330                         |  |
| 340   | 7.775  | 7.804                              | 7.832  | 7.861  | 7.889  | 7.918  | 7.947  | 7.975  | 8.004  | 8.033  | 8.062  | 340                         |  |
| 350   | 8.062  | 8.090                              | 8.119  | 8.148  | 8.177  | 8.206  | 8.235  | 8.264  | 8.292  | 8.321  | 8.350  | 350                         |  |
| 360   | 8.350  | 8.379                              | 8.408  | 8.437  | 8.466  | 8.495  | 8.524  | 8.553  | 8.583  | 8.612  | 8.641  | 360                         |  |
| 370   | 8.641  | 8.670                              | 8.699  | 8.728  | 8.757  | 8.787  | 8.816  | 8.845  | 8.874  | 8.904  | 8.933  | 370                         |  |
| 380   | 8.933  | 8.962                              | 8.992  | 9.021  | 9.050  | 9.080  | 9.109  | 9.139  | 9.168  | 9.198  | 9.227  | 380                         |  |
| 390   | 9.227  | 9.257                              | 9.286  | 9.316  | 9.345  | 9.375  | 9.404  | 9.434  | 9.464  | 9.493  | 9.523  | 390                         |  |
| 400   | 9.523  | 9.553                              | 9.582  | 9.612  | 9.642  | 9.671  | 9.701  | 9.731  | 9.761  | 9.791  | 9.820  | 400                         |  |
| 410   | 9.820  | 9.850                              | 9.880  | 9.910  | 9.940  | 9.970  | 10.000 | 10.030 | 10.060 | 10.090 | 10.120 | 410                         |  |
| 420   | 10.120 | 10.150                             | 10.180 | 10.210 | 10.240 | 10.270 | 10.300 | 10.330 | 10.360 | 10.390 | 10.420 | 420                         |  |
| 430   | 10.420 | 10.451                             | 10.481 | 10.511 | 10.541 | 10.572 | 10.602 | 10.632 | 10.662 | 10.693 | 10.723 | 430                         |  |
| 440   | 10.723 | 10.753                             | 10.784 | 10.814 | 10.845 | 10.875 | 10.905 | 10.936 | 10.966 | 10.997 | 11.027 | 440                         |  |
| 450   | 11.027 | 11.058                             | 11.088 | 11.119 | 11.149 | 11.180 | 11.211 | 11.242 | 11.272 | 11.302 | 11.333 | 450                         |  |
| 460   | 11.333 | 11.364                             | 11.394 | 11.425 | 11.456 | 11.487 | 11.517 | 11.548 | 11.579 | 11.610 | 11.640 | 460                         |  |
| 470   | 11.640 | 11.671                             | 11.702 | 11.733 | 11.764 | 11.795 | 11.826 | 11.857 | 11.888 | 11.918 | 11.949 | 470                         |  |
| 480   | 11.949 | 11.980                             | 12.011 | 12.042 | 12.073 | 12.104 | 12.135 | 12.166 | 12.198 | 12.229 | 12.260 | 480                         |  |
| 490   | 12.260 | 12.291                             | 12.322 | 12.353 | 12.384 | 12.416 | 12.447 | 12.478 | 12.509 | 12.540 | 12.572 | 490                         |  |
| 500   | 12.572 | 12.603                             | 12.634 | 12.666 | 12.697 | 12.728 | 12.760 | 12.791 | 12.822 | 12.854 | 12.885 | 500                         |  |
| 510   | 12.885 | 12.917                             | 12.948 | 12.979 | 13.011 | 13.042 | 13.074 | 13.105 | 13.137 | 13.168 | 13.200 | 510                         |  |
| 520   | 13.200 | 13.232                             | 13.263 | 13.295 | 13.326 | 13.358 | 13.390 | 13.421 | 13.453 | 13.485 | 13.516 | 520                         |  |
| 530   | 13.516 | 13.548                             | 13.580 | 13.611 | 13.643 | 13.675 | 13.707 | 13.739 | 13.770 | 13.802 | 13.834 | 530                         |  |
| 540   | 13.834 | 13.866                             | 13.898 | 13.930 | 13.961 | 13.993 | 14.025 | 14.057 | 14.089 | 14.121 | 14.153 | 540                         |  |
| 550   | 14.153 | 14.185                             | 14.217 | 14.249 | 14.281 | 14.313 | 14.345 | 14.377 | 14.409 | 14.441 | 14.474 | 550                         |  |
| 560   | 14.474 | 14.506                             | 14.538 | 14.570 | 14.602 | 14.634 | 14.666 | 14.699 | 14.731 | 14.763 | 14.795 | 560                         |  |
| 570   | 14.795 | 14.828                             | 14.860 | 14.892 | 14.924 | 14.957 | 14.989 | 15.021 | 15.054 | 15.086 | 15.118 | 570                         |  |
| 580   | 15.118 | 15.151                             | 15.183 | 15.216 | 15.248 | 15.280 | 15.313 | 15.345 | 15.378 | 15.410 | 15.443 | 580                         |  |
| 590   | 15.443 | 15.475                             | 15.508 | 15.540 | 15.573 | 15.605 | 15.638 | 15.671 | 15.703 | 15.736 | 15.769 | 590                         |  |
| 600   | 15.769 | 15.801                             | 15.834 | 15.866 | 15.899 | 15.932 | 15.965 | 15.997 | 16.030 | 16.063 | 16.096 | 600                         |  |
| 610   | 16.096 | 16.128                             | 16.161 | 16.194 | 16.227 | 16.259 | 16.292 | 16.325 | 16.358 | 16.391 | 16.424 | 610                         |  |
| 620   | 16.424 | 16.457                             | 16.490 | 16.523 | 16.555 | 16.588 | 16.621 | 16.654 | 16.687 | 16.720 | 16.753 | 620                         |  |
| 630   | 16.753 | 16.786                             | 16.819 | 16.852 | 16.885 | 16.919 | 16.952 | 16.985 | 17.018 | 17.051 | 17.084 | 630                         |  |
| 640   | 17.084 | 17.117                             | 17.150 | 17.184 | 17.217 | 17.250 | 17.283 | 17.316 | 17.350 | 17.383 | 17.416 | 640                         |  |
| 650   | 17.416 | 17.450                             | 17.483 | 17.516 | 17.549 | 17.583 | 17.616 | 17.649 | 17.683 | 17.716 | 17.750 | 650                         |  |
| 660   | 17.750 | 17.783                             | 17.816 | 17.850 | 17.883 | 17.917 | 17.950 | 17.984 | 18.017 | 18.051 | 18.084 | 660                         |  |
| 670   | 18.084 | 18.118                             | 18.151 | 18.185 | 18.218 | 18.252 | 18.285 | 18.319 | 18.353 | 18.386 | 18.420 | 670                         |  |
| 680   | 18.420 | 18.454                             | 18.487 | 18.521 | 18.555 | 18.588 | 18.622 | 18.656 | 18.689 | 18.723 | 18.757 | 680                         |  |
| 690   | 18.757 | 18.791                             | 18.824 | 18.858 | 18.892 | 18.926 | 18.960 | 18.993 | 19.027 | 19.061 | 19.095 | 690                         |  |
| 700   | 19.095 | 19.129                             | 19.163 | 19.197 | 19.230 | 19.264 | 19.298 | 19.332 | 19.366 | 19.400 | 19.434 | 700                         |  |
| 710   | 19.434 | 19.468                             | 19.502 | 19.536 | 19.570 | 19.604 | 19.638 | 19.672 | 19.706 | 19.740 | 19.774 | 710                         |  |
| 720   | 19.774 | 19.809                             | 19.843 | 19.877 | 19.911 | 19.945 | 19.979 | 20.013 | 20.047 | 20.081 | 20.116 | 720                         |  |
| 730   | 20.116 | 20.150                             | 20.184 | 20.218 | 20.252 | 20.287 | 20.321 | 20.355 | 20.389 | 20.423 | 20.458 | 730                         |  |
| 740   | 20.458 | 20.492                             | 20.526 | 20.560 | 20.595 | 20.629 | 20.663 | 20.698 | 20.732 | 20.766 | 20.801 | 740                         |  |
| 750   | 20.801 | 20.835                             | 20.869 |        |        |        |        |        |        |        |        | 750                         |  |

\* Converted from degrees Celsius (IPIS 1966).

TABLE 10.15—Type T thermocouples (deg C-millivolts).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Celsius (IPTS 1968) |        |        |        |        |        |        |        |        |        | Reference Junctions at 0 C |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------------------------|--|
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                            |  |
| -270  | -6.258 |  |        |        |        |        |        |        |        |        |        | -270                       |  |
| -260  | -6.232 | -6.236                                     | -6.239 | -6.242 | -6.245 | -6.248 | -6.251 | -6.253 | -6.255 | -6.256 | -6.258 | -260                       |  |
| -250  | -6.181 | -6.187                                     | -6.193 | -6.198 | -6.204 | -6.209 | -6.214 | -6.219 | -6.224 | -6.228 | -6.232 | -250                       |  |
| -240  | -6.105 | -6.114                                     | -6.122 | -6.130 | -6.138 | -6.146 | -6.153 | -6.160 | -6.167 | -6.174 | -6.181 | -240                       |  |
| -230  | -6.007 | -6.018                                     | -6.028 | -6.039 | -6.049 | -6.059 | -6.068 | -6.078 | -6.087 | -6.096 | -6.105 | -230                       |  |
| -220  | -5.889 | -5.901                                     | -5.914 | -5.926 | -5.938 | -5.950 | -5.962 | -5.973 | -5.985 | -5.996 | -6.007 | -220                       |  |
| -210  | -5.753 | -5.767                                     | -5.782 | -5.795 | -5.809 | -5.823 | -5.836 | -5.850 | -5.863 | -5.876 | -5.889 | -210                       |  |
| -200  | -5.603 | -5.619                                     | -5.634 | -5.650 | -5.665 | -5.680 | -5.695 | -5.710 |        |        |        | -200                       |  |
| -190  | -5.439 | -5.456                                     | -5.473 | -5.489 | -5.506 | -5.522 | -5.539 | -5.555 | -5.571 | -5.587 | -5.603 | -190                       |  |
| -180  | -5.261 | -5.279                                     | -5.297 | -5.315 | -5.333 | -5.351 | -5.369 | -5.387 | -5.404 | -5.421 | -5.439 | -180                       |  |
| -170  | -5.069 | -5.089                                     | -5.109 | -5.128 | -5.147 | -5.167 | -5.186 | -5.205 | -5.223 | -5.242 | -5.261 | -170                       |  |
| -160  | -4.865 | -4.886                                     | -4.907 | -4.928 | -4.948 | -4.969 | -4.989 | -5.010 | -5.030 | -5.050 | -5.069 | -160                       |  |
| -150  | -4.648 | -4.670                                     | -4.693 | -4.715 | -4.737 | -4.758 | -4.780 | -4.801 | -4.823 | -4.844 | -4.865 | -150                       |  |
| -140  | -4.419 | -4.442                                     | -4.466 | -4.489 | -4.512 | -4.535 | -4.558 | -4.581 | -4.603 | -4.626 | -4.648 | -140                       |  |
| -130  | -4.177 | -4.202                                     | -4.226 | -4.251 | -4.275 | -4.299 | -4.323 | -4.347 | -4.371 | -4.395 | -4.419 | -130                       |  |
| -120  | -3.923 | -3.949                                     | -3.974 | -4.000 | -4.026 | -4.051 | -4.077 | -4.102 | -4.127 | -4.152 | -4.177 | -120                       |  |
| -110  | -3.656 | -3.684                                     | -3.711 | -3.737 | -3.764 | -3.791 | -3.818 | -3.844 | -3.870 | -3.897 | -3.923 | -110                       |  |
| -100  | -3.378 | -3.407                                     | -3.435 | -3.463 | -3.491 | -3.519 | -3.547 | -3.574 | -3.602 | -3.629 | -3.656 | -100                       |  |
| -90   | -3.089 | -3.118                                     | -3.147 | -3.177 | -3.206 | -3.235 | -3.264 | -3.293 | -3.321 | -3.350 | -3.378 | -90                        |  |
| -80   | -2.788 | -2.818                                     | -2.849 | -2.879 | -2.909 | -2.939 | -2.970 | -2.999 | -3.029 | -3.059 | -3.089 | -80                        |  |
| -70   | -2.475 | -2.507                                     | -2.539 | -2.570 | -2.602 | -2.633 | -2.664 | -2.695 | -2.726 | -2.757 | -2.788 | -70                        |  |
| -60   | -2.152 | -2.185                                     | -2.218 | -2.250 | -2.283 | -2.315 | -2.348 | -2.380 | -2.412 | -2.444 | -2.475 | -60                        |  |
| -50   | -1.819 | -1.853                                     | -1.886 | -1.920 | -1.953 | -1.987 | -2.020 | -2.053 | -2.087 | -2.120 | -2.152 | -50                        |  |
| -40   | -1.475 | -1.510                                     | -1.544 | -1.579 | -1.614 | -1.648 | -1.682 | -1.717 | -1.751 | -1.785 | -1.819 | -40                        |  |
| -30   | -1.121 | -1.157                                     | -1.192 | -1.228 | -1.263 | -1.299 | -1.334 | -1.370 | -1.405 | -1.440 | -1.475 | -30                        |  |
| -20   | -0.757 | -0.794                                     | -0.830 | -0.867 | -0.903 | -0.940 | -0.976 | -1.013 | -1.049 | -1.085 | -1.121 | -20                        |  |
| -10   | -0.383 | -0.421                                     | -0.458 | -0.496 | -0.534 | -0.571 | -0.608 | -0.646 | -0.683 | -0.720 | -0.757 | -10                        |  |
| 0   | 0.000  | -0.039                                     | -0.077 | -0.116 | -0.154 | -0.193 | -0.231 | -0.269 | -0.307 | -0.345 | -0.383 | 0                          |  |
| 0   | 0.000  | 0.039                                      | 0.078  | 0.117  | 0.156  | 0.195  | 0.234  | 0.273  | 0.312  | 0.351  | 0.391  | 0                          |  |
| 10  | 0.391  | 0.430                                      | 0.470  | 0.510  | 0.549  | 0.589  | 0.629  | 0.669  | 0.709  | 0.749  | 0.789  | 10                         |  |
| 20  | 0.789  | 0.830                                      | 0.870  | 0.911  | 0.951  | 0.992  | 1.032  | 1.073  | 1.114  | 1.155  | 1.196  | 20                         |  |
| 30  | 1.196  | 1.237                                      | 1.279  | 1.320  | 1.361  | 1.403  | 1.444  | 1.486  | 1.528  | 1.569  | 1.611  | 30                         |  |
| 40  | 1.611  | 1.653                                      | 1.695  | 1.738  | 1.780  | 1.822  | 1.865  | 1.907  | 1.950  | 1.992  | 2.035  | 40                         |  |
| 50  | 2.035  | 2.078                                      | 2.121  | 2.164  | 2.207  | 2.250  | 2.294  | 2.337  | 2.380  | 2.424  | 2.467  | 50                         |  |
| 60  | 2.467  | 2.511                                      | 2.555  | 2.599  | 2.643  | 2.687  | 2.731  | 2.775  | 2.819  | 2.864  | 2.908  | 60                         |  |
| 70  | 2.908  | 2.953                                      | 2.997  | 3.042  | 3.087  | 3.131  | 3.176  | 3.221  | 3.266  | 3.312  | 3.357  | 70                         |  |
| 80  | 3.357  | 3.402                                      | 3.447  | 3.493  | 3.538  | 3.584  | 3.630  | 3.676  | 3.721  | 3.767  | 3.813  | 80                         |  |
| 90  | 3.813  | 3.859                                      | 3.906  | 3.952  | 3.998  | 4.044  | 4.091  | 4.137  | 4.184  | 4.231  | 4.277  | 90                         |  |
| 100   | 4.277  | 4.324                                      | 4.371  | 4.418  | 4.465  | 4.512  | 4.559  | 4.607  | 4.654  | 4.701  | 4.749  | 100                        |  |
| 110   | 4.749  | 4.796                                      | 4.844  | 4.891  | 4.939  | 4.987  | 5.035  | 5.083  | 5.131  | 5.179  | 5.227  | 110                        |  |
| 120   | 5.227  | 5.275                                      | 5.324  | 5.372  | 5.420  | 5.469  | 5.517  | 5.566  | 5.615  | 5.663  | 5.712  | 120                        |  |
| 130   | 5.712  | 5.761                                      | 5.810  | 5.859  | 5.908  | 5.957  | 6.007  | 6.056  | 6.105  | 6.155  | 6.204  | 130                        |  |
| 140   | 6.204  | 6.254                                      | 6.303  | 6.353  | 6.403  | 6.452  | 6.502  | 6.552  | 6.602  | 6.652  | 6.702  | 140                        |  |
| 150   | 6.702  | 6.753                                      | 6.803  | 6.853  | 6.903  | 6.954  | 7.004  | 7.055  | 7.106  | 7.156  | 7.207  | 150                        |  |
| 160   | 7.207  | 7.258                                      | 7.309  | 7.360  | 7.411  | 7.462  | 7.513  | 7.564  | 7.615  | 7.666  | 7.718  | 160                        |  |
| 170   | 7.718  | 7.769                                      | 7.821  | 7.872  | 7.924  | 7.975  | 8.027  | 8.079  | 8.131  | 8.183  | 8.235  | 170                        |  |
| 180   | 8.235  | 8.287                                      | 8.339  | 8.391  | 8.443  | 8.495  | 8.548  | 8.600  | 8.652  | 8.705  | 8.757  | 180                        |  |
| 190   | 8.757  | 8.810                                      | 8.863  | 8.915  | 8.968  | 9.021  | 9.074  | 9.127  | 9.180  | 9.233  | 9.286  | 190                        |  |
| 200   | 9.286  | 9.339                                      | 9.392  | 9.446  | 9.499  | 9.553  | 9.606  | 9.659  | 9.713  | 9.767  | 9.820  | 200                        |  |
| 210   | 9.820  | 9.874                                      | 9.928  | 9.982  | 10.036 | 10.090 | 10.144 | 10.198 | 10.252 | 10.306 | 10.360 | 210                        |  |
| 220   | 10.360 | 10.414                                     | 10.469 | 10.523 | 10.578 | 10.632 | 10.687 | 10.741 | 10.796 | 10.851 | 10.905 | 220                        |  |
| 230   | 10.905 | 10.960                                     | 11.015 | 11.070 | 11.125 | 11.180 | 11.235 | 11.290 | 11.345 | 11.401 | 11.456 | 230                        |  |
| 240   | 11.456 | 11.511                                     | 11.566 | 11.622 | 11.677 | 11.733 | 11.788 | 11.844 | 11.900 | 11.956 | 12.011 | 240                        |  |
| 250   | 12.011 | 12.067                                     | 12.123 | 12.179 | 12.235 | 12.291 | 12.347 | 12.403 | 12.459 | 12.515 | 12.572 | 250                        |  |
| 260   | 12.572 | 12.628                                     | 12.684 | 12.741 | 12.797 | 12.854 | 12.910 | 12.967 | 13.024 | 13.080 | 13.137 | 260                        |  |
| 270   | 13.137 | 13.194                                     | 13.251 | 13.307 | 13.364 | 13.421 | 13.478 | 13.535 | 13.592 | 13.650 | 13.707 | 270                        |  |
| 280   | 13.707 | 13.764                                     | 13.821 | 13.879 | 13.936 | 13.993 | 14.051 | 14.108 | 14.166 | 14.223 | 14.281 | 280                        |  |
| 290   | 14.281 | 14.339                                     | 14.396 | 14.454 | 14.512 | 14.570 | 14.628 | 14.686 | 14.744 | 14.802 | 14.860 | 290                        |  |
| 300   | 14.860 | 14.918                                     | 14.976 | 15.034 | 15.092 | 15.151 | 15.209 | 15.267 | 15.326 | 15.384 | 15.443 | 300                        |  |
| 310   | 15.443 | 15.501                                     | 15.560 | 15.619 | 15.677 | 15.736 | 15.795 | 15.853 | 15.912 | 15.971 | 16.030 | 310                        |  |
| 320   | 16.030 | 16.089                                     | 16.148 | 16.207 | 16.266 | 16.325 | 16.384 | 16.444 | 16.503 | 16.562 | 16.621 | 320                        |  |
| 330   | 16.621 | 16.681                                     | 16.740 | 16.800 | 16.859 | 16.919 | 16.978 | 17.038 | 17.097 | 17.157 | 17.217 | 330                        |  |
| 340   | 17.217 | 17.277                                     | 17.336 | 17.396 | 17.456 | 17.516 | 17.576 | 17.636 | 17.696 | 17.756 | 17.816 | 340                        |  |

TABLE 10.15—Type T thermocouples (continued).

| EMF in Absolute Millivolts                    |        | Temperature in Degrees Celsius (IPTS 1968) |        |        |        |        |        |        |        |        |        | Reference Junctions at 0 C |  |
|---|--------|--|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------------------------|--|
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |
| THERMOELECTRIC VOLTAGE IN ABSOLUTE MILLIVOLTS |        |  |        |        |        |        |        |        |        |        |        |                            |  |
| 350   | 17.816 | 17.877                                     | 17.937 | 17.997 | 18.057 | 18.118 | 18.178 | 18.238 | 18.299 | 18.359 | 18.420 | 350                        |  |
| 360   | 18.420 | 18.480                                     | 18.541 | 18.602 | 18.662 | 18.723 | 18.784 | 18.845 | 18.905 | 18.966 | 19.027 | 360                        |  |
| 370   | 19.027 | 19.088                                     | 19.149 | 19.210 | 19.271 | 19.332 | 19.393 | 19.455 | 19.516 | 19.577 | 19.638 | 370                        |  |
| 380   | 19.638 | 19.699                                     | 19.761 | 19.822 | 19.883 | 19.945 | 20.006 | 20.068 | 20.129 | 20.191 | 20.252 | 380                        |  |
| 390   | 20.252 | 20.314                                     | 20.376 | 20.437 | 20.499 | 20.560 | 20.622 | 20.684 | 20.746 | 20.807 | 20.869 | 390                        |  |
| 400   | 20.869 |  |        |        |        |        |        |        |        |        |        | 400                        |  |
| DEG C   | 0      | 1  | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     | DEG C                      |  |

TABLE 10.16—Power series coefficients for Type T thermocouples.

| Temperature Range | Degree | Coefficients  |        | Power of T Term |
|-------------------|--------|---------------|--------|-----------------|
| -270 to 0°C       | 14     | 3.8740773840  | E + 1  | 1               |
|                   |        | 4.4123932482  | E - 2  | 2               |
|                   |        | 1.1405238498  | E - 4  | 3               |
|                   |        | 1.9974406568  | E - 5  | 4               |
|                   |        | 9.0445401187  | E - 7  | 5               |
|                   |        | 2.2766018504  | E - 8  | 6               |
|                   |        | 3.6247409380  | E - 10 | 7               |
|                   |        | 3.8648924201  | E - 12 | 8               |
|                   |        | 2.8298678519  | E - 14 | 9               |
|                   |        | 1.4281383349  | E - 16 | 10              |
|                   |        | 4.8833254364  | E - 19 | 11              |
|                   |        | 1.0803474683  | E - 21 | 12              |
|                   |        | 1.3949291026  | E - 24 | 13              |
|                   |        | 7.9795893156  | E - 28 | 14              |
| 0 to 400°C        | 8      | 3.8740773840  | E + 1  | 1               |
|                   |        | 3.3190198092  | E - 2  | 2               |
|                   |        | 2.0714183645  | E - 4  | 3               |
|                   |        | -2.1945834823 | E - 6  | 4               |
|                   |        | 1.1031900550  | E - 8  | 5               |
|                   |        | -3.0927581898 | E - 11 | 6               |
|                   |        | 4.5653337165  | E - 14 | 7               |
|                   |        | -2.7616878040 | E - 17 | 8               |

TABLE 10.17—Power series coefficients for Type J thermocouples.

| Temperature Range | Degree | Coefficients  |        | Power of T Term |
|-------------------|--------|---------------|--------|-----------------|
| -210 to 760°C     | 7      | 5.0372753027  | E + 1  | 1               |
|                   |        | 3.0425491284  | E - 2  | 2               |
|                   |        | -8.5669750464 | E - 5  | 3               |
|                   |        | 1.3348825735  | E - 7  | 4               |
|                   |        | -1.7022405966 | E - 10 | 5               |
|                   |        | 1.9416091001  | E - 13 | 6               |
|                   |        | -9.6391844859 | E - 17 | 7               |

TABLE 10.18—Power series coefficients for Type E thermocouples.

| Temperature Range | Degree | Coefficients  |        | Power of T Term |
|-------------------|--------|---------------|--------|-----------------|
| -270 to 0°C       | 13     | 5.8695857799  | E + 1  | 1               |
|                   |        | 5.1667517705  | E - 2  | 2               |
|                   |        | -4.4652683347 | E - 4  | 3               |
|                   |        | -1.7346270905 | E - 5  | 4               |
|                   |        | -4.8719368427 | E - 7  | 5               |
|                   |        | -8.8896550447 | E - 9  | 6               |
|                   |        | -1.0930767375 | E - 10 | 7               |
|                   |        | -9.1784535039 | E - 13 | 8               |
|                   |        | -5.2575158521 | E - 15 | 9               |
|                   |        | -2.0169601996 | E - 17 | 10              |
|                   |        | -4.9502138782 | E - 20 | 11              |
|                   |        | -7.0177980633 | E - 23 | 12              |
|                   |        | -4.3671808488 | E - 26 | 13              |
| 0 to 1000°C       | 9      | 5.8695857799  | E + 1  | 1               |
|                   |        | 4.3110945462  | E - 2  | 2               |
|                   |        | 5.7220358202  | E - 5  | 3               |
|                   |        | -5.4020668085 | E - 7  | 4               |
|                   |        | 1.5425922111  | E - 9  | 5               |
|                   |        | -2.4850089136 | E - 12 | 6               |
|                   |        | 2.3389721459  | E - 15 | 7               |
|                   |        | -1.1946296815 | E - 18 | 8               |
|                   |        | 2.5561127497  | E - 22 | 9               |

TABLE 10.19—Power series coefficients for Type K thermocouples.

| Temperature Range | Degree  | Coefficients  |        | Power of T Term   |
|-------------------|---------|---------------|--------|---|
| -270 to 0°C       | 10      | 3.9475433139  | E + 1  | 1   |
|                   |         | 2.7465251138  | E - 2  | 2   |
|                   |         | -1.6565406716 | E - 4  | 3   |
|                   |         | -1.5190912392 | E - 6  | 4   |
|                   |         | -2.4581670924 | E - 8  | 5   |
|                   |         | -2.4757917816 | E - 10 | 6   |
|                   |         | -1.5585276173 | E - 12 | 7   |
|                   |         | -5.9729921255 | E - 15 | 8   |
|                   |         | -1.2688801216 | E - 17 | 9   |
|                   |         | -1.1382797374 | E - 20 | 10  |
| 0 to 1372°C       | 8 + exp | -1.8533063273 | E + 1  | 0   |
|                   |         | 3.8918344612  | E + 1  | 1   |
|                   |         | 1.6645154356  | E - 2  | 2   |
|                   |         | -7.8702374448 | E - 5  | 3   |
|                   |         | 2.2835785557  | E - 7  | 4   |
|                   |         | -3.5700231258 | E - 10 | 5   |
|                   |         | 2.9932909136  | E - 13 | 6   |
|                   |         | -1.2849848798 | E - 16 | 7   |
|                   |         | 2.2239974336  | E - 20 | 8   |
|                   |         |               |        | $+ 125 \exp \left[ - \frac{1}{2} \left( \frac{T - 127}{65} \right)^2 \right]$ |

TABLE 10.20—Power series coefficients for Type R thermocouples.

| Temperature Range | Degree | Coefficients  |        | Power of T Term |
|-------------------|--------|---------------|--------|-----------------|
| -50 to 631°C      | 7      | 5.2891395059  | E 0    | 1               |
|                   |        | 1.3911109947  | E - 2  | 2               |
|                   |        | -2.4005238430 | E - 5  | 3               |
|                   |        | 3.6201410595  | E - 8  | 4               |
|                   |        | -4.4645019036 | E - 11 | 5               |
|                   |        | 3.8497691865  | E - 14 | 6               |
|                   |        | -1.5372641559 | E - 17 | 7               |
| 631 to 1065°C     | 3      | -2.6418007025 | E ± 2  | 0               |
|                   |        | 8.0468680747  | E 0    | 1               |
|                   |        | 2.9892293723  | E - 3  | 2               |
|                   |        | -2.6876058617 | E - 7  | 3               |
| 1065 to 1665°C    | 3      | 1.4901702702  | E + 3  | 0               |
|                   |        | 2.8639867552  | E 0    | 1               |
|                   |        | 8.0823631189  | E - 3  | 2               |
|                   |        | -1.9338477638 | E - 6  | 3               |

TABLE 10.21—*Power series coefficients for Type S thermocouples.*

| Temperature Range | Degree | Coefficients  |        | Power of T Term |
|-------------------|--------|---------------|--------|-----------------|
| -50 to 631°C      | 6      | 5.3995782346  | E 0    | 1               |
|                   |        | 1.2519770000  | E - 2  | 2               |
|                   |        | -2.2448217997 | E - 5  | 3               |
|                   |        | 2.8452164949  | E - 8  | 4               |
|                   |        | -2.2440584544 | E - 11 | 5               |
|                   |        | 8.5054166936  | E - 15 | 6               |
| 631 to 1064°C     | 2      | -2.9824481615 | E + 2  | 0               |
|                   |        | 8.2375528221  | E 0    | 1               |
|                   |        | 1.6453909942  | E - 3  | 2               |
| 1064 to 1665°C    | 3      | 1.2766292175  | E + 3  | 0               |
|                   |        | 3.4970908041  | E 0    | 1               |
|                   |        | 6.3824648666  | E - 3  | 2               |
|                   |        | -1.5722424599 | E - 6  | 3               |

TABLE 10.22—*Power series coefficients for Type B thermocouples.*

| Temperature Range | Degree | Coefficients  |        | Power of T Term |
|-------------------|--------|---------------|--------|-----------------|
| 0 to 1820°C       | 8      | -2.4674601620 | E - 1  | 1               |
|                   |        | 5.9102111169  | E - 3  | 2               |
|                   |        | -1.4307123430 | E - 6  | 3               |
|                   |        | 2.1509149750  | E - 9  | 4               |
|                   |        | -3.1757800720 | E - 12 | 5               |
|                   |        | 2.4010367459  | E - 15 | 6               |
|                   |        | -9.0928148159 | E - 19 | 7               |
|                   |        | 1.3299505137  | E - 22 | 8               |

perature-emf relationships, to as many decimal places as have any useful significance, for the thermocouple types included in this standard. These data will be useful in all applications where discontinuities in the established reference values are objectionable, or where storage of complete tables is impractical.

### 10.3.2 Methods of Generation

The values of each of the seven thermocouple types given in Tables 10.2 to 10.15 are generated by power series equations according to Ref 1. The coefficients of these equations for the appropriate ranges are given in Tables 10.16 to 10.22. Note that these coefficients yield values of emf in microvolts. This method permits easy generation of the temperature-emf values by a digital

computer. It provides a smooth, continuous relationship, and the values will round off to the established temperature-emf values given in Tables 10.2 to 10.15 [2].<sup>2</sup>

Alternative generation schemes for temperature-emf relationships are described in Refs 3 and 4.

#### 10.4 References

- [1] Powell, R. L., Hall, W. J., Hyink, C. H., Sparks, L. L., Burns, G. W., Scroger, M. G., and Plumb, H. H., "Thermocouple Reference Tables Based on the IPTS-68," NBS Monograph 125, National Bureau of Standards, 1973.
- [2] ASTM Standard E 230 "Temperature-Electromotive Force (EMF) Tables for Thermocouples," *1980 Annual Book of ASTM Standards*, Part 44.
- [3] British Standard, BS 4937, 1973, is in substantial agreement with Ref 1.
- [4] Alternative generation schemes in use prior to 1973 are described in the following references:
  - (a) Benedict, R. P. and Ashby, H. F., "Improved Reference Tables for Thermocouples," *Temperature. Its Measurement and Control in Science and Industry*, Part 2, Vol. 3, 1962, p. 51.
  - (b) Benedict, R. P., "The Generation of Thermocouple Reference Tables," *Electrotechnology*, Nov. 1963, p. 80.
  - (c) Adams, R. K. and Simpson, R. L., "Review of Techniques for Determining Thermocouple EMF—Temperature Characteristics," *Temperature. Its Measurement and Control in Science and Industry*, Part 3, Vol. 4, 1972, p. 1603.
  - (d) Bedford, R. E. et al., "New Reference Tables for Platinum 10% Rhodium/Platinum and Platinum 13% Rhodium/Platinum Thermocouples," *Temperature. Its Measurement and Control in Science and Industry*, Part 3, Vol. 4, 1972, p. 1585.

<sup>2</sup>The italic numbers in brackets refer to the list of references appended to this chapter.



# Chapter 11—Cryogenics

---

## 11.1 General Remarks

Although there is some variation in the defined temperature range involved, cryogenics usually indicates concern with temperatures in the liquid oxygen range (about 90 K or  $-183^{\circ}\text{C}$ ) or lower. This temperature range will be discussed primarily in this chapter. Since a triple point (of water) or ice bath reference junction often is used, additional comments and values will be given for the entire subzero ( $0^{\circ}\text{C}$ ) range.

Most aspects of cryogenic thermometry are similar to those applicable at room or high temperatures. In particular, the measurement systems and thermoelectric theory are nearly identical. However, there are significant differences with respect to some materials, techniques or assembly, and fabrication, calibration schemes, and methods of practical usage. Fortunately the added difficulties with some details are offset by the removal of a few problems peculiar to high-temperature thermometry: chemical transformations are insignificant; oxidation, reduction, and impurity migration do not occur because of the low temperatures. Annealing of physical imperfections is also absent for the same reasons. Maintenance of fixed points and techniques of calibration are usually considerably easier and sometimes much more accurate. Thermal radiation is usually not important, at least if simple precautions are taken to account for it.

Several books have been written on thermometry and on the experimental techniques necessary for cryogenic research by Scott [1]<sup>1</sup> and by Hust et al [2] on cryogenic engineering, and by White [3] and by Rose-Innes [4] on smaller, scientific systems.

## 11.2 Materials

Many thermocouple materials developed for high-temperature usage have too low a sensitivity at low temperatures to be practical; others have a reasonable sensitivity, but are very erratic with large inhomogeneities and lot-to-lot variations. Only three of the letter-designated type thermocouples have proven themselves for cryogenic use: Types E, T, and K. Type E is definitely recommended as the most valuable for general low-temperature use. It is better because of its higher sensitivity (coupled with only average

<sup>1</sup> The italic numbers in brackets refer to the list of references appended to this chapter.

inhomogeneity voltages) and lower thermal conductivity of both thermocouple materials. The latter property is particularly important for obtaining good thermal tempering of measuring junctions. Tables for the total voltage and Seebeck coefficient are given in Section 11.3 for each of the thermocouples just mentioned. These tables were taken from Ref 5.

There are other, but uncommon, materials that have a higher sensitivity at very low temperatures, below 50 K: gold-cobalt and gold-iron. Both are negative thermoelectric materials and should be matched with KP or EP, "normal" silver, or less preferably, TP, to obtain a thermocouple pair. The older material, gold-cobalt (2.1 atomic percent cobalt) has been found to have significant instabilities caused by room-temperature annealing of the metastable solution of cobalt in gold. Because of those problems gold-cobalt should not be used any more in the future. The alloy gold-0.07 atomic percent iron has replaced gold-cobalt: it does not have alloying instabilities, it is more homogeneous, and it has a larger Seebeck coefficient.

A table giving the total voltage and Seebeck coefficient of KP or EP versus gold-0.07 atomic percent iron is given also in Section 11.3. This table is taken from data published by the National Bureau of Standards [6]. Reference tables for several other material combinations that are used as thermocouples in the cryogenic range are also given in this reference.

Figure 11.1 compares the Seebeck coefficients of various thermocouples used in the cryogenic range. The Seebeck coefficient of Type K is not shown, but it would be slightly above that of Type T.

### 11.3 Reference Tables (for use in the cryogenic range)

TABLE 11.1—Type E-thermoelectric voltage,  $E(T)$ , Seebeck coefficient,  $S(T)$ , and derivative of the Seebeck coefficient,  $dS/dT$  [5].

| $T, K$ | $E, \mu V$ | $S, \mu V/K$ | $dS/dT,$<br>$nV/K^2$ | $T, K$ | $E, \mu V$ | $S, \mu V/K$ | $dS/dT,$<br>$nV/K^2$ |
|--------|------------|--------------|----------------------|--------|------------|--------------|----------------------|
| 0      | 0.00       | -0.203       | 604.4                | 45     | 413.20     | 17.149       | 318.9                |
| 1      | 0.09       | 0.384        | 571.8                | 46     | 430.51     | 17.467       | 316.3                |
| 2      | 0.76       | 0.941        | 543.0                | 47     | 448.14     | 17.782       | 313.6                |
| 3      | 1.97       | 1.472        | 517.7                | 48     | 466.07     | 18.094       | 311.0                |
| 4      | 3.69       | 1.978        | 495.6                | 49     | 484.32     | 18.404       | 308.3                |
| 5      | 5.92       | 2.464        | 476.2                | 50     | 502.88     | 18.711       | 305.6                |
| 6      | 8.61       | 2.931        | 459.4                | 51     | 521.74     | 19.015       | 303.0                |
| 7      | 11.77      | 3.383        | 444.7                | 52     | 540.91     | 19.317       | 300.3                |
| 8      | 15.38      | 3.821        | 432.1                | 53     | 560.38     | 19.616       | 297.7                |
| 9      | 19.41      | 4.248        | 421.1                | 54     | 580.14     | 19.912       | 295.1                |
| 10     | 23.87      | 4.664        | 411.7                | 55     | 600.20     | 20.206       | 292.5                |
| 11     | 28.74      | 5.072        | 403.6                | 56     | 620.55     | 20.497       | 289.9                |
| 12     | 34.01      | 5.472        | 396.7                | 57     | 641.19     | 20.786       | 287.4                |
| 13     | 39.68      | 5.865        | 390.8                | 58     | 662.12     | 21.072       | 284.9                |
| 14     | 45.74      | 6.254        | 385.8                | 59     | 683.33     | 21.355       | 282.5                |

TABLE 11.1—(Continued).

| $T, K$ | $E, \mu V$ | $S, \mu V/K$ | $dS/dT,$<br>$nV/K^2$ | $T, K$ | $E, \mu V$ | $S, \mu V/K$ | $dS/dT,$<br>$nV/K^2$ |
|--------|------------|--------------|----------------------|--------|------------|--------------|----------------------|
| 15     | 52.18      | 6.637        | 381.5                | 60     | 704.83     | 21.637       | 280.0                |
| 16     | 59.01      | 7.017        | 377.8                | 61     | 726.61     | 21.915       | 277.7                |
| 17     | 66.22      | 7.393        | 374.6                | 62     | 748.66     | 22.192       | 275.4                |
| 18     | 73.80      | 7.766        | 371.9                | 63     | 770.99     | 22.466       | 273.1                |
| 19     | 81.75      | 8.137        | 369.5                | 64     | 793.59     | 22.738       | 270.9                |
| 20     | 90.07      | 8.505        | 367.4                | 65     | 816.47     | 23.008       | 268.8                |
| 21     | 98.76      | 8.872        | 365.6                | 66     | 839.61     | 23.276       | 266.7                |
| 22     | 107.81     | 9.237        | 363.9                | 67     | 863.02     | 23.541       | 264.6                |
| 23     | 117.23     | 9.600        | 362.3                | 68     | 886.69     | 23.805       | 262.6                |
| 24     | 127.01     | 9.961        | 360.8                | 69     | 910.63     | 24.067       | 260.7                |
| 25     | 137.15     | 10.321       | 359.3                | 70     | 934.82     | 24.326       | 258.8                |
| 26     | 147.65     | 10.680       | 357.9                | 71     | 959.28     | 24.584       | 256.9                |
| 27     | 158.51     | 11.037       | 356.4                | 72     | 983.99     | 24.840       | 255.1                |
| 28     | 169.73     | 11.393       | 354.9                | 73     | 1008.96    | 25.094       | 253.4                |
| 29     | 181.30     | 11.747       | 353.4                | 74     | 1034.18    | 25.347       | 251.7                |
| 30     | 193.22     | 12.099       | 351.8                | 75     | 1059.65    | 25.598       | 250.0                |
| 31     | 205.50     | 12.450       | 350.1                | 76     | 1085.37    | 25.847       | 248.4                |
| 32     | 218.12     | 12.800       | 348.4                | 77     | 1111.35    | 26.095       | 246.9                |
| 33     | 231.09     | 13.147       | 346.5                | 78     | 1137.56    | 26.341       | 245.4                |
| 34     | 244.41     | 13.493       | 344.6                | 79     | 1164.03    | 26.585       | 243.9                |
| 35     | 258.08     | 13.836       | 342.7                | 80     | 1190.73    | 26.829       | 242.4                |
| 36     | 272.09     | 14.178       | 340.6                | 81     | 1217.68    | 27.070       | 241.0                |
| 37     | 286.43     | 14.517       | 338.4                | 82     | 1244.87    | 27.311       | 239.7                |
| 38     | 301.12     | 14.855       | 336.2                | 83     | 1272.30    | 27.550       | 238.3                |
| 39     | 316.14     | 15.190       | 333.9                | 84     | 1299.97    | 27.787       | 237.0                |
| 40     | 331.50     | 15.523       | 331.5                | 85     | 1327.88    | 28.024       | 235.7                |
| 41     | 347.19     | 15.853       | 329.1                | 86     | 1356.02    | 28.259       | 234.5                |
| 42     | 363.20     | 16.181       | 326.6                | 87     | 1384.40    | 28.493       | 233.2                |
| 43     | 379.55     | 16.506       | 324.1                | 88     | 1413.01    | 28.725       | 232.0                |
| 44     | 396.21     | 16.829       | 321.5                | 89     | 1441.85    | 28.957       | 230.9                |
| 90     | 1470.92    | 29.187       | 229.7                | 135    | 3001.29    | 38.512       | 187.3                |
| 91     | 1500.22    | 29.416       | 228.6                | 136    | 3039.89    | 38.699       | 186.6                |
| 92     | 1529.75    | 29.644       | 227.4                | 137    | 3078.69    | 38.885       | 185.9                |
| 93     | 1559.51    | 29.871       | 226.3                | 138    | 3117.66    | 39.070       | 185.1                |
| 94     | 1589.49    | 30.097       | 225.2                | 139    | 3156.83    | 39.255       | 184.4                |
| 95     | 1619.70    | 30.321       | 224.1                | 140    | 3196.17    | 39.439       | 183.7                |
| 96     | 1650.13    | 30.545       | 223.1                | 141    | 3235.70    | 39.623       | 183.0                |
| 97     | 1680.79    | 30.768       | 222.0                | 142    | 3275.42    | 39.805       | 182.3                |
| 98     | 1711.67    | 30.989       | 221.0                | 143    | 3315.31    | 39.987       | 181.6                |
| 99     | 1742.77    | 31.210       | 219.9                | 144    | 3355.39    | 40.169       | 180.9                |
| 100    | 1774.09    | 31.429       | 218.9                | 145    | 3395.65    | 40.349       | 180.3                |
| 101    | 1805.63    | 31.647       | 217.9                | 146    | 3436.09    | 40.529       | 179.6                |
| 102    | 1837.38    | 31.865       | 216.9                | 147    | 3476.71    | 40.708       | 179.0                |
| 103    | 1869.36    | 32.081       | 215.9                | 148    | 3517.51    | 40.887       | 178.3                |
| 104    | 1901.54    | 32.297       | 214.9                | 149    | 3558.48    | 41.065       | 177.7                |
| 105    | 1933.95    | 32.511       | 213.9                | 150    | 3599.64    | 41.242       | 177.0                |
| 106    | 1966.57    | 32.724       | 212.9                | 151    | 3640.97    | 41.419       | 176.4                |
| 107    | 1999.40    | 32.937       | 211.9                | 152    | 3682.47    | 41.595       | 175.8                |

TABLE 11.1—(Continued).

| $T, K$ | $E, \mu V$ | $S, \mu V/K$ | $dS/dT,$<br>$nV/K^2$ | $T, K$ | $E, \mu V$ | $S, \mu V/K$ | $dS/dT,$<br>$nV/K^2$ |
|--------|------------|--------------|----------------------|--------|------------|--------------|----------------------|
| 108    | 2032.44    | 33.148       | 210.9                | 153    | 3724.16    | 41.771       | 175.2                |
| 109    | 2065.69    | 33.359       | 310.0                | 154    | 3766.02    | 41.946       | 174.6                |
| 110    | 2099.16    | 33.568       | 209.0                | 155    | 3808.05    | 42.120       | 173.9                |
| 111    | 2132.83    | 33.777       | 208.1                | 156    | 3850.26    | 42.293       | 173.3                |
| 112    | 2166.71    | 33.984       | 207.1                | 157    | 3892.64    | 42.466       | 172.7                |
| 113    | 2200.80    | 34.191       | 206.2                | 158    | 3935.19    | 42.639       | 172.1                |
| 114    | 2235.09    | 34.397       | 205.2                | 159    | 3977.91    | 42.811       | 171.5                |
| 115    | 2269.59    | 34.601       | 204.3                | 160    | 4020.81    | 42.982       | 170.9                |
| 116    | 2304.29    | 34.805       | 203.4                | 161    | 4063.88    | 42.153       | 170.3                |
| 117    | 2339.20    | 35.008       | 202.4                | 162    | 4107.11    | 43.323       | 169.7                |
| 118    | 2374.31    | 35.210       | 201.5                | 163    | 4150.52    | 43.492       | 169.1                |
| 119    | 2409.62    | 35.411       | 200.6                | 164    | 4194.10    | 43.661       | 168.5                |
| 120    | 2445.13    | 35.611       | 199.7                | 165    | 4237.84    | 43.829       | 167.9                |
| 121    | 2480.84    | 35.811       | 198.8                | 166    | 4281.76    | 43.997       | 167.3                |
| 122    | 2516.75    | 36.009       | 198.0                | 167    | 4325.84    | 44.164       | 166.7                |
| 123    | 2552.86    | 36.207       | 197.1                | 168    | 4370.08    | 44.330       | 166.1                |
| 124    | 2589.17    | 36.403       | 196.2                | 169    | 4414.50    | 44.496       | 165.5                |
| 125    | 2625.67    | 36.599       | 195.4                | 170    | 4459.07    | 44.661       | 164.9                |
| 126    | 2662.36    | 36.794       | 194.5                | 171    | 4503.82    | 44.826       | 164.3                |
| 127    | 2699.25    | 36.988       | 193.7                | 172    | 4548.73    | 44.990       | 163.7                |
| 128    | 2736.34    | 37.181       | 192.9                | 173    | 4593.80    | 45.153       | 163.1                |
| 129    | 2773.62    | 37.374       | 192.0                | 174    | 4639.03    | 45.316       | 162.5                |
| 130    | 2811.09    | 37.565       | 191.2                | 175    | 4684.43    | 45.478       | 161.8                |
| 131    | 2848.75    | 32.756       | 190.4                | 176    | 4729.99    | 45.640       | 161.2                |
| 132    | 2886.60    | 32.946       | 189.6                | 177    | 4775.71    | 45.800       | 160.6                |
| 133    | 2924.64    | 38.136       | 188.9                | 178    | 4821.59    | 45.961       | 160.0                |
| 134    | 2962.87    | 38.324       | 188.1                | 179    | 4867.63    | 45.120       | 159.4                |
| 180    | 4913.83    | 46.279       | 158.7                | 230    | 7413.67    | 53.482       | 130.9                |
| 181    | 4960.19    | 46.438       | 158.1                | 231    | 7467.22    | 53.613       | 130.4                |
| 182    | 5006.70    | 46.596       | 157.5                | 232    | 7520.89    | 53.743       | 129.9                |
| 183    | 5053.38    | 46.753       | 156.9                | 233    | 7574.70    | 53.872       | 129.4                |
| 184    | 5100.21    | 46.909       | 156.2                | 234    | 7628.64    | 54.002       | 129.0                |
| 185    | 5147.20    | 47.065       | 155.6                | 235    | 7682.70    | 54.130       | 128.5                |
| 186    | 5194.34    | 47.221       | 155.0                | 236    | 7736.90    | 54.259       | 128.0                |
| 187    | 5241.64    | 47.375       | 154.4                | 237    | 7791.22    | 54.386       | 127.5                |
| 188    | 5289.09    | 47.529       | 153.7                | 238    | 7845.67    | 54.514       | 127.1                |
| 189    | 5336.70    | 47.683       | 153.1                | 239    | 7900.25    | 54.641       | 126.6                |
| 190    | 5384.46    | 47.835       | 152.5                | 240    | 7954.95    | 54.767       | 126.1                |
| 191    | 5432.37    | 47.988       | 151.9                | 241    | 8009.78    | 54.893       | 125.7                |
| 192    | 5480.43    | 48.139       | 151.2                | 242    | 8064.74    | 55.018       | 125.2                |
| 193    | 5528.65    | 48.290       | 150.6                | 243    | 8119.82    | 55.143       | 124.8                |
| 194    | 5577.01    | 48.440       | 150.0                | 244    | 8175.02    | 55.268       | 124.3                |
| 195    | 5625.53    | 48.590       | 149.4                | 245    | 8230.35    | 55.392       | 123.9                |
| 196    | 5674.19    | 48.739       | 148.8                | 246    | 8285.81    | 55.516       | 123.5                |
| 197    | 5723.00    | 48.888       | 148.2                | 247    | 8341.38    | 55.639       | 123.1                |
| 198    | 5771.97    | 49.036       | 147.6                | 248    | 8397.09    | 55.762       | 122.7                |
| 199    | 5821.08    | 49.183       | 147.0                | 249    | 8452.91    | 55.884       | 122.3                |

TABLE 11.1—(Continued).

| <i>T</i> , K | <i>E</i> , $\mu\text{V}$ | <i>S</i> , $\mu\text{V}/\text{K}$ | $dS/dT$ ,<br>$\text{nV}/\text{K}^2$ | <i>T</i> , K | <i>E</i> , $\mu\text{V}$ | <i>S</i> , $\mu\text{V}/\text{K}$ | $dS/dT$ ,<br>$\text{nV}/\text{K}^2$ |
|--------------|--------------------------|-----------------------------------|-------------------------------------|--------------|--------------------------|-----------------------------------|-------------------------------------|
| 200          | 5870.33                  | 49.330                            | 146.4                               | 250          | 8508.85                  | 56.006                            | 121.9                               |
| 201          | 5919.74                  | 49.476                            | 145.9                               | 251          | 8564.92                  | 56.128                            | 121.5                               |
| 202          | 5969.28                  | 49.622                            | 145.3                               | 252          | 8621.11                  | 56.250                            | 121.2                               |
| 203          | 6018.98                  | 49.767                            | 144.7                               | 253          | 8677.42                  | 56.371                            | 120.8                               |
| 204          | 6068.82                  | 49.911                            | 144.1                               | 254          | 8733.85                  | 56.491                            | 120.5                               |
| 205          | 6118.80                  | 50.055                            | 143.6                               | 255          | 8790.40                  | 56.611                            | 120.1                               |
| 206          | 6168.93                  | 50.198                            | 143.0                               | 256          | 8847.07                  | 56.731                            | 119.8                               |
| 207          | 6219.20                  | 50.341                            | 142.5                               | 257          | 8903.86                  | 56.851                            | 119.4                               |
| 208          | 6269.61                  | 50.483                            | 141.9                               | 258          | 8960.78                  | 56.970                            | 119.1                               |
| 209          | 6320.16                  | 50.625                            | 141.4                               | 259          | 9017.81                  | 57.089                            | 118.7                               |
| 210          | 6370.86                  | 50.766                            | 140.9                               | 260          | 9074.95                  | 57.208                            | 118.3                               |
| 211          | 6421.69                  | 50.907                            | 140.3                               | 261          | 9132.22                  | 57.326                            | 117.9                               |
| 212          | 6472.67                  | 51.047                            | 139.8                               | 262          | 9189.61                  | 57.444                            | 117.4                               |
| 213          | 6523.79                  | 51.186                            | 139.3                               | 263          | 9247.11                  | 57.561                            | 116.9                               |
| 214          | 6575.04                  | 51.325                            | 138.8                               | 264          | 9304.73                  | 57.677                            | 116.3                               |
| 215          | 6626.44                  | 51.464                            | 138.3                               | 265          | 9362.46                  | 57.793                            | 115.6                               |
| 216          | 6677.97                  | 51.602                            | 137.8                               | 266          | 9420.31                  | 57.908                            | 114.8                               |
| 217          | 6729.64                  | 51.739                            | 137.3                               | 267          | 9478.28                  | 58.023                            | 113.9                               |
| 218          | 6781.45                  | 51.876                            | 136.8                               | 268          | 9536.36                  | 58.136                            | 112.8                               |
| 219          | 6833.39                  | 52.013                            | 136.3                               | 269          | 9594.55                  | 58.248                            | 111.5                               |
| 220          | 6885.47                  | 52.149                            | 135.8                               | 270          | 9652.85                  | 58.359                            | 110.0                               |
| 221          | 6937.69                  | 52.284                            | 135.3                               | 271          | 9711.27                  | 58.468                            | 108.2                               |
| 222          | 6990.04                  | 52.419                            | 134.8                               | 272          | 9769.79                  | 58.575                            | 106.2                               |
| 223          | 7042.53                  | 52.554                            | 134.3                               | 273          | 9828.42                  | 58.680                            | 103.7                               |
| 224          | 7095.15                  | 52.688                            | 133.8                               | 274          | 9887.15                  | 58.783                            | 100.9                               |
| 225          | 7147.90                  | 52.821                            | 133.3                               | 275          | 9945.98                  | 58.882                            | 97.6                                |
| 226          | 7200.79                  | 52.955                            | 132.8                               | 276          | 10004.91                 | 58.978                            | 93.8                                |
| 227          | 7253.81                  | 53.087                            | 132.3                               | 277          | 10063.94                 | 59.069                            | 89.3                                |
| 228          | 7306.97                  | 53.219                            | 131.9                               | 278          | 10123.05                 | 59.156                            | 84.2                                |
| 229          | 7360.25                  | 53.351                            | 131.4                               | 279          | 10182.25                 | 59.237                            | 78.2                                |
|              |                          |                                   |                                     | 280          | 10241.52                 | 59.312                            | 71.4                                |

TABLE 11.2—Type *T*-thermoelectric voltage, *E*(*T*), Seebeck coefficient, *S*(*T*), and derivative of the Seebeck coefficient,  $dS/dT$  [*S*].

| <i>T</i> , K | <i>E</i> , $\mu\text{V}$ | <i>S</i> , $\mu\text{V}/\text{K}$ | $dS/dT$ ,<br>$\text{nV}/\text{K}^2$ | <i>T</i> , K | <i>E</i> , $\mu\text{V}$ | <i>S</i> , $\mu\text{V}/\text{K}$ | $dS/dT$ ,<br>$\text{nV}/\text{K}^2$ |
|--------------|--------------------------|-----------------------------------|-------------------------------------|--------------|--------------------------|-----------------------------------|-------------------------------------|
| 0            | 0.00                     | -0.400                            | 526.6                               | 45           | 272.34                   | 11.245                            | 193.5                               |
| 1            | -0.15                    | 0.099                             | 473.2                               | 46           | 283.68                   | 11.437                            | 190.3                               |
| 2            | 0.18                     | 0.549                             | 428.0                               | 47           | 295.21                   | 11.625                            | 187.1                               |
| 3            | 0.94                     | 0.958                             | 390.1                               | 48           | 306.93                   | 11.811                            | 184.0                               |
| 4            | 2.09                     | 1.332                             | 358.4                               | 49           | 318.83                   | 11.993                            | 181.0                               |
| 5            | 3.59                     | 1.677                             | 332.3                               | 50           | 330.92                   | 12.173                            | 178.0                               |
| 6            | 5.43                     | 1.998                             | 310.9                               | 51           | 343.18                   | 12.349                            | 175.2                               |
| 7            | 7.58                     | 2.300                             | 293.5                               | 52           | 345.62                   | 12.523                            | 172.5                               |

TABLE 11.2—(Continued).

| $T, K$ | $E, \mu V$ | $S, \mu V/K$ | $dS/dT,$<br>$nV/K^2$ | $T, K$ | $E, \mu V$ | $S, \mu V/K$ | $dS/dT,$<br>$nV/K^2$ |
|--------|------------|--------------|----------------------|--------|------------|--------------|----------------------|
| 8      | 10.03      | 2.586        | 279.7                | 53     | 368.23     | 12.694       | 169.8                |
| 9      | 12.75      | 2.860        | 268.8                | 54     | 381.00     | 12.863       | 167.3                |
| 10     | 15.74      | 3.124        | 260.3                | 55     | 393.95     | 13.029       | 164.9                |
| 11     | 19.00      | 3.381        | 254.0                | 56     | 407.06     | 13.193       | 162.6                |
| 12     | 22.50      | 3.633        | 249.3                | 57     | 420.33     | 13.354       | 164.4                |
| 13     | 26.26      | 3.880        | 246.0                | 58     | 433.77     | 13.514       | 158.4                |
| 14     | 30.26      | 4.125        | 243.8                | 59     | 447.36     | 13.671       | 156.4                |
| 15     | 34.51      | 4.368        | 242.5                | 60     | 461.11     | 13.826       | 154.6                |
| 16     | 39.00      | 4.610        | 241.8                | 61     | 475.01     | 13.980       | 152.9                |
| 17     | 43.73      | 4.852        | 241.5                | 62     | 489.07     | 14.132       | 151.3                |
| 18     | 48.70      | 5.094        | 241.6                | 63     | 503.28     | 14.283       | 149.8                |
| 19     | 53.92      | 5.335        | 241.8                | 64     | 517.64     | 14.432       | 148.4                |
| 20     | 59.37      | 5.577        | 242.2                | 65     | 532.14     | 14.580       | 147.1                |
| 21     | 65.07      | 5.820        | 242.5                | 66     | 546.79     | 14.726       | 146.0                |
| 22     | 71.01      | 6.062        | 242.7                | 67     | 561.59     | 14.872       | 144.9                |
| 23     | 77.20      | 6.305        | 242.7                | 68     | 578.54     | 15.016       | 143.9                |
| 24     | 83.62      | 6.548        | 242.6                | 69     | 591.62     | 15.159       | 142.9                |
| 25     | 90.29      | 6.790        | 242.2                | 70     | 606.86     | 15.302       | 142.1                |
| 26     | 97.20      | 7.032        | 241.6                | 71     | 622.23     | 15.444       | 141.3                |
| 27     | 104.36     | 7.273        | 240.8                | 72     | 637.74     | 15.584       | 140.6                |
| 28     | 111.75     | 7.513        | 239.7                | 73     | 653.40     | 15.725       | 139.9                |
| 29     | 119.38     | 7.752        | 238.3                | 74     | 669.19     | 15.864       | 139.3                |
| 30     | 127.25     | 7.990        | 236.7                | 75     | 685.13     | 16.003       | 138.8                |
| 31     | 135.36     | 8.226        | 234.8                | 76     | 701.20     | 16.142       | 138.3                |
| 32     | 143.70     | 8.459        | 232.7                | 77     | 717.41     | 16.280       | 137.8                |
| 33     | 152.28     | 8.691        | 230.4                | 78     | 733.76     | 16.417       | 137.4                |
| 34     | 161.08     | 8.920        | 227.9                | 79     | 750.24     | 16.555       | 137.0                |
| 35     | 170.12     | 9.147        | 225.2                | 80     | 766.87     | 16.691       | 136.6                |
| 36     | 179.38     | 9.371        | 222.4                | 81     | 783.63     | 16.828       | 136.2                |
| 37     | 188.86     | 9.592        | 219.4                | 82     | 800.52     | 16.964       | 135.9                |
| 38     | 198.56     | 9.809        | 216.4                | 83     | 817.55     | 17.100       | 135.6                |
| 39     | 208.48     | 10.024       | 213.2                | 84     | 834.72     | 17.235       | 135.3                |
| 40     | 218.61     | 10.236       | 210.0                | 85     | 852.02     | 17.370       | 135.0                |
| 41     | 228.95     | 10.444       | 206.7                | 86     | 869.46     | 17.505       | 134.7                |
| 42     | 239.49     | 10.649       | 203.4                | 87     | 887.03     | 17.640       | 134.5                |
| 43     | 250.24     | 10.851       | 200.1                | 88     | 904.74     | 17.774       | 134.2                |
| 44     | 261.19     | 11.049       | 196.8                | 89     | 922.58     | 17.908       | 133.9                |
| 90     | 940.56     | 18.042       | 133.7                | 140    | 2004.33    | 24.420       | 123.2                |
| 91     | 958.66     | 18.175       | 133.4                | 141    | 2028.82    | 24.543       | 123.0                |
| 92     | 976.91     | 18.309       | 133.1                | 142    | 2053.42    | 24.666       | 122.9                |
| 93     | 995.28     | 18.442       | 132.9                | 143    | 2078.15    | 24.789       | 122.7                |
| 94     | 1013.79    | 18.574       | 132.6                | 144    | 2103.00    | 24.911       | 122.6                |
| 95     | 1032.43    | 18.707       | 132.3                | 145    | 2127.97    | 25.034       | 122.4                |
| 96     | 1051.20    | 18.839       | 132.1                | 146    | 2153.07    | 25.156       | 122.3                |
| 97     | 1070.11    | 18.971       | 131.8                | 147    | 2178.28    | 25.279       | 122.1                |
| 98     | 1089.14    | 19.102       | 131.5                | 148    | 2203.62    | 25.401       | 121.9                |
| 99     | 1108.31    | 19.234       | 131.2                | 149    | 2229.08    | 25.522       | 121.8                |

TABLE 11.2—(Continued).

| $T, K$ | $E, \mu V$ | $S, \mu V/K$ | $dS/dT,$<br>$nV/K^2$ | $T, K$ | $E, \mu V$ | $S, \mu V/K$ | $dS/dT,$<br>$nV/K^2$ |
|--------|------------|--------------|----------------------|--------|------------|--------------|----------------------|
| 100    | 1127.61    | 19.365       | 131.0                | 150    | 2254.67    | 25.644       | 121.6                |
| 101    | 1147.04    | 19.496       | 130.7                | 151    | 2280.37    | 25.766       | 121.4                |
| 102    | 1166.60    | 19.626       | 130.4                | 152    | 2306.20    | 25.887       | 121.2                |
| 103    | 1186.29    | 19.757       | 130.1                | 153    | 2332.15    | 26.008       | 121.0                |
| 104    | 1206.12    | 19.886       | 129.8                | 154    | 2358.21    | 26.129       | 120.7                |
| 105    | 1226.07    | 20.016       | 129.6                | 155    | 2384.40    | 26.249       | 120.5                |
| 106    | 1246.15    | 20.146       | 129.3                | 156    | 2410.71    | 26.370       | 120.3                |
| 107    | 1266.36    | 20.275       | 129.0                | 157    | 2437.14    | 26.490       | 120.1                |
| 108    | 1286.70    | 20.404       | 128.7                | 158    | 2463.69    | 26.610       | 119.8                |
| 109    | 1307.17    | 20.532       | 128.5                | 159    | 2490.36    | 26.730       | 119.6                |
| 110    | 1327.76    | 20.661       | 128.2                | 160    | 2517.15    | 26.849       | 119.3                |
| 111    | 1348.49    | 20.789       | 128.0                | 161    | 2544.06    | 26.968       | 119.0                |
| 112    | 1369.34    | 20.916       | 127.7                | 162    | 2571.09    | 27.087       | 118.8                |
| 113    | 1390.32    | 21.044       | 127.5                | 163    | 2598.24    | 27.206       | 118.5                |
| 114    | 1411.43    | 21.171       | 127.2                | 164    | 2625.50    | 27.324       | 118.2                |
| 115    | 1432.66    | 21.298       | 127.0                | 165    | 2652.88    | 27.442       | 118.0                |
| 116    | 1454.02    | 21.425       | 126.8                | 166    | 2680.39    | 27.560       | 117.7                |
| 117    | 1475.51    | 21.552       | 126.6                | 167    | 2708.00    | 27.678       | 117.4                |
| 118    | 1497.13    | 21.678       | 126.3                | 168    | 2735.74    | 27.795       | 117.1                |
| 119    | 1518.87    | 21.805       | 126.1                | 169    | 2763.59    | 27.912       | 116.8                |
| 120    | 1540.74    | 21.931       | 126.0                | 170    | 2791.56    | 28.029       | 116.6                |
| 121    | 1562.73    | 22.057       | 125.8                | 171    | 2819.65    | 28.145       | 116.3                |
| 122    | 1584.85    | 22.182       | 125.6                | 172    | 2847.85    | 28.261       | 116.0                |
| 123    | 1607.10    | 22.308       | 125.4                | 173    | 2876.17    | 28.377       | 115.7                |
| 124    | 1629.47    | 22.433       | 125.3                | 174    | 2904.61    | 28.493       | 115.5                |
| 125    | 1651.96    | 22.558       | 125.1                | 175    | 2933.16    | 28.608       | 115.2                |
| 126    | 1674.58    | 22.683       | 125.0                | 176    | 2961.82    | 28.723       | 114.9                |
| 127    | 1697.33    | 22.808       | 124.8                | 177    | 2990.60    | 28.838       | 114.7                |
| 128    | 1720.20    | 22.933       | 124.7                | 178    | 3019.50    | 28.952       | 114.4                |
| 129    | 1743.20    | 23.058       | 124.5                | 179    | 3048.51    | 29.067       | 114.2                |
| 130    | 1766.31    | 23.182       | 124.4                | 180    | 3077.63    | 29.181       | 113.9                |
| 131    | 1789.56    | 23.306       | 124.3                | 181    | 3106.87    | 29.294       | 113.7                |
| 132    | 1812.93    | 23.431       | 124.2                | 182    | 3136.22    | 29.408       | 113.4                |
| 133    | 1836.42    | 23.555       | 124.0                | 183    | 3165.68    | 29.521       | 113.2                |
| 134    | 1860.04    | 23.679       | 123.9                | 184    | 3195.28    | 29.634       | 113.0                |
| 135    | 1883.78    | 23.803       | 123.8                | 185    | 3224.95    | 29.747       | 112.8                |
| 136    | 1907.64    | 23.926       | 123.7                | 186    | 3254.76    | 29.860       | 112.5                |
| 137    | 1931.63    | 24.050       | 123.5                | 187    | 3284.67    | 29.972       | 112.3                |
| 138    | 1955.74    | 24.173       | 123.4                | 188    | 3314.70    | 30.085       | 112.1                |
| 139    | 1979.98    | 24.297       | 123.3                | 189    | 3344.84    | 30.197       | 111.9                |
| 190    | 3375.09    | 30.308       | 111.7                | 235    | 4848.69    | 35.093       | 100.0                |
| 191    | 3405.46    | 30.420       | 111.5                | 236    | 4883.84    | 35.193       | 99.9                 |
| 192    | 3435.93    | 30.531       | 111.3                | 237    | 4919.08    | 35.293       | 99.7                 |
| 193    | 3466.52    | 30.643       | 111.1                | 238    | 4954.42    | 35.392       | 99.5                 |
| 194    | 3497.22    | 30.754       | 111.0                | 239    | 4989.86    | 35.492       | 99.4                 |
| 195    | 3528.03    | 30.865       | 110.8                | 240    | 5025.40    | 35.591       | 99.3                 |
| 196    | 3558.95    | 30.975       | 110.6                | 241    | 5061.04    | 35.690       | 99.2                 |
| 197    | 3589.98    | 31.086       | 110.4                | 242    | 5096.78    | 35.789       | 99.1                 |

TABLE 11.2—(Continued).

| $T, K$ | $E, \mu V$ | $S, \mu V/K$ | $dS/dT,$<br>$nV/K^2$ | $T, K$ | $E, \mu V$ | $S, \mu V/K$ | $dS/dT,$<br>$nV/K^2$ |
|--------|------------|--------------|----------------------|--------|------------|--------------|----------------------|
| 198    | 3621.12    | 31.196       | 110.2                | 243    | 5132.62    | 35.888       | 99.0                 |
| 199    | 3652.37    | 31.306       | 110.0                | 244    | 5168.56    | 35.987       | 98.9                 |
| 200    | 3683.73    | 31.416       | 109.8                | 245    | 5204.60    | 36.086       | 98.8                 |
| 201    | 3715.20    | 31.526       | 109.6                | 246    | 5240.73    | 36.185       | 98.8                 |
| 202    | 3746.78    | 31.635       | 109.4                | 247    | 5276.97    | 36.284       | 98.7                 |
| 203    | 3778.47    | 31.744       | 109.2                | 248    | 5313.30    | 36.382       | 98.6                 |
| 204    | 3810.27    | 31.853       | 108.9                | 249    | 5349.73    | 36.481       | 98.5                 |
| 205    | 3842.18    | 31.962       | 108.7                | 250    | 5386.26    | 36.579       | 98.4                 |
| 206    | 3874.20    | 32.071       | 108.5                | 251    | 5422.89    | 36.678       | 98.3                 |
| 207    | 3906.32    | 32.179       | 108.2                | 252    | 5459.62    | 36.776       | 98.1                 |
| 208    | 3938.55    | 32.287       | 108.0                | 253    | 5496.44    | 36.874       | 97.9                 |
| 209    | 3970.90    | 32.395       | 107.7                | 254    | 5533.37    | 36.972       | 97.6                 |
| 210    | 4003.34    | 32.503       | 107.4                | 255    | 5570.39    | 37.069       | 97.3                 |
| 211    | 4035.90    | 32.610       | 107.2                | 256    | 5607.50    | 37.166       | 97.0                 |
| 212    | 4068.56    | 32.717       | 106.9                | 257    | 5644.72    | 37.263       | 96.6                 |
| 213    | 4101.34    | 32.824       | 106.6                | 258    | 5682.03    | 37.359       | 96.1                 |
| 214    | 4134.21    | 32.930       | 106.3                | 259    | 5719.44    | 37.455       | 95.6                 |
| 215    | 4167.20    | 33.036       | 106.0                | 260    | 5756.94    | 37.551       | 95.0                 |
| 216    | 4200.29    | 33.142       | 105.7                | 261    | 5794.54    | 37.645       | 94.3                 |
| 217    | 4233.48    | 33.248       | 105.4                | 262    | 5832.23    | 37.739       | 93.6                 |
| 218    | 4266.78    | 33.353       | 105.0                | 263    | 5870.02    | 37.833       | 92.9                 |
| 219    | 4300.19    | 33.458       | 104.7                | 264    | 5907.90    | 37.925       | 92.1                 |
| 220    | 4333.70    | 33.562       | 104.4                | 265    | 5945.87    | 38.017       | 91.3                 |
| 221    | 4367.31    | 33.667       | 104.0                | 266    | 5983.93    | 38.108       | 90.5                 |
| 222    | 4401.03    | 33.770       | 103.7                | 267    | 6022.08    | 38.198       | 89.8                 |
| 223    | 4434.85    | 33.874       | 103.4                | 268    | 6060.32    | 38.287       | 89.0                 |
| 224    | 4468.78    | 33.977       | 103.1                | 269    | 6098.66    | 38.376       | 88.4                 |
| 225    | 4502.81    | 34.080       | 102.7                | 270    | 6137.08    | 38.464       | 88.0                 |
| 226    | 4536.94    | 34.183       | 102.4                | 271    | 6175.58    | 38.552       | 87.7                 |
| 227    | 4571.17    | 34.285       | 102.1                | 272    | 6214.18    | 38.640       | 87.8                 |
| 228    | 4605.51    | 34.387       | 101.8                | 273    | 6252.86    | 38.728       | 88.2                 |
| 229    | 4639.94    | 34.488       | 101.5                | 274    | 6291.64    | 38.816       | 89.0                 |
| 230    | 4674.48    | 34.590       | 101.2                | 275    | 6330.50    | 38.906       | 90.5                 |
| 231    | 4709.12    | 34.691       | 101.0                | 276    | 6369.45    | 38.997       | 92.6                 |
| 232    | 4743.87    | 34.792       | 100.7                | 277    | 6408.49    | 39.091       | 95.6                 |
| 233    | 4778.71    | 34.892       | 100.5                | 278    | 6447.63    | 39.189       | 99.7                 |
| 234    | 4813.65    | 34.993       | 100.2                | 279    | 6486.87    | 39.291       | 105.0                |
|        |            |              |                      | 280    | 6526.22    | 39.399       | 111.8                |



TABLE 11.3—Type *K*-thermoelectric voltage,  $E(T)$ , Seebeck coefficient,  $S(T)$ , and derivative of Seebeck coefficient,  $dS/dT$  [5].

| $T$ , K | $E$ , $\mu\text{V}$ | $S$ , $\mu\text{V/K}$ | $dS/dT$ ,<br>$\text{nV/K}^2$ | $T$ , K | $E$ , $\mu\text{V}$ | $S$ , $\mu\text{V/K}$ | $dS/dT$ ,<br>$\text{nV/K}^2$ |
|---------|---------------------|-----------------------|------------------------------|---------|---------------------|-----------------------|------------------------------|
| 0       | 0.00                | 0.241                 | 146.9                        | 45      | 214.95              | 9.683                 | 212.9                        |
| 1       | 0.32                | 0.391                 | 154.3                        | 46      | 224.74              | 9.896                 | 211.8                        |
| 2       | 0.78                | 0.549                 | 161.3                        | 47      | 234.75              | 10.107                | 210.8                        |
| 3       | 1.42                | 0.714                 | 167.7                        | 48      | 244.96              | 10.317                | 209.7                        |
| 4       | 2.21                | 0.884                 | 173.7                        | 49      | 255.38              | 10.526                | 208.7                        |
| 5       | 3.19                | 1.061                 | 179.2                        | 50      | 266.01              | 10.735                | 207.6                        |
| 6       | 4.34                | 1.243                 | 184.3                        | 51      | 276.85              | 10.942                | 206.5                        |
| 7       | 5.67                | 1.429                 | 189.0                        | 52      | 287.89              | 11.148                | 205.5                        |
| 8       | 7.20                | 1.621                 | 193.4                        | 53      | 299.14              | 11.353                | 204.4                        |
| 9       | 8.92                | 1.816                 | 197.3                        | 54      | 310.60              | 11.556                | 203.3                        |
| 10      | 10.83               | 2.015                 | 200.9                        | 55      | 322.26              | 11.759                | 202.3                        |
| 11      | 12.95               | 2.218                 | 204.2                        | 56      | 334.12              | 11.961                | 201.2                        |
| 12      | 15.27               | 2.424                 | 207.2                        | 57      | 346.18              | 12.162                | 200.1                        |
| 13      | 17.80               | 2.632                 | 209.9                        | 58      | 358.44              | 12.361                | 199.1                        |
| 14      | 20.53               | 2.843                 | 212.3                        | 59      | 370.90              | 12.560                | 198.1                        |
| 15      | 23.48               | 3.057                 | 214.5                        | 60      | 383.56              | 12.757                | 197.0                        |
| 16      | 26.65               | 3.272                 | 216.4                        | 61      | 396.41              | 12.954                | 196.0                        |
| 17      | 30.03               | 3.489                 | 218.1                        | 62      | 409.47              | 13.149                | 195.0                        |
| 18      | 33.63               | 3.708                 | 219.5                        | 63      | 422.71              | 13.344                | 194.0                        |
| 19      | 37.45               | 3.928                 | 220.8                        | 64      | 436.15              | 13.537                | 193.0                        |
| 20      | 41.48               | 4.150                 | 221.9                        | 65      | 449.79              | 13.730                | 192.1                        |
| 21      | 45.75               | 4.372                 | 222.8                        | 66      | 463.61              | 13.922                | 191.1                        |
| 22      | 50.23               | 4.595                 | 223.5                        | 67      | 477.63              | 14.112                | 190.2                        |
| 23      | 54.94               | 4.819                 | 224.0                        | 68      | 491.84              | 14.302                | 189.2                        |
| 24      | 59.87               | 5.043                 | 224.4                        | 69      | 506.23              | 14.491                | 188.3                        |
| 25      | 65.02               | 5.268                 | 224.7                        | 70      | 520.82              | 14.678                | 187.4                        |
| 26      | 70.40               | 5.493                 | 224.9                        | 71      | 535.59              | 14.865                | 186.5                        |
| 27      | 76.01               | 5.718                 | 224.9                        | 72      | 550.55              | 15.051                | 185.6                        |
| 28      | 81.84               | 5.942                 | 224.8                        | 73      | 565.69              | 15.237                | 184.8                        |
| 29      | 87.89               | 6.167                 | 224.6                        | 74      | 581.02              | 15.421                | 183.9                        |
| 30      | 94.17               | 6.392                 | 224.3                        | 75      | 596.53              | 15.604                | 183.1                        |
| 31      | 100.68              | 6.616                 | 224.0                        | 76      | 612.23              | 15.787                | 182.2                        |
| 32      | 107.40              | 6.840                 | 223.5                        | 77      | 628.11              | 15.969                | 181.4                        |
| 33      | 114.36              | 7.063                 | 223.0                        | 78      | 644.17              | 16.150                | 180.6                        |
| 34      | 121.53              | 7.285                 | 222.4                        | 79      | 660.41              | 16.330                | 179.8                        |
| 35      | 128.93              | 7.508                 | 221.7                        | 80      | 676.83              | 16.510                | 179.1                        |
| 36      | 136.54              | 7.729                 | 221.0                        | 81      | 693.43              | 16.688                | 178.3                        |
| 37      | 144.38              | 7.950                 | 220.3                        | 82      | 710.20              | 16.866                | 177.5                        |
| 38      | 152.44              | 8.169                 | 219.4                        | 83      | 727.16              | 17.043                | 176.8                        |
| 39      | 160.72              | 8.388                 | 218.6                        | 84      | 744.29              | 17.220                | 176.1                        |
| 40      | 169.22              | 8.607                 | 217.7                        | 85      | 761.60              | 17.396                | 175.3                        |
| 41      | 177.94              | 8.824                 | 216.8                        | 86      | 779.08              | 17.571                | 174.6                        |
| 42      | 186.87              | 9.040                 | 215.8                        | 87      | 796.74              | 17.745                | 173.9                        |
| 43      | 196.02              | 9.256                 | 214.9                        | 88      | 814.57              | 17.918                | 173.2                        |
| 44      | 205.38              | 9.470                 | 213.9                        | 89      | 832.58              | 18.091                | 172.6                        |
| 90      | 850.75              | 18.264                | 171.9                        | 140     | 1966.10             | 26.107                | 142.3                        |
| 91      | 869.10              | 18.435                | 171.2                        | 141     | 1992.28             | 26.249                | 141.7                        |

TABLE 11.3—(Continued).

| $T, K$ | $E, \mu V$ | $S, \mu V/K$ | $dS/dT,$<br>$nV/K^2$ | $T, K$ | $E, \mu V$ | $S, \mu V/K$ | $dS/dT,$<br>$nV/K^2$ |
|--------|------------|--------------|----------------------|--------|------------|--------------|----------------------|
| 92     | 887.62     | 18.606       | 170.6                | 142    | 2018.60    | 26.391       | 141.1                |
| 93     | 906.31     | 18.776       | 169.9                | 143    | 2045.06    | 26.532       | 140.6                |
| 94     | 925.18     | 18.946       | 169.3                | 144    | 2071.66    | 26.672       | 140.0                |
| 95     | 944.21     | 19.115       | 168.6                | 145    | 2098.40    | 26.811       | 139.4                |
| 96     | 963.40     | 19.283       | 168.0                | 146    | 2125.28    | 26.950       | 138.8                |
| 97     | 982.77     | 19.451       | 167.4                | 147    | 2152.30    | 27.089       | 138.2                |
| 98     | 1002.31    | 19.618       | 166.8                | 148    | 2179.46    | 27.227       | 137.6                |
| 99     | 1022.01    | 19.784       | 166.2                | 149    | 2206.75    | 27.364       | 137.0                |
| 100    | 1041.87    | 19.950       | 165.5                | 150    | 2234.19    | 27.501       | 136.4                |
| 101    | 1061.91    | 20.115       | 164.9                | 151    | 2261.76    | 27.637       | 135.7                |
| 102    | 1082.11    | 20.280       | 164.3                | 152    | 2289.46    | 27.772       | 135.1                |
| 103    | 1102.47    | 20.444       | 163.7                | 153    | 2317.30    | 27.907       | 134.5                |
| 104    | 1122.99    | 20.608       | 163.2                | 154    | 2345.27    | 28.041       | 133.9                |
| 105    | 1143.68    | 20.770       | 162.6                | 155    | 2373.38    | 28.175       | 133.3                |
| 106    | 1164.53    | 20.933       | 162.0                | 156    | 2401.62    | 28.308       | 132.7                |
| 107    | 1185.55    | 21.094       | 161.4                | 157    | 2430.00    | 28.440       | 132.1                |
| 108    | 1206.72    | 21.255       | 160.8                | 158    | 2458.50    | 28.572       | 131.5                |
| 109    | 1228.06    | 21.416       | 160.2                | 159    | 2487.14    | 28.703       | 130.9                |
| 110    | 1249.55    | 21.576       | 159.7                | 160    | 2515.91    | 28.834       | 130.3                |
| 111    | 1271.21    | 21.735       | 159.1                | 161    | 2544.81    | 28.964       | 129.7                |
| 112    | 1293.02    | 21.894       | 158.5                | 162    | 2573.84    | 29.093       | 129.0                |
| 113    | 1315.00    | 22.052       | 157.9                | 163    | 2603.00    | 29.222       | 128.4                |
| 114    | 1337.13    | 22.210       | 157.4                | 164    | 2632.28    | 29.350       | 127.8                |
| 115    | 1359.42    | 22.367       | 156.8                | 165    | 2661.70    | 29.478       | 127.2                |
| 116    | 1381.86    | 22.524       | 156.2                | 166    | 2691.24    | 29.604       | 126.6                |
| 117    | 1404.46    | 22.679       | 155.6                | 167    | 2720.90    | 29.731       | 126.0                |
| 118    | 1427.22    | 22.835       | 155.1                | 168    | 2750.70    | 29.856       | 125.3                |
| 119    | 1450.13    | 22.990       | 154.5                | 169    | 2780.62    | 29.981       | 124.7                |
| 120    | 1473.20    | 23.144       | 153.9                | 170    | 2810.66    | 30.106       | 124.1                |
| 121    | 1496.42    | 23.297       | 153.4                | 171    | 2840.83    | 30.230       | 123.5                |
| 122    | 1519.80    | 23.451       | 152.8                | 172    | 2871.12    | 30.353       | 122.9                |
| 123    | 1543.32    | 23.603       | 152.2                | 173    | 2901.53    | 30.475       | 122.2                |
| 124    | 1567.00    | 23.755       | 151.6                | 174    | 2932.07    | 30.597       | 121.6                |
| 125    | 1590.83    | 23.906       | 151.1                | 175    | 2962.73    | 30.718       | 121.0                |
| 126    | 1614.81    | 24.057       | 150.5                | 176    | 2993.51    | 30.839       | 120.4                |
| 127    | 1638.95    | 24.207       | 149.9                | 177    | 3024.41    | 30.959       | 119.7                |
| 128    | 1663.23    | 24.357       | 149.3                | 178    | 3055.42    | 31.079       | 119.1                |
| 129    | 1687.66    | 24.506       | 148.8                | 179    | 3086.56    | 31.197       | 118.5                |
| 130    | 1712.24    | 24.654       | 148.2                | 180    | 3117.82    | 31.316       | 117.9                |
| 131    | 1736.97    | 24.802       | 147.6                | 181    | 3149.19    | 31.433       | 117.2                |
| 132    | 1761.84    | 24.950       | 147.0                | 182    | 3180.68    | 31.550       | 116.6                |
| 133    | 1786.87    | 25.096       | 146.4                | 183    | 3212.29    | 31.666       | 116.0                |
| 134    | 1812.04    | 25.243       | 145.9                | 184    | 3244.02    | 31.782       | 115.3                |
| 135    | 1837.35    | 25.388       | 145.3                | 185    | 3275.86    | 31.897       | 114.7                |
| 136    | 1862.81    | 25.533       | 144.7                | 186    | 3307.81    | 32.011       | 114.1                |
| 137    | 1888.42    | 25.678       | 144.1                | 187    | 3339.88    | 32.125       | 113.4                |
| 138    | 1914.17    | 25.821       | 143.5                | 188    | 3372.06    | 32.238       | 112.8                |
| 139    | 1940.06    | 25.965       | 142.9                | 189    | 3404.36    | 32.351       | 112.2                |

TABLE 11.3—(Continued).

| $T, K$ | $E, \mu V$ | $S, \mu V/K$ | $dS/dT,$<br>$nV/K^2$ | $T, K$ | $E, \mu V$ | $S, \mu V/K$ | $dS/dT,$<br>$nV/K^2$ |
|--------|------------|--------------|----------------------|--------|------------|--------------|----------------------|
| 190    | 3436.76    | 32.463       | 111.5                | 235    | 5000.69    | 36.825       | 82.2                 |
| 191    | 3469.28    | 32.574       | 110.9                | 236    | 5037.55    | 36.907       | 81.6                 |
| 192    | 3501.91    | 32.684       | 110.3                | 237    | 5074.50    | 36.988       | 80.9                 |
| 193    | 3534.65    | 32.794       | 109.6                | 238    | 5111.53    | 37.069       | 80.3                 |
| 194    | 3567.50    | 32.904       | 109.0                | 239    | 5148.64    | 37.149       | 79.6                 |
| 195    | 3600.46    | 33.012       | 108.3                | 240    | 5185.83    | 37.228       | 79.0                 |
| 196    | 3633.52    | 33.120       | 107.7                | 241    | 5223.10    | 37.307       | 78.4                 |
| 197    | 3666.70    | 33.228       | 107.1                | 242    | 5260.44    | 37.385       | 77.7                 |
| 198    | 3699.98    | 33.334       | 106.4                | 243    | 5297.87    | 37.462       | 77.1                 |
| 199    | 3733.36    | 33.440       | 105.8                | 244    | 5335.37    | 37.539       | 76.4                 |
| 200    | 3766.86    | 33.546       | 105.1                | 245    | 5372.94    | 37.615       | 75.8                 |
| 201    | 3800.46    | 33.651       | 104.5                | 246    | 5410.60    | 37.691       | 75.1                 |
| 202    | 3834.16    | 33.755       | 103.8                | 247    | 5448.32    | 37.765       | 74.5                 |
| 203    | 3867.96    | 33.858       | 103.2                | 248    | 5486.13    | 37.840       | 73.8                 |
| 204    | 3901.87    | 33.961       | 102.5                | 249    | 5524.00    | 37.913       | 73.2                 |
| 205    | 3935.89    | 34.063       | 101.9                | 250    | 5561.95    | 37.986       | 72.5                 |
| 206    | 3970.00    | 34.165       | 101.2                | 251    | 5599.98    | 38.058       | 71.9                 |
| 207    | 4004.22    | 34.266       | 100.6                | 252    | 5638.07    | 38.130       | 71.2                 |
| 208    | 4038.53    | 34.366       | 99.9                 | 253    | 5676.23    | 38.201       | 70.6                 |
| 209    | 4072.95    | 34.466       | 99.3                 | 254    | 5714.47    | 38.271       | 69.9                 |
| 210    | 4107.46    | 34.565       | 98.6                 | 255    | 5752.78    | 38.340       | 69.2                 |
| 211    | 4142.08    | 34.663       | 98.0                 | 256    | 5791.15    | 38.409       | 68.5                 |
| 212    | 4176.79    | 34.761       | 97.3                 | 257    | 5829.59    | 38.477       | 67.9                 |
| 213    | 4211.60    | 34.857       | 96.7                 | 258    | 5868.10    | 38.545       | 67.2                 |
| 214    | 4246.50    | 34.954       | 96.0                 | 259    | 5906.68    | 38.612       | 66.5                 |
| 215    | 4281.51    | 35.049       | 95.3                 | 260    | 5945.33    | 38.678       | 65.8                 |
| 216    | 4316.60    | 35.144       | 94.7                 | 261    | 5984.04    | 38.743       | 65.1                 |
| 217    | 4351.79    | 35.239       | 94.0                 | 262    | 6022.81    | 38.808       | 64.3                 |
| 218    | 4387.08    | 35.333       | 93.4                 | 263    | 6061.65    | 38.872       | 63.6                 |
| 219    | 4422.46    | 35.426       | 92.7                 | 264    | 6100.56    | 38.935       | 62.8                 |
| 220    | 4457.93    | 35.518       | 92.1                 | 265    | 6139.52    | 38.998       | 62.1                 |
| 221    | 4493.49    | 35.610       | 91.4                 | 266    | 6178.55    | 39.059       | 61.3                 |
| 222    | 4529.15    | 35.701       | 90.7                 | 267    | 6217.64    | 39.120       | 60.5                 |
| 223    | 4564.90    | 35.791       | 90.1                 | 268    | 6256.79    | 39.180       | 59.6                 |
| 224    | 4600.73    | 35.881       | 89.4                 | 269    | 6296.00    | 39.239       | 58.8                 |
| 225    | 4636.66    | 35.970       | 88.8                 | 270    | 6335.27    | 39.298       | 57.9                 |
| 226    | 4672.67    | 36.059       | 88.1                 | 271    | 6374.60    | 39.355       | 57.0                 |
| 227    | 4708.77    | 36.146       | 87.5                 | 272    | 6413.98    | 39.412       | 56.1                 |
| 228    | 4744.96    | 36.233       | 86.8                 | 273    | 6453.42    | 39.467       | 55.1                 |
| 229    | 4781.24    | 36.320       | 86.2                 | 274    | 6492.91    | 39.522       | 54.1                 |
| 230    | 4817.60    | 36.406       | 85.5                 | 275    | 6532.46    | 39.575       | 53.0                 |
| 231    | 4854.05    | 36.491       | 84.8                 | 276    | 6572.06    | 39.628       | 51.9                 |
| 232    | 4890.59    | 36.575       | 84.2                 | 277    | 6611.72    | 39.679       | 50.8                 |
| 233    | 4927.20    | 36.659       | 83.5                 | 278    | 6651.42    | 39.729       | 49.6                 |
| 234    | 4963.90    | 36.743       | 82.9                 | 279    | 6691.18    | 39.778       | 48.4                 |
|        |            |              |                      | 280    | 6730.98    | 39.826       | 47.1                 |

TABLE 11.4—*Thermocouple, KP or EP versus gold-0.07 atomic percent iron-thermoelectric voltage, Seebeck coefficient, and derivative of the Seebeck coefficient;  $E = f(T)$  [6].*

| $T, K$ | $E, \mu V$ | $S, \mu V/K$ | $dS/dT,$<br>$nV/K^2$ | $T, K$ | $E, \mu V$ | $S, \mu V/K$ | $dS/dT,$<br>$nV/K^2$ |
|--------|------------|--------------|----------------------|--------|------------|--------------|----------------------|
| 0      | 0.00       | 0.000        | 0.0                  | 45     | 710.22     | 16.569       | 26.9                 |
| 1      | 7.85       | 8.673        | 1565.8               | 46     | 726.81     | 16.597       | 29.3                 |
| 2      | 17.27      | 10.127       | 1346.7               | 47     | 743.42     | 16.628       | 31.4                 |
| 3      | 28.04      | 11.375       | 1152.4               | 48     | 760.06     | 16.660       | 33.3                 |
| 4      | 39.96      | 12.439       | 980.4                | 49     | 776.74     | 16.694       | 35.0                 |
| 5      | 52.86      | 13.342       | 828.8                | 50     | 793.45     | 16.730       | 36.5                 |
| 6      | 66.59      | 14.103       | 695.4                | 51     | 810.20     | 16.767       | 37.8                 |
| 7      | 81.03      | 14.739       | 578.6                | 52     | 826.99     | 16.806       | 38.9                 |
| 8      | 96.04      | 15.265       | 476.7                | 53     | 843.81     | 16.845       | 39.9                 |
| 9      | 111.52     | 15.697       | 388.1                | 54     | 860.68     | 16.885       | 40.7                 |
| 10     | 127.40     | 16.045       | 311.5                | 55     | 877.58     | 16.926       | 41.4                 |
| 11     | 143.59     | 16.323       | 245.6                | 56     | 894.53     | 16.968       | 42.0                 |
| 12     | 160.03     | 16.540       | 189.2                | 57     | 911.52     | 17.010       | 42.5                 |
| 13     | 176.65     | 16.704       | 141.4                | 58     | 928.55     | 17.053       | 42.9                 |
| 14     | 193.42     | 16.825       | 101.0                | 59     | 945.63     | 17.096       | 43.2                 |
| 15     | 210.29     | 16.909       | 67.3                 | 60     | 962.74     | 17.139       | 43.4                 |
| 16     | 227.23     | 16.962       | 39.5                 | 61     | 979.90     | 17.183       | 43.6                 |
| 17     | 244.21     | 16.989       | 16.8                 | 62     | 997.11     | 17.226       | 43.7                 |
| 18     | 261.20     | 16.997       | -1.4                 | 63     | 1014.36    | 17.270       | 43.7                 |
| 19     | 278.19     | 16.988       | -15.7                | 64     | 1031.65    | 17.314       | 43.7                 |
| 20     | 295.17     | 16.966       | -26.6                | 65     | 1048.99    | 17.358       | 43.7                 |
| 21     | 312.12     | 16.935       | -34.6                | 66     | 1066.36    | 17.401       | 43.7                 |
| 22     | 329.04     | 16.898       | -40.1                | 67     | 1083.79    | 17.445       | 43.6                 |
| 23     | 345.92     | 16.856       | -43.5                | 68     | 1101.25    | 17.489       | 43.5                 |
| 24     | 362.75     | 16.811       | -45.1                | 69     | 1118.76    | 17.532       | 43.4                 |
| 25     | 379.54     | 16.766       | -45.3                | 70     | 1136.32    | 17.575       | 43.3                 |
| 26     | 396.28     | 16.721       | -44.2                | 71     | 1153.92    | 17.619       | 43.2                 |
| 27     | 412.98     | 16.678       | -42.1                | 72     | 1171.56    | 17.662       | 43.1                 |
| 28     | 429.64     | 16.637       | -39.2                | 73     | 1189.24    | 17.705       | 42.9                 |
| 29     | 446.26     | 16.600       | -35.7                | 74     | 1206.96    | 17.748       | 42.8                 |
| 30     | 462.84     | 16.566       | -31.8                | 75     | 1224.73    | 17.790       | 42.7                 |
| 31     | 479.39     | 16.536       | -27.5                | 76     | 1242.55    | 17.833       | 42.6                 |
| 32     | 495.92     | 16.511       | -23.0                | 77     | 1260.40    | 17.875       | 42.4                 |
| 33     | 512.42     | 16.490       | -18.4                | 78     | 1278.30    | 17.918       | 42.3                 |
| 34     | 528.90     | 16.474       | -13.8                | 79     | 1296.24    | 17.960       | 42.2                 |
| 35     | 545.37     | 16.463       | -9.2                 | 80     | 1314.22    | 18.002       | 42.0                 |
| 36     | 561.83     | 16.456       | -4.7                 | 81     | 1332.24    | 18.044       | 41.9                 |
| 37     | 578.28     | 16.453       | -0.4                 | 82     | 1350.30    | 18.086       | 41.8                 |
| 38     | 594.73     | 16.455       | 3.8                  | 83     | 1368.41    | 18.128       | 41.6                 |
| 39     | 611.19     | 16.461       | 7.8                  | 84     | 1386.56    | 18.169       | 41.5                 |
| 40     | 627.66     | 16.471       | 11.6                 | 85     | 1404.75    | 18.211       | 41.3                 |
| 41     | 644.13     | 16.484       | 15.2                 | 86     | 1422.98    | 18.252       | 41.2                 |
| 42     | 660.63     | 16.501       | 18.5                 | 87     | 1441.25    | 18.293       | 41.0                 |
| 43     | 677.14     | 16.521       | 21.5                 | 88     | 1459.57    | 18.334       | 40.9                 |
| 44     | 693.67     | 16.544       | 24.3                 | 89     | 1477.92    | 18.375       | 40.7                 |
| 90     | 1496.32    | 18.415       | 40.5                 | 140    | 2462.15    | 20.094       | 26.7                 |
| 91     | 1514.75    | 18.456       | 40.3                 | 141    | 2482.25    | 20.120       | 26.5                 |

TABLE 11.4—(Continued).

| $T, K$ | $E, \mu V$ | $S, \mu V/K$ | $dS/dT,$<br>$nV/K^2$ | $T, K$ | $E, \mu V$ | $S, \mu V/K$ | $dS/dT,$<br>$nV/K^2$ |
|--------|------------|--------------|----------------------|--------|------------|--------------|----------------------|
| 92     | 1533.23    | 18.496       | 40.2                 | 142    | 2502.39    | 20.147       | 26.3                 |
| 93     | 1551.74    | 18.536       | 40.0                 | 143    | 2522.55    | 20.173       | 26.1                 |
| 94     | 1570.30    | 18.576       | 39.7                 | 144    | 2542.73    | 20.199       | 26.0                 |
| 95     | 1588.89    | 18.615       | 39.5                 | 145    | 2562.94    | 20.225       | 25.8                 |
| 96     | 1607.53    | 18.655       | 39.3                 | 146    | 2583.18    | 20.250       | 25.6                 |
| 97     | 1626.20    | 18.694       | 39.1                 | 147    | 2603.45    | 20.276       | 25.4                 |
| 98     | 1644.92    | 18.733       | 38.8                 | 148    | 2623.73    | 20.301       | 25.3                 |
| 99     | 1663.67    | 18.772       | 38.5                 | 149    | 2644.05    | 20.327       | 25.1                 |
| 100    | 1682.46    | 18.810       | 38.3                 | 150    | 2664.39    | 20.352       | 24.9                 |
| 101    | 1701.29    | 18.848       | 38.0                 | 151    | 2684.75    | 20.376       | 24.7                 |
| 102    | 1720.16    | 18.886       | 37.7                 | 152    | 2705.14    | 20.401       | 24.6                 |
| 103    | 1739.06    | 18.924       | 37.4                 | 153    | 2725.55    | 20.426       | 24.4                 |
| 104    | 1758.00    | 18.961       | 37.1                 | 154    | 2745.99    | 20.450       | 24.2                 |
| 105    | 1776.98    | 18.998       | 36.8                 | 155    | 2766.45    | 20.474       | 24.1                 |
| 106    | 1796.00    | 19.035       | 36.5                 | 156    | 2786.94    | 20.498       | 23.9                 |
| 107    | 1815.05    | 19.071       | 36.2                 | 157    | 2807.45    | 20.522       | 23.7                 |
| 108    | 1834.14    | 19.107       | 35.8                 | 158    | 2827.98    | 20.545       | 23.5                 |
| 109    | 1853.27    | 19.143       | 35.5                 | 159    | 2848.54    | 20.569       | 23.4                 |
| 110    | 1872.43    | 19.178       | 35.2                 | 160    | 2869.12    | 20.592       | 23.2                 |
| 111    | 1891.62    | 19.213       | 34.8                 | 161    | 2889.72    | 20.615       | 23.0                 |
| 112    | 1910.85    | 19.248       | 34.5                 | 162    | 2910.35    | 20.638       | 22.8                 |
| 113    | 1930.12    | 19.282       | 34.2                 | 163    | 2931.00    | 20.661       | 22.6                 |
| 114    | 1949.42    | 19.316       | 33.8                 | 164    | 2951.67    | 20.683       | 22.5                 |
| 115    | 1968.75    | 19.350       | 33.5                 | 165    | 2972.37    | 20.706       | 22.3                 |
| 116    | 1988.12    | 19.383       | 33.2                 | 166    | 2993.08    | 20.728       | 22.1                 |
| 117    | 2007.52    | 19.416       | 32.8                 | 167    | 3013.82    | 20.750       | 21.9                 |
| 118    | 2026.95    | 19.449       | 32.5                 | 168    | 3034.58    | 20.772       | 21.7                 |
| 119    | 2046.41    | 19.481       | 32.2                 | 169    | 3055.37    | 20.793       | 21.5                 |
| 120    | 2065.91    | 19.513       | 31.8                 | 170    | 3076.17    | 20.815       | 21.3                 |
| 121    | 2085.44    | 19.545       | 31.5                 | 171    | 3096.99    | 20.836       | 21.1                 |
| 122    | 2105.00    | 19.576       | 31.2                 | 172    | 3117.84    | 20.857       | 21.0                 |
| 123    | 2124.59    | 19.607       | 30.9                 | 173    | 3138.71    | 20.878       | 20.8                 |
| 124    | 2144.21    | 19.638       | 30.6                 | 174    | 3159.60    | 20.899       | 20.6                 |
| 125    | 2163.87    | 19.668       | 30.3                 | 175    | 3180.51    | 20.919       | 20.4                 |
| 126    | 2183.55    | 19.698       | 30.0                 | 176    | 3201.44    | 20.939       | 20.2                 |
| 127    | 2203.26    | 19.728       | 29.7                 | 177    | 3222.38    | 20.960       | 20.1                 |
| 128    | 2223.00    | 19.758       | 29.4                 | 178    | 3243.35    | 20.980       | 19.9                 |
| 129    | 2242.78    | 19.787       | 29.2                 | 179    | 3264.34    | 20.999       | 19.7                 |
| 130    | 2262.58    | 19.816       | 28.9                 | 180    | 3285.35    | 21.019       | 19.6                 |
| 131    | 2282.41    | 19.845       | 28.7                 | 181    | 3306.38    | 21.038       | 19.4                 |
| 132    | 2302.27    | 19.873       | 28.4                 | 182    | 3327.43    | 21.058       | 19.2                 |
| 133    | 2322.16    | 19.902       | 28.2                 | 183    | 3348.50    | 21.077       | 19.1                 |
| 134    | 2342.07    | 19.930       | 28.0                 | 184    | 3369.58    | 21.096       | 18.9                 |
| 135    | 2362.02    | 19.958       | 27.7                 | 185    | 3390.69    | 21.115       | 18.8                 |
| 136    | 2381.99    | 19.985       | 27.5                 | 186    | 3411.81    | 21.133       | 18.6                 |
| 137    | 2401.99    | 20.013       | 27.3                 | 187    | 3432.96    | 21.152       | 18.5                 |
| 138    | 2422.01    | 20.040       | 27.1                 | 188    | 3454.12    | 21.171       | 18.4                 |
| 139    | 2442.07    | 20.067       | 26.9                 | 189    | 3475.30    | 21.189       | 18.3                 |

TABLE 11.4—(Continued).

| $T, K$ | $E, \mu V$ | $S, \mu V/K$ | $dS/dT,$<br>$nV/K^2$ | $T, K$ | $E, \mu V$ | $S, \mu V/K$ | $dS/dT,$<br>$nV/K^2$ |
|--------|------------|--------------|----------------------|--------|------------|--------------|----------------------|
| 190    | 3496.49    | 21.207       | 18.1                 | 235    | 4467.28    | 21.881       | 10.3                 |
| 191    | 3517.71    | 21.225       | 18.0                 | 236    | 4489.17    | 21.891       | 10.1                 |
| 192    | 3538.94    | 21.243       | 17.9                 | 237    | 4511.06    | 21.901       | 9.9                  |
| 193    | 3560.20    | 21.261       | 17.8                 | 238    | 4532.97    | 21.911       | 9.8                  |
| 194    | 3581.47    | 21.279       | 17.7                 | 239    | 4554.88    | 21.921       | 9.6                  |
| 195    | 3602.75    | 21.296       | 17.6                 | 240    | 4576.81    | 21.930       | 9.5                  |
| 196    | 3624.06    | 21.314       | 17.5                 | 241    | 4598.74    | 21.940       | 9.4                  |
| 197    | 3645.38    | 21.331       | 17.4                 | 242    | 4620.69    | 21.949       | 9.3                  |
| 198    | 3666.72    | 21.348       | 17.3                 | 243    | 4642.64    | 21.958       | 9.3                  |
| 199    | 3688.08    | 21.366       | 17.2                 | 244    | 4664.61    | 21.968       | 9.2                  |
| 200    | 3709.45    | 21.383       | 17.1                 | 245    | 4686.58    | 21.977       | 9.2                  |
| 201    | 3730.84    | 21.400       | 17.0                 | 246    | 4708.56    | 21.986       | 9.3                  |
| 202    | 3752.25    | 21.417       | 16.9                 | 247    | 4730.55    | 21.995       | 9.3                  |
| 203    | 3773.68    | 21.434       | 16.8                 | 248    | 4752.55    | 22.005       | 9.4                  |
| 204    | 3795.12    | 21.450       | 16.7                 | 249    | 4774.56    | 22.014       | 9.5                  |
| 205    | 3816.58    | 21.467       | 16.5                 | 250    | 4796.58    | 22.024       | 9.6                  |
| 206    | 3838.05    | 21.483       | 16.4                 | 251    | 4818.61    | 22.034       | 9.8                  |
| 207    | 3859.54    | 21.500       | 16.3                 | 252    | 4840.64    | 22.043       | 10.0                 |
| 208    | 3881.05    | 21.516       | 16.2                 | 253    | 4862.69    | 22.053       | 10.2                 |
| 209    | 3902.58    | 21.532       | 16.0                 | 254    | 4884.75    | 22.064       | 10.3                 |
| 210    | 3924.12    | 21.548       | 15.9                 | 255    | 4906.82    | 22.074       | 10.6                 |
| 211    | 3945.67    | 21.564       | 15.8                 | 256    | 4928.90    | 22.085       | 10.8                 |
| 212    | 3967.24    | 21.580       | 15.6                 | 257    | 4950.99    | 22.096       | 11.0                 |
| 213    | 3988.83    | 21.595       | 15.4                 | 258    | 4973.09    | 22.107       | 11.1                 |
| 214    | 4010.43    | 21.610       | 15.3                 | 259    | 4995.20    | 22.118       | 11.3                 |
| 215    | 4032.05    | 21.626       | 15.1                 | 260    | 5017.33    | 22.129       | 11.5                 |
| 216    | 4053.69    | 21.641       | 14.9                 | 261    | 5039.46    | 22.141       | 11.6                 |
| 217    | 4075.33    | 21.655       | 14.7                 | 262    | 5061.61    | 22.152       | 11.6                 |
| 218    | 4097.00    | 21.670       | 14.5                 | 263    | 5083.77    | 22.164       | 11.7                 |
| 219    | 4118.67    | 21.684       | 14.3                 | 264    | 5105.94    | 22.176       | 11.6                 |
| 220    | 4140.36    | 21.698       | 14.0                 | 265    | 5128.12    | 22.187       | 11.5                 |
| 221    | 4162.07    | 21.712       | 13.8                 | 266    | 5150.31    | 22.199       | 11.3                 |
| 222    | 4183.79    | 21.726       | 13.6                 | 267    | 5172.52    | 22.210       | 11.1                 |
| 223    | 4205.52    | 21.739       | 13.3                 | 268    | 5194.73    | 22.221       | 10.7                 |
| 224    | 4227.27    | 21.753       | 13.1                 | 269    | 5216.96    | 22.231       | 10.3                 |
| 225    | 4249.03    | 21.766       | 12.8                 | 270    | 5239.19    | 22.241       | 9.7                  |
| 226    | 4270.80    | 21.778       | 12.5                 | 271    | 5261.44    | 22.251       | 9.0                  |
| 227    | 4292.58    | 21.791       | 12.3                 | 272    | 5283.70    | 22.259       | 8.2                  |
| 228    | 4314.38    | 21.803       | 12.0                 | 273    | 5305.96    | 22.267       | 7.3                  |
| 229    | 4336.19    | 21.815       | 11.8                 | 274    | 5328.23    | 22.274       | 6.3                  |
| 230    | 4358.01    | 21.826       | 11.5                 | 275    | 5350.51    | 22.280       | 5.2                  |
| 231    | 4379.84    | 21.838       | 11.3                 | 276    | 5372.79    | 22.284       | 4.0                  |
| 232    | 4401.68    | 21.849       | 11.0                 | 277    | 5395.08    | 22.288       | 2.7                  |
| 233    | 4423.54    | 21.860       | 10.8                 | 278    | 5417.36    | 22.290       | 1.3                  |
| 234    | 4445.40    | 21.870       | 10.5                 | 279    | 5439.65    | 22.290       | -0.1                 |

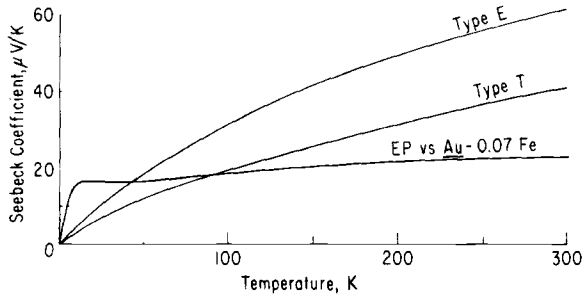


FIG. 11.1—Seebeck coefficients for Types E, T, and EP versus Au-0.07 Fe.

#### 11.4 References

- [1] Scott, R. B., *Cryogenic Engineering*. Van Nostrand, Princeton, N.J., 1959.
- [2] Hust, J. G., Powell, R. L., and Sparks, L. L., "Methods for Cryogenic Thermocouple Thermometry," *Temperature, Its Measurement and Control in Science and Industry*, Part 3, Vol. 4, 1972, p. 1525.
- [3] White, G. K., *Experimental Techniques in Low Temperature Physics*. Oxford University Press, London, 1959.
- [4] Rose-Innes, A. C., *Low Temperature Techniques*. Van Nostrand, Princeton, N.J., 1964.
- [5] Sparks, L. L., Powell, R. L., and Hall, W. J., "Reference Tables for Low-Temperature Thermocouples," NBS Monograph 124, National Bureau of Standards, 1972.
- [6] Sparks, L. L. and Powell, R. L., "Low Temperature Thermocouples: KP, "Normal" Silver, and Copper Versus Au-0.02 at % Fe and Au-0.07 at % Fe," *Journal of Research*. National Bureau of Standards, Vol. 76A, No. 3, May-June 1972.

# Chapter 12—Temperature Measurement Uncertainty

---

## 12.1 The General Problem

Every measurement has associated with it an error. This is a real certain value which really exists but cannot be known. It is different from the uncertainty of the measurement, which reflects only our understanding of the error. This chapter will deal primarily with the uncertainty.

An error may be caused by a mistake or by a broken instrument as well as by the usual variation in parameters affecting the temperature measurement. A mistake, like connecting a Type E thermocouple to a Type K instrument or using a broken instrument, in which perhaps a reference diode has failed, is regrettable but cannot be analyzed by usual statistical methods. Hence, these events are not treated herein.

Aside from mistakes and broken instruments, errors due to imprecision are apparent in a simple example: Suppose you want to heat a pot of water to 135°F. You insert a proper thermocouple and take a reading. If you take another reading, they will not be the same unless your experimental technique is too poor to resolve the difference. If you further check with another thermocouple or at a different point in the pot, or call an assistant to check you, or try another instrument, you probably will get as many different answers as the number of measurements made. This variation is to be expected—it reflects the uncertainty of the measurement. It may not present a problem. If you just want the water to wash your dishes, and will be happy with any temperature 125 to 145°F you probably need read no further. But if you are using this as a reagent where  $\pm 0.5$  degree is important, you need to estimate the error, and you need to know how well you know the error.

As in all statistical analysis, the credibility of the work is enhanced by its success in predicting. When the analyst predicts a variability which is grossly different from that observed in a test, his judgment is flawed. Either his model or his analysis is wrong. Statistics do not lie, but they can be misleading by misapplication or by intent.

In the discussion which follows, no attempt will be made to teach statistics. This topic has been covered more than adequately by Benedict [1],<sup>1</sup> Chatfield [2], Spiegel [3], Abernethy [4], and the ASTM Committee E-11 on Statistical Techniques [5]. Certain terms developed by these authors are redefined for

<sup>1</sup>The italic numbers in brackets refer to the list of references appended to this paper.



convenience in paragraph 12.2 in the context of temperature measurements, and examples of their use are given in paragraph 12.3. The reader who wants to apply these tools will probably need to study some of the references if he is not familiar with their use.

## 12.2 Tools of the Trade

The language of measurement uncertainty is largely the language of statistics, and, like statistics, it is often misunderstood. Statistical words are very precise in their meaning, like legal terms, and he who uses them carelessly does so not only at his own risk but also at that of the reader. For convenience, the following terms are defined here in the context of thermocouple measurements.

### 12.2.1 Average and Mean

*Average* and *mean* are synonymous and are best defined by the equation

$$\text{average } X = \Sigma x_i/n, \text{ denoted } \bar{X}$$

where  $n$  is the number of measurements  $X_i$ . The definition " $\bar{X} = (X_{\max} + X_{\min})/2$ ," though commonly used in other applications, has no place in measurement uncertainty. The symbol  $\bar{X}$  is used for the average of a set of measurements;  $\mu$  is the average of the total population.

The term *across* is introduced at this point. Like many statistical terms, an average is always across a specific group of data. The average across a series of readings (subset) will differ from the average across another subset, and from the average of the total population, which is seldom known. We must always know what we are averaging across.

### 12.2.2 Normal or Gaussian Distribution

*Normal* or *Gaussian distribution* is defined by the formula

$$f(x) = \frac{1}{\sigma\sqrt{2\pi}} e^{-1/2(x-\mu)^2/\sigma^2}$$

where  $\sigma$  is the standard deviation of the total population. In the analysis of measurement uncertainty, this formula is seldom used directly, but it defines the dispersion that usually exists in real physical data. The careful investigator will always check the normality of his test data before applying normal statistics to it. A visual check is often sufficient, especially with the aid of probability-plot paper (See 12.3.4).

### 12.2.3 Standard Deviation and Variance

The *standard deviation* and *variance* are measures of the precision or scatter of normally distributed data, that is, the extent to which such data departs from the mean. The variance is the sum of the squares of the deviations of the individual measurements from the mean, divided by the degrees of freedom. The standard deviation is the square root of the variance. An estimate of the standard deviation is  $s$  defined as

$$s = \sqrt{\frac{\Sigma(X_i - \bar{X})^2}{n - 1}}$$

Obviously, the variance,  $s^2$ , is the same equation without the radical. The impact of moderately priced personal calculators on these evaluations is clear. Statistical calculations can be performed easily which would probably be too tedious to perform longhand.

### 12.2.4 Bias, Precision, and Uncertainty

*Bias*, *precision*, and *uncertainty* are the key terms for describing defects in measurement, confusing at times because of careless use. *Precision* is the scatter, usually random, between measurements in the same set. *Bias* is the systematic difference between the means of two or more sets. *Uncertainty* is a less rigorous term which tries to combine bias and precision into a single term for talking purposes. One definition, by Abernethy [4], is  $\pm(b + t_{95}s)$ , where  $b$  is the best estimate of the limit of uncorrected bias,  $s$  is the precision, and  $t_{95}$  is the 95<sup>th</sup> percentile value of the two tailed Student t distribution. In words, it is the largest error which can reasonably be expected. An important rule is that an uncertainty statement is never made without including: (1) bias, (2) precision, (3) degrees of freedom, and (4) confidence interval. The opportunity for confusion lies in the fact that a component of uncertainty can move between bias and precision depending on the uncertainty being assessed; for example, the bias between reels of thermocouple wire becomes reel-to-reel precision when evaluating the uncertainty of K thermocouple measurements in general. The extent to which it can be "corrected out" of the uncertainty of the smaller set depends on the extent of calibration activities. The importance of identifying the restraints of the uncertainty statement is evident.

*Degrees of freedom* (df) is a term which is used in many of the equations of uncertainty, and relates to the size of the data sample on which the calculation is based. Chatfield [2] defines it as the number of independent comparisons available. For example in the formula for the average,  $df = n$ . In the formula for standard deviation it is  $(n - 1)$ , since there is only one difference between two values, one degree of freedom is lost. Similarly the con-

stands in a regression equation each consume one degree of freedom as shown in paragraph 12.3.5.

### 12.2.5 Precision of the Mean

The *precision of the mean* is an important concept in temperature measurement. As the number of independent measurements of the same temperature is increased, the uncertainty of our knowledge of the true mean decreases, specifically by the square root of the number of measurements.

$$s_{\text{mean}} = \frac{s}{\sqrt{n}}$$

where  $n$  is the number of independent measurements. This can be applied to the time average, space average, production norm, or to any other set. For discussion see paragraph 12.3.3.

### 12.2.6 Regression Line or Least-Square Line

A *regression line* or *least-squares line* represents the equation which minimizes the sum of the squares of the displacements of the individual data points in a set from the line. The line may be a straight line or a polynomial, exponential, or any other form.

## 12.3 Typical Applications

### 12.3.1 General Considerations

The discussions herein will be confined to Type K, because of the availability of a statistically significant quantity of data for this thermocouple type. The same statistical concepts can be applied to other types.

ANSI/ASTM E 230 describes the temperature-emf characteristics of Type K wire. The "limits of error" stated in this standard are definitive, not statistical. Wire which does not conform to the stated limits is simply not Type K. Further, the limits of error are defined as referring only to new wire as delivered, and not to include the effects of insulating, sheathing, or exposure to operating conditions of the application. The statistical treatment discussed herein is, in a large part, similarly limited.

Topics to be discussed include: (1) the improvement in uncertainty which can be realized, especially at low temperatures, by calibration; (2) the use of the precision of the mean of several thermocouples; (3) probability plots; and (4) the use of regression analysis to eliminate variations for cause from random variations.

### 12.3.2 Wire Calibration

The Type K temperature-emf relationship, described by algorithm in NBS MN 125 [6], and tables presented in NBS 125 and ASTM E 230, are the results of empirical data developed by NBS from experimental data on real Type K thermocouples from several sources and including several sizes of wire. In other words, these documents present statistical information believed to represent the typical Type K thermocouple. Whether or not the deviations of the individual thermocouples tested from the algorithm were normally distributed is not known. We also do not know the scatter of these data about the K-curve.

Sanders [7] presents observations on incoming inspection calibrations performed by a large user of 20-28 B&S gage Type K wire with "soft" insulation. A small quantity of sheathed wire was considered separately. An analysis of variance was made to assess the effect of various insulations, cable makeup, vendors, and wire gages on the precision or bias of the calibration. The only significant influence was that of wire gage. The data are shown in Table 12.1. Precision is stated as two-standard deviations.

From these data it is clear that, first, the typical wire received by this user is systematically different from the K-curve as shown in Fig. 12.1, probably because of the difference in the range of sizes tested by the National Bureau of Standards (NBS) and this user. Thus, if he plans to use thermocouples made from this wire without further calibration, he would be advised to modify the K-curve by the bias curve of Table 12.1. Secondly, if he uses this modified curve, he can expect that such couples individually will vary from

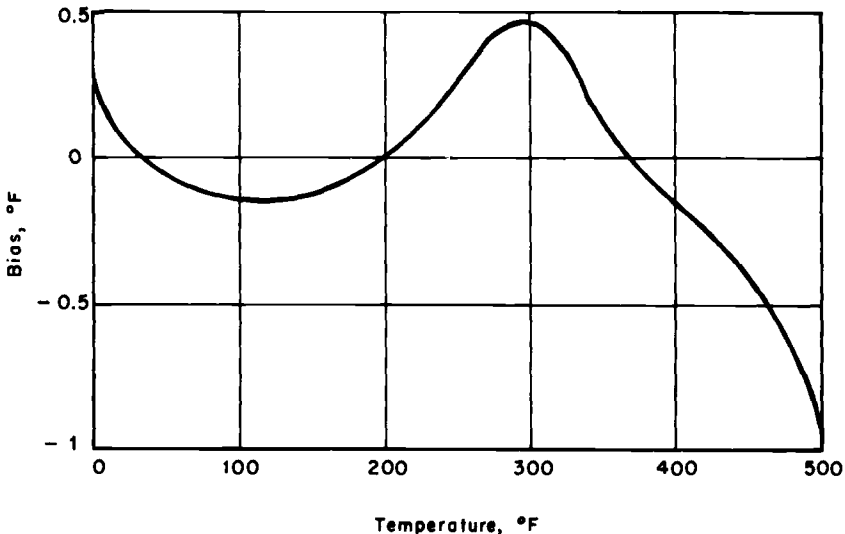


FIG. 12.1—Bias of a typical Type K wire.

TABLE 12.1—Accuracy of unsheathed thermocouples.

| Temperature °F,<br>T | Bias °F,<br>b | Overall<br>Precision °F,<br>$t_{95}$ | In-Reel<br>Precision °F,<br>$t_{95}$ | Uncertainty °F,<br>U |
|----------------------|---------------|--------------------------------------|--------------------------------------|----------------------|
| 0                    | 0.28          | ±0.09                                | ±0.08                                | 0.37                 |
| 32                   | 0.00          | ±0.06                                | ±0.06                                | 0.06                 |
| 65                   | -0.16         | ±0.18                                | ±0.06                                | 0.34                 |
| 100                  | -0.14         | ±0.29                                | ±0.08                                | 0.43                 |
| 150                  | -0.10         | ±0.51                                | ±0.11                                | 0.61                 |
| 200                  | 0.00          | ±0.68                                | ±0.11                                | 0.68                 |
| 250                  | 0.26          | ±0.96                                | ±0.15                                | 1.22                 |
| 300                  | 0.47          | ±0.09                                | ±0.18                                | 1.56                 |
| 350                  | 0.13          | ±1.30                                | ±0.20                                | 1.43                 |
| 400                  | -0.15         | ±1.40                                | ±0.24                                | 1.55                 |
| 450                  | -0.41         | ±1.48                                | ±0.28                                | 1.89                 |
| 500                  | -0.91         | ±1.33                                | ±0.38                                | 2.24                 |

the curve by the precision shown in the table, which is substantially less than the  $\pm 2$  deg permitted by ASTM E 230. If he does not correct for the bias, he can expect the true value to lie between the bounds of total uncertainty listed in the table, which is slightly in excess of the specification.

Sanders further concludes that the reel-to-reel precision, as expected, is worse than the precision within a reel; that is, that thermocouples whose readings are to be compared should be made, if possible, from the same reel of wire, especially if individual calibrations are not performed. If a piece of thermocouple wire is calibrated and then the junction is cut off in order to fabricate a probe, the calibration will be valid within 0.05°F for that probe if the new junction is within a few inches of the calibration junction. If it is more than a few inches away, the full in-reel precision will be developed. Similar calibration data for a limited sample of sheathed wire are given in Table 12.2, for comparison only.

The material discussed in the previous table represents a large, but specific, subset of small gage Type K wire below 500°F. Similar tests on a different data subset should be expected to vary to some extent, depending upon sample and measurement differences. However, the basic conclusions should hold, that the uncertainty can be reduced by batch calibration and further reduced by specific calibrations.

### 12.3.3 Means and Profiles

In all areas of human knowledge, iteration is one of the most respected ways to stress or reinforce impressions. If you are surprised at what you see, you take a second look. If you want to be sure what time your plane leaves, you check again. If you want confidence in the results of an experiment, you repeat it. It is then not surprising that the mean of several readings of a

TABLE 12.2—Accuracy of sheathed thermocouples.

| Temperature °F,<br>T | Bias °F,<br>b | Overall<br>Precision °F,<br>$t_{95S}$ | In-Reel<br>Precision °F,<br>$t_{95S}$ | Uncertainty °F,<br>U |
|----------------------|---------------|---------------------------------------|---------------------------------------|----------------------|
| 100                  | -0.13         | ±0.37                                 | ±0.10                                 | 0.50                 |
| 150                  | +0.01         | ±0.50                                 | ±0.14                                 | 0.51                 |
| 200                  | +0.35         | ±0.70                                 | ±0.30                                 | 1.05                 |
| 250                  | +0.82         | ±1.12                                 | ±0.42                                 | 1.94                 |
| 300                  | +1.09         | ±1.36                                 | ±0.52                                 | 2.45                 |
| 350                  | +0.78         | ±1.45                                 | ±0.61                                 | 2.23                 |
| 400                  | +0.65         | ±1.51                                 | ±0.68                                 | 2.16                 |
| 450                  | +0.74         | ±1.57                                 | ±0.90                                 | 2.31                 |
| 500                  | +0.69         | ±1.40                                 | ±0.96                                 | 2.09                 |

temperature, or of the readings of several sensors, or of the temperature-emf characteristics of a pair of alloy ingots lends more confidence than a single reading. Statistics provides the means to quantify this increase in confidence. Like all statistical tools, it must be properly used.

In the development of a turbine engine, the gas temperature at a particular axial section may be measured by one hundred or more sensors. For component efficiency studies the mean temperature at this section is a needed parameter. To assess incremental improvement in performance, the accuracy of this temperature can be quite critical. When a single probe is used, several error components exist. First, and usually dominant, is the temperature variation in space and time at different points across the section. Another error component is the degree to which the kinetic energy of the gas stream is not converted to junction temperature (aerodynamic recovery) (see 9.1.4). Others include manufacturing tolerances, conduction errors, and wire calibration. The latter is usually corrected out.

If we use 100 sensors the space profile, the manufacturing tolerances and the random errors in calibrating are reduced by  $\sqrt{n} = 10$ . Now when we compare the mean temperature before and after a change in configuration, the minimum significant change in performance is reduced by an order of magnitude. Note that the same improvement does not apply to the individual measurements in the set.

Further information may be derived from the same data for different purposes. The performance of the engine may be affected by the uniformity of the gas temperature, which is quantified by the standard deviation of the individual temperatures. This will also predict the maximum temperatures, which will affect the life of metal parts. A check of the normality of the data may show that a pattern exists.

It is important to realize the significance of the precision of the mean. It does us no good to improve the precision of measurement of the mean unless the mean is what we are going to use. For example, in calibration we fre-

quently use an array of thermocouples to establish the degree of uniformity of temperatures of a liquid bath in which we will calibrate thermocouples. We can use the standard deviation of the measurements as a measure of uniformity, but we cannot claim knowledge of the local bath temperature to within the precision of the mean. Specifically

$$T_i = \bar{T} \pm ts, \text{ not } \bar{T} \pm ts/\sqrt{n}$$

where

- $T_i$  = local temperature at the location of the test sensor,
- $\bar{T}$  = mean of temperature measurements,
- $s$  = standard deviation of temperature measurements, and
- $t$  = Student's  $t$ .

#### 12.3.4 Probability Paper

Paragraph 12.2.2 refers to the normality of data and the need to assure yourself that data are normally distributed before applying the mathematics of classical statistics. Actually, the determination of this property can directly answer some questions and lead to accuracy improvement.

The normal or Gaussian distribution, plotted as error versus frequency of occurrence, yields the familiar "bell-shaped" curve. The integral of this curve, plotting error versus cumulative frequency, is an ogive. If the frequency axis of the ogive is properly warped, a special "probability paper" is created, on which normally distributed data are plotted as a straight line or "prob-plot" which is easily evaluated as to its straightness. Figure 12.2 reproduces this probability plot, which is commercially available from several sources. King [8], describes the mechanics of using this paper.

When the data are properly ranked and plotted on prob-plot paper, the nature of existing nonnormalities is often revealed. Data which are skewed to the left or right will plot concave upward or downward, respectively. One of the more common revelations is that the data are bimodal or polymodal. Such data will appear as a series of line segments of different slopes. This indicates that the data come from more than one subset, having different standard deviations or means or both. Data which are flatter or more peaked will yield plots which are similar to polymodal.

Figure 12.3 shows a straight line of finite slope, terminated at the top by a segment of zero slope. In real data the transition may be less sharp. Let us look at what we can conclude from this plot. First, unless there is an *a priori* reason to expect nonnormal temperature distribution, the highest temperatures which occurred were not measured.

If the data were taken from 1000 thermocouples in an engine or furnace, the mean temperature is shown to be 2500 deg (the 50th percentile), and there should have been 10 readings in excess of 2900 and one in excess of

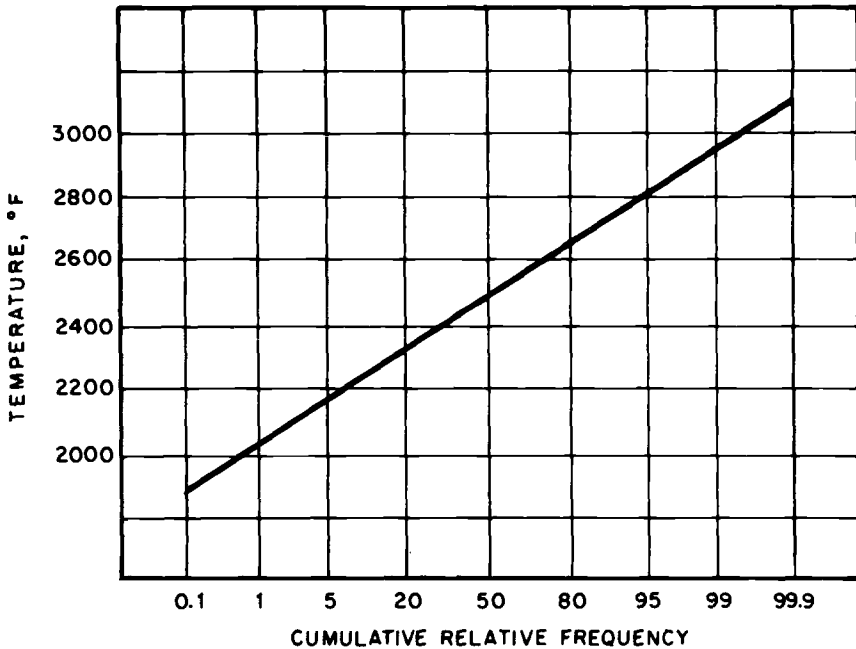


FIG. 12.2—Typical probability plot.

3000. Perhaps some of them burned out (truncation). Perhaps the experimenter thought he had reason to doubt any readings as high as 2900 (editing or false outlier rejection). Or perhaps there were no thermocouples located at the hottest spots (sampling error). But the evidence is clear, the probability of existence of temperatures above 3000 is high and cannot be rejected lightly. If the data are taken from 1000 successive readings of a single thermocouple, the reasoning is the same and the conclusions equally valid in the time domain. You do not have to have seen a temperature in excess of 3000 to have good reason to believe it occurred.

### 12.3.5 Regression Analyses

Regression analysis is used statistically to express a set of data in an analytical relationship. This relationship can be used to predict values of the dependent variable at values of the independent variable between those for which test data exists. The expression can be also used to smooth the curve of test data, based on physical knowledge beyond the mere statistics, for example, we may know from physical facts that the true relation is linear, polynomial, or exponential, and need only to determine a few constants to define it. Redundant data points beyond the number of constants to be de-



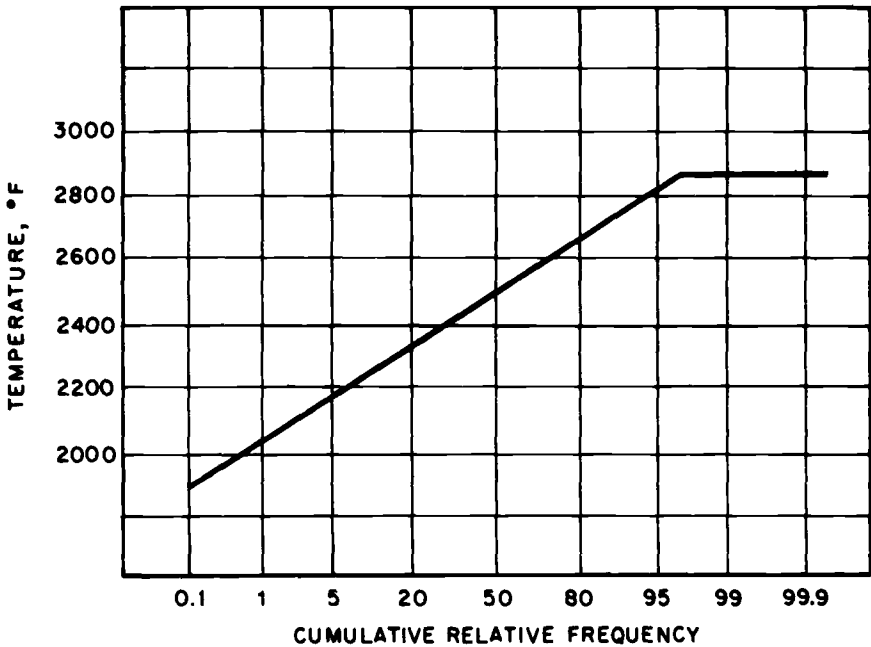


FIG. 12.3—Typical probability plot—truncated data.

rived are required to provide degrees of freedom in order to establish confidence in the constants. This confidence is an expression of the “goodness of fit” of the curve and is called the standard error of estimate (SEE) expressed by

$$SEE = \sqrt{\frac{\sum(Y_i - Y_{ci})^2}{n - (1 + q)}}$$

where

$Y_{ci}$  = predicted value of  $Y_i = f(X_i)$ ,

$Y_i$  = measured value of  $Y_i$  at  $X_i$ ,

$n$  = number of data points, and

$q$  = order of the derived equation.

The same SEE is used to assess the scatter of the data points around the curve. Obviously, if the scatter of the original data is large, this fact will be reflected in a large SEE of the curve, which implies a large uncertainty in the constants. Conversely, experimental data closely grouped around a simple, well-defined regression curve will produce a low value of SEE which indicates the precision of both the coefficients and the test data.

Care must be taken to avoid over fitting a curve to experimental data. Most physical relationships can be expressed with relatively few constants, for example, a low order polynomial. Any set of data, on the other hand, can be well described by a polynomial with a number of constants equal to the number of data points. Such a fit will generally be meaningless. The SEE will have increased because of the decrease in the degrees of freedom (denominator), and the equation will perfectly describe what you already know, while becoming worthless to predict interpolated or extrapolated values. A very interesting account of the regression of the temperature- $\epsilon$ m tables is given in NBS-125 [6] and the references contained therein. In this unusual case the large quantity of data (degrees of freedom) permits regression to as much as a 14th order equation to reduce the SEE to the order of one microvolt, while retaining sufficient degrees of freedom.

Regression analysis is one of several techniques which can be used to identify a causal relationship between two variables. Other techniques such as correlation and analysis of variance (ANOVA) are somewhat more sophisticated and are discussed by Chatfield [2].

Thermocouples often are accused of drifting with time in use. If we have a series of data points representing time versus error determined by reference to noble metal thermocouples, resistance thermometer, optical pyrometer, or other alternate technique, there will be a data scatter for one or more experimental reasons between the points. One way to decide whether the error is a linear function of time is to determine the coefficients of a linear regression of the data. If there is no linear relationship, the SEE will approximate the standard deviation; if the points all fall on a straight line, it will be zero.

## 12.4 References

- [1] Benedict, R. P., *Fundamentals of Temperature, Pressure, and Flow Measurements*, 2nd edition, Wiley, New York, 1977, Chapter 10.
- [2] Chatfield, C., *Statistics for Technology*, Wiley, New York, 1978.
- [3] Spiegel, M. R., *Theory and Problems of Statistics*, Scham's Outline Series, McGraw-Hill, New York, 1961.
- [4] Abernethy, R. B. et al, "Uncertainty in Gas Turbine Measurements," Revised 1980, Instrument Society of America, 1483-3.
- [5] "ASTM Standards on Precision and Accuracy for Various Applications," American Society for Testing and Materials, 1977.
- [6] Powell, R. L. et al, "Thermocouple Reference Tables Based on the IPTS-68," National Bureau of Standards MN-125, Department of Commerce, Washington, D.C., 1974.
- [7] Sanders, D. G., "Accuracy of Type K Thermocouples Below 500°: A Statistical Analysis," *Transactions*, Vol. 1, No. 4, Instrument Society of America, 1974.
- [8] King, J. R., "Probability Charts for Decision Making," Industrial Press, Inc., New York, 1971.
- [9] Ku, H. H., Ed., "Precision Measurement and Calibration: Statistical Concepts and Procedures," *NBS Special Publication 300*, Vol. 1, U.S. Government Printing Offices, 1969. (Paper 5.2 Statistical Concepts in Metrology).

## Chapter 13—Terminology

---

**calibrate**, *v.*: 1. *general*—to determine the indication or output of a measuring device with respect to that of a standard.

2. *thermocouple*—to determine the emf developed by a thermocouple with respect to temperature established by a standard.

**calibration point**, *n.*: 1. *general*—a specific value, established by a standard, at which the indication or output of a measuring device is determined.

2. *thermocouple*—a temperature, established by a standard, at which the emf developed by a thermocouple is determined.

**Celsius**, *n.*—the designation of the degree on the International Practical Temperature Scale. Also used for the name of the Scale, as “Celsius temperature scale.” Formerly (prior to 1948) called “centigrade.”

**centigrade**, *n.*—the designation of the degree on the International Temperature Scale prior to 1948. (See *Celsius*.)

**coaxial thermocouple element**, *n.*—a thermocouple element consisting of a thermoelement in wire form, within a thermoelement in tube form with the two thermoelements insulated from each other and from the tube except at the measuring junction.

**connection head**, *n.*—a housing enclosing a terminal block for an electrical temperature-sensing device and usually provided with threaded openings for attachment to a protecting tube and for attachment of conduit.

**defining fixed points**, *n.*—the reproducible temperatures upon which the International Practical Temperature Scale is based.

**degree**, *n.*—the unit of a temperature scale. See Celsius, centigrade, Fahrenheit.

**electromotive force (emf)**, *n.*—the electrical potential difference which produces or tends to produce an electric current.

**extension wire**, *n.*—a pair of wires having such temperature-emf characteristics relative to the thermocouple with which the wires are intended to be used that, when properly connected to the thermocouple, the reference junction is transferred to the other end of the wires.

**Fahrenheit**, *n.*—the designation of the degree and the temperature scale used commonly in public life and engineering circles in English-speaking countries. Related to the International Practical Temperature Scale by means of the equation

$$t_F = 9/5 t_C + 32$$

**fixed point**, *n.*—a reproducible temperature of equilibrium between different phases of a material. (See *defining fixed points* and *secondary reference points*.)

**freezing point**, *n.*—the fixed point between the solid and liquid phases of a material when approached from the liquid phase under a pressure of 1 standard atm (101325 N/m<sup>2</sup>). For a pure material this is also the melting point.

**ice point**, *n.*—the fixed point between ice and air-saturated water under a pressure of 1 standard atm (101325 N/m<sup>2</sup>). This temperature is 0°C on the International Practical Temperature Scale.

**International Practical Temperature Scale of 1948 (IPTS-48)**, *n.*—the temperature scale adopted by the 11th General Conference on Weights and Measures in 1960. Replaced in 1968 by the International Practical Temperature Scale of 1968.

**International Practical Temperature Scale of 1968 (IPTS-68)**, *n.*—the temperature scale, which through adoption by the 13th General Conference on Weights and Measures in 1968, is defined in terms of fixed and reproducible equilibrium temperatures (defining fixed points) to which numerical values have been assigned, and equations establishing the relation

- between temperature and the indications of sensing instruments calibrated by means of the values assigned to the defining fixed points.
- kelvin**, *n.*—the designation of the thermodynamic temperature scale and the interval on this scale. This kelvin scale was defined by the Tenth General Conference on Weights and Measures in 1954 by assigning the temperature of 273.16 K to the triple point of water. Also the interval on the International Practical Kelvin Temperature Scale.
- liquid-in-glass thermometer**, *n.*—a temperature-measuring instrument whose indications are based on the temperature coefficient of expansion of a liquid relative to that of its containing glass envelope.
- lower range-value**, *n.*—the lowest quantity that an instrument is adjusted to measure.
- measuring junction**, *n.*—that junction of a thermocouple which is subjected to the temperature to be measured.
- melting point**, *n.*—the fixed point between the solid and liquid phases of a material when approached from the solid phase under a pressure of 1 standard atm (101325 N/m<sup>2</sup>). For a pure material this is also the freezing point.
- Peltier coefficient**, *n.*—the reversible heat which is absorbed or evolved at a thermocouple junction when unit current passes in unit time. Synonymous with *Peltier emf*.
- Peltier emf**, *n.*—synonymous with *Peltier coefficient*.
- platinum 27 (Pt-27)**, *n.*—the platinum standard to which the National Bureau of Standards referred thermoelectric measurements prior to 1973.
- platinum 67 (Pt-67)**, *n.*—the platinum standard used by the National Bureau of Standards after 1972 as the reference to which thermoelectric measurements are referred.
- potentiometer, Group A**, *n.*—a laboratory high-precision type potentiometer having limits of error of approximately 0.2  $\mu$ V at 1000  $\mu$ V, and 5  $\mu$ V or less at 50 000  $\mu$ V.
- potentiometer, Group B**, *n.*—a laboratory precision type potentiometer having limits of error of approximately 1  $\mu$ V at 1000  $\mu$ V and 12  $\mu$ V or less at 50 000  $\mu$ V.
- primary standard thermocouple**, *n.*—a thermocouple that has had its temperature-emf relationship determined in accordance with methods described in the text establishing the International Practical Temperature Scale.
- protecting tube**, *n.*—a tube designed to enclose a temperature-sensing device and protect it from the deleterious effects of the environment. It may provide for attachment to a connection head but is not primarily designed for pressure-tight attachment to a vessel.
- range**, *n.*—the region between the limits within which a quantity is measured. It is expressed by stating the lower and upper range-values.
- reference junction**, *n.*—that junction of a thermocouple which is at a known temperature.
- refractory metal thermocouple**, *n.*—a thermocouple whose thermoelements have melting points above that of 60 percent platinum-40 percent rhodium, 1935°C (3515°F).
- resistance, insulation (sheathed thermocouple wire)**, *n.*—the measured resistance between wires or between wires and sheath multiplied by the length of the wire expressed in megohms (or ohms) per foot (or meter) of length. (NOTE: The resistance varies inversely with the length.)
- secondary reference points**, *n.*—reproducible temperatures (other than the *defining fixed points*) listed in the text establishing the International Practical Temperature Scale as being useful for calibration purposes.
- secondary standard thermocouple**, *n.*—a thermocouple that has had its temperature-emf relationship determined by reference to a primary standard of temperature.
- Seebeck coefficient**, *n.*—the rate of change of thermal emf with temperature at a given temperature. Normally expressed as emf per unit of temperature. Synonymous with *thermoelectric power*.
- Seebeck emf**, *n.*—the net emf set up in a thermocouple under condition of zero current. It represents the algebraic sum of the Peltier and Thomson emf. Synonymous with *thermal emf*.
- sheathed thermocouple**, *n.*—a thermocouple having its thermoelements, and sometimes its measuring junction, embedded in ceramic insulation compacted within a metal protecting tube.
- sheathed thermocouple wire**, *n.*—one or more pairs of thermoelements (without measuring junction(s)) embedded in ceramic insulation compacted within a metal protecting tube.

- sheathed thermoelement**, *n.*—a thermoelement embedded in ceramic insulation compacted within a metal protecting tube.
- span**, *n.*—the algebraic difference between the upper and lower range-values.
- standard platinum resistance thermometer (SPRT)**, *n.*—a thermometer which meets all the requirements described in the text establishing the International Practical Temperature Scale.
- standard thermoelement**, *n.*—a thermoelement that has been calibrated with reference to platinum 67 (Pt-67).
- test thermocouple**, *n.*—a thermocouple that is to have its temperature-emf relationship determined by reference to a temperature standard.
- test thermoelement**, *n.*—a thermoelement that is to be calibrated with reference to platinum 67 (Pt-67) by comparing its thermal emf with that of a standard thermoelement.
- thermal electromotive force (thermal emf)**, *n.*—the net emf set up in a thermocouple under conditions of zero current. Synonymous with *Seebeck emf*.
- thermocouple**, *n.*—two dissimilar thermoelements so joined as to produce a thermal emf when the junctions are at different temperatures.
- thermocouple assembly**, *n.*—an assembly consisting of a thermocouple element and one or more associated parts such as terminal block, connection head, and protecting tube.
- thermocouple element**, *n.*—a pair of bare or insulated thermoelements joined at one end to form a measuring junction and intended for use as a thermocouple or as part of a thermocouple assembly.
- thermocouple, Type E, B, J, K, R, S, or T**, *n.*—a thermocouple having an emf-temperature relationship corresponding to the appropriate letter-designated table in ASTM Standard E 230, Temperature-Electromotive Force (EMF) Tables for Thermocouples, within the limits of error specified in that Standard.
- thermoelectric power**, *n.*—the rate of change of thermal emf with temperature at a given temperature. Synonymous with *Seebeck coefficient*. Normally expressed as emf per unit of temperature.
- thermoelectric pyrometer**, *n.*—an instrument that senses the output of a thermocouple and converts it to equivalent temperature units.
- thermoelement**, *n.*—one of the two dissimilar electrical conductors comprising a thermocouple.
- thermopile**, *n.*—a number of thermocouples connected in series, arranged so that alternate junctions are at the reference temperature and at the measured temperature, to increase the output for a given temperature difference between reference and measuring junctions.
- thermowell**, *n.*—a closed end reentrant tube designed for the insertion of a temperature-sensing element, and provided with means for pressure-tight attachment to a vessel.
- Thomson coefficient**, *n.*—the rate at which heat is absorbed or evolved reversibly in a thermoelement, per unit temperature difference per unit current.
- Thomson emf**, *n.*—the product of the Thomson coefficient and the temperature difference across a thermoelement.
- triple point (water)**, *n.*—the temperature of equilibrium between ice, water, and water vapor. This temperature is  $+0.01^{\circ}\text{C}$  on the International Practical Temperature Scale of 1948.
- upper range-value**, *n.*—the highest quantity that an instrument is adjusted to measure.
- working standard thermocouple**, *n.*—a thermocouple that has had its temperature-emf relationship determined by reference to a secondary standard of temperature.

# Index

## A

- Alloy melting point (Table), 60
- Annealing of thermocouples, 117
- Assemblies, thermocouple, 62, 80
  - Illustrations, 74
- Automatic ice point, 106
- Average value of set of data, 238

## B

- B, thermocouple type, 20
  - Application, 25
  - Chemical composition (Table), 26
  - Electrical resistance (Table), 33
    - Change of with temperature (Table), 32
  - Emf versus temperature
    - Graph, 34
    - Tables, 165-173
  - Environmental limits (Table), 27
  - Extension wires for (Table), 36
  - Physical properties (Table), 30
  - Power series expansion for, 220
  - Seebeck coefficients (Table), 23, 29
  - Trade names for, list of, 25
  - Upper temperature limits (Table), 28
- Becquerel, 5
- Bias of test data set, 239
  - Graph, 241

## C

- Calibration, 112
  - Comparison methods for, 126

## Calibration (continued)

- Data, raw, analysis of, 131
  - Graphs, 132-137
- Fixed point methods for, 124
- In laboratory furnaces, 126, 139
- In stirred liquid baths, 129, 139
- Instruments for, 139
- Interpolation methods for, 131
- Methods of, 120
- Of single thermoelements, 136
- Of used thermocouples, 130
- Procedure for, 139
- Test specimen for, 137
- Uncertainties in, 121
  - For comparison methods, 122
  - For fixed point methods, 122
  - Statistical consideration of, 241
  - Tables of, 122-124
- Ceramic-insulated sheathed thermocouples, 81
- Chromium-nickel thermocouple types (*see* Nickel-chromium types)
- Circuits
  - Industrial, typical (Illustration), 17
  - Potentiometer, 99
    - Illustration, 100
  - Test, for single element (Illustration), 138
  - Thermoelectric, 14
- Clausius, Rudolph, 3
- Coefficients, power series expansion, 217-220
- Color code for insulated thermocouple and, extension wire (Table), 68

Comparison calibration, 126  
 Compatibility of materials, high temperature, 58  
 Connecting head, thermocouple, 62  
 Illustration, 74  
 Connections, thermocouple circuit, 73  
 Connectors, thermocouple, 63  
 Illustration, 74  
 Constant temperature oven, 106  
 Cooling, thermoelectric, 4  
 Correction factor, dynamic, 146  
 Cryogenic thermometry, 222  
 Seebeck coefficients for (Graph), 236

## D

Data, calibration, analysis of, 131  
 Graphs, 132-137  
 Defining points, IPTS-68 (Table), 114  
 Definitions (*see* Terminology)  
 Deviation, standard, 239  
 Difference from standard table, calibration interpolation by, 133  
 Digital indicator, 97, 98  
 Distribution, normal, 238  
 Doping of thermoelement, 55  
 Duplex wire color code (Table), 68  
 Dynamic correction factor, 146

## E

E, thermocouple type, 20  
 Application, 23  
 Chemical composition (Table), 26  
 Electrical resistance (Table), 33  
 Change of with temperature (Table), 32  
 Emf versus temperature  
 Graph, 34  
 Tables, 174-179

E, thermocouple type (continued)  
 Environmental limits (Table), 26  
 E, thermocouple type  
 Extension wires for (Table), 36  
 Physical properties (Table), 30  
 Power series expansion for, 218  
 Seebeck coefficients (Table), 23, 29  
 Cryogenic (Graph), 236  
 Trade names for, list of, 25  
 Upper temperature limits  
 Graph, 22  
 Table, 28  
 Element, thermocouple, 62, 63  
 Emf measurement, 97, 118  
 Entropy, 3, 8  
 Error, sources of, 30, 109  
 Errors, statistical consideration of, 237  
 Extension wires, thermocouple, 27  
 Categories for, 30  
 Color code for (Table), 68  
 Errors arising from, 30  
 Graph, 38  
 Reasons for using, 29  
 Extensions, copper (Illustration), 16, 17

## F

Fabrication, thermocouple, 62  
 Fixed point calibration, 124  
 Fourier heat conduction, 6  
 Fourier, Jean, 3  
 Fourier's law, 11  
 Freedom, degrees of, 239  
 Freezing point calibration, 125  
 Furnaces, calibration, 126

## G

Galvanic error, 109  
 Gold-cobalt thermoelements, 223  
 Gold-iron thermoelements, 223

Gold-0.07 atomic-percent iron  
thermoelements, 223  
Seebeck coefficient (Graph), 236

## H

Hardware, thermocouple, 62  
Head, thermocouple connecting, 62  
Illustration, 74  
Heat transfer, 147  
High-temperature compatibility, 58  
Historical development,  
thermoelectric, 3  
Homogeneity, thermoelement, 119  
Homogeneous metals, law of, 13

## I

Ice point cell, 104  
Automatic type, 106  
Illustration, 105  
Immersion error, 109  
Inhomogeneity, thermoelement, 119  
Installation effects, thermocouple,  
143  
Analysis of, 147  
Insulation, thermoelement  
Compacted ceramic, 82  
Construction (Illustration), 82  
Dimensions of (Graph), 83  
Materials characteristics  
(Table), 84  
Hard ceramic, 66  
Properties (Table), 70  
Types of (Illustration), 69  
Nonceramic, 63  
Characteristics (Table), 67  
Color code for (Table), 68  
Intermediate metals, law of, 14  
Intermediate temperatures, law of,  
14  
Illustration, 16  
Iridium-alloy thermocouples, 39,  
43, 45

Iridium-alloy thermocouples  
(continued)  
Characteristics (Tables), 43, 47  
Emf versus temperature (Graphs),  
42, 46  
Extension wires for, 36  
IPTS-68, 112  
Fixed points for (Table), 114  
Interpolation instruments for, 113  
Secondary points for (Table), 116  
Working standards for  
High-temperature standards,  
117  
Liquid-in-glass thermometer,  
117  
Resistance thermometer, 116  
Thermocouples, 117

## J

J, thermocouple type, 20  
Application, 22  
Chemical composition (Table), 26  
Electrical resistance (Table), 33  
Change of with temperature  
(Table), 32  
Emf versus temperature  
Graph, 34  
Tables, 180-187  
Environmental limits (Table), 26  
Extension wires for (Table), 36  
Physical properties (Table), 30  
Power series expansion for, 218  
Seebeck coefficients (Table),  
23, 29  
Trade names for, list of, 25  
Upper temperature limits  
Graphs, 22  
Table, 28  
Joule heating, 7  
Joule, James, 3

## K

K, thermocouple type, 20  
Application, 24



- K, thermocouple type (continued)  
 Chemical composition (Table), 26  
 Electrical resistance (Table), 33  
 Change of with temperature (Table), 32  
 Emf versus temperature (Graph), 34
- K, thermocouple type Emf versus temperature (Tables), 188-195
- Environmental limits (Table), 26, 27
- Extension wires for (Table), 36
- Physical properties (Table), 30
- Power series expansion for, 219
- Seebeck coefficients (Table), 23, 29
- Trade names for, list of, 25
- Upper temperature limits  
 Graphs, 22  
 Table, 28
- Kelvin, Lord  
 (see Thompson, William)
- Kelvin relations, 7

## L

- Laboratory furnace, calibration in, 126
- Laws of thermoelectric circuits, 13
- Least squares fit, 134, 240
- Limits of error, thermocouple (Table), 164

## M

- Matching error, thermocouple wire, 109
- Mean, precision of, 240
- Mean value of set of data, 238
- Measurement uncertainty, consideration of, 237

- Melting point calibration, 125
- Melting points, alloy (Table), 60
- Metal-sheathed thermocouples, 81
- Metals, law of homogeneous, 13
- Metals, law of intermediate, 14  
 Illustration, 15
- Millivoltmeter, 97
- Molten metal bath, calibration in, 128
- Molybdenum-nickel thermocouples (see Nickel-molybdenum thermocouples)
- Moving surface probes, 152

## N

- Nickel-chromium thermocouple types (see also Type K thermocouples), 49
- Characteristics (Table), 51
- "Chromel-Alumel," 52
- Comparative graph, 50
- "Geminol," 50
- Nickel-chromium-silicon versus nickel-silicon, 53
- "Thermo-Kanthal Special," 52
- "Tophel II-Nial II," 52
- Nickel-molybdenum types, 54
- Extension wires for, 56
- Graph of emf versus temperature, 55
- Physical data (Table), 56
- Nonstandard thermocouple types, 35

## O

- Ohm, Georg, 3
- Ohm's law, 11
- Onsager, Lars, 12
- Onsager relations, 8
- Oven, constant temperature, 106

## P

- Palladium-alloy thermocouples, 39
  - Characteristics (Table), 43
  - Thermal emf (Graph), 42
- Peltier coefficient, 5
  - Effect, 4
  - Heating and cooling, 4, 7
  - Voltage, 5
- Peltier, Jean, 3
- Platinel thermocouple, 46
  - Characteristics (Table), 49
  - Comparative graph, 48
- Platinum-alloy thermocouples
  - Annealing of, 117
  - Comparative graphs, 40, 42, 44, 48
  - Extension wires for (Table), 36
  - In comparison calibration, 126
  - Nonstandard types of, 39, 42, 45, 46
    - Characteristics (Tables), 41, 43, 45, 49
  - Standard types (*see* Types B, R, S)
- Potentiometer, 97, 98
  - Circuit for, 100
  - Precision type, 100
    - Laboratory, 100
    - Plant, 101
    - Portable, 101
  - Recording, 101
  - Semi-precision type, 101
- Power series expansion coefficients for thermoelectric voltages, 217-220
- Prandtl number, 146
- Precision of set of data, 239
- Probability plot, 244
  - Illustration, 245, 246
- Protecting tube, thermocouple
  - 62, 66
    - Assembly (Illustration), 74
    - Ceramic, 72

Protecting tube, thermocouple  
(continued)

- Installation effects of, 147
- Metal, 69
- Metal ceramic, 73
- Selection guide (Table), 75-79

## R

- R, thermocouple type, 20
  - Application, 24
  - Chemical composition (Table), 26
  - Electrical resistance (Table), 33
    - Change of with temperature (Table), 32
  - Emf versus temperature
    - Graph, 34
    - Tables, 196-204
  - Environmental limits (Table), 27
  - Extension wires for (Table), 36
  - Physical properties (Table), 30
  - Power series expansion for, 219
  - Seebeck coefficients (Table), 23, 29
  - Trade names for, list of, 25
  - Upper temperature limits (Table), 28
- Ramp change in temperature, response to, 144
  - Graph, 144
- Recalibration of used thermoelements, 130
- Recording potentiometer, 101
- Recovery, adiabatic, of moving gas, 145
- Reference junction, 103
  - Automatic ice point type, 106
  - Compensation for, 103
  - Constant temperature oven type, 106
  - Electrical compensation for, 107
  - Errors arising in, 109
  - Ice point cell type, 104
    - Illustration, 105

Reference junction (continued)  
 Mechanically compensating type, 108  
 Triple point cell type, 104  
 Zone box type, 107  
 Reference tables  
 For cryogenic range, 223-235  
 For standard types, 165-217  
 List of standardized, 163  
 Reference thermometer, 116  
 Regression analysis, 245  
 Regression line for set of data, 240  
 Response time, thermocouple, 143  
 Rhenium-tungsten thermocouples  
 (*see* Tungsten-rhenium)  
 Rhodium alloy thermocouples  
 Characteristics (Table), 41, 47  
 Comparative graphs for, 40, 46  
 Nonstandard types, 39, 43, 45  
 Standard types (*see* Types B, R, S)

## S

S, thermocouple type, 20  
 Application, 24  
 Chemical composition (Table), 26  
 Electrical resistance (Table), 33  
 S, thermocouple type  
 Change of resistance with temperature (Table), 32  
 Emf versus temperature  
 Graph, 34  
 Tables, 205-213  
 Environmental limits (Table), 27  
 Extension wires for (Table), 36  
 Physical properties (Table), 30  
 Power series expansion for, 220  
 Seebeck coefficients (Table), 23, 29  
 Trade names for, list of, 25  
 Upper temperature limits (Table), 28  
 Scale, temperature, 112

Seebeck coefficient, 4, 103  
 Seebeck effect, 3, 5, 7  
 Seebeck, Thomas, 3  
 Sheathed thermocouples, 81  
 Applications, 94  
 Compatibility of materials in, 85  
 Table, 87  
 Connections for (Illustration), 94  
 Dimensions for  
 Graph, 83  
 Tables, 88  
 Expansion, thermal, coefficients (Table), 84  
 Exposed junctions for, 89  
 Illustration, 93  
 Fittings for (Illustration), 95  
 Grounded junctions for, 89  
 Illustration, 93  
 Precautions in use of, 85  
 Reduced-diameter junctions for, 93  
 Illustration, 93  
 Sheath material properties (Table), 86  
 Sheaths for, 85  
 Terminations for, 94  
 Testing of, 89  
 Table, 90-92  
 Thermowells, installation in (Illustration), 95  
 Ungrounded junctions for, 93  
 Illustration, 93  
 Wires for, 85  
 "Single-wire" thermocouple, 150  
 Specimen, calibration test, 137  
 Standard cell, 102  
 Standard thermocouple types, 20, 162  
 Statistical analysis of measurements, 237  
 Step change in temperature, response to, 143  
 Graph, 144  
 Stirred liquid baths, calibration in, 129

Surface probes, 151  
 Analysis of errors in, 154  
 Commercial types of, 156  
 Errors in, 153  
 For current-carrying surfaces, 153  
 Minimizing errors in, 156  
 Surface temperature measurement,  
 148  
 Installation methods for, 149

## T

T, thermocouple type, 20  
 Application, 20  
 Chemical composition (Table), 26  
 Electrical resistance (Table), 33  
 Change of with temperature  
 (Table), 32  
 Emf versus temperature  
 Graph, 34  
 Tables, 214–217  
 Environmental limits (Table), 26  
 Extension wires for (Table), 36  
 Physical properties (Table), 30  
 Power series expansion for, 217  
 Seebeck coefficients (Table),  
 23, 29  
 T, thermocouple type (continued)  
 Trade names for, list of, 25  
 Upper temperature limits  
 Graph, 22  
 Table, 28  
 Temperatures, intermediate, law of,  
 14  
 Illustration, 16  
 Terminology, 248  
 Thermal expansion coefficients  
 (Table), 84  
 Thermal time constant, 143  
 Thermocouple reference tables, list  
 of, 163  
 Smoothing of, 163  
 Generation of, 220  
 Thermocouple reference tables, list  
 of (continued)  
 Coefficients for generating,  
 217–220  
 Thermodynamics, laws of, 7  
 Thermoelectric theory, 3  
 Thermoelement designations and  
 trade names, list of, 25  
 Thermoelements, 62  
 Illustration, 64  
 Thermometer, reference, 116  
 Thermowells, 71  
 Installation effects of, 146  
 Selection guide (Table), 75–79  
 Types of (Illustration), 72  
 Thompson (*see also* Kelvin), 3  
 Thompson coefficient, 6  
 Thompson effect, 6  
 Thompson, William, 3  
 Time constant, thermal, 143  
 Triple point cell, 104  
 Tube, protecting (*see* protecting  
 tube)  
 Two potentiometer calibration  
 method, 127  
 Tungsten-rhenium thermocouple  
 types, 54  
 Characteristics of (Table), 59  
 Emf versus temperature (Graph),  
 58  
 Extension wires for (Table), 36  
 Uncertainties in calibration of  
 (Tables), 123, 124  
 Types, thermocouple standard,  
 20, 162

## U

Uncertainties  
 In calibration, 121  
 In measurement, 237  
 Uncertainty envelope, 134  
 Plots of, 134, 136, 137  
 Uncertainty of set of data, 239

Upper temperature limits (Table),  
21

**V**

Variance of set of data, 239  
Volta, Alessandro, 3

**Z**

Zener diode, 102  
Zone box type reference junction,  
107

ISBN 0-8031-0502-9