

Designation: D7964/D7964M - 14

Standard Test Method for Determining Activity of Fluid Catalytic Cracking (FCC) Catalysts in a Fluidized Bed¹

This standard is issued under the fixed designation D7964/D7964M; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ε) indicates an editorial change since the last revision or reapproval.

1. Scope

1.1 This test method covers determining the activity and coke selectivity of either equilibrium or laboratory deactivated fluid catalytic cracking (FCC) catalysts. The activity is evaluated on the basis of mass percent conversion of gas oil feed in a fluidized bed reactor. The coke yield is defined as the mass of carbon laid down on the catalyst, also expressed as a percent of the gas oil feed. The scope of the round robin will be limited to the determination of activity and coke. All other analyses are thus beyond this scope and should be noted as "optional."

1.2 The values stated in either SI units or inch-pound units are to be regarded separately as standard. The values stated in each system may not be exact equivalents; therefore, each system shall be used independently of the other. Combining values from the two systems may result in non-conformance with the standard.

1.3 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

2. Referenced Documents

- 2.1 ASTM Standards:²
- D2887 Test Method for Boiling Range Distribution of Petroleum Fractions by Gas Chromatography
- D4463 Guide for Metals Free Steam Deactivation of Fresh Fluid Cracking Catalysts
- E105 Practice for Probability Sampling of Materials
- E177 Practice for Use of the Terms Precision and Bias in ASTM Test Methods
- E691 Practice for Conducting an Interlaboratory Study to Determine the Precision of a Test Method

3. Terminology

3.1 Definitions of Terms Specific to This Standard:

3.1.1 *activity*—a measure of the rate of a specific catalytic reaction, calculated in the present case by dividing conversion by the difference of 100 minus conversion.

3.1.2 *catalyst/oil (C/O) ratio*—the mass of catalyst used in the test divided by the mass of feed fed to the reactor.

3.1.3 *coke*—mass of carbon laid down on the catalyst during the FCC reaction times 1.083.

3.1.4 *conversion*—the starting mass of reactant feed minus the mass of the liquid product that boils above 221°C [430°F]; this delta is then reported as a percentage of the starting mass of feed.

3.1.5 *delivery time*—this is the time, in seconds, during which feed is introduced to the reactor.

3.1.6 FCC-fluid catalytic cracking.

3.1.7 gasoline— C_5 compounds through compounds boiling at 221°C [430°F].

3.1.8 *HCO*—the heavy cycle oil product, which is defined to have a minimum boiling point of 343° C [650°F].

3.1.9 *LCO*—the light cycle oil product, which is defined to have a boiling point range of 221 to 343° C [430 to 650° F].

3.1.10 *liquid product*—all products formed in the catalytic reaction that can be condensed in the chiller bath afterward, usually a combination of gasoline, LCO, and HCO, but can contain a trace of C_4 and C_4 minus compounds.

3.1.11 *normalized product yield*—the result obtained when each product yield has been corrected for non-perfect mass balances.

3.1.11.1 *Discussion*—For a run to be judged acceptable, the total recovery, mass % of feed, should be in the range of 96 to 102 % prior to normalization. If the recovery is outside this range the test data should be discarded.

3.1.12 *product yield*—one hundred times the mass of a specific product divided by the mass of feed used in the test.

3.1.13 *selectivity*—same as yield. Selectivity generally refers to how much of a particular product, such as coke, is formed during a chemical reaction; selectivity is related to, but

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² For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

different from, conversion, which is the total amount of all products formed during the reaction.

4. Summary of Test Method

4.1 A sample of FCC catalyst is contacted with gas oil in a fluidized bed reactor using a specified reaction temperature, a specified mass of catalyst and oil, and specified oil feed rate. Reaction products (liquid product, gas, and coke on catalyst) are analyzed. Conversion, coke, and individual product yields are calculated for each experiment.

4.2 Following analysis of the products, the total recovery (that is, mass balance) of the feed as converted and unconverted products is determined. If the recovery is less than 96 % or greater than 102 %, then the test is rejected as unsatisfactory (an outlier).

4.3 For each catalyst tested, a normalized conversion or activity and a coke mass are determined.

5. Significance and Use

5.1 The fluidized bed test provides data to assess the relative performances of FCC catalysts. Because results are affected by catalyst pretreatment, feedstock characteristics, and operating parameters, this test method is written specifically to address the accuracy and precision when a common catalyst and oil are tested under the same conditions but at different sites, using Kayser Technologies Advanced Catalytic Evaluation (ACE) unit.^{3,4}Analytical procedures may vary among the sites. However, significant variations are not expected.

Note 1—ASTM International takes no position respecting the validity of any patent rights asserted in connection with any item mentioned in this standard. Users of this standard are expressly advised that determination of the validity of any such patent rights, and the risk of infringement of such rights, are entirely their own responsibility.

5.2 The standard reaction temperature for purposes of the accuracy and precision statement is 532°C [990°F]. Other reaction temperatures can be used in practice; however, yield data developed at temperatures other than 532°C [990°F] will not be the same. Also, test precision may be different at other reaction temperatures.

6. Apparatus

6.1 The fluidized bed reactor of this test method is shown in Fig. 1. The full ACE apparatus also includes a feed delivery system and both a gas and a liquid collection system. In a typical gas collection system, water is displaced by the collected gas and the volume of displaced water provides a quantitative measurement of the amount of gas collected. Committee D32 can only suggest and will not recommend nor certify any specific vendor. However, significant variations from the test apparatus of this method most likely will result in significantly different activity and selectivity data from identical catalyst samples.

⁴ Trademarked, ACE Technology.



FIG. 1 Fluidized Bed Reactor

³ The fluidized bed reactor described herein is covered by US Patent 6,069,012. Interested parties are invited to identify an alternative(s) to this patented reactor system. Alternative(s) should be submitted to the ASTM International Headquarters. Your comments will receive careful consideration at a meeting of the responsible technical committee,¹ which you may attend.

6.2 Chromatographic Equipment:

6.2.1 Liquid product analyses should be performed using Test Method D2887 on a gas chromatograph (GC) equipped with a flame ionization detector.

6.2.2 Gas product analyses may be accomplished in two parts. First, a GC equipped with a thermal conductivity detector is needed for quantitative identification of H₂ and N₂. H₂S can optionally be detected, but will not be quantitative in units that collect gas by water displacement. The second part of the analysis requires a GC equipped with either FID or TCD, for the separation and quantitative identification of hydrocarbon species. Typically, the following compounds are individually quantified: methane, ethane, ethylene, propane, propylene, n-butane, iso-butane, 1-butene and iso-butene, cis-2-butene, trans-2-butene, iso-pentane, n-pentane, and the unsaturated C_5 isomers (C₅ olefins). For purposes of this test method and round robin the higher boiling gaseous compounds will be lumped into a C_6^+ fraction. If C_5 olefins are not separately identified, then they are included with the C_6^+ lump as well. The mass of the C_5 's and the C_6^+ group are mathematically added to the gasoline liquid fraction.

6.3 Carbon analysis of a representative sample of the spent catalyst (that is, after the cracking reaction has been completed) may be accomplished using a commercially available carbon analyzer if the ACE unit being used does not have catalyst regeneration capability. If the ACE is a model that does have regeneration capability, then the carbon on catalyst is back calculated from the CO₂ evolved in the flue gas during the regeneration cycle.

7. Sampling

7.1 A sampling procedure is needed. Practice E105 is appropriate.

8. Sample Preparation

8.1 Equilibrium Catalysts—Dry samples and remove coke by heating a shallow (less than 10 mm thick) bed of catalyst in a porcelain crucible at $590 \pm 20^{\circ}$ C [1094 $\pm 36^{\circ}$ F] for a length of time sufficient to remove any coke. This typically requires approximately 3 h. Sufficient air should be available in the furnace to burn the sample free of coke. Insufficient coke removal is indicated by a difference in color of the top and bottom layers. The hot crucible is cooled in a desiccator to prevent moisture pickup. Only equilibrium catalyst will be used in the precision and bias statement of this test method.

Note 2—Heavily coked samples may be damaged by sintering or deactivation if oxidation is allowed to occur too rapidly, leading to artificially low catalytic activity and surface area.

8.2 *Fresh Catalysts*—Fresh catalyst samples should be steam treated prior to ACE testing. Steaming procedures such as those specified in Guide D4463 may be used. However, specific conditions (temperature, partial pressure of steam, and time) should be chosen such that the steamed catalyst properties (activity, zeolite and matrix surface areas, and unit cell size) approximate those found in equilibrium FCC catalysts of the same type.

9. Procedure

9.1 Reactor Preparation:

9.1.1 The oil feed line on the ACE unit is meant to be changed with some regularity. Whenever the oil feed line pressure exceeds 1.5 psig, the feed line should be changed. For purpose of this round robin, install a feed line that yields a 1.125 in. injector height. Injector height is defined as the distance from the lowest point of the conical reactor bottom to the bottom end of the feed injector.

9.1.2 The drier tube and humidifier should be serviced as described in the ACE Operating Manual.

9.1.3 The ACE CO_2 analyzer should be calibrated as described in the ACE Operating Manual.

9.2 Preparation of Syringe and Liquid Product Receiver:

9.2.1 Preheat the gas oil feedstock to $170 \pm 5^{\circ}$ C [338 \pm 9°F], at which temperature a typical Gulf Coast gas oil will flow easily into the syringe and can be accurately delivered to the reactor. Set the oil feed pump to deliver feed at the prescribed rate for this testing. Calibration of the feed rate is a manual process consisting of changing the speed setting on the pump and performing a feed test. The oil feed line is opened so that oil can be delivered into a tared beaker. The amount per minute is recorded and the test repeated until the oil mass collected is on target.

Note 3—If heavier feedstocks are used, the measured rate may be inconsistent. The syringe temperature can be increased to $220 \pm 5^{\circ}C$ [428 $\pm 9^{\circ}F$] as long as this does not exceed the initial boiling point of the oil.

9.2.2 A small plug of glass wool should be placed in the outlet of the receiver to reduce the carryover of C_5^+ aerosol into the gas collection vessel. Obtain the initial mass of the liquid product receiver(s) including the glass wool.

9.2.3 Install receiver(s) and connect the gas line to the gas collection system. Open the gas vent valve to prevent premature collection of purge gas.

9.2.4 Prepare ethylene glycol bath(s) for the receiver(s) if needed. Immerse the receiver(s) to the level of the gas outlet line(s). Maintain the bath temperature at -15° C [10°F].

9.2.5 *Pressure Test*—Pressurize the reactor to 20 kPa [150 mm Hg] nitrogen and close the gas vent and nitrogen supply valves. Watch the pressure gages for 2 min to determine if any significant leaks occur. If no leaks are apparent using the criteria specified in the ACE Operating Manual, then open the gas vent valve carefully to release pressure.

9.3 Performing the Run:

9.3.1 Set up the run conditions in the ACE control interface. Up to 6 runs can be programmed to run automatically on the ACE unit.

9.3.2 Once the reaction is complete and the gas has been collected, record the volume of displaced water (V_B), the gas temperature (T_R), and atmospheric pressure (P_R). Typically this is done through the ACE control interface. After being mixed, the collected gases may then be analyzed immediately by syringe sampling or by forcing from the gas collection system into a gas sampling loop or a sealable gas sample bag for storage and later analysis.

9.3.3 If using a Model R or R+ unit, then the carbon mass determined by IR must be recorded for later analysis of products. If using an ACE unit that is not equipped with

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catalyst regeneration capability (Model AP or P), then alternatively the catalyst can be removed from the reactor for carbon analysis as described in 9.4.8.

9.4 Analyses of Products:

9.4.1 Remove the liquid product receiver(s) and immediately cork the top. After removing the liquid receiver from the bath, the outside is rinsed with water and then with acetone. It is allowed to dry on a rack for 20 min. The contents will warm up a bit during this time so the cork remains in the receiver until final weighing.

9.4.2 Collect the liquid holdup in the reactor exit line and around the reactor-receiver joint with a tared cotton wool swab or other suitable material. Determine the mass of this liquid and record (WQ). Experience indicates this liquid material is predominantly unconverted feed.

9.4.3 The receiver is weighed for mass balance purposes and the mass recorded.

9.4.4 The vial containing the liquid product is removed and placed in the autoinjector tray of the simulated distillation analyzer, typically an Agilent gas chromatograph equipped with appropriate software for boiling point analysis.

9.4.5 Using Test Method D2887, simulated distillation, determine the mass percentage of the liquid products boiling in the ranges of gasoline, IBP to 221°C [430°F] and LCO, 221 to 343°C [430 to 650°F]. The remaining product is the HCO, 343+°C [650+°F].

9.4.6 Analyze the gas product collected using a single GC or a combination of GCs that will permit quantitative volume (mole) % determination of H₂, H₂S, C₁, C₂'s, C₃'s, C₄'s, C₅ saturates, C_5 olefins, and a C_6^+ lump that need not be resolved to make a reasonable approximation for the molecular weight of the gaseous hydrocarbons.

9.4.7 The amount of carbon deposited on catalyst is easily derived from the Model R or R+ Advanced Catalytic Evaluation (ACE) unit by using the panel mounted infrared analyzer provided with the ACE module. An equivalent analyzer, which will totalize the CO/CO_2 in the flue gas during catalyst regeneration is acceptable.

9.4.8 Alternatively, carbon analysis of a representative sample of the spent catalyst may be done by using equipment such as that supplied by LECO (Model CR-800), Horiba (Model EMIA), or Coulometrics (Model CM-5600).⁵

10. Calculation

10.1 Gas Product:

10.1.1 The total volume of gas collected (including purge gas) is determined from the volume of water displaced by:

$$V_t^o = V_B \cdot \frac{273 \text{ K}}{273 \text{ K} + T_R} \cdot \frac{P_R}{101.3 \text{ kPa}} \text{ cm}^3 \text{ STP}$$
(1)

where:

101.3 kPa = 760 mm Hg,= standard volume of gas collected, cm^3 , V_t^o

 V_B = volume of water displaced during the test and is equivalent to the actual volume of gas collected, cm3, gas temperature, °C, and T_R

$$=$$
 gas temperature, \in $=$ gas pressure, kPa.

10.1.2 To find the volume of each gas component:

$$V_i = N_i V_t^o / 100 \tag{2}$$

where:

 V_i = volume of the *i*th gaseous product, and N_i = mole % of the *i*th component in the gas.

10.1.3 To find the mass (absolute) of each component:

$$W_i = \frac{V_i \cdot M_i}{22.412}$$
g (3)

where:

 W_i = mass of the *i*th gaseous product, g, and

 M_i = molecular weight of the *i*th gaseous product.

10.1.4 The molecular weight of the C_6^+ unresolved lump is assumed to be 89.

10.1.5 The total mass of products collected in the gas phase is:

$$W_g = \Sigma W_i \text{ (sum over all components)}$$
 (4)

where:

 W_g = total mass of all gaseous products, g.

10.1.6 Coke:

10.1.6.1 When the total mass of carbon is derived from ACE unit (9.4.7), the total mass of coke (in grams) on the catalyst W_{coke} is:

$$W_{\rm coke} = W_{\rm carbon} \cdot 1.083 \tag{5}$$

where:

 W_{carbon} = mass of carbon from ACE unit.

10.1.6.2 When measuring carbon by means of a carbon analyzer (9.4.5), the total mass of coke (in grams) on the catalyst W_{coke} is:

$$W_{\text{coke}} = x_K \cdot W_{\text{cat}} \ 1.083 \ /100 \tag{6}$$

where:

 x_K = mass % carbon on catalyst, and W_{cat} = mass of catalyst.

Note 4-The 1.083 factor assumes one mole of hydrogen is associated with one mole of carbon.

10.2 Mass Balance (Recovery):

10.2.1 To determine the quality of the test, the mass balance can be calculated as follows:

$$R = (W_g + W_L + W_c) / W_f \cdot 100 \%$$
(7)

where:

R = recovery, mass % of feed, and

 W_f = mass of oil feed.

10.2.2 For a run to be judged acceptable, the R should be in the range of 96 to 102 %. If the recovery is outside this range, the test data should be discarded.

10.3 Determination of Unnormalized Yields:

⁵ Interested parties are invited to identify an alternative(s) to the analytical instruments specified for measuring carbon. Alternative(s) should be submitted to the ASTM International Headquarters. Your comments will receive careful consideration at a meeting of the responsible technical committee, which you may attend.

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10.3.1 Each measured product can be expressed as an actual yield, mass % of feed as follows:

10.3.1.1 Gas Components H_2 - C_4 's:

$$Y_i = W_i / W_f \cdot 100 \tag{8}$$

where:

 Y_i = unnormalized yield of the *i*th gaseous product expressed as mass % of feed.

10.3.1.2 Gasoline:

$$Y_{g} = \left[X_{g}\left(W_{L}\right) + W_{i}(C_{5}^{+})\right] / W_{F} \cdot 100 \%$$
(9)

where:

- Y_g = unnormalized yield of the gasoline, mass % of feed,
- X_g = mass fraction of gasoline in the combined liquid products,
- $W_i(C_5^+)$ = mass of all C₅'s plus the unresolved C₆⁺ lump in the gas sample, and

 Y_L = total liquid product collected in liquid receiver.

10.3.1.3 LCO:

$$Y_1 = X_1(W_L) / W_F \cdot 100 \%$$
 (10)

where:

- Y_1 = unnormalized yield of the LCO products, mass % of feed,
- X_1 = mass fraction of LCO products in the combined liquid products, and

 W_L = total liquid product collected in liquid receiver.

10.3.1.4 HCO:

$$Y_h = \left[\left(X_h \cdot W_L \right) + W_Q \right] / W_F \cdot 100 \%$$
(11)

where:

- Y_h = the unnormalized yield of the HCO products, mass % of feed,
- X_h = the mass fraction of HCO products in the combined liquid products, and
- W_L = total liquid product collected in liquid receiver.

10.3.1.5 Coke:

$$Y_c = \left(W_{\text{coke}} / W_f\right) \cdot 100 \ \% \tag{12}$$

where:

 Y_c = unnormalized yield of coke, mass % of feed.

10.3.1.6 Conversion:

Conversion unnormalized wt % = 100 % $-(Y_1 + Y_h)$ (13)

10.4 Yield Normalization:

10.4.1 Unless the mass balance is 100 %, the raw yield will require normalization. The simplest way is normalization of all yields assuming loss (or gain) is proportional to the actual yield.

$$Y_i^o = \frac{Y_i}{R} \cdot 100 \ \% \tag{14}$$

where:

 Y_i^o = normalized product yield of the *i*th product, mass % of feed.

Conversion (normalized) mass
$$\% = 100 \% - (Y_1^o + Y_h^o)$$
 (15)

11. Precision and Bias

11.1 The precision of this test method is based on an interlaboratory study conducted in 2012. Seven laboratories participated in this study. Each of the laboratories was asked to report twelve replicate test results for a single fluid cracking catalyst. Six out of seven laboratories reported twelve replicates. One laboratory reported ten replicates. A total of 21 characteristics were analyzed as part of the study. Every "test result" reported represents an individual determination. Practice E691 was followed for the design and analysis of the data; however, the data from outlier laboratories were excluded from the precision calculations when appropriate. The details are given in ASTM Research Report No. RR:D32-1042.⁶

11.1.1 *Repeatability* (r)—The difference between repetitive results obtained by the same operator in a given laboratory applying the same test method with the same apparatus under constant operating conditions on identical test material within short intervals of time would in the long run, in the normal and correct operation of the test method, exceed the following values only in one case in 20.

11.1.1.1 Repeatability can be interpreted as the maximum difference between two results, obtained under repeatability conditions, that is accepted as plausible due to random causes under normal and correct operation of the test method

11.1.1.2 Repeatability limits are listed in Table 1 below.

11.1.2 *Reproducibility* (R)—The difference between two single and independent results obtained by different operators applying the same test method in different laboratories using different apparatus on identical test material would, in the long run, in the normal and correct operation of the test method, exceed the following values only in one case in 20.

⁶ Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR:D32-1042. Contact ASTM Customer Service at service@astm.org.

Analysis	Average ^A x	Repeatability Standard Deviation S _r	Reproducibility Standard Deviation s _R	Repeatability Limit r	Reproducibilit Limit R
Normalized Conversion, mass % of feed Normalized Coke yield, mass % of feed	76.029 5.397	0.599 0.152	1.626 0.307	1.678 0.425	4.552 0.861
Mass balance	99.124	1.166	1.521	3.266	4.258

^A The average of the laboratories' calculated averages.

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11.1.2.1 Reproducibility can be interpreted as the maximum difference between two results, obtained under reproducibility conditions, that is accepted as plausible due to random causes under normal and correct operation of the test method.

11.1.2.2 Reproducibility limits are listed in Table 1 below.

11.1.3 The above terms (repeatability limit and reproducibility limit) are used as specified in Practice E177.

11.1.4 Any judgment in accordance with statements 11.1.1 and 11.1.2 would normally have an approximate 95 % probability of being correct, however the precision statistics obtained in this ILS must not be treated as exact mathematical quantities which are applicable to all circumstances and uses. The limited number of materials tested and laboratories reporting results guarantees that there will be times when differences greater than predicted by the ILS results will arise, sometimes with considerably greater or smaller frequency than the 95 % probability limit would imply. The repeatability limit and the reproducibility limit should be considered as general guides, and the associated probability of 95 % as only a rough indicator of what can be expected.

11.2 *Bias*—At the time of the study, there was no accepted reference material suitable for determining the bias for this test method, therefore no statement on bias is being made.

11.3 The precision statement was determined through statistical examination of 1428 results, from six laboratories, on a single catalyst. This precision statement can be used to judge the equivalency of two test results, provided that the materials used are close in characteristics to the materials used in this study.

12. Keywords

12.1 ACE; catalysts; FCC; fluid cracking catalyst; microactivity; selectivity

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