



Standard Test Method for In Situ Compressive Stress Within Solid Unit Masonry Estimated Using Flatjack Measurements¹

This standard is issued under the fixed designation C1196; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ϵ) indicates an editorial change since the last revision or reapproval.

1. Scope*

1.1 This test method covers the determination of the average compressive stress in existing unreinforced solid-unit masonry (see [Note 1](#)). This test method concerns the measurement of in-situ compressive stress in existing masonry by use of thin, bladder-like flatjack devices that are installed in cut mortar joints in the masonry wall. This test method provides a relatively non-destructive means of determining masonry properties in place.

NOTE 1—Solid-unit masonry is that built with stone, concrete, or clay units whose net area is equal to or greater than 75 % of the gross area.

1.2 The values stated in inch-pound units are to be regarded as standard. The values given in parentheses are mathematical conversions to SI units that are provided for information only and are not considered standard.

1.3 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

2. Referenced Documents

2.1 ASTM Standards:²

[C1180 Terminology of Mortar and Grout for Unit Masonry](#)
[C1232 Terminology of Masonry](#)

[E74 Practice of Calibration of Force-Measuring Instruments for Verifying the Force Indication of Testing Machines](#)

3. Terminology

3.1 Definitions of Terms Specific to This Standard:

3.1.1 *shim, n*—item inserted into a flatjack slot prior to testing to minimize the inflation of the test flatjack.

¹ This test method is under the jurisdiction of ASTM Committee C15 on Manufactured Masonry Units and is the direct responsibility of Subcommittee C15.04 on Research.

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² For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

3.1.1.1 *Discussion*—The use of shims may be necessary during testing to achieve a tight fit of the flatjack in the slot and to ensure uniform transfer of pressure (stress) to the masonry over the complete area of the flatjack. See Annex A1 for further discussion on allowable types of shims.

3.1.2 *spacer*—metal plate used in the calibration process to control flatjack thickness.

3.2 For definitions of other terms used in this test method refer to Terminology [C1180](#) for mortar and grout and Terminology [C1232](#) for masonry.

4. Summary of Test Method

4.1 When a slot is formed in the masonry, compressive stress at that point will cause the masonry above and below the slot to move together. Compressive stress in the masonry may be measured by inserting a flatjack into the slot and increasing its internal pressure until the original distance between points above and below the slot is restored. The state of compressive stress in the masonry is approximately equal to the flatjack pressure multiplied by factors which account for the physical characteristics of the jack and the ratio of (a) the bearing area of the jack in contact with the masonry to (b) the bearing area of the slot.

5. Significance and Use

5.1 Stress is applied as pressure over the area of the flatjack. In the case of multi-wythe masonry, stress is estimated only in the wythe in which the flatjack is inserted. Stress in other wythes may be different.

6. Apparatus

6.1 Flatjack:

6.1.1 A flatjack is a thin envelope-like bladder with inlet and outlet ports which may be pressurized with hydraulic fluid. Flatjacks may be of any shape in plan, and are designed to be compatible with the masonry being tested. Typical configurations are shown in [Fig. 1](#).

6.1.2 For determination of the state of compressive stress, dimension A should be equal to or greater than the length of a single masonry unit, but not less than 8 in. (200 mm). Dimension B should be equal to or greater than the thickness of one wythe and not less than 3 in. (75 mm). The radius, R , for

*A Summary of Changes section appears at the end of this standard

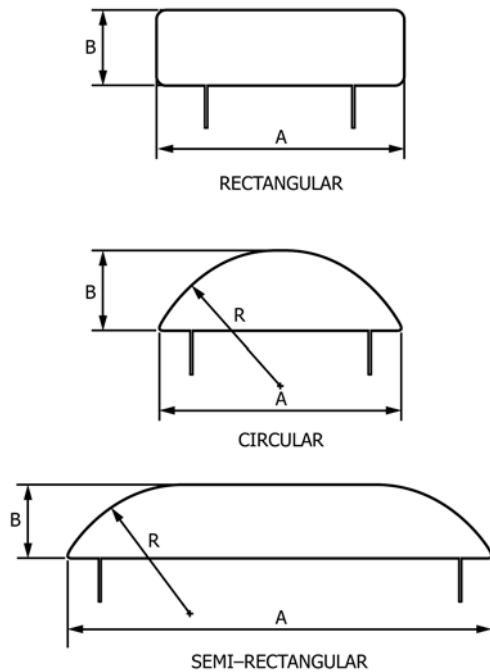


FIG. 1 Flatjack Configurations (Plan View)

circular and semi-rectangular flatjacks shall be equal to the radius of the circular saw blade used to cut the slot.

6.1.3 Flatjacks shall be made of metal or other material such that the flatjack in a slot in masonry will be capable of applying operating pressures up to the expected maximum flatjack pressure. See Note 2. Metal flatjacks suitable for this purpose shall be made of type 304 stainless steel sheet of 0.024 in. (0.6 mm) to 0.048 in. (1.2 mm) in thickness with welded seams along the edges and incorporating hydraulic inlet or outlet ports.

NOTE 2—A maximum operating pressure of 1000 psi (6.9 MPa) or less is often adequate for older existing masonry, but flatjacks with higher operating pressures may be required for more recently constructed buildings. Flatjacks manufactured with flexible polymers that have operating pressure ranges of less than 1000 psi (6.9 MPa) may be useful for stress measurements in some historic masonry.

6.1.4 Calibrate all flatjacks as described in Section 8 to determine their pressure-applied load characteristics.

6.2 *Hydraulic System*—A hydraulic pump with hydraulic hoses is required. Hose connections shall fit the flatjack inlet port. Measure pressure using gages calibrated to a traceable standard having both an accuracy of 1 % of full hydraulic scale and an appropriate operating range. The hydraulic system shall be capable of maintaining constant pressure within 1 % of full scale for at least 5 min.

6.3 *Displacement Measurement*—Measure displacements of the masonry by a mechanical gage extensometer which measures the distance between fixed gage points on the masonry as shown in Fig. 2. The method or device used to measure deformations shall be capable of deformation measurements up to $\frac{3}{16}$ in. (5 mm). Deformation measurements shall have an accuracy of at least ± 0.005 % of gage length.

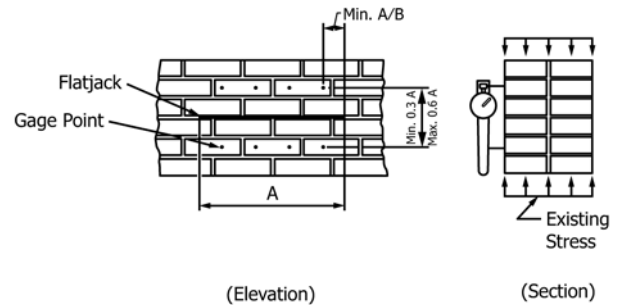


FIG. 2 Flatjack Test Setup for In Situ Stress Measurement

6.4 *Gage Points*—Use adhered metal discs or embedded metal inserts as gage points during the measurement process. Attach gage points securely to the masonry (using a rigid adhesive for discs or cementitious grout for plugs) which will prevent movement and ensure the required measurement accuracy. The gage points shall have a conical depression at their center, compatible with the pointed elements of the extensometer. The angles of the depression of the cone and the extensometer points shall be the same.

7. Preparation of Slots

7.1 Slots in masonry are normally prepared by removing the mortar from masonry bed joints to avoid disfiguring the masonry. Remove all mortar in the bed joint, so that pressure exerted by a flatjack shall be directly against the surfaces of the masonry units.

7.2 The plan geometry of the slot shall be similar to that of the flatjack being used. Plan dimensions of the prepared slot shall not exceed those of the flatjack by more than $\frac{1}{2}$ in. (12 mm).

7.3 Prepare rectangular slots into which rectangular flatjacks are to be inserted by drilling adjacent or overlapping holes (stitch drilling) and subsequently using a drill, bar, or tool to remove mortar and produce a slot of desired dimensions with smooth upper and lower surfaces. Other tools, such as oscillating blade grinders that can be reliably used to form rectangular slots in masonry mortar joints without damaging the surrounding masonry, are also permitted to be used.

7.4 Prepare slots for circular and semi-rectangular flatjacks using circular saws of sufficient radius to provide the depth required (Fig. 1, dimension B). Use carbide or diamond tipped blades to remove all mortar from the slot.

8. Calibration

8.1 A flatjack has an inherent stiffness which resists expansion when the jack is pressurized. Therefore, the fluid pressure in the flatjack is greater than the stress the flatjack applies to masonry. A flatjack must be calibrated to provide a conversion factor, K_m , to relate internal fluid pressure to stress applied.

8.2 Calibrate flatjacks in a compression machine of at least 100 kip (450 kN) capacity which has been calibrated according to Practice E74.

8.3 Place a 2 in. (50 mm) thick steel bearing plate on the lower platen of the compression machine. The bearing plate

shall be of sufficient size to completely cover the flatjack being calibrated. Place the flatjack on the lower bearing plate such that the edge of the flatjack with the inlet/outlet ports is coincident with the edge of the bearing plate. Place steel spacers around the other edges of the flatjack. The thickness of the spacers shall be 0.015 to 0.050 in. (0.38 to 1.27 mm) greater than the sum of the combined thickness of the two sheets plus the thickness of inlet/outlet port used in fabrication of the flatjack. Place the upper 2 in. (50 mm) thick bearing plate on top of the spacers and flatjack, and align it to be directly above the lower bearing plate. Position the bearing plate/flatjack/spacer assembly on the lower platen such that the centroid of the area of the flatjack is within ¼ in. (6 mm) of the axis of thrust of the test machine. The calibration setup is illustrated in Fig. 3.

8.4 Raise or lower the moveable platen such that both platens are in contact with the bearing plates. Apply a pre-load sufficient to provide full contact between the bearing plates and the spacers, equivalent to 10 psi (0.07 MPa) over the gross area of the flatjack.

8.5 The distance between platens must be held constant during the calibration procedure. Fix the displacement of the test machine at this point if using a displacement-control machine. If not, attach displacement gages (mechanical or electrical) such that the distance between platens established by the procedures of paragraph 8.4 can be held constant when using a force-control test machine.

8.6 Pressurize and depressurize the flatjack three times over the full operating pressure range. Do not exceed the maximum flatjack operating pressure.

8.6.1 While holding the distance between the platens constant, increase the pressure in the flatjack in equal increments to within 5 percent of the maximum flatjack operating pressure. Use at least 10 equal increments between 0 psi and

the maximum flatjack operating pressure. At each increment, record flatjack hydraulic pressure and force applied by the test machine.

8.7 Calculate the load applied by the flatjack as internal pressure times gross flatjack area. Plot flatjack load versus load measured by the test machine with the flatjack load on the horizontal axis of the plot. The slope of the line is equal to the flatjack constant, that is, the conversion factor:

$$K_m = P_{\text{machine}} \div P_{\text{flatjack}} \quad (1)$$

8.8 Recalibrate flatjacks after using five times or when distortion appears excessive.

9. Procedure

9.1 The location at which compressive stress estimates are performed is dictated by engineering objectives. The basic arrangement is illustrated in Fig. 2. At the desired location or locations the following steps should be taken:

9.2 Select and mark a visible line on the masonry to define the location and length of slots to be formed.

9.3 Attach at least four pairs of equally spaced gage discs or embedded plugs vertically aligned above and below the slot as shown in Fig. 2. Each row of gage points thus formed shall be equally spaced above and below the flatjack. The minimum gage length shall be 0.3 times the length, A , where A is the length of the flatjack as shown in Fig. 1. The maximum gage length shall be 0.6 times the length, A , of the flatjack. The first and last locations shall be located not less than ⅛ of dimension A inward toward the center of the slot from each end, as shown in Fig. 2.

NOTE 3—Alternative instrumentation configurations are acceptable if controlled laboratory tests are conducted to verify the validity of the alternate instrumentation approach. Examples of alternate configurations are shown in Fig. 4. These references provide additional information about

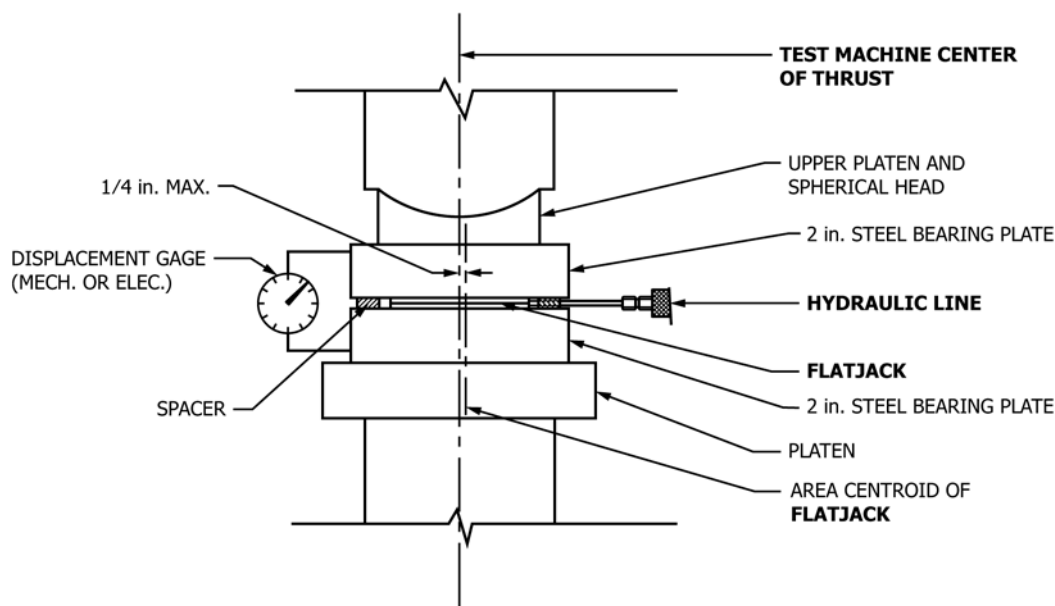


FIG. 3 Flatjack Calibration Setup (Elevation View)

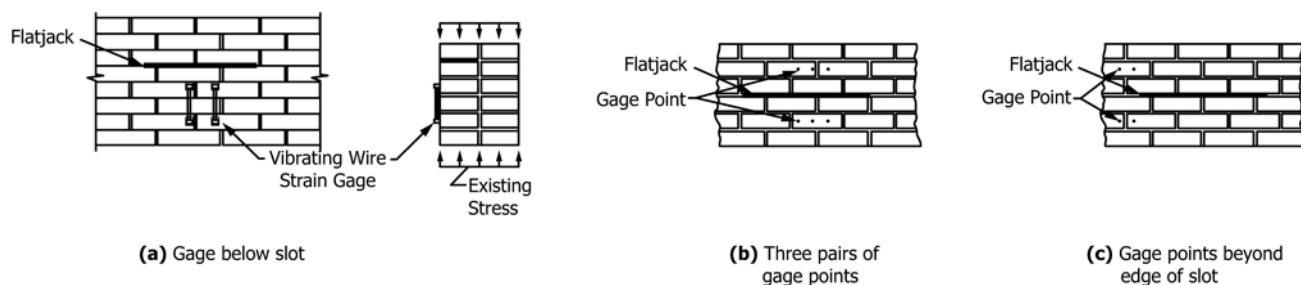


FIG. 4 Examples of Alternative Instrumentation Approaches

alternate instrumentation for flatjack testing.³⁻⁵

9.4 Measure the initial distance between each pair of gage points.

9.5 Prepare the slot (see **Note 4**) (see **Section 7**) and record the measured slot dimensions and the time. Clean slots of all mortar and brick particles prior to the insertion of flatjacks.

NOTE 4—The location of the slot shall be at least $1\frac{1}{2}$ flatjack lengths from wall openings or ends.

9.6 Repeat step 9.4 after the slot has been prepared to obtain the initial deviation from the original gage distances.

9.7 Insert the flatjack into the slot. Shim as required to achieve a tight fit and bridge over any interior voids in the masonry. See the Annex for a description of flatjack shims and their use.

9.8 Connect hydraulic hoses and fill the calibrated flatjack with hydraulic fluid until pressure begins to develop.

9.9 In order to *seat* the flatjack and any shims, pressurize the flatjack to approximately 50 % of the estimated maximum flatjack pressure (which corresponds to the estimated compressive stress in the masonry). Reduce the flatjack pressure to zero.

9.10 Increase pressure in the flatjack to 25 %, 50 %, and 75 % of the estimated maximum pressure holding the pressure steady at each level. At each increment, measure and record the distance between each pair of gage points. Three repetitions of displacement measurement are required at each gage point. It is recommended that the test be conducted as soon as possible after formation of the slot: the time taken for load application shall be approximately equal to the time elapsed since formation of the slot to minimize the effects of creep deformations.

9.11 Continue pressurizing until the original gage distances are restored. The allowable average deviation from the original gage length shall be the greater of ± 0.0005 in. (± 0.013 mm) or $\frac{1}{20}$ th of the maximum initial deviation, with no single deviation exceeding the greater of ± 0.001 in. (± 0.025 mm) or

$\frac{1}{10}$ th of the maximum deviation. Tests in which these limits are exceeded shall be considered invalid. Record the final flatjack pressure.

9.12 Reduce the flatjack pressure to zero.

9.13 A second repetition of 9.10 and 9.11 is recommended to verify the final flatjack pressure.

9.14 Disconnect hoses and remove the flatjack. The slot may be filled with mortar or other suitable material of a color and strength similar to the original mortar.

10. Calculation

10.1 Calculate the average compressive stress in the masonry, f_m , as:

$$f_m = K_m K_a p \quad (2)$$

where:

K_m = a dimensionless constant which reflects the geometrical and stiffness properties of the flatjack, as determined by **Section 8**,

K_a = the ratio of measured area of the flatjack to the average measured area of the slot, and

p = flatjack pressure required to restore the gage points to the distance initially measured between them within the tolerance allowed, psi or MPa.

11. Report

11.1 Report each in situ stress determination including the following information:

11.2 Description of the testing conditions, for example, site, geographical location, environmental conditions, (for example, temperature), building identification, date of construction (if available), and name of the engineer/technician conducting the test. Include details of the type and quality of construction.

11.3 Identity and description of the specific test location in the structure and reason for the test.

11.4 Description and sources (if possible) of the masonry materials at the test location including a general condition statement, an elevation drawing, and other pertinent material data.

11.5 Method of forming the slot, a diagram of the slot, adjacent masonry, location of gage points, and all pertinent dimensions.

11.6 Description and source of the flatjack used, instrumentation, hydraulic system, flatjack installation, that is, use of shims, and other pertinent information.

³ Ronca, P., "The Significance of the Gauging System in the Flatjack In-Situ Stress Test for Masonry: Experimental Investigation," *The Masonry Society Journal*, Vol 14, No. 1, August 1996.

⁴ Schuller, M., "Flatjack Methods for Diagnosis of Modern Masonry," *Proceedings, On-Site Control and Evaluation of Masonry Structures*, Binda, L., deVekey, R., editors, RILEM, 2001.

⁵ Coombs J., Tanner J.E., "Development of Laboratories for Masonry Testing and Non-Destructive Evaluation," *The Masonry Society Journal*, Vol 26, No. 2, 2008, pp. 9-20.

11.7 Data sheets listing measurements taken at each pressure level.

11.8 The pressure at which the initial gage length was restored.

11.9 Flatjack calibration factor, K_m , and derivation.

11.10 Flatjack/slot area ratio, K_a , and calculation.

11.11 Magnitude of compressive stress and calculation.

11.12 Other observations.

12. Precision and Bias

12.1 The test data which is available shows the coefficient of variation of this test method to be as great as 20 % and it is

recommended that a minimum of three tests be conducted in the same general area to verify test results. Additional data is being assembled to verify the precision of the test method.

12.2 Laboratory studies have shown that the in situ stress test exhibits no inherent bias in predicting the state of compressive stress present in the masonry, that is, the method may over or under estimate the actual compressive stress.

13. Keywords

13.1 compressive stress; flatjack; in situ; masonry; nondestructive evaluation

ANNEX

(Mandatory Information)

A1. FLATJACK SHIMS

A1.1 The use of shims may be necessary during testing to achieve a tight fit of the flatjack in the slot and to ensure uniform transfer of pressure (stress) to the masonry over the complete area of the flatjack. Excessive deformations of the flatjack will cause inaccurate test results and could change the flatjack calibration factor K_m . Also it may be difficult to remove the flatjack from the slot after testing if it has deformed into voids. Grouting of the flatjack in the slot is not allowed, as the grout from the slot would flow into voids and cracks, altering the local behavior of the masonry.

A1.2 Three types of shims may be used: single piece shims, multiple piece shims, and fluid cushion shims.

A1.2.1 *Single Piece Shims*—Stiff metal shims having the same shape and size as the flatjack can be used to span voids in the masonry (see Fig. A1.1). Single piece shims should be placed between the flatjack and the irregular masonry surface,

and should be of sufficient thickness such that the flatjack fits tightly in the slot. To avoid damage to the flatjack after testing, it is recommended that the single piece shim be removed from the slot before attempting to remove the flatjack.

A1.2.2 *Multiple Piece Shims*—Metal shims made of several pieces can be used if the slot is irregular or of nonuniform thickness over its length (see Fig. A1.2). The individual pieces must fit tightly together and, in the case of an irregular slot, shall be of sufficient thickness to ensure a tight fit of the flatjack over its entire area. To avoid damage to the flatjack after the completion of testing, it is recommended that the multiple piece shims be removed from the slot before the flatjack is removed.

A1.2.3 *Fluid Cushion Shims*—Additional flatjacks, of geometry identical to the working flatjack, (Note A1.1) may be used as fluid shims. The fluid shim or shims should be inserted adjacent to the working flatjack, against the surface of the masonry. It may be necessary to use more than one fluid shim if the slot is thick in order to ensure a tight fit of the working flatjack in the slot. In this case, install fluid shims above and below the working flatjack. The fluid shims are seated initially by pressurizing to 75 to 80 % of the maximum predicted masonry in situ compressive strength. This allows the shim to deform into voids and irregularities in the slot. The shim pressure should be reduced to 5 to 10 psi (0.03 to 0.07 MPa) and the hydraulic line closed before proceeding with the test. After completion of the test, remove the working flatjack and the fluid cushion shim(s) from the slot.

NOTE A1.1—A *working flatjack* is one used in the test to estimate in situ stress and is the active flatjack as opposed to flatjacks used as fluid shims.

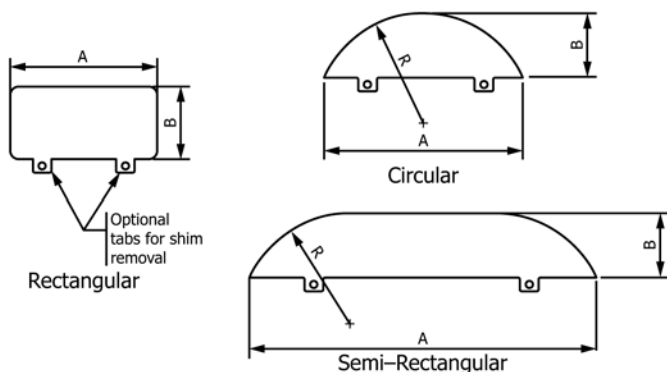


FIG. A1.1 Single Piece Shims (Plan View)

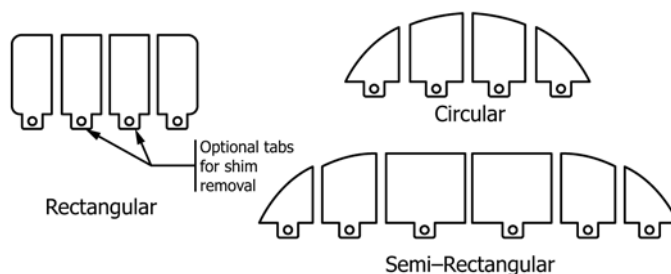


FIG. A1.2 Multiple Piece Shims (Plan View)

SUMMARY OF CHANGES

Committee C15 has identified the location of selected changes to this standard since the last issue (C1196 – 14) that may impact the use of this standard. (December 1, 2014)

- (1) Modified 2.1 to add Terminology C1180 and Terminology C1232.
- (2) Added Section 3 on Terminology and subsequent sections were renumbered.
- (3) Modified 8.3 and Fig. 3 to establish consistent use of the terms “shim” and “spacer.”

Committee C15 has identified the location of selected changes to this standard since the last issue (C1196 – 09) that may impact the use of this standard. (Approved July 1, 2014)

- (1) Changes have been made to 1.1, 7.3 and 7.4 to allow various means of creating slots.
- (2) Changes have been made to 6.1.1 and 9.8 to allow various hydraulic fluids.
- (3) Change has been made to 8.3 to modify spacer thickness requirement.
- (4) Change has been made to 8.4 to clarify moveable platen procedure.
- (5) Changes have been made to Fig. 3 to properly illustrate calibration alignment.

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