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Characterization Of Particulate Emissions From Refinery Process Heaters And Boilers

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**American Petroleum Institute
2101 L Street, Northwest
Washington, D.C. 20037**





CHARACTERIZATION OF PARTICULATE EMISSIONS
FROM REFINERY PROCESS HEATERS AND BOILERS

Prepared by:

ROY F. WESTON, INC.
WESTON WAY
WEST CHESTER, PENNSYLVANIA 19380

Prepared for:

AMERICAN PETROLEUM INSTITUTE
2101 L Street, Northwest
Washington, DC 20037



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1.0 EXECUTIVE SUMMARY

This report presents the results of a field testing effort to characterize particulate emissions from refinery combustion sources. The effort included 155 tests on two process heaters and three boilers over a one year period. The units are described in Table 1-1 along with process conditions and number of tests by category.

The major objective of this program was to determine emission factors, size distribution, and chemical composition of particulates from refinery combustion sources. This was accomplished by measuring and analyzing source emissions from several types of units under a variety of fuel firing and excess air conditions. The tests were run under steady load conditions.

Key study findings and data interpretation are presented in Section 4. A brief discussion of major study findings is given below.

1.1 Particulate Emission Rates

Particulate emission rates for heaters and boilers on 100 percent gas or 100 percent oil were less than those predicted by EPA emission factors (AP-42).¹ Emission rates for 100 percent gas or 100 percent oil firing ranged from 7 to 87 percent of the values predicted by AP-42. EPA particulate emission factors are shown on pages 8 and 12 in the report and compared to our test data. Emission rates for the two units firing 100 percent gas ranged from 7 to 65 percent of the lower range predicted by AP-42 estimates. Emission rates for the two units firing 100 percent oil ranged from 52 to 87 percent of the AP-42 estimates. Fuel oil emission test results are compared with AP-42 data in Figure 4-1 of the text. Although survey data are lower than the

¹The U.S. Environmental Protection Agency developed emission factors from tests conducted on industrial process boilers firing either 100 percent gas or 100 percent fuel oil. These factors were published in AP-42, "Compilation of Air Pollution Emission Factors," Third Edition, with Supplements 1 through 13. During this project, tests were conducted under both single- and mixed-fuel-firing conditions. Results from tests completed under single fuel conditions are compared directly herein with the AP-42 factors. For those tests performed under mixed-fuel-firing conditions, comparison emission factors were calculated by proportioning the AP-42 emission factors for oil and gas based on the heat rate of each fuel.

Table 1-1
UNIT DESCRIPTIONS AND DATA BASE

| Refinery | Source | Type of Unit | Max. Design Rating 10 ⁶ BTU/hr | Condition No. | Description of Conditions | | No. of Tests by Type | | |
|----------|--------|----------------|--|------------------|---------------------------------------|--|--------------------------|------------------|------------------------------|
| | | | | | Fuel Firing Ratio % Gas : % Oil | % O ₂ at Test Site (Boiler) | Particulate ¹ | PSD ² | NO _x ³ |
| A | 1 | Process Heater | 315 | 1 | 97.3 | 2.3 | 3 | 1 | 3 |
| | | | | 2 | 95.7 | 4.3 | 3 | 1 | 3 |
| | | | | 3 | 51.49 | 4.0 | 3 | 1 | 3 |
| | | | | 4 | 55.46 | 5.4 | 3 | 1 | 3 |
| B | 1 | Process Heater | 60.1 | 1 | 100.0 | 4.1 | 3 | - | 3 |
| | | | | 2 | 100.0 | 6.0 | 3 | - | 3 |
| | | | | 3 | 100.0 | 6.8 (2.9) | 3 | 1 | 3 |
| | | | | 4 | 100.0 | 8.6 (4.7) | 3 | - | 3 |
| A | 2- | Boiler | 215 | 1 | 63:31 | 8.9 (5.2) | 2 | 2 | 2 |
| | | | | 2 | 75:25 | 9.7 (6.5) | 2 | 2 | 2 |
| | | | | 3 | 40:60 | 8.7 (5.5) | 3 | 3 | 3 |
| | | | | 4 | 40:60 | 10.0 (6.8) | 3 | 3 | 3 |
| B | 2 | Boiler | 576 | 1 | 31:69 | 5.0 | 3 | 3 | 3 |
| | | | | 2 | 29:71 | 6.7 | 3 | 3 | 3 |
| | | | | 3 | 0:100 | 4.9 | 3 | 3 | 3 |
| | | | | 4 | 0:100 | 6.6 | 3 | 3 | 3 |
| C | 1 | Boiler | 200 | 1 | 43:57 | 9.1 (5.4) | 3 | 3 | 3 |
| | | | | 2 | 37:63 | 10.1 (6.5) | 3 | 3 | 3 |
| | | | | 3 | 0:100 | 7.3 (3.7) | 3 | 3 | 3 |
| | | | | 4 | 0:100 | 9.6 (5.4) | 3 | 3 | 3 |
| | | | | | TOTALS | 58 | 39 | 58 | |

¹EPA Method 5 as specified in Code of Federal Regulations, Title 40, Part 60, Appendix A, "Standards of Performance for New Stationary Sources," August 18, 1977.

²PSD = particle size distribution. Testing was performed according to Operating Manual for Andersen 2000, Inc., "Mark III Particle Sizing Stack Samplers," Andersen 2000 Inc., P. O. Box 20769, Atlanta, GA.

³EPA Method 7. Code of Federal Regulations, Title 40, Part 60, Appendix A, "Standards of Performance for New Stationary Sources," August 18, 1977.

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AP-42 predicted values, the data are within the range of data used to develop the AP-42 correlation.

Emission rates for mixed-fuel-firing ranged from 9 percent of the AP-42 lower limit to 125 percent of the AP-42 upper limit. Emissions from three of the four units were below those predicted by AP-42.

The effect of excess air on mass emissions was examined. Over the range of excess air conditions tested, no significant effects were observed.

1.2 Particle Size Distribution

The particle size distribution (PSD) test results indicate that relatively small particles are produced during both gas and oil firing. The data show that ~ 50 weight (wt) percent of the particles for most tests were submicron ($< 1 \mu\text{m}$). An average of about 75 percent of the particles by weight were $< 10 \mu\text{m}$ effective aerodynamic diameter. Excess air showed no effect on size distributions. The data show that a greater weight percentage of small particles is formed during gas firing than for oil- and mixed-fuel-fired conditions.

1.3 Chemical Composition

Particles were analyzed for heavy metals, extractable organics, sulfates, nitrates, and elemental carbon, hydrogen, and nitrogen. The particles generally contained small quantities of metals (< 2 wt percent) and no nitrates (< 0.1 wt percent). Organics content varied widely from less than 1 percent to over 50 percent. Sulfate content ranged from 25 to 85 wt percent. The remaining chemical constituents were not identified in this study.

1.4 Nitrogen Oxides

Results of limited oxides of nitrogen testing indicated that NO_x emissions increased with rising excess air levels and also with the proportion of oil fired in those sources.



2.0 INTRODUCTION

2.1 Background

The importance of airborne particulate size and chemical composition is being examined by EPA as the Agency considers revising the National Ambient Air Quality Standard for particulate matter. The impact of discrete size fractions and fine or respirable particles is being considered rather than the currently controlled total suspended particulate (TSP) matter.

As mandated by the Federal Clean Air Act, the promulgation of a revised particulate standard could have impact on control strategies and revisions to the existing State Implementation Plans. This would affect many source types, including refinery combustion sources (i.e., steam generators and process heaters) and non-fired sources (e.g., FCC stacks and cokers). The purpose of this test program is to provide a preliminary data base of particulate emission rates, size distributions, and chemical compositions.

2.2 The Study Objectives

The objectives of this program were:

1. To determine particulate emission factors.
2. To obtain particle size distribution data.
3. To determine the chemical composition of the particulate.

2.3 The Project Organization

The test program determined the particulate mass emission rates, particle size distribution, and chemical composition (i.e., sulfates, heavy metals, nitrates, and elemental analyses) from process heaters and steam-generating boilers. These data were related to fuel composition and to predicted AP-42 emission rates. Nitrogen oxides emission rates were measured and compared to predicted AP-42 values to demonstrate the relationship between particulates generation and nitrous oxide formation. The effects of excess air levels were examined for each test unit. Testing on the first unit started 14 July 1981, and on 19 May 1982 all testing was completed. A total of 155 tests on two heaters and three boilers were conducted.



2.4 Field Test Methods

Standard test methods were employed in the program as follows:

1. Mass emissions - EPA Method 5.
2. Particle size distribution - Andersen impactor.
3. NO_x - EPA Method 7.



3.0 DESCRIPTIONS OF UNITS TESTED

Five sources (two heaters and three boilers) were surveyed under this contract. A brief description of each unit is presented below. Additional information on each unit is provided in Appendix B.

3.1 Process Heaters

3.1.1 Refinery A - Source 1

This source is a 1978 Foster Wheeler side-fired horizontal radiant-tube crude process heater. It has a maximum gross fired duty of 315×10^6 Btu/hr; fuel ratios can be varied from 0 to 100 percent gas or oil.

3.1.2 Refinery B - Source 1

This source is a 1978 G.C. Broach Company vertical-fired process heater on a hydrotreating unit used for desulfurization of diesel distillate. Unit processing capacity is 25,000 barrels per operating day (bpd). Its maximum fired duty is 60.1×10^6 Btu/hr and it is typically operated at 25 percent of maximum duty. It is designed to only fire 100 percent plant fuel gas.

3.2 Boilers

3.2.1 Refinery A - Source 2

This source is a Riley Stoker boiler constructed in 1948. It is a balanced draft, end-horizontal-fired boiler with radiant tubes and horizontal section convection tubes. It has a maximum gross fired duty of 215×10^6 Btu/hr; fuel ratios can be varied from 0 to 100 percent refinery fuel gas or oil.

3.2.2 Refinery B - Source 2

This horizontal-fired steam generator, built in 1978 by Riley Stoker, is of a natural circulation, water tube-type design. Its steam production capacity is 440×10^3 lb/hr at a maximum heat rating of 576×10^6 Btu/hr. Its fuel-firing ratio is infinitely adjustable but is currently limited to about 30 percent gas based on the availability of process fuel gas.

3.2.3 Refinery C - Source 1

This boiler was designed by Babcock and Wilcox and constructed in 1942. It is a balanced draft, horizontal-fired unit with a maximum steam rating of 125,000 lb/hr at 750°F and 700 psig. The boiler has a design efficiency of 86 percent and is rated at 200×10^6 Btu/hr. It can be fired on gas or oil or any combination thereof.

4.0 RESULTS OF MEASUREMENTS

4.1 Mass Emissions

4.1.1 Process Heaters

Process heater emission factors based on the front-half catch¹ are compared to those from AP-42 in Table 4-1. Key particulate data and results are listed, by run, in Tables 4-2 and 4-3 for Refinery A Source 1 and Refinery B Source 1, respectively. Detailed data are included in Appendix A.

Data for Refinery A process heater were obtained while the source fired a combination of process gas and a No. 4 fuel oil (0.09 wt percent S, <0.01 wt percent ash) ranging from 51 to 97 percent gas on a Btu basis. The measured particulate emission factors were all less than the lower limits of the prorated EPA emission factor ranges for all combinations of fuel-firing and excess air. The average measured particulate emission factor was $0.0024 \pm 0.0006 \text{ lb}/10^6 \text{ Btu}$. The lower limits of the prorated EPA emission factor ranges varied from 0.0055 to 0.027 $\text{lb}/10^6 \text{ Btu}$.

Refinery B process heater operated on 100 percent fuel gas at its typical firing rate during the survey. The measured particulate emissions factors were an order of magnitude less than the lower limit of the AP-42 predicted range. As expected, the average measure particulate emission factor, $0.0004 \text{ lb}/10^6 \text{ Btu}$, was significantly less than the value obtained for the mixed-oil-gas-firing of Refinery A process heater.

Particulate emissions were measured at two excess air levels for each source. Excess air levels were monitored by stack percent O₂. The stack O₂ level varied from 2.0 to 5.5 percent for Refinery A Source 1 and from 4.1 to 6.0 percent for Refinery B Source 1. Two of the three tests indicated insignificant effects of excess air on particulate emissions. One test on the Refinery A heater, at very low excess air, showed increased emission rates.

Front-half and total (front-half plus back-half) particulate were measured.¹ For Refinery A heater (mixed-fuel-fired), the front-half catch averaged 62 percent of the total particulate. For Refinery B heater (gas-fired), the front-half particulate averaged 17 percent of the total catch.

¹Terms are defined in Appendix C.

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Table 4-1
Summary of Particulate Emission Factors from Process Heaters

| Refinery | Source | Test Run Numbers ⁴ | Fuel Firing Ratio Gas : % Gas | Percent Oil at Test Location | Heat Input 10 ⁶ BTU/hr | Fuel Firing Rate | | | Particulate Emission Factors ¹ | | |
|----------|--------|-------------------------------|-------------------------------|------------------------------|-----------------------------------|------------------|------------------|---------------------|---|----------------|------|
| | | | | | | Gas ³ | Oil ³ | 10 ³ gph | Measured EPA 2 | Measured EPA 3 | |
| A | | 1 | 1,2,3 | 97:3 | 2.0 | 262 | 0.212 | 0.054 | 0.0031 | 0.0055-0.014 | --- |
| | | | 4,5,6 | 93:7 | 4.0 | 257 | 0.200 | 0.125 | 0.0017 | 0.0073-0.015 | --- |
| | | | 7,9,11 | 51:49 | 4.0 | 270 | 0.115 | 0.914 | 0.0023 | 0.027-0.031 | --- |
| | | | 8,12,13 | 54:46 | 5.5 | 252 | 0.113 | 0.802 | 0.0023 | 0.025-0.029 | --- |
| B | | 1 | 4,5,6 | 100:0 | 4.1 | 15 | 0.015 | --- | 0.0004 | 0.0019-0.015 | 0.39 |
| | | | 1,2,3 | 100:0 | 6.0 | 16 | 0.016 | --- | 0.0003 | 0.0049-0.015 | 0.35 |

¹ Particulate is defined in this section as that material collected by EPA Method 5 (front-half catch).

² Values shown for single fuel firing conditions were calculated using AP-42 Emission Factors and actual fuel firing rates and fuel sample analysis results. Those shown for mixed fuel firing were calculated by proportioning the AP-42 Emission Factors for gas and oil based on the heat rate of each fuel using the following equation:

$$\frac{\text{lb Particulate}}{10^6 \text{ BTU}} = \frac{\text{Gas Emission Factor (AP-42)}}{\text{TOTAL FIRED DUTY}} + \frac{\text{Oil Emission Factor (AP-42)}}{\text{TOTAL FIRED DUTY}}$$

³ Values obtained from AP-42 Third Edition. Grade 4 oil was fired in Refinery A process heater.

⁴ Run 10 was discounted because of process swings during test.

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REFINERY A

SOURCE NO. 1

Table 4-2

SUMMARY OF TEST RESULTS

| Test Run Number ¹ | SUMMARY OF TEST RESULTS | | | | | | Eight | Twelve | Thirteen |
|--|-------------------------|-------|-------|------|------|------|-------|--------|----------|
| | One | Two | Three | Four | Five | Six | | | |
| Fuel Firing Ratio % Gas : % Oil | 100:0 | 100:0 | 91:9 | 94:6 | 91:9 | 94:6 | 46:54 | 46:54 | 61:39 |
| Percent O ₂ at Test Location | 2.3 | 2.3 | 2.3 | 4.4 | 4.3 | 4.3 | 3.8 | 4.1 | 4.1 |
| Particulate Results | | | | | | | | 5.2 | 5.5 |
| Front-Half | | | | | | | | | |
| Concentration, grains/dscf, $\times 10^{-3}$ | 3.0 | 1.6 | 2.2 | 0.7 | 1.3 | 1.3 | 1.9 | 1.3 | 1.1 |
| Mass Emission Rate, pounds/hour | 1.1 | 0.56 | 0.78 | 0.26 | 0.50 | 0.57 | 0.80 | 0.54 | 0.52 |
| Series Average Mass Emission Rate, lbs/hr | | 0.81 | | | 0.44 | | | 0.62 | |
| Total | | | | | | | | | |
| Concentration, grains/dscf, $\times 10^{-3}$ | 4.0 | 2.5 | 3.3 | 1.3 | 2.1 | 2.3 | 2.5 | 3.0 | 2.1 |
| Mass Emission Rate, pounds/hour | 1.4 | 0.91 | 1.2 | 0.50 | 0.81 | 0.99 | 1.1 | 1.3 | 0.97 |
| Series Average Mass Emission Rate, lbs/hr | | 1.2 | | | 0.77 | | | 1.1 | |
| NO _x Emissions, as NO ₂ ² | | | | | | | | | |
| Concentration, ppm by Volume, dry basis | 30. | 51. | 42. | 64. | 59. | 77. | 112. | 142. | 138. |
| Concentration, lbs/dscf, $\times 10^{-6}$ | 3.6 | 6.1 | 5.0 | 7.6 | 7.0 | 9.2 | 13. | 17. | 17. |
| Mass Emission Rate, pounds/hour | 8.8 | 15. | 12. | 21. | 19. | 28. | 40. | 51. | 53. |
| Series Average Mass Emission Rate, lbs/hr | | 12. | | | 23. | | | 48. | |

¹Run 10 was discounted because of process swings during test.
²Results shown are averages of three (3) grab samples.

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REFINERY B

SOURCE 1

TABLE 4-3

SUMMARY OF TEST RESULTS

| Test Run Number | Four | Five | Six | One | Two | Three |
|---|-------|-------|-------|-------|-------|-------|
| Fuel Firing Ratio, %Gas : 30 i1 | 100:0 | 100:0 | 100:0 | 100:0 | 100:0 | 100:0 |
| Percent O2 at test location | 4.0 | 4.0 | 4.4 | 6.3 | 5.8 | 5.9 |
| Particulate Results | | | | | | |
| Front-Half | | | | | | |
| Concentration, grains/dscf, $\times 10^{-5}$ | 11.8 | 2.23 | 21.5 | 5.68 | 18.6 | 10.1 |
| Mass Emission Rate, lbs/hr, $\times 10^{-3}$ | 5.76 | 1.04 | 10.2 | 2.74 | 9.06 | 4.99 |
| Series Average Mass Emission Rate, lbs/hr, $\times 10^{-3}$ | | 5.67 | | | 5.60 | |
| Total | | | | | | |
| Concentration, grains/dscf, $\times 10^{-5}$ | 64.6 | 62.7 | 77.6 | 54.7 | 84.0 | 58.8 |
| Mass Emission Rate, lbs/hr, $\times 10^{-3}$ | 31.5 | 29.3 | 36.6 | 26.4 | 41.0 | 29.0 |
| Series Average Mass Emission Rate, lbs/hr, $\times 10^{-3}$ | | 32.5 | | | 32.1 | |
| NOx Emissions, as NO ₂ ¹ | | | | | | |
| Concentration, ppm by volume, dry basis | 48.5 | 50.6 | 60.4 | 64.8 | 55.1 | 58.2 |
| Concentration, lbs/dscf, $\times 10^{-6}$ | 5.79 | 6.05 | 8.16 | 7.74 | 6.58 | 6.95 |
| Mass Emission Rate, lbs/hr | 1.97 | 1.98 | 2.69 | 2.62 | 2.25 | 2.40 |
| Series Average Mass Emission Rate, lbs/hr | | 2.21 | | | 2.42 | |

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¹Results shown are averages of three (3) grab samples.

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4.1.2 Boilers

Boiler particulate emissions factors, based on the front-half catch, are compared with AP-42 emission factors in Table 4-4. Summarized data can be found in Tables 4-5, 4-6, and 4-7 for Refinery A, B, and C boilers, respectively. Detailed data are included in Appendix A.

During 100 percent gas-firing conditions for Refinery A boiler, the average emission rate, $0.0022 \pm .0012 \text{ lb}/10^6 \text{ Btu}$, was less than the lower limit of the predicted EPA emission factor ($0.0045 \text{ lb}/10^6 \text{ Btu}$). During 100 percent oil-firing conditions for Refinery B and C boilers, the average measured emission rates were also less than the EPA-predicted rates:

| Refinery | Average Emission Factor, $\text{lb}/10^6 \text{ Btu}$ | Predicted EPA AP-42 Value*, $\text{lb}/10^6 \text{ Btu}$ |
|----------|--|---|
| B | $0.035 \pm .003$ | 0.069 |
| C | $0.071 \pm .022$ | 0.10 |

*Based on fuel composition and firing rates

Although the survey data are lower than the AP-42 predicted values, the data are within the range of data used to develop the AP-42 correlation (see Figure 4-1).

Particulate emission factors were estimated for mixed-fuel-firing on Refinery boilers A, B, and C by prorating AP-42 values based on fuel heat contents and firing rates. These prorated AP-42 values are compared to average measured emission rates below:

| Refinery | Average Emission Factor, $\text{lb}/10^6 \text{ Btu}$ | Range of Prorated EPA AP-42 Values, $\text{lb}/10^6 \text{ Btu}$ |
|----------|--|--|
| A | $0.012 \pm .004$ | $0.012 - 0.027$ |
| B | $0.030 \pm .005$ | $0.049 - 0.053$ |
| C | $0.078 \pm .009$ | $0.059 - 0.068$ |

The test data, shown in Table 4-4, generally indicated that mass emissions increased with the proportion of oil fired but showed no correlation with excess air over the range of excess air conditions studied.

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TABLE 4-4
Summary of Particulate Emission Factors from Boilers

| Refinery Source | Test Run Numbers | Fuel Firing Ratio % Gas : % Oil | Percent O ₂ at Test Location (Boiler) | Heat Input Rate 10 ⁶ BTU/hr | Fuel Firing Rate 10 ⁶ ft ³ /hr | Gas 10 ⁶ ft ³ /hr | Oil 10 ³ gph | Measured | Particulate Emission Factor ¹ | | |
|-----------------|------------------|------------------------------------|--|---|---|--|----------------------------|--------------|--|--|--|
| | | | | | | | | | EPA ² 1b/10 ⁶ BTU | EPA ² 1b/10 ⁶ BTU | Measured 1b/10 ³ gal oil |
| -12- | A 2 | 7.8, 9 | 100:0 | 6.8 (2.9) | 199 | 0.181 | --- | 0.0030 | 0.0045-0.014 | 3.3 | 5-15----- |
| | 10, 11, 12 | 100:0 | 8.6 (4.7) | 204 | 0.185 | --- | 0.0013 | 0.0045-0.014 | 1.5 | 5-15----- | |
| | 13, 14 | 69, 31 | 8.9 (5.2) | 196 | 0.123 | 0.411 | 0.0066 | 0.014-0.020 | --- | 5-15----- | |
| | 15, 16 | 75, 25 | 9.7 (6.5) | 194 | 0.132 | 0.328 | 0.0072 | 0.012-0.019 | --- | 5-15----- | |
| | 1, 2, 3 | 40, 60 | 8.7 (5.5) | 182 | 0.066 | 0.737 | 0.016 | 0.023-0.027 | --- | 5-15----- | |
| | 4, 5, 6 | 40, 60 | 10.0 (6.8) | 187 | 0.068 | 0.758 | 0.014 | 0.023-0.027 | --- | 5-15----- | |
| | B 2 | 1, 2, 3 | 31:69 | 5.0 | 549 | 0.114 | 2.53 | 0.028 | 0.049-0.052 | --- | 5-15----- |
| | 4, 5, 6 | 29, 71 | 6.7 | 541 | 0.103 | 2.59 | 0.032 | 0.050-0.053 | --- | 5-15----- | |
| | 10, 11, 12 | 0:100 | 4.9 | 560 | --- | 3.75 | 0.035 | 0.059 | (5.2) | 5-15----- | |
| | 7, 8, 9 | 0:100 | 6.6 | 567 | --- | 3.80 | 0.035 | 0.069 | (5.2) | 5-15----- | |
| | C 1 | 7.8, 9 | 43:57 | 9.1 (5.4) | 172 | 0.072 | 0.653 | 0.079 | 0.059-0.063 | --- | 5-15----- |
| | 10, 11, 12 | 37, 63 | 10.1 (6.5) | 160 | 0.057 | 0.674 | 0.076 | 0.065-0.068 | --- | 5-15----- | |
| | 1, 2, 3 | 0:100 | 7.3 (3.7) | 203 | --- | 1.36 | 0.054 | 0.10 | (8.0) | 5-15----- | |
| | 4, 5, 6 | 0:100 | 9.6 (5.4) | 155 | --- | 1.04 | 0.088 | 0.10 | (13) | 5-15----- | |

¹Particulate is defined in this section as that material collected by EPA Method 5 (front-half catch).

²Values shown for single fuel firing conditions were calculated using AP-42 Emission factors and actual fuel firing rates and fuel sample analysis results. Those shown for mixed fuel firing were calculated by prorating the AP-42 Emission Factors for gas and oil based on the heat rate of each fuel using the following equation:

$$\frac{1b \text{ Particulate}}{10^6 \text{ BTU}} = \frac{\text{Gas Emission Factor}}{(\text{Gas Fired Duty}) (\text{AP-42 Factor})} + \frac{\text{Oil Emission Factor}}{(\text{Oil Fired Duty}) (\text{AP-42 Factor})}$$

³The AP-42 Particulate Emission Factors for residual oil combustion are best described, on the average, as a function of fuel oil grade and sulfur content, as shown below: Grade 6 oil: 1b/10³ gal = 10 (S) + 3, where S is the percentage, by weight, of sulfur in the oil.

| | |
|---|------|
| Grade 5 oil: 10 lb/10 ³ gal. | 0.22 |
| Grade 4 oil: 7 lb/10 ³ gal. | 0.73 |
| For Refinery A, wt. % S in the oil = 0.22 | 0.19 |
| For Refinery B, wt. % S in the oil = 0.73 | 0.73 |
| For Refinery C, wt. % S in the oil = 1.19 | 1.19 |

⁴Grade 6 oil was fired in all boiler sources.

For Refinery A, wt. % S in the oil = 0.22
For Refinery B, wt. % S in the oil = 0.73
For Refinery C, wt. % S in the oil = 1.19

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**AMERICAN PETROLEUM INSTITUTE
REFINERY A**

SOURCE ?

TABLE 4-5
SUMMARY OF TEST RESULTS

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Results shown are averages of three (3) grab samples.

AMERICAN PETROLEUM INSTITUTE
REFINERY B
SOURCE 2
TABLE 4-6
SUMMARY OF TEST RESULTS

| Test Run Number | One | | | Four | | | Five | | | Six | | | Ten | | | Eleven | | | Twelve | | | Seven | | | Eight | | | Nine | | |
|--|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--------|-------|-------|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|--|
| | Two | Three | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Fuel Firing Ratio, % Gas : % Oil | 27:73 | 33:67 | 33:67 | 31:69 | 27:73 | 27:73 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | | |
| Percent O ₂ at Test Location | 4.8 | 5.0 | 5.1 | 6.7 | 6.7 | 6.6 | 4.9 | 4.9 | 5.0 | 4.7 | 5.0 | 4.7 | 6.5 | 6.5 | 6.7 | 6.6 | 6.5 | 6.7 | 6.6 | 6.5 | 6.7 | 6.6 | 6.5 | 6.7 | 6.6 | 6.5 | 6.7 | 6.6 | | |
| <u>Particulate Results</u> | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Front-Half | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Concentration, grains/dscf | 0.017 | 0.013 | 0.011 | 0.013 | 0.013 | 0.015 | 0.014 | 0.019 | 0.019 | 0.019 | 0.015 | 0.015 | 0.019 | 0.019 | 0.019 | 0.019 | 0.019 | 0.019 | 0.019 | 0.017 | 0.017 | 0.016 | 0.016 | 0.016 | 0.016 | 0.016 | 0.016 | 0.016 | | |
| Mass Emission Rate, pounds/hour | 18.2 | 14.7 | 12.3 | 16.2 | 18.8 | 17.5 | 20.4 | 21.3 | 16.6 | 19.9 | 20.7 | 19.1 | 19.9 | 20.7 | 19.1 | 19.9 | 20.7 | 19.1 | 19.9 | 19.9 | 19.9 | 19.9 | 19.9 | 19.9 | 19.9 | 19.9 | 19.9 | 19.9 | | |
| Series Average Mass Emission Rate, lbs/hr | 15.1 | 15.1 | 15.1 | 17.5 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 | | |
| Total | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Concentration, grains/dscf | 0.019 | 0.014 | 0.014 | 0.013 | 0.013 | 0.016 | 0.015 | 0.019 | 0.019 | 0.020 | 0.019 | 0.019 | 0.020 | 0.019 | 0.020 | 0.019 | 0.020 | 0.019 | 0.018 | 0.018 | 0.018 | 0.016 | 0.016 | 0.016 | 0.016 | 0.016 | 0.016 | 0.016 | | |
| Mass Emission Rate, pounds/hour | 20.3 | 15.0 | 15.0 | 16.3 | 19.3 | 18.9 | 20.9 | 21.9 | 20.3 | 21.0 | 21.0 | 21.0 | 21.0 | 21.0 | 21.0 | 21.0 | 21.0 | 21.0 | 21.2 | 21.3 | 21.3 | 21.3 | 21.3 | 21.3 | 21.3 | 21.3 | 21.3 | 21.3 | | |
| Series Average Mass Emission Rate, lbs/hr | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | 16.8 | | |
| <u>NO_x Emissions, as NO₂¹</u> | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Concentration, ppm by volume, dry basis | 110. | 106. | 127. | 125. | 79.8 | 115. | 131. | 133. | 140. | 130. | 132. | 130. | 130. | 132. | 130. | 132. | 130. | 132. | 130. | 132. | 130. | 132. | 130. | 132. | 130. | 132. | 130. | 132. | 130. | |
| Concentration, lbs/dscf, x 10-6 | 13.2 | 12.7 | 15.2 | 14.9 | 9.53 | 13.8 | 15.6 | 15.9 | 16.8 | 123. | 129. | 129. | 129. | 129. | 129. | 129. | 129. | 129. | 130. | 135. | 135. | 135. | 135. | 135. | 135. | 135. | 135. | 135. | | |
| Mass Emission Rate, lbs/hr | 98.0 | 98.1 | 117. | 131. | 81.2 | 118. | 121. | 123. | 129. | 110. | 124. | 124. | 124. | 124. | 124. | 124. | 124. | 124. | 131. | 131. | 131. | 131. | 131. | 131. | 131. | 131. | 131. | 131. | | |
| Series Average Mass Emission Rate, lbs/hr | 104. | 104. | 104. | 104. | 104. | 104. | 104. | 104. | 104. | 104. | 104. | 104. | 104. | 104. | 104. | 104. | 104. | 104. | 104. | 104. | 104. | 104. | 104. | 104. | 104. | 104. | 104. | 104. | 104. | |

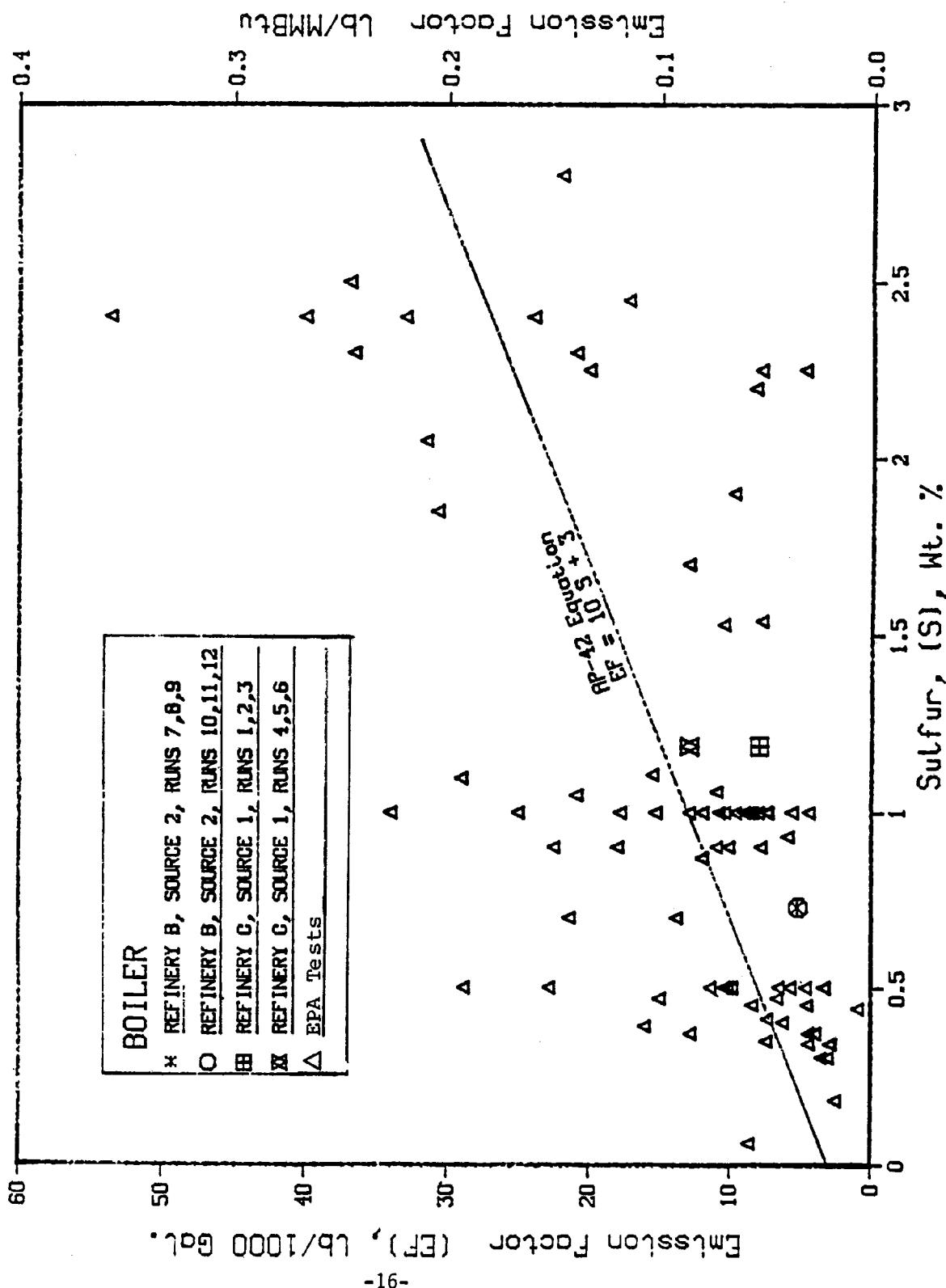
¹Results shown are averages of three (3) grab samples.

AMERICAN PETROLEUM INSTITUTE
REFINERY C
SOURCE 1
TABLE 4-7
SUMMARY OF TEST RESULTS

| Test Run Number | Seven | Eight | Nine | Ten | | | Eleven | | | Twelve | | | One | Two | Three | Four | Five | Six |
|--|-------|-------|-------|-------|-------|-------|--------|-------|-------|--------|-------|-------|-------|-------|-------|-------|-------|-----|
| | | | | Front | Half | Total | Front | Half | Total | Front | Half | Total | | | | | | |
| Fuel Firing Ratio, % Gas : % Oil | 47:53 | 36:64 | 48:52 | 43:57 | 33:67 | 35:65 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | 0:100 | |
| Percent O ₂ at Test Location | 9.2 | 9.1 | 9.1 | 10.5 | 10.2 | 9.7 | 7.5 | 7.5 | 7.5 | 7.2 | 9.5 | 9.5 | 9.6 | 9.5 | 9.5 | 9.6 | 9.6 | |
| Percent O ₂ Exiting Boiler | 5.5 | 5.4 | 5.4 | 6.4 | 6.6 | 6.5 | 3.5 | 4.0 | 3.5 | 3.5 | 5.4 | 5.4 | 5.5 | 5.4 | 5.4 | 5.5 | 5.5 | |
| <u>Particulate Results</u> | | | | | | | | | | | | | | | | | | |
| Concentration, grains/dscf | 0.030 | 0.037 | 0.035 | 0.034 | 0.027 | 0.029 | 0.021 | 0.030 | 0.027 | 0.038 | 0.039 | 0.031 | | | | | | |
| Mass Emission Rate, pounds/hour | 12.2 | 14.9 | 13.8 | 13.2 | 11.1 | 12.0 | 8.29 | 12.9 | 11.4 | 14.6 | 14.8 | 14.8 | 11.8 | | | | | |
| Series Average Mass Emission Rate, lbs/hr | 13.6 | | | 12.1 | | | 10.9 | | | | | | 13.7 | | | | | |
| <u>Total</u> | | | | | | | | | | | | | | | | | | |
| Concentration, grains/dscf | 0.031 | 0.042 | 0.040 | 0.035 | 0.028 | 0.031 | 0.027 | 0.032 | 0.038 | 0.041 | 0.049 | 0.034 | | | | | | |
| Mass Emission Rate, pounds/hour | 12.5 | 16.8 | 15.5 | 13.3 | 11.3 | 13.0 | 10.9 | 13.5 | 16.0 | 15.7 | 18.5 | 18.5 | 13.1 | | | | | |
| Series Average Mass Emission Rate, lbs/hr | 14.9 | | | 12.5 | | | 13.5 | | | | | | 15.8 | | | | | |
| <u>NO_x Emissions, as NO₂¹</u> | | | | | | | | | | | | | | | | | | |
| Concentration, ppm by volume, dry basis | 134. | | | 121. | 118. | | 130. | 127. | 109. | 157. | 123. | 191. | 170. | 162. | 158. | | | |
| Concentration, lbs/dscf, x 10 ⁻⁶ | | 16.0 | | 14.4 | 14.1 | 15.5 | 15.1 | 13.0 | 18.8 | 14.7 | 22.8 | | 19.3 | 18.9 | | | | |
| Mass Emission Rate, lbs/hr | 45.1 | 40.1 | 38.6 | 41.9 | 43.3 | 37.9 | 52.7 | 43.8 | 67.4 | 54.6 | | | 54.9 | 51.1 | 51.0 | | | |
| Series Average Mass Emission Rate, lbs/hr | 41.3 | | | | 41.0 | | | | | | | | | 52.3 | | | | |

¹Results shown are averages of the three (3) grab samples.

FIGURE 4-1
COMPARISON OF MEASURED PARTICULATE EMISSIONS
TO EPA'S AP-42 CORRELATION FOR
NO. 6 OIL-FIRED FURNACES





The impact of fuel mixture on front-half/back-half particulate catches was examined. The percentage front-half to total particulate catch was inversely related to the proportion of gas fired in the boilers:

| Refinery | Average % Gas Fired | Front Half:Total Particulate Catch, % |
|----------|---------------------|---------------------------------------|
| B | 15 | 94 |
| C | 20 | 89 |
| A | 71 | 47 |

4.2 Size Distribution

4.2.1 Process Heaters

Particle size distribution (PSD) data were obtained only for Refinery A heater (see Table 4-8 below for results summary). Single tests were performed at 70 percent gas : 30-percent oil-firing condition at two different oxygen levels. No PSD data were obtained for Refinery B heater because the extremely low particulate loading (average of 1.2×10^{-4} gr/dscf) prevented the attainment of sufficient mass with the impactor over a reasonable sampling period.

Additional PSD data are included in Appendix A.

TABLE 4-8

REFINERY A SOURCE 1
PARTICLE SIZE DISTRIBUTION DATA

| Fuel-Firing Ratio % Gas: % Oil | Percent O ₂ at Test Location | <u>Mass Percent Less Than Stated Size</u> | | | |
|-----------------------------------|---|---|--------|--------|---------|
| | | 0.3 um | 1.0 um | 3.0 um | 10.0 um |
| 70:30 | 3.9 | 84 | 86 | 87 | 88 |
| 70:30 | 5.5 | 70 | 72 | 73 | 76 |

The above data are presented graphically in Figure 4-2.

AMERICAN PETROLEUM INSTITUTE
REFINERY A SOURCE 1

PARTICLE SIZE DISTRIBUTION TEST RESULTS AT 70% GAS : 30% OIL

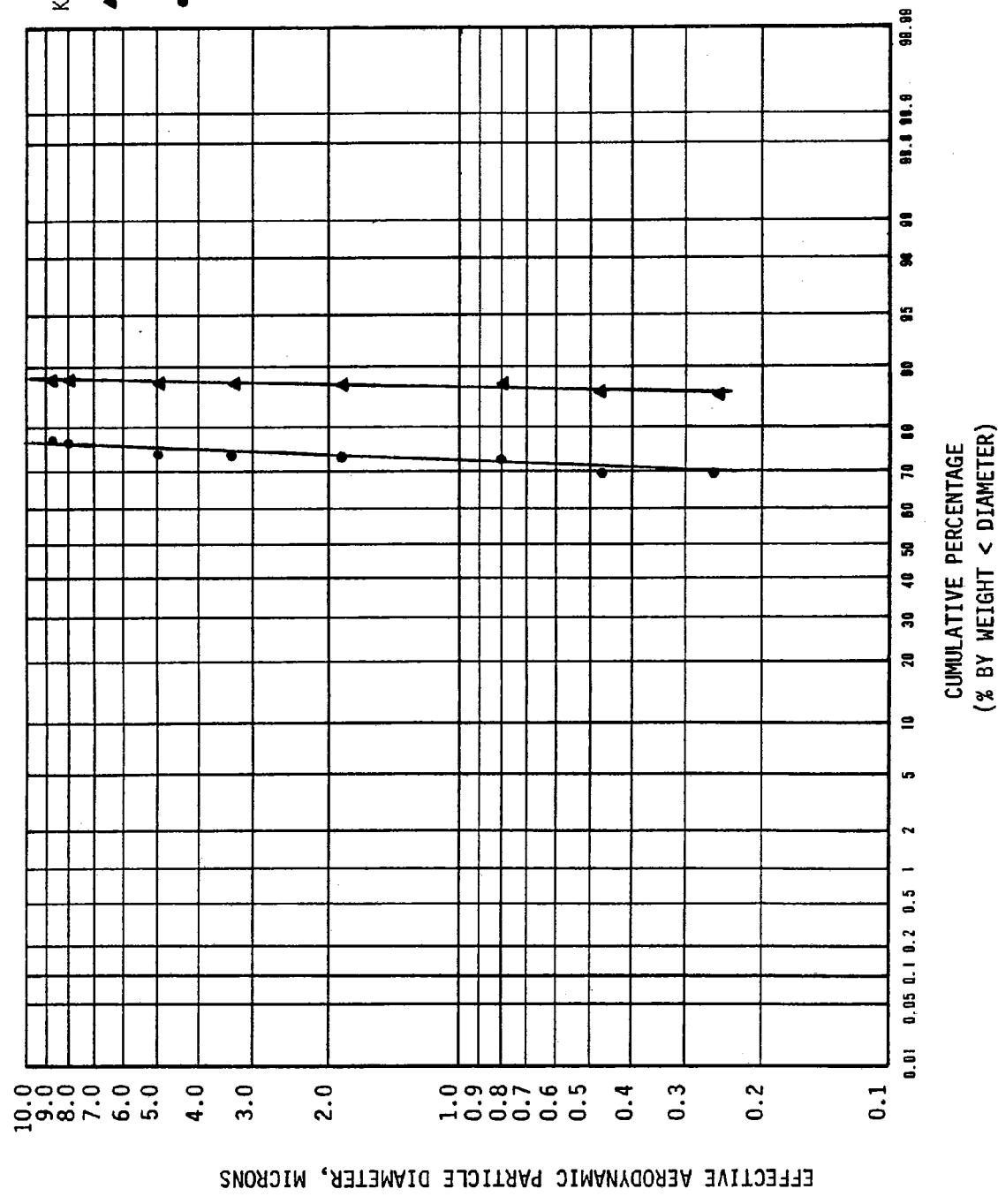


FIGURE 4-2



4.2.2 Boilers

Average PSD data for the three boilers are presented in Table 4-9. Mean mass percent less than 0.3, 1.0, 3.0, and 10 um data are shown for tests performed at each process condition. Detailed information for all PSD tests is contained in Appendix A.

Data from the single PSD test conducted under 100 percent gas-firing conditions are plotted in Figure 4-3. The range, mean, standard deviation, and quartile groups of the PSD data for all mixed fuel and for all 100 percent oil-firing conditions are shown graphically in Figures 4-4 and 4-5, respectively.

The size distributions are combined by fuel fired as shown in Table 4-10:

TABLE 4-10

CUMULATIVE WEIGHT PERCENTAGE LESS
THAN DIAMETER BY FUEL CONDITION

| Particle Size Range, um | 100% Gas | 100% Oil | Mixed |
|----------------------------|----------|-------------|-------------|
| ≤ 0.3 | 73 | 44 ± 11 | 44 ± 14 |
| ≤ 1.0 | 78 | 55 ± 9 | 53 ± 13 |
| ≤ 3.0 | 82 | 68 ± 7 | 63 ± 11 |
| ≤ 10.0 | 85 | 79 ± 6 | 72 ± 9 |

For submicron particles, the data show that a greater weight percentage of smaller particles is formed during gas-firing than for oil- and mixed-fuel-fired conditions. For particles greater than 1 um, no significant differences between fuel types were observed.

Under 100 percent gas-firing conditions, ~ 73 percent of the particles by weight were ≤ 0.3 um effective aerodynamic diameter (EAD). For oil, 40 to 50 percent of the particles by weight were ≤ 0.3 um effective aerodynamic diameter. No consistent effects of excess air on PSD were found.

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TABLE 4-9

AVERAGE PARTICLE SIZE DISTRIBUTION DATA SUMMARY FOR BOILER SOURCES

| Refinery/ Source | Fuel Firing Ratio % Gas : % Oil | Percent O ₂ at Boiler | Mass Percent Less than Stated Size and Standard Deviation | | | |
|---------------------|---------------------------------------|-------------------------------------|--|---------|---------|---------|
| | | | 0.3 um | 1.0 um | 3.0 um | 10.0 um |
| A/2 | 100:0 | 2.9 | 73 | 78 | 82 | 85 |
| | 69:31 | 5.2 | 49 ± 9 | 57 ± 11 | 63 ± 13 | 70 ± 12 |
| | 75:25 | 6.5 | 43 ± 4 | 55 ± 6 | 66 ± 8 | 76 ± 9 |
| | 40:60 | 5.4 | 38 ± 7 | 48 ± 6 | 58 ± 5 | 70 ± 3 |
| | 40:60 | 6.8 | 50 ± 3 | 57 ± 8 | 66 ± 5 | 73 ± 2 |
| B/2 | 31:69 | 5.0 | 65 ± 7 | 61 ± 10 | 77 ± 11 | 82 ± 13 |
| | 28:72 | 6.7 | 28 ± 11 | 39 ± 11 | 51 ± 10 | 64 ± 7 |
| | 0:100 | 4.9 | 44 ± 17 | 54 ± 14 | 64 ± 11 | 75 ± 8 |
| | 0:100 | 6.6 | 42 ± 5 | 55 ± 8 | 67 ± 9 | 77 ± 9 |
| C/1 | 44:56 | 5.4 | 29 ± 6 | 41 ± 8 | 53 ± 10 | 66 ± 9 |
| | 37:63 | 6.5 | 47 ± 4 | 59 ± 5 | 68 ± 7 | 78 ± 8 |
| | 0:100 | 3.7 | 40 ± 13 | 55 ± 9 | 70 ± 4 | 82 ± 1 |
| | 0:100 | 5.4 | 50 ± 11 | 62 ± 9 | 72 ± 6 | 82 ± 4 |

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REFINERY A SOURCE 2

PARTICLE SIZE DISTRIBUTION TEST RESULTS UNDER 100% GAS FIRING CONDITIONS

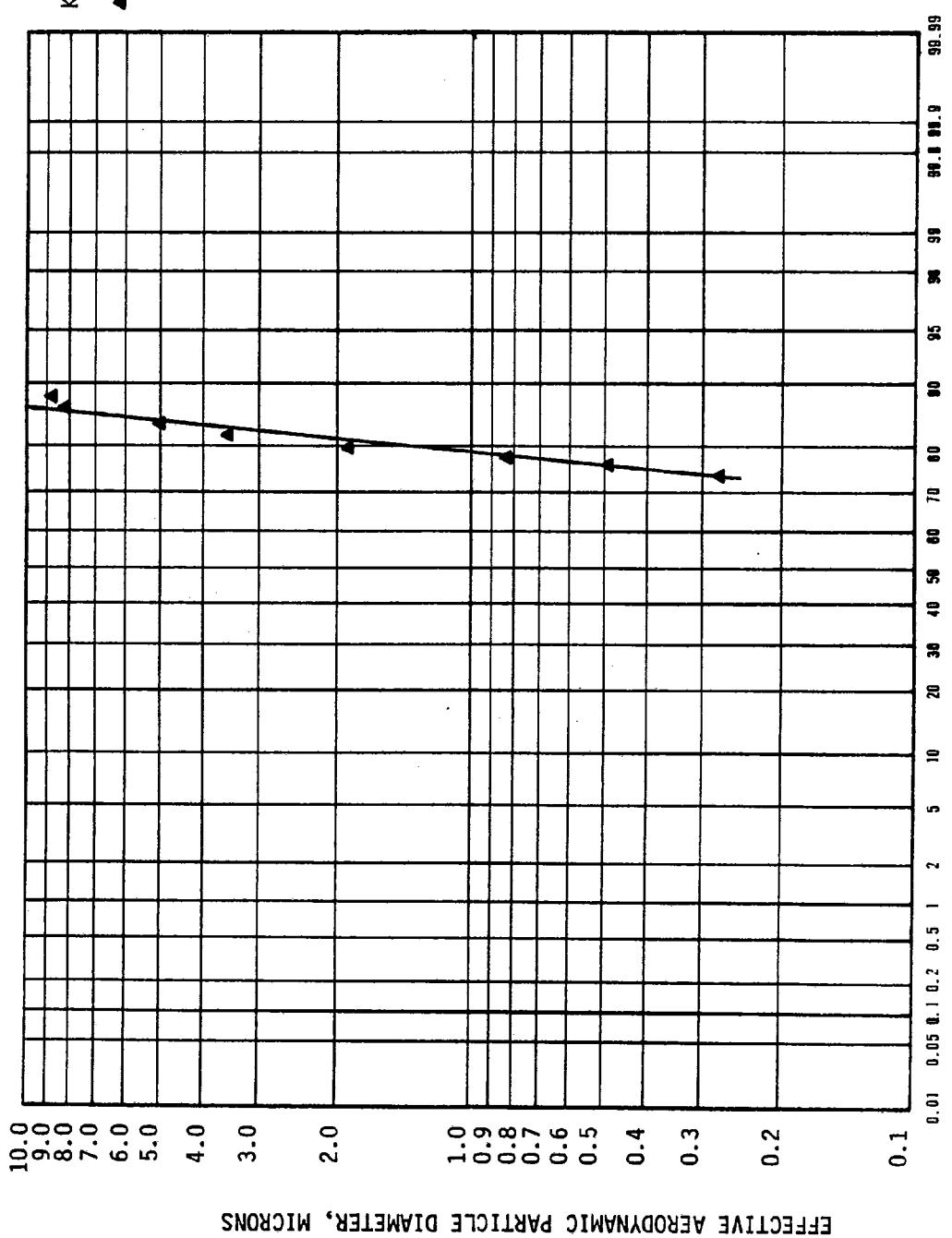
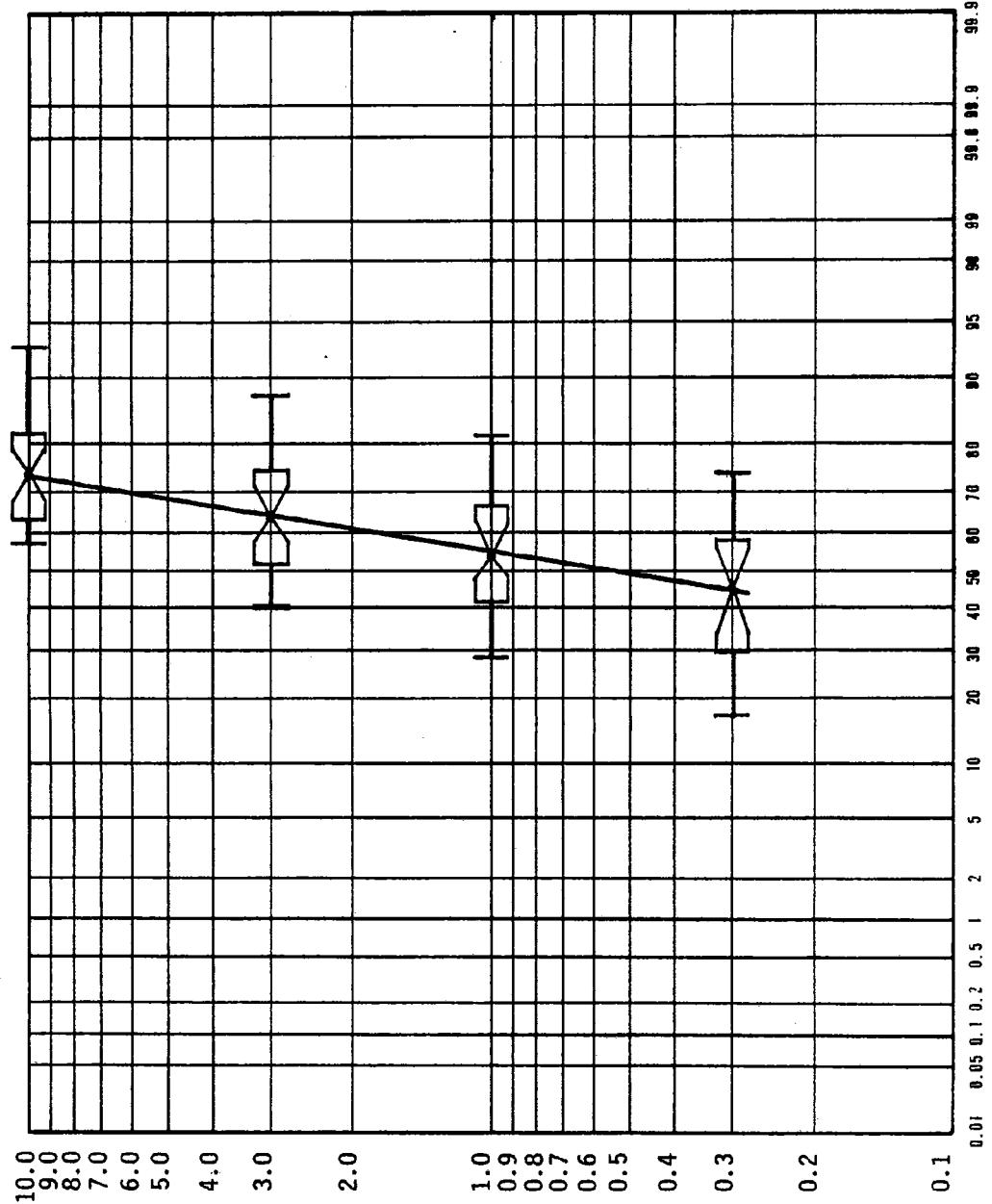


FIGURE 4-3

AMERICAN PETROLEUM INSTITUTE
BOILER SOURCES

SUMMARY OF PARTICLE SIZE DISTRIBUTION TEST RESULTS UNDER MIXED FUEL FIRING CONDITIONS



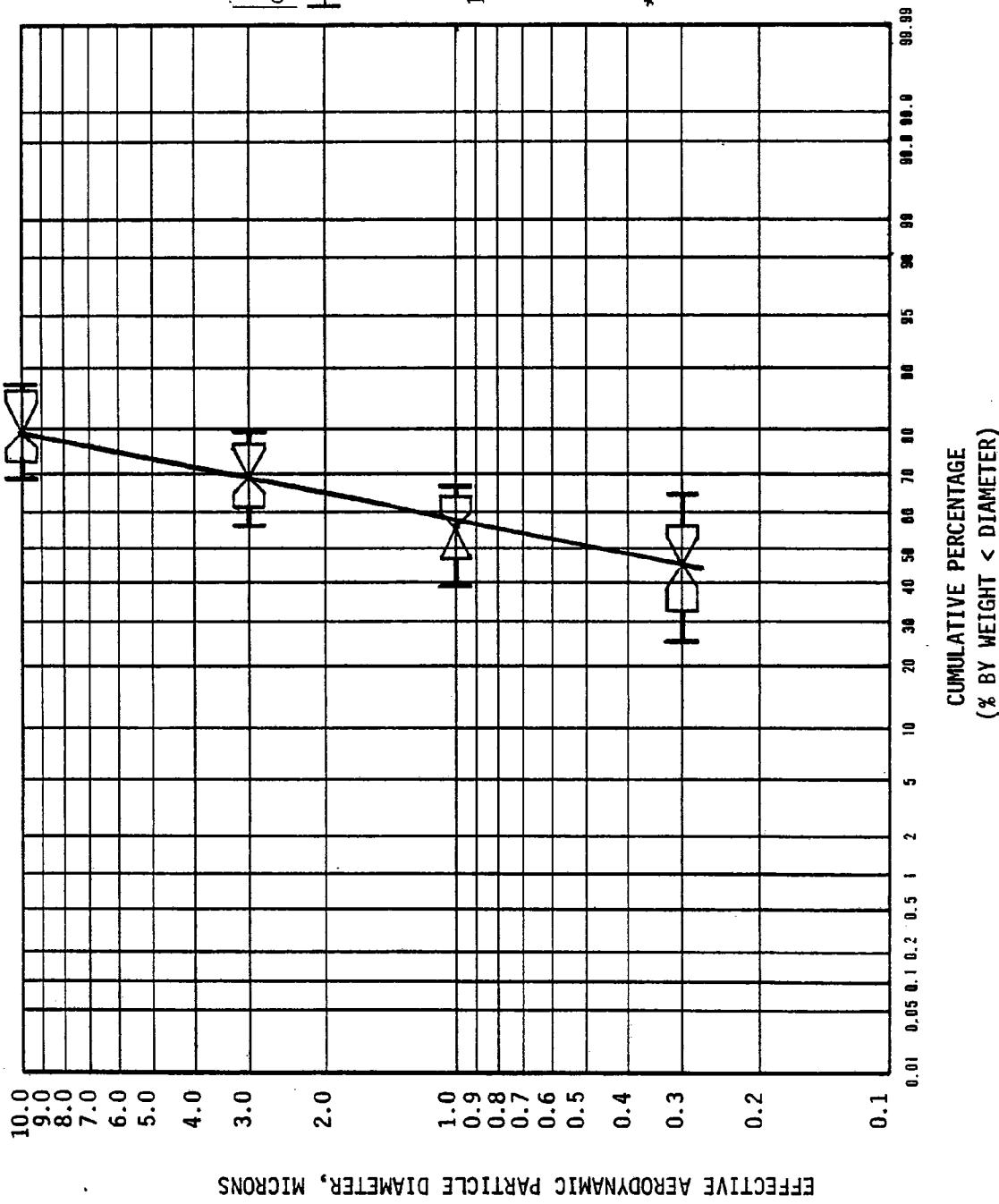
EFFECTIONAL AERODYNAMIC PARTICLE DIAMETER, MICRONS

-22-

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AMERICAN PETROLEUM INSTITUTE
BOILER SOURCES

SUMMARY OF PARTICLE SIZE DISTRIBUTION TEST RESULTS UNDER 100% OIL FIRING CONDITIONS



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4.3 Chemical Composition of Particulates

Particulates were analyzed for metal content, sulfates, nitrates and carbon, hydrogen, and nitrogen. The chemical composition of composite fuel oil samples was determined.

4.3.1 Process Heaters

The fuel oil analysis for Refinery A process heater tests is shown in Table 4-11. The fuel was a No. 4 fuel oil and had a relatively low sulfur and ash content. Detailed fuel analysis results are shown in Appendix A.

Particulate chemical analyses are presented for Refinery A heater in Tables 4-12 and 4-13. There was insufficient sample (<20 mg/test) at Refinery B heater (from the 6 to 9 hour-long tests) to conduct tests other than gravimetric analyses.

The total heavy metals content of the front-half particulate sample residues was <1.4 percent by weight for Refinery A heater. Small amounts (0.02 to 0.85 percent by weight) of chromium, copper, nickel, and zinc were detected in the front-half samples residues during some of the tests. It is believed that most of the chromium and nickel found in the Test Run No. 1 sample originated from the stainless steel nozzle of the sampling train since these values were out of line with those determined in the other tests. Essentially no heavy metals were captured in the back-half catch samples. Some arsenic and mercury (0.39 and 0.12 ppm by weight, respectively) were detected in the composite fuel oil sample but not in the source samples. Since arsenic, mercury, and selenium are relatively volatile metals, it is expected that those compounds would not have been effectively captured by an EPA Method 5 particulate train.

Elemental analysis was performed on front- and back-half catches. The results are presented in Table 4-13.

Sulfate was the major component of both front-half and back-half sample residues. The sulfate content of the front-half samples averaged 53 percent (by weight) while the back-half catches averaged 68 percent. The data indicate no effect of excess air or fuel sulfur content on particulate sulfur content. The sulfur content of particulate collected during 100 percent gas-fired conditions was higher than expected based on the typical sulfur content of fuel gas. This could possibly be attributed to the flaking-off of stack sulfur particulate from previous oil-firing



TABLE 4-11

REFINERY "A" FUEL OIL COMPOSITE SAMPLE ANALYSIS

| Analyte | Result |
|------------------------------|--------|
| Ash, % | <0.01 |
| Carbon, % | 86.9 |
| Hydrogen, % | 12.3 |
| Nitrogen, % | 0.16 |
| Oxygen, % | 0.52 |
| Sulfur, % | 0.09 |
| Metals, ppm by weight | |
| Arsenic | 0.39 |
| Barium | 0.18 |
| Cadmium | <0.04 |
| Chromium | <0.04 |
| Copper | 0.10 |
| Lead | <0.04 |
| Mercury | 0.12 |
| Nickel | 0.08 |
| Selenium | 0.19 |
| Vanadium | 0.04 |
| Zinc | 5.5 |

AMERICAN PETROLEUM INSTITUTE

REFINERY A

SOURCE 1

TABLE 4-12

MISCELLANEOUS ANALYTICAL RESULTS - METALS^{1,2}

| TEST RUN NUMBER: | One | | Four | | Seven | | Eight | |
|---|----------------|---------------|----------------|---------------|----------------|---------------|----------------|---------------|
| TEST DATE: | 7/14/81 | | 7/16/81 | | 7/18/81 | | 7/18/81 | |
| FUEL FIRING RATIO, % GAS : % OIL: | 100:0 | | 94:6 | | 46:54 | | 48:52 | |
| PERCENT O ₂ AT TEST LOCATION: | 2.3 | | 4.4 | | 3.8 | | 5.2 | |
| RESIDUE CATCH FRACTION ANALYSIS: | Front- half | Back- half | Front- half | Back- half | Front- half | Back- half | Front- half | Back- half |
| PARTICULATE CATCH RATIO, % FRONT-HALF: BACK-HALF: | 74:26 | | 51:49 | | 73:27 | | 74:26 | |
| <u>HEAVY METALS CONTENT, % BY WEIGHT</u> | | | | | | | | |
| Cr | 0.85 | 0.02 | 0.14 | ND | 0.09 | ND | 0.07 | ND |
| Cu | 0.03 | ND | 0.03 | ND | ND | ND | 0.02 | ND |
| Ni | 0.35 | ND | ND | ND | 0.04 | ND | ND | ND |
| Zn | 0.14 | ND | 0.12 | ND | 0.15 | ND | 0.15 | ND |

¹Note that barium, cadmium, lead and vanadium were not found in any of the samples.

²Key: ND = Not Detected (<0.01% by weight).

AMERICAN PETROLEUM INSTITUTE
 REFINERY A SOURCE 1
 STACK No. 1 (HEATER)

TABLE 4-13

SUMMARY OF ELEMENTAL AND ION CHROMATOGRAPHIC ANALYTICAL RESULTS

| Test Run Number | Test Date | Fuel Firing Ratio % Gas : % Oil / % O ₂ | Residue Catch Fraction Analysis | Particulate Catch Ratio % Front-half : % Back-half | Parameter, % by Weight | | |
|-----------------|-----------|--|---------------------------------|---|------------------------|-----|-----|
| | | | | | Elemental Analysis (1) | | |
| | | | | | C | H | N |
| Two | 7/15/81 | 100:0/2.3 | Front-half | <1 | 1.4 | 2.3 | 44 |
| | | | Back-half | 61:39 | 20 | 4.1 | 3.2 |
| Five | 7/16/81 | 91:9/4.3 | Front-half | <1 | 2.7 | 1.4 | 60 |
| | | | Back-half | 62:38 | 10 | 3.1 | 1.4 |
| Eleven | 7/20/81 | 61:39/4.1 | Front-half | <1 | 2.7 | 1.8 | 49 |
| | | | Back-half | 54:46 | 7.5 | 2.8 | 3.9 |
| Thirteen | 7/21/81 | 58:42/5.4 | Front-half | 51:49 | 4.6 | 3.3 | 3.1 |
| | | | Back-half | | 1.8 | 3.1 | 4.4 |
| | | | | | | | 61 |
| | | | | | | | < 2 |
| | | | | | | | < 2 |
| | | | | | | | < 2 |
| | | | | | | | < 2 |
| | | | | | | | < 2 |

(1) Elemental analysis results shown are questionable. Large errors due to working with small amounts of residue are probable.

operations. On the other hand, it might be attributed to artifact formation and weighing errors associated with small quantities of material analyzed. No nitrate particulate (<2 percent) was detected in any samples. The remaining chemical constituents of the particulate were not identified in this study.

4.3.2 Boilers

Metals content, sulfates, nitrates, extractable organics, and elemental analyses were determined. For comparison purposes, the chemical composition of test fuels is shown in Table 4-14. Detailed fuel analyses are presented in Appendix A.

No cadmium, silver, aluminum, calcium, magnesium, tin, or silica was detected in particulate samples from these test boilers (see Table 4-15). Small amounts (<1 percent) of barium, chromium, copper, lead, zinc, and potassium were found in some particulate residues. Greater amounts (up to 2 to 5 percent) of nickel, vanadium, sodium, and iron were measured in some particulate residues. Data from 100 percent oil tests were examined for a metals balance. Metals in the particulate residues were traceable to the fuel burned although a balance was not obtained in all cases. The metals contents of the process fuel gases were less than that of the fuel oils on a comparable Btu basis. As can be seen from Table 4-15, the front-half (filterable particulate) samples contained a greater percentage of metals than did the back-half (condensable particulate) catches in most instances.

The elemental analyses indicate that the carbon, hydrogen, and nitrogen content of the front-half samples is affected by excess air. As excess air was increased, the carbon, hydrogen, and nitrogen content was found to decrease. No such trend was evident for the back-half elemental analysis data. The back-half elemental analysis results for Refineries B and C are believed to contain large (\pm 50 percent) errors. These errors are introduced from accumulative weighing errors on samples in the 1 to 10 mg range in large (100 to 150 mg) containers and from analyzer errors from working at or below the normal limit of quantitation of the instrument. See Table 4-16 for results.

Sulfate particulate was a significant (25 to 83 percent by weight) constituent of front- and back-half catch residues for both gas and oil firing. Excess air levels and the fuel composition had no effect on the wt percent sulfate in the particulate when firing fuel oil (see Table 4-17).

Nitrate was not detected in any sample (<0.1 percent by weight). Chloride analyses were performed on Refinery A particulate catch residues but none was found (<0.1 percent by weight). The remaining chemical constituents of the particulates were not identified.



TABLE 4-14

FUEL OIL COMPOSITE SAMPLES ANALYSIS FOR BOILER SOURCES

| Analyte | Results | | |
|------------------------------|------------|------------|------------|
| | Refinery A | Refinery B | Refinery C |
| Ash, % | 0.02 | 0.03 | 0.02 |
| Carbon, % | 87.0 | 86.8 | 86.8 |
| Hydrogen, % | 12.2 | 11.3 | 11.2 |
| Nitrogen, % | 0.30 | 0.22 | 0.18 |
| Oxygen, % | 0.26 | 0.87 | 0.61 |
| Sulfur, % | 0.22 | 0.73 | 1.19 |
| Metals, ppm by weight | | | |
| Arsenic | <0.2 | <0.2 | <0.2 |
| Barium | 1.9 | 0.7 | 0.75 |
| Cadmium | <0.5 | <0.5 | <0.5 |
| Chromium | <0.5 | 0.7 | <0.5 |
| Copper | 3.0 | 1.5 | <0.5 |
| Lead | <0.5 | 5.4 | <0.5 |
| Mercury | 0.03 | 0.05 | 0.07 |
| Nickel | 21 | 11 | 11 |
| Selenium | 0.26 | <0.1 | 0.49 |
| Vanadium | <0.5 | 2.1 | 31 |
| Zinc | 10 | 6.7 | 1.7 |

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TABLE 4-15
MISCELLANEOUS ANALYTICAL RESULTS - METALS^{1,2}

| Refinery/ Source | Test Run Number | Test Date | Fuel Firing Ratio % Gas : % Oil | Boiler % O ₂ | Particulate Fraction | Particulate Catch % FH : % BH | METALS CONTENT, % BY WEIGHT | | | | | | | | | |
|---------------------|-----------------------|--------------|--|----------------------------|-------------------------|-------------------------------------|-----------------------------|------|------|------|------|------|------|-----|-----|------|
| | | | | | | | Ba | Cr | Cu | Ni | Pb | V | Zn | K | Na | Fe |
| A/2 | Seven | 5/8/82 | 100:0 | 2.9 | Front-half | 52:48 | ND | 0.02 | 0.01 | 0.12 | ND | 0.07 | 0.16 | ND | ND | 1.1 |
| | Ten | 5/10/82 | 100:0 | 4.8 | Front-half | 35:65 | 0.48 | ND | 0.02 | 0.29 | ND | 0.18 | 0.34 | ND | ND | 0.88 |
| Thirteen | 5/12/82 | 68:32 | 5.3 | Front-half | 63:37 | 0.53 | 0.02 | 0.09 | 3.1 | ND | 0.63 | 0.75 | 0.14 | 1.5 | 4.2 | |
| Fifteen | 5/13/82 | 75:25 | 6.5 | Front-half | 50:50 | 0.54 | 0.02 | 0.06 | 2.9 | ND | 0.61 | 0.69 | 0.34 | 2.3 | 4.7 | |
| One | 5/4/82 | 40:60 | 5.5 | Front-half | 53:47 | 0.27 | 0.05 | 0.06 | 3.2 | ND | 0.66 | 0.51 | 0.17 | 1.4 | 4.7 | |
| Four | 5/6/82 | 41:59 | 6.8 | Front-half | 58:42 | 0.36 | 0.02 | 0.05 | 3.6 | ND | 0.75 | 0.53 | 0.12 | 1.4 | 4.1 | |
| B/2 | One | 12/11/81 | 27:73 | 4.8 | Front-half | 90:10 | 0.29 | 0.04 | 0.07 | 0.86 | 0.51 | 0.96 | 0.39 | --- | --- | |
| | Four | 12/13/81 | 31:69 | 6.7 | Front-half | 99:01 | 0.38 | 0.05 | 0.08 | 1.3 | 0.58 | 1.4 | 0.46 | --- | --- | |
| | Ten | 12/17/81 | 0:100 | 4.9 | Front-half | 98:02 | 0.44 | 0.05 | 0.06 | 1.4 | 0.49 | 1.3 | 0.49 | --- | --- | |
| | Seven | 12/15/81 | 0:100 | 6.5 | Front-half | 94:06 | 0.34 | 0.05 | 0.07 | 0.14 | 0.50 | 1.3 | 0.48 | --- | --- | |
| C/1 | Seven | 3/3/82 | 47:53 | 5.5 | Front-half | 98:02 | 0.02 | 0.02 | 0.01 | 0.63 | 0.02 | 1.4 | 0.06 | --- | --- | |
| | Ten | 3/22/82 | 43:57 | 6.4 | Front-half | 99:01 | 0.03 | 0.02 | 0.01 | 0.16 | ND | 0.11 | --- | --- | --- | |
| | One | 2/17/82 | 0:100 | 3.5 | Front-half | 76:24 | 0.05 | 0.09 | 0.02 | 0.23 | 0.05 | 1.1 | 0.09 | --- | --- | |
| | Four | 2/22/82 | 0:100 | 5.4 | Front-half | 93:07 | 0.03 | 0.02 | 0.01 | 0.42 | ND | 1.7 | 0.04 | --- | --- | |

¹Note that cadmium, silver, aluminum, calcium, magnesium, tin and silica were not found in any samples analyzed.

²Key: ND = Not Detected (<0.01% by weight).
--- = Means parameter not run.

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TABLE 4-16

SUMMARY OF ELEMENTAL AND ION CHROMATOGRAPHIC ANALYTICAL RESULTS

| Refinery | Test Run Number | Test Date | Fuel Firing Ratio % Gas : % Oil | Percent O ₂ Existing Boiler (at test point) | Residue Catch Fraction Analysis | Particulate Catch Ratio % Front-half: % Back-half: | PARAMETER, % BY WEIGHT | | | | |
|----------|-----------------|-----------|---------------------------------|--|---------------------------------|--|------------------------|-----|-----|----------|----------------------------------|
| | | | | | | | C | H | N | Analysis | Ion Chromatographic Analysis (1) |
| A | Eight | 5/8/82 | 100:0 | 3.0 (7.0) | Front-half Back-half | 32:68 | 24 | 6.9 | 0.9 | 41 | ND |
| | Eleven | 5/10/82 | 100:0 | 4.6 (8.7) | Front-half Back-half | 27:73 | 13 | 4.2 | 1.8 | 49 | ND |
| Fourteen | 5/12/82 | 70:30 | 5.1 (9.0) | Front-half Back-half | 46:54 | 12 | 4.0 | 1.2 | 32 | ND | |
| Sixteen | 5/13/82 | 74:26 | 6.4 (9.8) | Front-half Back-half | 42:58 | 13 | 3.8 | 0.8 | 39 | ND | |
| Two | 5/15/82 | 40:60 | 5.3 (8.6) | Front-half Back-half | 59:41 | 5.1 | 4.5 | 0.6 | 28 | ND | |
| Five | 5/7/82 | 40:60 | 6.8 (10.0) | Front-half Back-half | 48:52 | 8.5 | 2.4 | 0.1 | 32 | ND | |
| B | Two | 12/12/81 | 33:67 | --- | Front-half Back-half | 3.3 | 3.8 | 1.0 | 43 | ND | |
| Five | 12/14/81 | 27:73 | --- | Front-half Back-half | 98:02 | 3.1 | 4.1 | 0.9 | 31 | ND | |
| Eleven | 12/17/81 | 0:100 | --- | Front-half Back-half | 48:52 | 5.9 | 2.3 | 0.3 | 46 | ND | |
| Eight | 12/16/81 | 0:100 | --- | Front-half Back-half | 42 | 4.2 | 0.8 | 46 | ND | ND | |
| C | Eight | 3/4/82 | 36:54 | 9.1 (5.4) | Front-half Back-half | 97:03 | 13 | 3.1 | 0.4 | 45 | ND |
| Eleven | 3/23/82 | 33:67 | 10.2 (6.6) | Front-half Back-half | 97:03 | 8.7 | 1.3 | 0.2 | 32 | ND | |
| Two | 2/18/82 | 0:100 | 7.5 (4.0) | Front-half Back-half | 97:03 | 22 | 4.3 | 2.5 | 71 | ND | |
| Five | 2/22/82 | 0:100 | 9.5 (5.4) | Front-half Back-half | 88:12 | 4.3 | 1.3 | 0.2 | 25 | ND | |
| | | | | | Front-half Back-half | 21 | 5.2 | 2.7 | 70 | ND | |
| | | | | | Front-half Back-half | 43 | 6.5 | 2.8 | 62 | ND | |
| | | | | | Front-half Back-half | 25 | 2.3 | 0.4 | 35 | ND | |
| | | | | | Front-half Back-half | 4.2 | 3.6 | 0.1 | 75 | ND | |
| | | | | | Front-half Back-half | 6.9 | 2.4 | 0.2 | 26 | ND | |
| | | | | | Front-half Back-half | 27 | 5.4 | 7.1 | 49 | ND | |
| | | | | | Front-half Back-half | 15 | 2.0 | 0.2 | 60 | ND | |
| | | | | | Front-half Back-half | 21 | 3.4 | 2.6 | 40 | ND | |
| | | | | | Front-half Back-half | 5.0 | 2.6 | 0.1 | 60 | ND | |
| | | | | | Front-half Back-half | 0.8 | 1.2 | 0.1 | 83 | ND | |

(1) ND = Not Detected (<0.1% by weight).

TABLE 4-17
PERCENT FUEL SULFUR CONVERTED TO PARTICULATE

| Refinery/ Source | Fuel Oil Sulfur Content, % | % Oil Fired in Boiler | % O ₂ Exiting Boiler | Sulfate Particulate Emission Rate, as S, 1b/hr | Fuel Input to Boiler, 1b/hr | % Fuel Sulfur Converted to Particulate |
|---------------------|----------------------------------|-----------------------------|---------------------------------------|--|--------------------------------------|---|
| A/2 | 0.22 | 30 | 5.1 | 0.32 | 7.0 | 4.6 |
| | | 26 | 6.4 | 0.46 | 5.6 | 8.2 |
| | | 60 | 5.3 | 0.57 | 1.3 | 4.5 |
| B/2 | 0.73 | 67 | 5.0 | 2.2 | 14.8 | 1.5 |
| | | 73 | 6.7 | 2.1 | 15.1 | 1.4 |
| | | 100 | 5.0 | 1.9 | 21.8 | 0.9 |
| C/1 | 1.19 | 54 | 5.4 | 2.2 | 6.2 | 3.6 |
| | | 67 | 6.6 | 1.0 | 6.4 | 1.6 |
| | | 100 | 4.0 | 2.7 | 13.0 | 2.0 |
| | | 100 | 5.4 | 4.0 | 9.9 | 4.0 |



Analytical results (Table 4-18) showed that a greater percentage of solvent extractable material was produced under gas-firing conditions than for oil. Back-half catches contained a higher proportion of solvent extractables than did the front-half samples. Excess air levels had no effect on the solvent extractable content of the particulate.

4.4 NO_x Emissions

The NO_x emission test results are presented in this section. The data are compared to EPA AP-42 emission factors in Tables 4-19 and 4-20. More detailed NO_x information is contained in Appendix A.

4.4.1 Heaters and Boilers

Survey findings for all sources are compared to AP-42 emission factors in Tables 4-19 and 4-20.

TABLE 4-19

COMPARISON OF MEASURED VS. AP-42 NO_x EMISSION FACTORS

| Refinery/ Source | Fuel Firing Condition % Gas : % Oil | Percent of Predicted AP-42 Emission Factor ¹ |
|---------------------|--|--|
| A/1 (Heater) | 95:5 | 16 |
| | 53:47 | 35 |
| B/1 (Heater) | 100:0 | 100 |
| A/2 (Boiler) | 100:0 | 23 |
| | 72:28 | 63 |
| | 40:60 | 80 |
| B/2 (Boiler) | 30:70 | 31 |
| | 0:100 | 32 |
| C/1 (Boiler) | 40:60 | 76 |
| | 0:100 | 129 |

¹For mixed-fuel-firing conditions, measured values are compared to prorated AP-42 factors.

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TABLE 4-18
SOLVENT EXTRACTABLES RESULTS

| Refinery | Test Run Number | Test Date | Fuel Firing Ratio % Gas : % Oil | Percent O ₂ Exiting Boiler (at test point) | Particulate Catch Ratio % Front-half:% Back-half | Residue Catch Fraction Analysis | Solvent Extractables, % by Weight ¹ |
|----------|-----------------|-----------|------------------------------------|---|---|--|--|
| A | Nine | 5/9/82 | 100:0 | 2.9 (6.6) | 35:65 | Front-half Back-half | 13 32 |
| | Twelve | 5/11/82 | 100:0 | 4.6 (8.5) | 36:64 | Front-half Back-half | 53 88 |
| | Three | 5/5/82 | 59:41 | 5.5 (8.9) | 55:45 | Front-half Back-half | 15 56 |
| | Six | 5/7/82 | 58:42 | 6.8 (10.0) | 52:48 | Front-half Back-half | 12 31 |
| B | Three | 12/12/81 | 33:67 | --- | 82:18 | Front-half Back-half | 0.8 7.1 |
| | Six | 12/14/81 | 27:73 | --- | 93:07 | Front-half Back-half | 0.2 73 |
| | Twelve | 12/18/81 | 0:100 | --- | 82:18 | Front-half Back-half | 0.8 77 |
| | Nine | 12/16/81 | 0:100 | --- | 96:04 | Front-half Back-half | 0.8 61 |
| C | Nine | 3/4/82 | 48:52 | 5.4 (9.1) | 89:11 | Front-half Back-half | 2.3 79 |
| | Twelve | 3/23/82 | 37:63 | 6.5 (9.7) | 92:08 | Front-half Back-half | 0.9 73 |
| | Three | 2/19/82 | 0:100 | 3.5 (7.2) | 71:29 | Front-half Back-half | 0.05 6.4 |
| | Six | 2/23/82 | 0:100 | 5.5 (9.6) | 90:10 | Front-half Back-half | 0.09 17 |

¹Large weighing errors ($\pm 50\%$) may be present in results for those samples containing <10 mg of particulate.



The above data indicate that measured NO_x emissions are usually lower than predicted by AP-42. Data in Table 4-20 show that NO_x emissions increase with rising excess air levels and quantity of oil fired.

The reader is referred to AP-42 for a discussion of emissions dependency on the grade and composition of fuel, the type and size of boiler, the firing and loading practices used, and the level of equipment maintenance. Some of the differences between measured and predicted NO_x emissions shown in the above table are due to the way AP-42 categorizes heaters and boilers. This is especially true for Refinery/Source A/1 and A/2 when firing gas.

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TABLE 4-20
SUMMARY OF NO_x EMISSION FACTORS FROM PROCESS HEATERS AND BOILERS

| Refinery | Source | Test Run Numbers | Fuel Firing Ratio % Gas : % Oil | Percent O ₂ at Test Location (at Boiler) | Heat Input Rate 10 ⁶ BTU/hr | Fuel Firing Rate 10 ⁶ ft ³ /hr | Measured 0 <i>i</i> 1 | EPA ¹ 1b/10 ⁶ BTU | Measured 1b/10 ⁶ SCF gas (1b/10 ³ gal oil) | EPA ² 1b/10 ⁶ SCF gas; 1b/10 ³ gal oil |
|----------|------------|------------------|---------------------------------|---|--|--|-----------------------|---|--|---|
| | | | | | | | Gas | 10 ³ gph | 1b/10 ⁶ BTU | |
| A | 1 (Heater) | 1,2,3 | 97.3 | 2.0 | 262 | 0.212 | 0.054 | 0.048 | 0.42 | --- |
| | | 4,5,6 | 93.7 | 4.0 | 257 | 0.200 | 0.125 | 0.088 | 0.42 | --- |
| | | 7,9,11,15 | 51.49 | 4.0 | 270 | 0.115 | 0.914 | 0.18 | 0.58 | --- |
| B | 1 (Heater) | 8,12,13 | 54.46 | 5.5 | 252 | 0.113 | 0.802 | 0.21 | 0.55 | --- |
| | | 4,5,6 | 100.0 | 4.1 | 15 | 0.015 | --- | 0.148 | 0.117-0.225 | 151 |
| | | 1,2,3 | 100.0 | 6.0 | 16 | 0.016 | --- | 0.149 | 0.117-0.225 | 152 |
| C | 2 (Boiler) | 10,11,12 | 100.0 | 6.8 { (2.9) } | 199 | 0.181 | --- | 0.11 | 0.55 | 110 |
| | | 13,14 | 69.31 | 8.6 { (4.7) } | 204 | 0.185 | --- | 0.18 | 0.57 | 180 |
| | | 15,16 | 75.25 | 9.7 { (6.5) } | 196 | 0.123 | 0.411 | 0.31 | 0.48 | 576 |
| B | 2 (Boiler) | 1,2,3 | 40.60 | 8.7 { (5.5) } | 194 | 0.132 | 0.328 | 0.29 | 0.48 | 567:583 |
| | | 4,5,6 | 40.60 | 10.0 { (6.8) } | 182 | 0.066 | 0.737 | 0.33 | 0.42 | 518:58 |
| | | 1,2,3 | 31.69 | 5.0 | 187 | 0.068 | 0.758 | 0.35 | 0.43 | 532:58 |
| C | 1 (Boiler) | 4,5,6 | 29.71 | 6.7 | 549 | 0.114 | 2.53 | 0.19 | 0.62 | --- |
| | | 10,11,12 | 0:100 | 4.9 | 541 | 0.103 | 2.59 | 0.20 | 0.62 | --- |
| | | 7,8,9 | 0:100 | 6.6 | 560 | --- | 3.75 | 0.22 | 0.70 | (33) |
| -36- | 1 (Boiler) | 10,11,12 | 37.63 | 9.1 { (5.4) } | 172 | 0.072 | 0.653 | 0.24 | 0.35 | --- |
| | | 1,2,3 | 0:100 | 7.3 { (3.7) } | 160 | 0.057 | 0.674 | 0.26 | 0.31 | 525:354 |
| | | 4,5,6 | 0:100 | 9.6 { (5.4) } | 203 | --- | 1.36 | 0.27 | 0.23 | (40) |
| | | | | 155 | --- | 1.04 | 0.34 | 0.23 | (50) | --- |

¹Calculated using the following equation: $\frac{1b \text{ NO}_x}{10^6 \text{ BTU}} = \frac{(\text{Gas Fired Duty})(\text{AP-42 Factor})}{(\text{Oil Fired Duty})} + (\text{Oil Fired Duty}) \frac{\text{Gas Emission Factor}}{\text{Factor}}$

TOTAL FIRED DUTY

²Values obtained from AP-42 Third Edition, April 1981, assuming all units to be non-tangentially fired. Gas emission factors were calculated by correcting the maximum gross load boiler emission factor for units >100 x 10⁶ BTU/hr (= 700 1b NO_x/10⁶ BTU) with a load reduction coefficient determined from actual load conditions.

³Oil emission factor based on Refinery A, Source 2 fuel composition of N content = 0.30 wt % and 1b NO_x/10³ gal oil = 22 + 400N² = 58

⁴Oil emission factor based on Refinery C, Source 1 fuel composition of N content = 0.18 wt % and 1b NO_x/10³ gal oil = 22 + 400N² = 36

⁵Run 10 was discounted because of process swings during test.

APPENDIX A

DETAILED TEST DATA AND TEST RESULT SUMMARIES

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AMERICAN PETROLEUM INSTITUTE
REFINERY A
SOURCE NO. 1

Table A-1
SUMMARY OF PARTICULATE TEST DATA

Test Data

| | 1 7/14/81 1328-1818 | 2 7/15/81 0855-1325 | 3 7/15/81 1433-1950 |
|--|---------------------------|---------------------------|---------------------------|
|--|---------------------------|---------------------------|---------------------------|

Sampling Data

| | | | |
|---|-------|-------|-------|
| Sampling Duration, minutes | 240.0 | 240.0 | 240.0 |
| Nozzle Diameter, inches | 0.562 | 0.562 | 0.555 |
| Barometric Pressure, inches mercury | 29.70 | 29.77 | 29.77 |
| Average Orifice Pressure Differential, inches water | 1.68 | 1.65 | 1.65 |
| Average Dry Gas Temperature at Meter, °F | 96. | 97. | 95. |
| Total Water Collected by Train, ml | 585.5 | 648.4 | 625.0 |
| Standard Volume of Water Vapor Collected, cubic feet | 27.6 | 30.5 | 27.7 |
| Dry Gas Meter Calibration Factor, dimensionless | 0.994 | 0.994 | 0.994 |
| Sample Volume at Meter Conditions, cubic feet ¹ | 167.6 | 164.7 | 164.7 |
| Sample Volume at Standard Conditions, cubic feet ¹ | 157.8 | 155.0 | 155.7 |

Gas Stream Composition

| | | | |
|---|-------|-------|-------|
| CO ₂ , percent by volume | 8.8 | 8.7 | 8.8 |
| O ₂ , percent by volume | 2.3 | 2.3 | 2.3 |
| CO, percent by volume | 0.0 | 0.0 | 0.0 |
| N ₂ , percent by volume | 88.9 | 89.0 | 88.9 |
| Moisture in Gas Stream, percent by volume | 14.9 | 16.5 | 15.9 |
| Mole Fraction of Dry Gas | 0.851 | 0.836 | 0.841 |
| Molecular Weight of Dry Gas | 29.5 | 29.5 | 29.5 |
| Molecular Weight of Wet Gas | 27.8 | 27.6 | 27.7 |

Gas Stream Velocity and Volumetric Flow

| | | | |
|---|---------|---------|---------|
| Static Pressure, inches water | - 0.43 | - 0.41 | - 0.41 |
| Absolute Pressure, inches mercury | 29.7 | 29.7 | 29.7 |
| Average Temperature, °F | 324. | 329. | 327. |
| Pitot Tube Calibration Coefficient, dimensionless | 0.84 | 0.84 | 0.84 |
| Total Number of Traverse Points | 24.0 | 24.0 | 24.0 |
| Velocity at Actual Conditions, feet/second | 10.6 | 11.0 | 10.9 |
| Stack/duct Cross-Sectional Area, square feet | 113.1 | 113.1 | 113.1 |
| Volumetric Flow, Wet Actual cubic feet/minute | 71,900. | 74,600. | 74,100. |
| Volumetric Flow, Dry Standard cubic feet/minute | 40,900. | 41,500. | 41,600. |

Percent Isokinetic

| | | |
|-------|-------|-------|
| 105.6 | 102.2 | 105.0 |
|-------|-------|-------|

Unit/Process Operations Data

| | | | |
|---|-------|-------|------|
| Fuel Firing Ratio, % Gas: % oil | 100:0 | 100:0 | 91:9 |
| Percent O ₂ at test location | 2.3 | 2.3 | 2.3 |

¹Standard Conditions = 68°F (20°C) and 29.92 inches (760 mm) mercury, dry basis.

AMERICAN PETROLEUM INSTITUTE
REFINERY A
SOURCE NO. 1
STACK NO. 1
Table A-2

SUMMARY OF PARTICULATE AND NO_x TEST RESULTS

Test Data

| | 1 7/14/81 1328-1818 | 2 7/15/81 0855-1325 | 3 7/15/81 1433-1950 |
|-----------------|---------------------------|---------------------------|---------------------------|
| Test Run Number | | | |
| Test Date | | | |
| Test Time | | | |

Gas Flow Volumes

| | (1) | 40,900. 71,900. | 41,500. 74,600. | 41,600. 74,100. |
|--------------------------------|-----|--------------------|--------------------|--------------------|
| Dry Standard Cubic Feet/Minute | | | | |
| Wet Actual Cubic Feet/Minute | | | | |

Particulate Analysis Report

| | | | |
|--|--------|--------|--------|
| Front-Half Acetone Wash Residue Wt., grams | 0.0264 | 0.0095 | 0.0102 |
| Front-Half Methylene Chloride Wash Residue Wt., grams | --- | --- | 0.0063 |
| Filter Catch Wt., grams | 0.0042 | 0.0062 | 0.0055 |
| Front-Half Catch Wt. Sub-total, grams | 0.0306 | 0.0157 | 0.0220 |
| Methylene Chloride Extraction of Impinger Contents/Wash Residue wt., grams | --- | --- | 0.0002 |
| Impinger Contents/Wash Residue Wt., grams | 0.0070 | 0.0061 | 0.0071 |
| Back-Half Acetone Wash Residue Wt., grams | 0.0035 | 0.0038 | 0.0015 |
| Back-Half Methylene Chloride Wash Residue Wt., grams | --- | --- | 0.0027 |
| Back Half Catch Wt. Sub-total, grams | 0.0105 | 0.0099 | 0.0115 |
| Total Catch Weight, grams | 0.0411 | 0.0256 | 0.0335 |

Particulate Results

Front-Half

| | | | |
|---|-----|------|------|
| Concentration, grains/dry standard cubic foot, $\times 10^{-3}$ | 3.0 | 1.6 | 2.2 |
| Mass Emission Rate, pounds/hour | 1.1 | 0.56 | 0.78 |

Total

| | | | |
|---|-----|------|-----|
| Concentration, grains/dry standard cubic foot, $\times 10^{-3}$ | 4.0 | 2.5 | 3.3 |
| Mass Emission Rate, pounds/hour | 1.4 | 0.91 | 1.2 |

NO_x Emissions, as NO₂ ⁽²⁾

| | | | |
|--|-----|-----|-----|
| Concentration, Parts/million by Volume, dry basis | 30. | 51. | 42. |
| Concentration, Pounds/Dry Standard Cubic Foot $\times 10^{-6}$ | 3.6 | 6.1 | 5.0 |
| Mass Emission Rate, Pounds/Hour | 8.8 | 15. | 12, |

⁽¹⁾Standard Conditions = 68°F (20°C) and 29.92 Inches Hg.

⁽²⁾Results shown are averages of three (3) grab samples.

AMERICAN PETROLEUM INSTITUTE
REFINERY A
SOURCE NO. 1
STACK NO. 1
Table A-3

SUMMARY OF PARTICULATE TEST DATA

Test Data

| | 4 | 5 | 6 |
|-----------------|-----------|-----------|-----------|
| Test Run Number | 7/16/81 | 7/16/81 | 7/17/81 |
| Test Date | 0843-1321 | 1402-1825 | 0925-1405 |
| Test Period | | | |

Sampling Data

| | | | |
|---|-------|-------|-------|
| Sampling Duration, minutes | 240.0 | 240.0 | 240.0 |
| Nozzle Diameter, inches | 0.562 | 0.555 | 0.562 |
| Barometric Pressure, inches mercury | 29.75 | 29.75 | 29.88 |
| Average Orifice Pressure Differential, inches water | 1.99 | 1.99 | 2.39 |
| Average Dry Gas Temperature at Meter, °F | 92. | 89. | 93. |
| Total Water Collected by Train, ml | 660.0 | 655.0 | 715.0 |
| Standard Volume of Water Vapor Collected, cubic feet | 31.1 | 30.8 | 33.7 |
| Dry Gas Meter Calibration Factor, dimensionless | 0.994 | 0.994 | 0.994 |
| Sample Volume at Meter Conditions, cubic feet ¹ | 181.9 | 181.0 | 196.6 |
| Sample Volume at Standard Conditions, cubic feet ¹ | 172.7 | 172.9 | 187.5 |

Gas Stream Composition

| | | | |
|---|-------|-------|-------|
| CO ₂ , percent by volume | 7.8 | 7.9 | 8.1 |
| O ₂ , percent by volume | 4.4 | 4.3 | 4.3 |
| CO, percent by volume | 0.0 | 0.0 | 0.0 |
| N ₂ , percent by volume | 87.8 | 87.8 | 87.6 |
| Moisture in Gas Stream, percent by volume | 15.2 | 15.1 | 15.2 |
| Mole Fraction of Dry Gas | 0.848 | 0.849 | 0.848 |
| Molecular Weight of Dry Gas | 29.4 | 29.4 | 29.5 |
| Molecular Weight of Wet Gas | 27.7 | 27.7 | 27.7 |

Gas Stream Velocity and Volumetric Flow

| | | | |
|---|---------|---------|---------|
| Static Pressure, inches water | ~ 0.42 | ~ 0.42 | ~ 0.43 |
| Absolute Pressure, inches mercury | 29.7 | 29.7 | 29.9 |
| Average Temperature, °F | 338. | 339. | 336. |
| Pitot Tube Calibration Coefficient, dimensionless | 0.840 | 0.840 | 0.840 |
| Total Number of Traverse Points | 24.0 | 24.0 | 24.0 |
| Velocity at Actual Conditions, feet/second | 12.2 | 12.1 | 13.1 |
| Stack/duct Cross-Sectional Area, square feet | 113.1 | 113.1 | 113.1 |
| Volumetric Flow, Wet Actual cubic feet/minute | 82,700. | 82,400. | 89,500. |
| Volumetric Flow, Dry Standard cubic feet/minute | 46,000. | 45,900. | 50,200. |

Percent Isokinetic

| | | | |
|--|-------|-------|-------|
| | 102.6 | 105.7 | 102.2 |
|--|-------|-------|-------|

Unit/Process Operations Data

| | | | |
|---|------|------|------|
| Fuel Firing Ratio, % Gas: % oil | 94.6 | 91.9 | 94.6 |
| Percent O ₂ at test location | 4.4 | 4.3 | 4.3 |

¹Standard Conditions = 68°F (20°C) and 29.92 inches (760 mm) mercury, dry basis.

AMERICAN PETROLEUM INSTITUTE
REFINERY A
SOURCE NO. 1
STACK NO. 1
Table A-4

SUMMARY OF PARTICULATE AND NO_x TEST RESULTS

Test Data

| | 4 | 5 | 6 |
|-----------------|-----------|-----------|-----------|
| Test Run Number | 7/16/81 | 7/16/81 | 7/17/81 |
| Test Date | 0843-1321 | 1402-1825 | 0952-1406 |
| Test Time | | | |

Gas Flow Volumes

| | | | |
|---|---------|---------|---------|
| Dry Standard Cubic Feet/Minute ⁽¹⁾ | 46,000. | 45,900. | 50,200. |
| Wet Actual Cubic Feet/Minute | 82,700. | 82,400. | 89,500. |

Particulate Analysis Report

| | | | |
|--|--------|--------|--------|
| Front-Half Acetone Wash Residue Wt., grams | 0.0044 | 0.0077 | 0.0072 |
| Front-Half Methylene Chloride Wash Residue Wt., grams | --- | --- | 0.0014 |
| Filter Catch Wt., grams | 0.0029 | 0.0066 | 0.0075 |
| Front-Half Catch Wt. Sub-total, grams | 0.0073 | 0.0143 | 0.0161 |
| Methylene Chloride Extraction of Impinger Contents/Wash Residue wt., grams | --- | --- | 0.0003 |
| Impinger Contents/Wash Residue Wt., grams | 0.0033 | 0.0068 | 0.0066 |
| Back-Half Acetone Wash Residue Wt., grams | 0.0036 | 0.0021 | 0.0013 |
| Back-Half Methylene Chloride Wash Residue Wt., grams | --- | --- | 0.0039 |
| Back Half Catch Wt. Sub-total, grams | 0.0069 | 0.0089 | 0.0121 |
| Total Catch Weight, grams | 0.0142 | 0.0232 | 0.0282 |

Particulate Results

Front-Half

| | | | |
|---|------|------|------|
| Concentration, grains/dry standard cubic foot, $\times 10^{-3}$ | 0.7 | 1.3 | 1.3 |
| Mass Emission Rate, pounds/hour | 0.26 | 0.50 | 0.57 |

Total

| | | | |
|---|------|------|------|
| Concentration, grains/dry standard cubic foot, $\times 10^{-3}$ | 1.3 | 2.1 | 2.3 |
| Mass Emission Rate, pounds/hour | 0.50 | 0.81 | 0.99 |

NO_x Emissions, as NO₂⁽²⁾

| | | | |
|--|-----|-----|-----|
| Concentration, Parts/million by Volume, dry basis | 64. | 59. | 77. |
| Concentration, Pounds/Dry Standard Cubic Foot $\times 10^{-6}$ | 7.6 | 7.0 | 9.2 |
| Mass Emission Rate, Pounds/Hour | 21. | 19. | 28. |

⁽¹⁾Standard Conditions = 60°F (20°C) and 29.92 Inches Hg.

⁽²⁾Results shown are averages of three (3) grab samples.

AMERICAN PETROLEUM INSTITUTE

REFINERY A

SOURCE NO. 1

STACK NO. 1

Table A-5

SUMMARY OF PARTICULATE TEST DATATest Data

| | 7 7/18/81 1100-1524 | 9 7/19/81 0838-1254 | 11 7/20/81 1001-1421 |
|--|---------------------------|---------------------------|----------------------------|
|--|---------------------------|---------------------------|----------------------------|

Sampling Data

| | | | |
|---|-------|-------|-------|
| Sampling Duration, minutes | 240.0 | 240.0 | 240.0 |
| Nozzle Diameter, inches | 0.555 | 0.555 | 0.562 |
| Barometric Pressure, inches mercury | 29.84 | 29.86 | 29.86 |
| Average Orifice Pressure Differential, inches water | 2.53 | 2.41 | 2.66 |
| Average Dry Gas Temperature at Meter, °F | 96. | 98. | 98. |
| Total Water Collected by Train, ml | 751.0 | 745.5 | 797.5 |
| Standard Volume of Water Vapor Collected, cubic feet | 35.4 | 35.1 | 37.5 |
| Dry Gas Meter Calibration Factor, dimensionless | 0.994 | 0.994 | 0.994 |
| Sample Volume at Meter Conditions, cubic feet | 202.9 | 200.1 | 209.9 |
| Sample Volume at Standard Conditions, cubic feet ¹ | 191.7 | 188.8 | 198.5 |

Gas Stream Composition

| | | | |
|---|-------|-------|-------|
| CO ₂ , percent by volume | 10.9 | 10.5 | 10.3 |
| O ₂ , percent by volume | 3.8 | 4.1 | 4.1 |
| CO, percent by volume | 0.0 | 0.0 | 0.0 |
| N ₂ , percent by volume | 85.3 | 85.4 | 85.6 |
| Moisture in Gas Stream, percent by volume | 15.6 | 15.7 | 15.9 |
| Mole Fraction of Dry Gas | 0.844 | 0.843 | 0.841 |
| Molecular Weight of Dry Gas | 29.9 | 29.8 | 29.8 |
| Molecular Weight of Wet Gas | 28.0 | 28.0 | 27.9 |

Gas Stream Velocity and Volumetric Flow

| | | | |
|---|---------|---------|---------|
| Static Pressure, inches water | -0.43 | -0.44 | -0.44 |
| Absolute Pressure, inches mercury | 29.8 | 29.8 | 29.8 |
| Average Temperature, °F | 333. | 339. | 338. |
| Pitot Tube Calibration Coefficient, dimensionless | 0.840 | 0.840 | 0.840 |
| Total Number of Traverse Points | 24.0 | 24.0 | 24.0 |
| Velocity at Actual Conditions, feet/second | 13.1 | 13.4 | 14.1 |
| Stack/duct Cross-Sectional Area, square feet | 113.1 | 113.1 | 113.1 |
| Volumetric Flow, Wet Actual cubic feet/minute | 89,100. | 90,900. | 95,800. |
| Volumetric Flow, Dry Standard cubic feet/minute | 49,900. | 50,500. | 53,100. |

Percent Isokinetic

107.8 104.9 102.2

Unit/Process Operations Data

| | | | |
|---|-------|-------|-------|
| Fuel Firing Ratio, % Gas: % Oil | 46:54 | 46:54 | 61:39 |
| Percent O ₂ at test location | 3.8 | 4.1 | 4.1 |

¹Standard Conditions = 68°F (20°C) and 29.92 inches (760 mm) mercury, dry basis.

AMERICAN PETROLEUM INSTITUTE

REFINERY A

SOURCE NO. 1

STACK NO. 1

Table A-6

SUMMARY OF PARTICULATE AND NO_x TEST RESULTSTest Data

| | | | |
|-----------------|-----------|-----------|-----------|
| Test Run Number | 7 | 9 | 11 |
| Test Date | 7/18/81 | 7/19/81 | 7/20/81 |
| Test Time | 1100-1524 | 0838-1254 | 1001-1421 |

Gas Flow Volumes

| | | | |
|------------------------------------|---------|---------|---------|
| Dry Standard Cubic Feet/Minute (1) | 49,900. | 50,500. | 53,100. |
| Wet Actual Cubic Feet/Minute | 89,100. | 90,900. | 95,800. |

Particulate Analysis Report

| | | | |
|--|--------|--------|--------|
| Front-Half Acetone Wash Residue Wt., grams | 0.0099 | 0.0063 | 0.0095 |
| Front-Half Methylene Chloride Wash Residue Wt., grams | --- | 0.0013 | --- |
| Filter Catch Wt., grams | 0.0132 | 0.0077 | 0.0052 |
| Front-Half Catch Wt. Sub-total, grams | 0.0231 | 0.0153 | 0.0147 |
| Methylene Chloride Extraction of Impinger Contents/Wash Residue wt., grams | --- | 0.0004 | --- |
| Impinger Contents/Wash Residue Wt., grams | 0.0070 | 0.0170 | 0.0084 |
| Back-Half Acetone Wash Residue Wt., grams | 0.0015 | 0.0009 | 0.0042 |
| Back-Half Methylene Chloride Wash Residue Wt., grams | --- | 0.0026 | --- |
| Back Half Catch Wt. Sub-total, grams | 0.0085 | 0.0209 | 0.0126 |
| Total Catch Weight, grams | 0.0316 | 0.0362 | 0.0273 |

Particulate ResultsFront-Half

| | | | |
|---|------|------|------|
| Concentration, grains/dry standard cubic foot, $\times 10^{-3}$ | 1.9 | 1.3 | 1.1 |
| Mass Emission Rate, pounds/hour | 0.80 | 0.54 | 0.52 |

Total

| | | | |
|---|-----|-----|------|
| Concentration, grains/dry standard cubic foot, $\times 10^{-3}$ | 2.5 | 3.0 | 2.1 |
| Mass Emission Rate, pounds/hour | 1.1 | 1.3 | 0.97 |

NO_x Emissions, as NO₂ (2)

| | | | |
|--|------|------|------|
| Concentration, Parts/million by Volume, dry basis | 112. | 142. | 138. |
| Concentration, Pounds/Dry Standard Cubic Foot $\times 10^{-6}$ | 13. | 17. | 17. |
| Mass Emission Rate, Pounds/Hour | 40. | 51. | 53. |

(1) Standard Conditions = 68°F (20°C) and 29.92 Inches Hg.

(2) Results shown are averages of three (3) grab samples.

AMERICAN PETROLEUM INSTITUTE
REFINERY A
SOURCE NO. 1
STACK NO. 1
Table A-7

SUMMARY OF PARTICULATE TEST DATA

Test Data

| | 8 | 12 | 13 |
|-----------------|-----------|-----------|-----------|
| Test Run Number | 7/18/81 | 7/21/81 | 7/21/81 |
| Test Date | 1616-1852 | 0824-1239 | 1317-1728 |
| Test Period | | | |

Sampling Data

| | | | |
|---|-------|-------|-------|
| Sampling Duration, minutes | 144.0 | 240.0 | 240.0 |
| Nozzle Diameter, inches | 0.562 | 0.562 | 0.555 |
| Barometric Pressure, inches mercury | 29.84 | 29.84 | 29.84 |
| Average Orifice Pressure Differential, inches water | 2.48 | 2.51 | 2.70 |
| Average Dry Gas Temperature at Meter, °F | 91. | 96. | 96. |
| Total Water Collected by Train, ml | 439.5 | 677.0 | 752.0 |
| Standard Volume of Water Vapor Collected, cubic feet | 20.7 | 31.9 | 35.4 |
| Dry Gas Meter Calibration Factor, dimensionless | 0.994 | 0.994 | 0.994 |
| Sample Volume at Meter Conditions, cubic feet ¹ | 121.4 | 203.0 | 211.3 |
| Sample Volume at Standard Conditions, cubic feet ¹ | 116.0 | 192.4 | 200.2 |

Gas Stream Composition

| | | | |
|---|-------|-------|-------|
| CO ₂ , percent by volume | 10.4 | 9.7 | 9.9 |
| O ₂ , percent by volume | 5.2 | 5.5 | 5.4 |
| CO, percent by volume | 0.0 | 0.0 | 0.0 |
| N ₂ , percent by volume | 84.4 | 84.8 | 84.7 |
| Moisture in Gas Stream, percent by volume | 15.1 | 14.2 | 15.0 |
| Mole Fraction of Dry Gas | 0.849 | 0.858 | 0.850 |
| Molecular Weight of Dry Gas | 29.9 | 29.8 | 29.8 |
| Molecular Weight of Wet Gas | 28.1 | 28.1 | 28.0 |

Gas Stream Velocity and Volumetric Flow

| | | | |
|---|---------|---------|---------|
| Static Pressure, inches water | - 0.43 | - 0.45 | - 0.44 |
| Absolute Pressure, inches mercury | 29.8 | 29.8 | 29.8 |
| Average Temperature, °F | 338. | 349. | 345. |
| Pitot Tube Calibration Coefficient, dimensionless | 0.84 | 0.84 | 0.84 |
| Total Number of Traverse Points | 24.0 | 24.0 | 24.0 |
| Velocity at Actual Conditions, feet/second | 13.2 | 13.6 | 14.1 |
| Stack/duct Cross-Sectional Area, square feet | 113.1 | 113.1 | 113.1 |
| Volumetric Flow, Wet Actual cubic feet/minute | 89,700. | 92,100. | 95,900. |
| Volumetric Flow, Dry Standard cubic feet/minute | 50,200. | 51,400. | 53,200. |

Percent Isokinetic

| | | | |
|--|-------|-------|-------|
| | 105.4 | 102.4 | 105.5 |
|--|-------|-------|-------|

Unit/Process Operations Data

| | | | |
|--|-------|-------|-------|
| Fuel Firing Ratio, % Gas: % O ₂ | 48:52 | 57:43 | 58:42 |
| Percent O ₂ at test location | 5.2 | 5.5 | 5.4 |

¹Standard Conditions = 68°F (20°C) and 29.92 inches (760 mm) mercury, dry basis.

AMERICAN PETROLEUM INSTITUTE

REFINERY A

SOURCE NO. 1

STACK NO. 1

Table A-8

SUMMARY OF PARTICULATE AND NO_x TEST RESULTSTest Data

| | 8 7/18/81 1616-1852 | 12 7/21/81 0824-1239 | 13 7/21/81 1317-1728 |
|-----------------|---------------------------|----------------------------|----------------------------|
| Test Run Number | 8 | 12 | 13 |
| Test Date | 7/18/81 | 7/21/81 | 7/21/81 |
| Test Time | 1616-1852 | 0824-1239 | 1317-1728 |

Gas Flow Volumes

| | | | |
|---|---------|---------|---------|
| Dry Standard Cubic Feet/Minute ⁽¹⁾ | 50,200. | 51,400. | 53,200. |
| Wet Actual Cubic Feet/Minute | 89,700. | 92,100. | 95,900. |

Particulate Analysis Report

| | | | |
|--|--------|--------|--------|
| Front-Half Acetone Wash Residue Wt., grams | 0.0059 | 0.0114 | 0.0077 |
| Front-Half Methylene Chloride Wash Residue Wt., grams | --- | 0.0017 | --- |
| Filter Catch Wt., grams | 0.0064 | 0.0051 | 0.0032 |
| Front-Half Catch Wt. Sub-total, grams | 0.0123 | 0.0182 | 0.0109 |
| Methylene Chloride Extraction of Impinger Contents/Wash Residue wt., grams | --- | 0.0002 | --- |
| Impinger Contents/Wash Residue Wt., grams | 0.0026 | 0.0076 | 0.0070 |
| Back-Half Acetone Wash Residue Wt., grams | 0.0017 | 0.0009 | 0.0034 |
| Back-Half Methylene Chloride Wash Residue Wt., grams | --- | 0.0016 | --- |
| Back Half Catch Wt. Sub-total, grams | 0.0043 | 0.0103 | 0.0104 |
| Total Catch Weight, grams | 0.0166 | 0.0285 | 0.0213 |

Particulate ResultsFront-Half

| | | | |
|---|------|------|------|
| Concentration, grains/dry standard cubic foot, $\times 10^{-3}$ | 1.6 | 1.5 | 0.8 |
| Mass Emission Rate, pounds/hour | 0.70 | 0.64 | 0.38 |

Total

| | | | |
|---|------|-----|------|
| Concentration, grains/dry standard cubic foot, $\times 10^{-3}$ | 2.2 | 2.3 | 1.6 |
| Mass Emission Rate, pounds/hour | 0.95 | 1.0 | 0.75 |

NO_x Emissions, as NO₂⁽²⁾

| | | | |
|--|------|------|------|
| Concentration, Parts/million by Volume, dry basis | 126. | 162. | 136. |
| Concentration, Pounds/Dry Standard Cubic Foot $\times 10^{-6}$ | 15. | 19. | 16. |
| Mass Emission Rate, Pounds/Hour | 45. | 60. | 52. |

⁽¹⁾Standard Conditions = 68°F (20°C) and 29.92 inches Hg.⁽²⁾Results shown are averages of three (3) grab samples.

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REFINERY A SOURCE 1

Table A-9
PARTICLE SIZE DISTRIBUTION DATA¹

| Date | Fuel Firing Ratio %Gas:%Oil | Percent O ₂ at Test Location | Mass Percent Less than Stated Size | | | |
|---------|--------------------------------|--|------------------------------------|--------|--------|--------|
| | | | 0.3 um | 1.0 um | 3.0 um | 10. um |
| 7/15/81 | 96:4 ² | 2.3 | 13 | 18 | 28 | 37 |
| 7/16/81 | 93:7 | 4.4 | 3.8 | 18 | 44 | 78 |
| 7/18/81 | 46:54 | 3.8 | 12 | 29 | 50 | 71 |
| 7/21/81 | 58:42 | 5.5 | 10 | 29 | 54 | 80 |

¹This data is questionable since no impactor preseparator was used during these tests. Some large particle bounce-off and reintrainment may have occurred.

²Results from this test are suspect since several large particulate flakes, apparently originating from process equipment surfaces, were collected on the top stage of the impactor.

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REFINERY A

SOURCE 1

Table A-10

PARTICLE SIZE DISTRIBUTION*

| | | |
|---|---|-------|
| Run: One | Barometric Pressure(in. Hg) | 29.99 |
| Date: 5/18/82 | Stack Temperature($^{\circ}$ F.) | 357. |
| Traverse Point No. Sampled: B-3 A-4 | Sample Time(min.) | 600. |
| Fuel Firing Ratio, %Gas:%Oil 70:30 | Sample Volume(cfm) | 371.2 |
| Percent O ₂ (at test location) 3.9 | Moisture(%H ₂ O) | 16.8 |
| Dry Standard Cubic Feet/Minute 48,800. | Meter Temperature($^{\circ}$ F.) | 81. |
| Wet Actual Cubic Feet/Minute 90,700. | Flow Setting, ΔH (in. H ₂ O) | 1.3 |
| Sample Flow Rate (at stack conditions): | Nozzle Diameter(in.) | 0.490 |
| | Static Pressure(in. H ₂ O) | -0.40 |
| | Meter γ | 0.998 |
| | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|-----------------------|-----------------------------------|---------------|
| 1 | 5.1 | 12.5 | 87.5 | 8.5 |
| 2 | 0.0 | 0.0 | 87.5 | 7.9 |
| 3 | 0.2 | 0.5 | 87.0 | 4.9 |
| 4 | 0.1 | 0.2 | 86.8 | 3.3 |
| 5 | 0.3 | 0.7 | 86.1 | 1.8 |
| 6 | 0.0 | 0.0 | 86.1 | 0.79 |
| 7 | 0.3 | 0.7 | 85.4 | 0.47 |
| 8 | 0.4 | 1.0 | 84.4 | 0.24 |
| Backup Filter | 34.6 | 84.4 | 0.0 | ---- |
| TOTAL | 41.0 | ---- | ---- | ---- |

A-10

*Data plotted in Figure 4-2.

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REFINERY A

SOURCE 1

Table A-11

PARTICLE SIZE DISTRIBUTION *

| | | |
|---|---|-------|
| Run: Two | Barometric Pressure(in. Hg) | 29.95 |
| Date: 5/19/82 | Stack Temperature(⁰ F) | 814. |
| Traverse Point No. Sampled: B-2 C-3 | Sample Time(min.) | 382. |
| Fuel Firing Ratio, %Gas:%Oil 70:30 | Sample Volume(cf) | 234.6 |
| Percent O ₂ (at test location) 5.5 | Moisture(%H ₂ O) | 15.5 |
| Dry Standard cubic Feet/Minute 54,000. | Meter Temperature(⁰ F) | 79. |
| Wet Actual Cubic Feet/Minute 98,600. | Flow Setting, ΔH (in. H ₂ O) | 1.3 |
| Sample Flow Rate (at stack conditions): 1.10 cfm | Nozzle Diameter(in.) | 0.490 |
| | Static Pressure(in. H ₂ O) | -0.42 |
| | Meter γ | 0.998 |
| | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|--------------|-----------------------|-----------------------------------|---------------|
| 1 | 6.3 | 22.9 | 77.1 | 8.6 |
| 2 | 0.5 | 1.8 | 75.3 | 8.0 |
| 3 | 0.5 | 1.8 | 73.5 | 5.0 |
| 4 | 0.2 | 0.7 | 72.8 | 3.3 |
| 5 | 0.2 | 0.7 | 72.1 | 1.8 |
| 6 | 0.1 | 0.4 | 71.7 | 0.80 |
| 7 | 0.6 | 2.2 | 69.5 | 0.47 |
| 8 | 0.0 | 0.0 | 69.5 | 0.25 |
| Backup Filter | 19.1 | 69.5 | 0.0 | ---- |
| TOTAL | 27.5 | ---- | ---- | ---- |

A-11

*Data plotted in Figure 4-2.

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REFINERY A

SOURCE 1

Table A-12

PARTICLE SIZE DISTRIBUTION

Run: Performed during particulate tests four and five.

Date: 7/16/81

Traverse Point No. Sampled: 05-C6

Fuel Firing Ratio, %Gas:%Oil 93:7

Percent O₂ (at test location) 4.4

Barometric Pressure(in. Hg) 29.75

Stack Temperature(⁰F) 338.

Sample Time(min.) 420.

Sample Volume(cf) 203.2

Moisture(%H₂O) 15.2

Meter Temperature(⁰F) 91.

Flow Setting, ΔH (in. H₂O) 0.74

Nozzle Diameter(in.) 0.433

Static Pressure(in. H₂O) -0.42

Meter γ 1.002

Sample Vac.(in. Hg) 1.0

Sample Flow Rate
(at stack conditions): 0.83 cfm

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|--------------------------|---|------------------|
| 1 | 4.5 | 16.6 | 83.4 | 9.8 |
| 2 | 2.4 | 8.9 | 74.5 | 9.1 |
| 3 | 4.1 | 15.1 | 59.4 | 5.7 |
| 4 | 2.1 | 7.8 | 51.6 | 3.8 |
| 5 | 4.1 | 15.1 | 36.5 | 2.0 |
| 6 | 4.0 | 14.8 | 21.7 | 0.94 |
| 7 | 3.2 | 11.8 | 9.9 | 0.59 |
| 8 | 1.7 | 6.3 | 3.6 | 0.30 |
| Backup Filter | 1.0 | 3.6 | 0.0 | ---- |
| TOTAL | 27.1 | ---- | ---- | ---- |

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REFINERY A

SOURCE 1

Table A-13

PARTICLE SIZE DISTRIBUTION

Run: Performed during particulate tests
two and three

Date: 7/15/81

Traverse Point No. Sampled: D5-C4

Fuel Firing Ratio, %Gas:%Oil 96:4

Percent O₂ (at test location) 2.3

Barometric Pressure(in. Hg) 29.88

Stack Temperature(⁰F) 327.

Sample Time(min.) 420.

Sample Volume(cf) 206.8

Moisture(%H₂O) 16.2

Meter Temperature(⁰F) 95.

Flow Setting, ΔH (in. H₂O) 0.74

Nozzle Diameter(in.) 0.433

Static Pressure(in. H₂O) -0.40

Meter γ 1.002

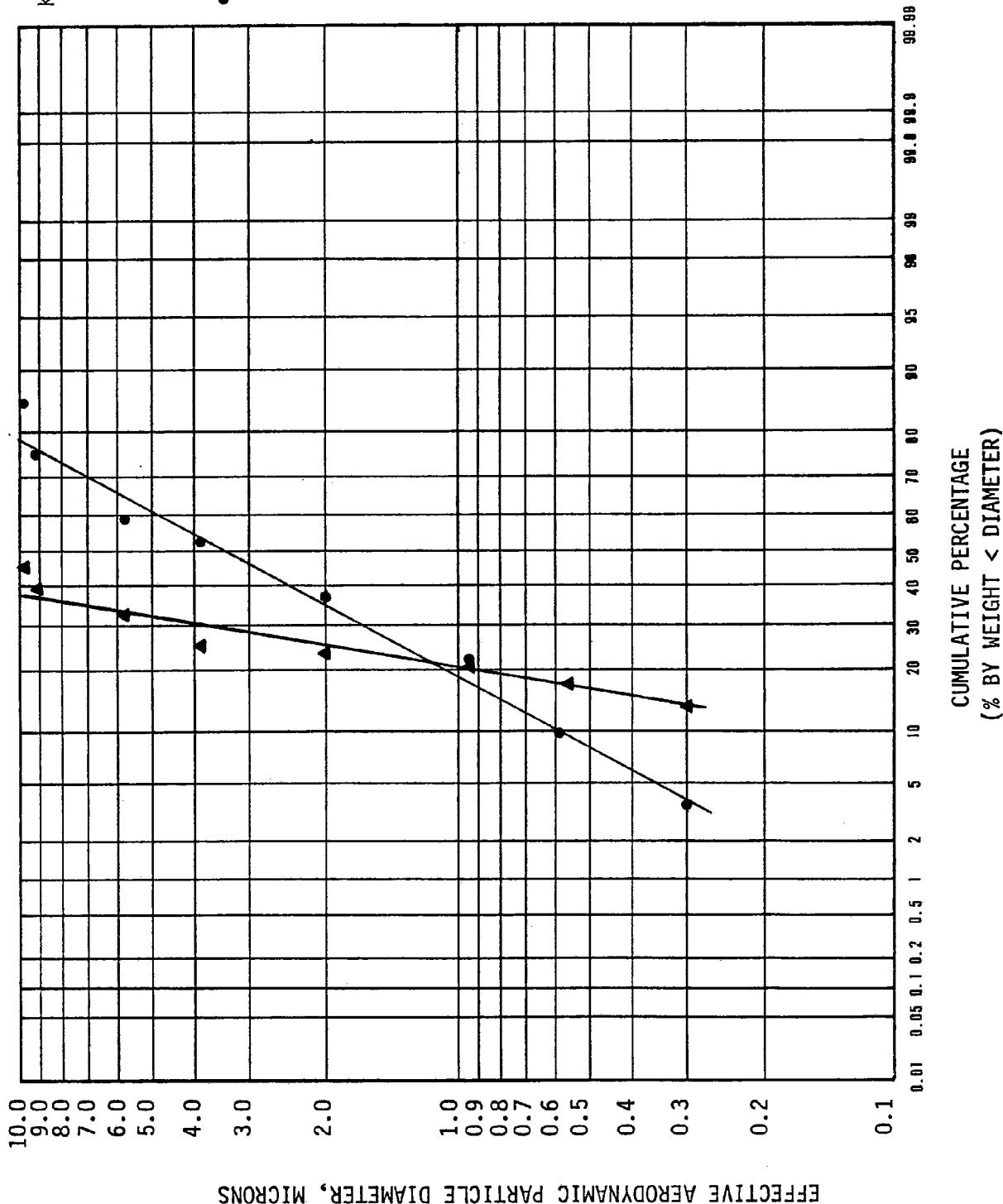
Sample Vac.(in. Hg) 1.0

Sample Flow Rate
(at stack conditions): 0.84 cfm

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|--------------------------|---|------------------|
| 1 | 5.2 | 55.3 | 44.7 | 9.8 |
| 2 | 0.5 | 5.3 | 39.4 | 9.0 |
| 3 | 0.7 | 7.5 | 31.9 | 5.6 |
| 4 | 0.6 | 6.4 | 25.5 | 3.8 |
| 5 | 0.3 | 3.2 | 22.3 | 2.0 |
| 6 | 0.2 | 2.1 | 20.2 | 0.93 |
| 7 | 0.3 | 3.2 | 17.0 | 0.55 |
| 8 | 0.4 | 4.3 | 12.7 | 0.30 |
| Backup Filter | 1.2 | 12.7 | 0.0 | ---- |
| TOTAL | 9.4 | ---- | ---- | ---- |

A-13

PARTICLE SIZE DISTRIBUTION TEST RESULTS



A-14

AMERICAN PETROLEUM INSTITUTE

REFINERY A

SOURCE 1

Table A-14

PARTICLE SIZE DISTRIBUTION

Run: Performed during particulate test seven.

Date: 7/18/81

Traverse Point No. Sampled: C4-D5

Fuel Firing Ratio, %Gas:%Oil 46:54

Percent O₂ (at test location) 3.8

Barometric Pressure(in. Hg) 29.84

Stack Temperature(⁰F) 333.

Sample Time(min.) 240.

Sample Volume(cf) 117.3

Moisture(%H₂O) 15.6

Meter Temperature(⁰F) 91.

Flow Setting, ΔH (in. H₂O) 0.76

Nozzle Diameter(in.) 0.433

Static Pressure(in. H₂O) -0.43

Meter γ 1.002

Sample Vac.(in. Hg) 1.0

Sample Flow Rate
(at stack conditions): 0.84 cfm

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|--------------------------|---|------------------|
| 1 | 6.6 | 15.8 | 84.2 | 9.8 |
| 2 | 4.5 | 10.8 | 73.4 | 9.1 |
| 3 | 5.7 | 13.7 | 59.7 | 5.6 |
| 4 | 4.6 | 11.0 | 48.7 | 3.8 |
| 5 | 4.1 | 9.8 | 38.9 | 2.0 |
| 6 | 4.4 | 10.6 | 28.3 | 0.93 |
| 7 | 4.3 | 10.3 | 18.0 | 0.55 |
| 8 | 2.5 | 6.0 | 12.0 | 0.29 |
| Backup Filter | 5.0 | 12.0 | 0.0 | ---- |
| TOTAL | 41.7 | ---- | ---- | ---- |

AMERICAN PETROLEUM INSTITUTE

REFINERY A

SOURCE 1

Table A-15

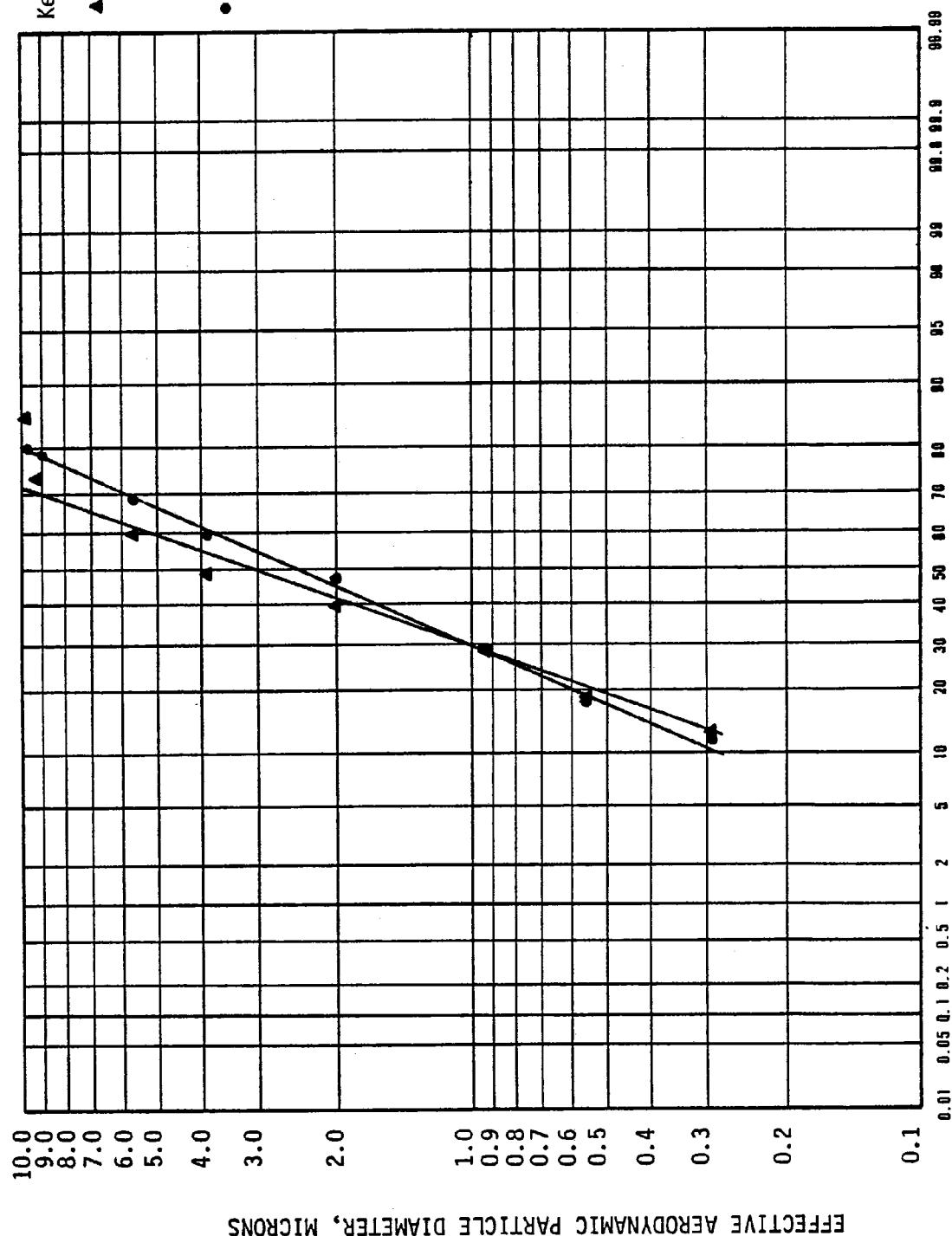
PARTICLE SIZE DISTRIBUTION

Run: Performed during particulate tests twelve and thirteen
 Date: 7/21/81
 Traverse Point No. Sampled: C5-D4
 Fuel Firing Ratio, %Gas:%Oil 58:42
 Percent O₂ (at test location) 5.5
 Sample Flow Rate (at stack conditions): 0.85 cfm

| | |
|---|-------|
| Barometric Pressure(in. Hg) | 29.84 |
| Stack Temperature(⁰ F) | 345. |
| Sample Time(min.) | 480. |
| Sample Volume(cf) | 238.3 |
| Moisture(%H ₂ O) | 14.6 |
| Meter Temperature(⁰ F) | 92. |
| Flow Setting, ΔH (in. H ₂ O) | 0.76 |
| Nozzle Diameter(in.) | 0.433 |
| Static Pressure(in. H ₂ O) | -0.44 |
| Meter γ | 1.002 |
| Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|--------------|-----------------------|-----------------------------------|---------------|
| 1 | 0.7 | 20.0 | 80.0 | 9.7 |
| 2 | 0.1 | 2.9 | 77.1 | 9.0 |
| 3 | 0.3 | 8.6 | 68.5 | 5.6 |
| 4 | 0.3 | 8.6 | 59.9 | 3.8 |
| 5 | 0.5 | 14.3 | 45.6 | 2.0 |
| 6 | 0.6 | 17.1 | 28.5 | 0.93 |
| 7 | 0.4 | 11.4 | 17.1 | 0.55 |
| 8 | 0.2 | 5.7 | 11.4 | 0.29 |
| Backup Filter | 0.4 | 11.4 | 0.0 | ---- |
| TOTAL | 3.5 | ---- | ---- | ---- |

AMERICAN PETROLEUM INSTITUTE
 REFINERY A SOURCE 1
 PARTICLE SIZE DISTRIBUTION TEST RESULTS



A-17

AMERICAN PETROLEUM INSTITUTE

REFINERY A

SOURCE 1

Table A-16

ANALYSIS OF RESULTS OF FUEL OIL COMPOSITE SAMPLES

| | Tests 7,8,9, 11, 12 & 13 | PSD Tests 1 and 2 |
|-------------------------|-----------------------------|----------------------|
| | 7/18-21/81 | 5/18-19/82 |
| Ash, % | < 0.01 | < 0.01 |
| Carbon, % | 86.9 | 86.9 |
| Hydrogen, % | 12.3 | 12.5 |
| Nitrogen, % | 0.16 | 0.20 |
| Oxygen, % | 0.52 | 0.17 |
| Sulfur, % | 0.09 | 0.27 |
| Density, lbs/gal. | 7.509 | 7.651 |
| Heating Value, BTU/lb. | 19,245. | 19,170. |
| Heating Value, BTU/gal. | 144,511 | 146,660. |
| Viscosity, SUS @ 100°F. | 89.2 | 292. |
| Viscosity, SUS @ 122°F. | 67.0 | 154. |
| Viscosity, SUS @ 210°F. | 37.6 | 48.7 |
| Gravity, API | 25.4 | -- |
| Metals, ppm by weight | | |
| Arsenic | 0.39 | < 0.17 |
| Barium | 0.18 | 0.20 |
| Cadmium | < 0.04 | < 0.50 |
| Chromium | < 0.04 | < 0.50 |
| Copper | 0.10 | 3.0 |
| Lead | < 0.04 | < 0.50 |
| Mercury | 0.12 | 0.02 |
| Nickel | 0.08 | 2.0 |
| Selenium | < 0.19 | 1.8 |
| Vanadium | < 0.04 | < 0.50 |
| Zinc | 5.5 | 18. |

AMERICAN PETROLEUM INSTITUTE

REFINERY B

SOURCE 1

TABLE A-17

SUMMARY OF PARTICULATE TEST DATATest Data

| | 1 12/30/81 1023-1643 | 2 12/31/81 0958-1610 | 3 1/1/82 0828-1800 |
|--|----------------------------|----------------------------|--------------------------|
|--|----------------------------|----------------------------|--------------------------|

Sampling Data

| | | | |
|---|-------|---------|---------|
| Sampling Duration, minutes | 360.0 | 360.0 | 540.0 |
| Nozzle Diameter, inches | 0.618 | 0.776 | 0.776 |
| Barometric Pressure, inches mercury | 30.25 | 30.14 | 30.03 |
| Average Orifice Pressure Differential, inches water | 1.22 | 3.09 | 3.20 |
| Average Dry Gas Temperature at Meter, °F | 72. | 94. | 91. |
| Total Water Collected by Train, ml | 758.0 | 1,268.0 | 1,918.0 |
| Standard Volume of Water Vapor Collected, cubic feet | 35.7 | 59.7 | 90.3 |
| Dry Gas Meter Calibration Factor, dimensionless | 0.991 | 0.991 | 0.991 |
| Sample Volume at Meter Conditions, cubic feet | 218.1 | 346.8 | 524.3 |
| Sample Volume at Standard Conditions, cubic feet ¹ | 217.4 | 332.4 | 503.9 |

Gas Stream Composition

| | | | |
|---|-------|-------|-------|
| CO ₂ , percent by volume | 7.9 | 8.1 | 8.2 |
| O ₂ , percent by volume | 6.3 | 5.8 | 5.9 |
| CO, percent by volume | 0.0 | 0.0 | 0.0 |
| N ₂ , percent by volume | 85.8 | 86.1 | 85.9 |
| Moisture in Gas Stream, percent by volume | 14.1 | 15.2 | 15.2 |
| Mole Fraction of Dry Gas | 0.859 | 0.848 | 0.848 |
| Molecular Weight of Dry Gas | 29.5 | 29.5 | 29.6 |
| Molecular Weight of Wet Gas | 27.9 | 27.8 | 27.8 |

Gas Stream Velocity and Volumetric Flow

| | | | |
|---|---------|---------|---------|
| Static Pressure, inches water | - 0.06 | - 0.04 | - 0.05 |
| Absolute Pressure, inches mercury | 30.3 | 30.1 | 30.0 |
| Average Temperature, °F | 587. | 579. | 587. |
| Pitot Tube Calibration Coefficient, dimensionless | 0.840 | 0.840 | 0.840 |
| Total Number of Traverse Points | 12.0 | 12.0 | 12.0 |
| Velocity at Actual Conditions, feet/second | 10.9 | 11.1 | 11.4 |
| Stack/duct Cross-Sectional Area, square feet | 19.6 | 19.6 | 19.6 |
| Volumetric Flow, Wet Actual cubic feet/minute | 12,900. | 13,100. | 13,400. |
| Volumetric Flow, Dry Standard cubic feet/minute | 5,630. | 5,690. | 5,760. |

Percent Isokinetic

101.1 97.0 96.9

Unit/Process Operations Data

| | | | |
|---|-------|-------|-------|
| Fuel Firing Ratio, % Gas:% Oil | 100:0 | 100:0 | 100:0 |
| Percent O ₂ at test location | 6.3 | 5.8 | 5.9 |
| Unit Charge Rate,BPH | 1200. | 1200. | 1200. |

¹Standard Conditions = 68°F (20°C) and 29.92 inches (760 mm) mercury, dry basis.

AMERICAN PETROLEUM INSTITUTE

REFINERY 6

SOURCE 1

TABLE A-18

SUMMARY OF PARTICULATE AND NO_x TEST RESULTSTest Data

| | 1 12/30/81 1023-1643 | 2 12/31/81 0958-1610 | 3 1/1/82 0828-1800 |
|--|----------------------------|----------------------------|--------------------------|
|--|----------------------------|----------------------------|--------------------------|

Gas Flow Volumes

| | | | |
|---|---------|---------|---------|
| Dry Standard Cubic Feet/Minute ⁽¹⁾ | 5,630. | 5,690. | 5,760. |
| Wet Actual Cubic Feet/Minute | 12,900. | 13,100. | 13,400. |

Particulate Analysis Report

| | | | |
|---|--------|--------|--------|
| Front-Half Acetone Wash Residue Wt., grams | 0.0005 | 0.0033 | 0.0028 |
| Front-Half Methylene Chloride Wash Residue Wt., grams | ----- | 0.0002 | ----- |
| Filter Catch Wt., grams | 0.0003 | 0.0005 | 0.0005 |
| Front-Half Catch Wt. Sub-total, grams | 0.0008 | 0.0040 | 0.0033 |
| Methylene Chloride Extraction of Impinger Contents/Wash Residue wt., grams----- | 0.0006 | ----- | ----- |
| Impinger Contents/Wash Residue Wt., grams | 0.0062 | 0.0052 | 0.0074 |
| Back-Half Acetone Wash Residue Wt., grams | 0.0007 | 0.0025 | 0.0085 |
| Back-Half Methylene Chloride Wash Residue Wt., grams | ----- | 0.0058 | ----- |
| Back Half Catch Wt. Sub-total, grams | 0.0069 | 0.0141 | 0.0159 |
| Total Catch Weight, grams | 0.0077 | 0.0181 | 0.0192 |

Particulate ResultsFront-Half

| | | | |
|---|------|------|------|
| Concentration, grains/dry standard cubic foot, $\times 10^{-5}$ | 5.68 | 18.6 | 10.1 |
| Mass Emission Rate, pounds/hour, $\times 10^{-3}$ | 2.74 | 9.06 | 4.99 |

Total

| | | | |
|--|------|------|------|
| Concentration, grains/dry standard cubic foot $\times 10^{-5}$ | 54.7 | 84.0 | 58.8 |
| Mass Emission Rate, pounds/hour, $\times 10^{-3}$ | 26.4 | 41.0 | 29.0 |

NO_x Emissions, as NO₂⁽²⁾

| | | | |
|--|------|------|------|
| Concentration, Parts/million by Volume, dry basis | 64.8 | 55.1 | 58.2 |
| Concentration, Pounds/Dry Standard Cubic Foot $\times 10^{-6}$ | 7.74 | 6.58 | 6.95 |
| Mass Emission Rate, Pounds/Hour | 2.62 | 2.25 | 2.40 |

⁽¹⁾Standard Conditions = 68°F (20°C) and 29.92 Inches Hg.⁽²⁾Results shown are averages of three (3) grab samples.

AMERICAN PETROLEUM INSTITUTE

REFINERY 8

SOURCE 1

TABLE A-19

Test DataSUMMARY OF PARTICULATE TEST DATA

| | | | |
|-----------------|-----------|-----------|-----------|
| Test Run Number | 4 | 5 | 6 |
| Test Date | 1/2/82 | 1/3/82 | 1/4/82 |
| Test Period | 0829-1457 | 0829-1754 | 1026-1635 |

Sampling Data

| | | | |
|--|---------|---------|---------|
| Sampling Duration, minutes | 360.0 | 540.0 | 360.0 |
| Nozzle Diameter, inches | 0.776 | 0.776 | 0.776 |
| Barometric Pressure, inches mercury | 29.93 | 29.85 | 30.29 |
| Average Orifice Pressure Differential, inches water | 3.23 | 2.97 | 2.91 |
| Average Dry Gas Temperature at Meter, °F | 85. | 88. | 92. |
| Total Water Collected by Train, ml | 1,487.0 | 2,095.0 | 1,188.0 |
| Standard Volume of Water Vapor Collected, cubic feet | 70.0 | 98.6 | 55.9 |
| Dry Gas Meter Calibration Factor, dimensionless | 0.991 | 0.991 | 0.991 |
| Sample Volume at Meter Conditions, cubic feet | 350.5 | 505.4 | 333.1 |
| Sample Volume at Standard Conditions, cubic feet | 339.4 | 485.1 | 322.3 |

Gas Stream Composition

| | | | |
|---|-------|-------|-------|
| CO ₂ , percent by volume | 9.3 | 9.3 | 8.9 |
| O ₂ , percent by volume | 4.0 | 4.0 | 4.4 |
| CO, percent by volume | 0.0 | 0.0 | 0.0 |
| N ₂ , percent by volume | 86.7 | 86.7 | 86.7 |
| Moisture in Gas Stream, percent by volume | 17.1 | 16.9 | 14.8 |
| Mole Fraction of Dry Gas | 0.829 | 0.831 | 0.852 |
| Molecular Weight of Dry Gas | 29.7 | 29.6 | 29.6 |
| Molecular Weight of Wet Gas | 27.7 | 27.7 | 27.9 |

Gas Stream Velocity and Volumetric Flow

| | | | |
|---|---------|---------|---------|
| Static Pressure, inches water | - 0.06 | - 0.05 | - 0.04 |
| Absolute Pressure, inches mercury | 29.9 | 29.9 | 30.3 |
| Average Temperature, °F | 572. | 569. | 576. |
| Pitot Tube Calibration Coefficient, dimensionless | 0.840 | 0.840 | 0.840 |
| Total Number of Traverse Points | 12.0 | 12.0 | 12.0 |
| Velocity at Actual Conditions, feet/second | 11.4 | 10.9 | 10.6 |
| Stack/duct Cross-Sectional Area, square feet | 19.6 | 19.6 | 19.6 |
| Volumetric Flow, Wet Actual cubic feet/minute | 13,400. | 12,800. | 12,500. |
| Volumetric Flow, Dry Standard cubic feet/minute | 5,690. | 5,460. | 5,500. |

Percent Isokinetic

| | | |
|------|------|------|
| 99.2 | 98.3 | 97.2 |
|------|------|------|

Unit/Process Operations Data

| | | | |
|---|-------|-------|-------|
| Fuel Firing Ratio, % Gas:% Oil | 100:0 | 100:0 | 100:0 |
| Percent O ₂ at test location | 4.0 | 4.0 | 4.4 |
| Unit Charge Rate,BPH | 1200. | 1200. | 1028. |

¹Standard Conditions = 68°F (20°C) and 29.92 inches (760 mm) mercury, dry basis.

A-21

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REFINERY B

SOURCE 1

TABLE A-20

SUMMARY OF PARTICULATE AND NO_x TEST RESULTSTest Data

| | <u>4</u> 1/2/82 0839-1457 | <u>5</u> 1/3/82 0829-1754 | <u>6</u> 1/4/82 1026-1635 |
|--|---------------------------------|---------------------------------|---------------------------------|
|--|---------------------------------|---------------------------------|---------------------------------|

Gas Flow Volumes

| | | | |
|---|---------|---------|---------|
| Dry Standard Cubic Feet/Minute ⁽¹⁾ | 5,690. | 5,460. | 5,500. |
| Wet Actual Cubic Feet/Minute | 13,400. | 12,800. | 12,500. |

Particulate Analysis Report

| | | | |
|--|--------|--------|--------|
| Front-Half Acetone Wash Residue Wt., grams | 0.0012 | 0.0002 | 0.0035 |
| Front-Half Methylene Chloride Wash Residue Wt., grams | ----- | ----- | 0.0006 |
| Filter Catch Wt., grams | 0.0014 | 0.0005 | 0.0004 |
| Front-Half Catch Wt. Sub-total, grams | 0.0026 | 0.0007 | 0.0045 |
| Methylene Chloride Extraction of Impinger Contents/Wash Residue Wt., grams | ----- | ----- | 0.0004 |
| Impinger Contents/Wash Residue Wt., grams | 0.0056 | 0.0143 | 0.0049 |
| Back-Half Acetone Wash Residue Wt., grams | 0.0060 | 0.0047 | 0.0019 |
| Back-Half Methylene Chloride Wash Residue Wt., grams | ----- | ----- | 0.0045 |
| Back Half Catch Wt. Sub-total, grams | 0.0116 | 0.0190 | 0.0117 |
| Total Catch Weight, grams | 0.0142 | 0.0197 | 0.0162 |

Particulate ResultsFront-Half

| | | | |
|---|------|------|------|
| Concentration, grains/dry standard cubic foot, $\times 10^{-5}$ | 11.8 | 2.23 | 21.5 |
| Mass Emission Rate, pounds/hour, $\times 10^{-3}$ | 5.76 | 1.04 | 10.2 |

Total

| | | | |
|---|------|------|------|
| Concentration, grains/dry standard cubic foot, $\times 10^{-5}$ | 64.6 | 62.7 | 77.6 |
| Mass Emission Rate, pounds/hour, $\times 10^{-3}$ | 31.5 | 29.3 | 36.6 |

NO_x Emissions, as NO₂⁽²⁾

| | | | |
|--|------|------|------|
| Concentration, Parts/million by Volume, dry basis | 48.5 | 50.6 | 68.4 |
| Concentration, Pounds/Dry Standard Cubic Foot $\times 10^{-6}$ | 5.79 | 6.05 | 8.16 |
| Mass Emission Rate, Pounds/Hour | 1.97 | 1.98 | 2.69 |

⁽¹⁾Standard Conditions = 68°F (20°C) and 29.92 inches Hg.⁽²⁾Results shown are averages of three (3) grab samples.

A-22

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REFINERY A

SOURCE 2

Table A-21

SUMMARY OF PARTICULATE TEST DATATest Data

| | <u>1</u> 5/4/82 0832-1300 | <u>2</u> 5/5/82 0755-1130 | <u>3</u> 5/5/82 1224-1558 |
|--|---------------------------------|---------------------------------|---------------------------------|
|--|---------------------------------|---------------------------------|---------------------------------|

Sampling Data

| | | | |
|---|-------|-------|-------|
| Sampling Duration, minutes | 240.0 | 192.0 | 192.0 |
| Nozzle Diameter, inches | 0.253 | 0.253 | 0.250 |
| Barometric Pressure, inches mercury | 29.96 | 30.07 | 30.07 |
| Average Orifice Pressure Differential, inches water | 1.59 | 1.53 | 1.61 |
| Average Dry Gas Temperature at Meter, °F | 79. | 76. | 82. |
| Total Water Collected by Train, ml | 385.0 | 320.5 | 312.0 |
| Standard Volume of Water Vapor Collected, cubic feet | 18.1 | 15.1 | 14.7 |
| Dry Gas Meter Calibration Factor, dimensionless | 0.998 | 0.998 | 0.998 |
| Sample Volume at Meter Conditions, cubic feet | 156.5 | 123.6 | 126.6 |
| Sample Volume at Standard Conditions, cubic feet ¹ | 153.8 | 122.6 | 124.2 |

Gas Stream Composition

| | | | |
|---|-------|-------|-------|
| CO ₂ , percent by volume | 8.7 | 8.9 | 8.9 |
| O ₂ , percent by volume | 8.7 | 8.6 | 8.9 |
| CO, percent by volume | 0.0 | 0.0 | 0.0 |
| N ₂ , percent by volume | 82.6 | 82.5 | 82.2 |
| Moisture in Gas Stream, percent by volume | 10.5 | 11.0 | 10.6 |
| Mole Fraction of Dry Gas | 0.895 | 0.890 | 0.894 |
| Molecular Weight of Dry Gas | 29.7 | 29.8 | 29.8 |
| Molecular Weight of Wet Gas | 28.5 | 28.5 | 28.5 |

Gas Stream Velocity and Volumetric Flow

| | | | |
|---|---------|---------|---------|
| Static Pressure, inches water | - 0.74 | - 0.69 | - 0.59 |
| Absolute Pressure, inches mercury | 30.0 | 30.0 | 30.0 |
| Average Temperature, °F | 315. | 314. | 317. |
| Pitot Tube Calibration Coefficient, dimensionless | 0.84 | 0.85 | 0.84 |
| Total Number of Traverse Points | 48.0 | 48.0 | 48.0 |
| Velocity at Actual Conditions, feet/second | 48.7 | 47.5 | 48.7 |
| Stack/duct Cross-Sectional Area, square feet | 22.7 | 22.7 | 22.7 |
| Volumetric Flow, Wet Actual cubic feet/minute | 66,300. | 64,600. | 66,400. |
| Volumetric Flow, Dry Standard cubic feet/minute | 40,600. | 39,400. | 40,500. |

Percent Isokinetic

102.7 105.3 106.4

Unit/Process Operations Data

| | | | |
|---|-------|-------|-------|
| Fuel Firing Ratio, %Gas:% Oil | 40:60 | 40:60 | 40:60 |
| Percent O ₂ Existing Boiler | 5.5 | 5.3 | 5.5 |
| Percent O ₂ at Test Location | 8.7 | 8.6 | 8.9 |
| Steam Load, 10 ³ lbs/hr | 126. | 127. | 128. |

¹ Standard Conditions = 68°F (20°C) and 29.92 inches (760 mm) mercury, dry basis.

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REFINERY A

SOURCE 2

Table A-22

SUMMARY OF PARTICULATE AND NO_x TEST RESULTSTest Data

| | 1 5/4/82 0832-1300 | 2 5/5/82 0755-1130 | 3 5/5/82 1224-1558 |
|--|--------------------------|--------------------------|--------------------------|
|--|--------------------------|--------------------------|--------------------------|

Gas Flow Volumes

| | | | |
|---|---------|---------|---------|
| Dry Standard Cubic Feet/Minute ⁽¹⁾ | 40,600. | 39,400. | 40,500. |
| Wet Actual Cubic Feet/Hinute | 66,300. | 64,600. | 66,400. |

Particulate Analysis Report

| | | | |
|--|--------|--------|--------|
| Front-Half Acetone Wash Residue Wt., grams | 0.0193 | 0.0190 | 0.0186 |
| Front-Half Hethylene Chloride Wash Residue Wt., grams | ----- | ----- | 0.0091 |
| Filter Catch Wt., grams | 0.0639 | 0.0445 | 0.0411 |
| Front-Half Catch Wt. Sub-total, grams | 0.0832 | 0.0635 | 0.0688 |
| Hethylene Chloride Extraction of Impinger Contents/Wash Residue Wt., grams | ----- | ----- | 0.0013 |
| Impinger Contents/Wash Residue Wt., grams | 0.0740 | 0.0422 | 0.0249 |
| Back-Half Acetone Wash Residue Wt., grams | 0.0014 | 0.0020 | 0.0040 |
| Back-Half Hethylene Chloride Wash Residue Wt., grams | ----- | ----- | 0.0260 |
| Back Half Catch Wt. Sub-total, grams | 0.0754 | 0.0442 | 0.0562 |
| Total Catch Weight, grams | 0.1586 | 0.1077 | 0.1250 |

Particulate ResultsFront-Half

| | | | |
|---|-----|-----|-----|
| Concentration, grains/dry standard cubic foot, $\times 10^{-3}$ | 8.3 | 8.0 | 8.5 |
| Mass Emission Rate, pounds/hour | 2.9 | 2.7 | 3.0 |

Total

| | | | |
|---|------|------|------|
| Concentration, grains/dry standard cubic foot, $\times 10^{-3}$ | 15.9 | 13.6 | 15.5 |
| Mass Emission Rate, pounds/hour | 5.5 | 4.6 | 5.4 |

NO_x Emissions, as NO₂⁽²⁾

| | | | |
|--|------|------|------|
| Concentration, Parts/million by Volume, dry basis | 200. | 211. | 211. |
| Concentration, Pounds/Dry Standard Cubic Foot $\times 10^{-6}$ | 23.8 | 25.2 | 25.2 |
| Mass Emission Rate, Pounds/Hour | 58. | 60. | 61. |

⁽¹⁾Standard Conditions = 68°F (20°C) and 29.92 inches Hg.⁽²⁾Results shown are averages of three (3) grab samples.

AMERICAN PETROLEUM INSTITUTE
REFINERY A
SOURCE 2
Table A-23

SUMMARY OF PARTICULATE TEST DATA

Test Data

| | 4 | 5 | 6 |
|-----------------|-----------|-----------|-----------|
| Test Run Number | 5/6/82 | 5/7/82 | 5/7/82 |
| Test Date | 0924-1530 | 0836-1305 | 1348-1720 |
| Test Period | | | |

Sampling Data

| | | | |
|---|-------|-------|-------|
| Sampling Duration, minutes | 240.0 | 240.0 | 192.0 |
| Nozzle Diameter, inches | 0.253 | 0.250 | 0.253 |
| Barometric Pressure, inches mercury | 30.04 | 29.93 | 29.93 |
| Average Orifice Pressure Differential, inches water | 1.64 | 2.06 | 2.12 |
| Average Dry Gas Temperature at Meter, °F | 81. | 81. | 80. |
| Total Water Collected by Train, ml | 385.5 | 394.0 | 317.0 |
| Standard Volume of Water Vapor Collected, cubic feet | 18.1 | 18.5 | 14.9 |
| Dry Gas Meter Calibration Factor, dimensionless | 0.998 | 0.998 | 0.998 |
| Sample Volume at Meter Conditions, cubic feet | 160.2 | 178.5 | 145.1 |
| Sample Volume at Standard Conditions, cubic feet ¹ | 157.2 | 174.8 | 142.4 |

Gas Stream Composition

| | | | |
|---|-------|-------|-------|
| CO ₂ , percent by volume | 7.8 | 7.7 | 7.7 |
| O ₂ , percent by volume | 10.0 | 10.0 | 10.0 |
| CO, percent by volume | 0.0 | 0.0 | 0.0 |
| N ₂ , percent by volume | 82.2 | 82.3 | 82.3 |
| Moisture in Gas Stream, percent by volume | 10.4 | 9.6 | 9.5 |
| Mole Fraction of Dry Gas | 0.896 | 0.904 | 0.905 |
| Molecular Weight of Dry Gas | 29.6 | 29.6 | 29.6 |
| Molecular Weight of Wet Gas | 28.4 | 28.5 | 28.5 |

Gas Stream Velocity and Volumetric Flow

| | | | |
|---|---------|---------|---------|
| Static Pressure, inches water | - 0.69 | - 0.71 | - 0.66 |
| Absolute Pressure, inches mercury | 30.0 | 29.9 | 29.9 |
| Average Temperature, °F | 318. | 314. | 318. |
| Pitot Tube Calibration Coefficient, dimensionless | 0.84 | 0.84 | 0.84 |
| Total Number of Traverse Points | 48.0 | 48.0 | 48.0 |
| Velocity at Actual Conditions, feet/second | 49.3 | 55.0 | 56.0 |
| Stack/duct Cross-Sectional Area, square feet | 22.7 | 22.7 | 22.7 |
| Volumetric Flow, Wet Actual cubic feet/minute | 67,100. | 74,900. | 76,300. |
| Volumetric Flow, Dry Standard cubic feet/minute | 40,900. | 46,100. | 46,800. |

Percent Isokinetic

| | | |
|-------|-------|-------|
| 104.0 | 105.1 | 103.1 |
|-------|-------|-------|

Unit/Process Operations Data

| | | | |
|---|-------|-------|-------|
| Fuel Firing Ratio, %Gas:% Oil | 41:59 | 40:60 | 39:61 |
| Percent O ₂ Exiting Boiler | 6.8 | 6.8 | 6.8 |
| Percent O ₂ at Test Location | 10.0 | 10.0 | 10.0 |
| Steam Load 10 ³ lbs/hr | 129. | 130. | 133. |

¹Standard Conditions = 68°F (20°C) and 29.92 inches (760 mm) mercury, dry basis.

AMERICAN PETROLEUM INSTITUTE
REFINERY A
SOURCE 2

Table A-24
SUMMARY OF PARTICULATE AND NO_x TEST RESULTS

Test Data

| | 4 | 5 | 6 |
|-----------------|-----------|-----------|-----------|
| Test Run Number | 5/6/82 | 5/7/82 | 5/7/82 |
| Test Date | 0924-1530 | 0836-1305 | 1348-1720 |
| Test Time | | | |

Gas Flow Volumes

| | | | |
|---|---------|---------|---------|
| Dry Standard Cubic Feet/Minute ⁽¹⁾ | 40,900. | 46,100. | 46,800. |
| Wet Actual Cubic Feet/Minute | 67,100. | 74,900. | 76,300. |

Particulate Analysis Report

| | | | |
|--|--------|--------|--------|
| Front-Half Acetone Wash Residue Wt., grams | 0.0165 | 0.0275 | 0.0121 |
| Front-Half Methylene Chloride Wash Residue Wt., grams | ----- | ----- | 0.0070 |
| Filter Catch Wt., grams | 0.0497 | 0.0540 | 0.0468 |
| Front-Half Catch Wt. Sub-total, grams | 0.0662 | 0.0815 | 0.0659 |
| Methylene Chloride Extraction of Impinger Contents/Wash Residue Wt., grams | ----- | ----- | 0.0007 |
| Impinger Contents/Wash Residue Wt., grams | 0.0460 | 0.0841 | 0.0416 |
| Back-Half Acetone Wash Residue Wt., grams | 0.0042 | 0.0034 | 0.0007 |
| Back-Half Methylene Chloride Wash Residue Wt., grams | ----- | ----- | 0.0175 |
| Back Half Catch Wt. Sub-total, grams | 0.0502 | 0.0875 | 0.0605 |
| Total Catch Weight, grams | 0.1164 | 0.1690 | 0.1264 |

Particulate ResultsFront-Half

| | | | |
|---|-----|-----|-----|
| Concentration, grains/dry standard cubic foot, $\times 10^{-3}$ | 6.5 | 7.2 | 7.1 |
| Hass Emission Rate, pounds/hour | 2.3 | 2.8 | 2.9 |

Total

| | | | |
|---|------|------|------|
| Concentration, grains/dry standard cubic foot, $\times 10^{-3}$ | 11.4 | 14.9 | 13.7 |
| Hass Emission Rate, pounds/hour | 4.0 | 5.9 | 5.5 |

NO_x Emissions, as NO₂⁽²⁾

| | | | |
|--|------|------|------|
| Concentration, Parts/million by Volume, dry basis | 194. | 212. | 206. |
| Concentration, Pounds/Dry Standard Cubic Foot $\times 10^{-6}$ | 23.2 | 25.3 | 24.6 |
| Hass Emission Rate, Pounds/Hour | 57. | 70. | 69. |

⁽¹⁾Standard Conditions = 68°F (20°C) and 29.92 Inches Hg.
⁽²⁾Results shown are averages of three (3) grab samples.

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REFINERY A

SOURCE 2

Table A-25

SUMMARY OF PARTICULATE TEST DATATest Data

| Test Run Number | 7 | 8 | 9 |
|-----------------|-----------|-----------|-----------|
| Test Date | 5/8/82 | 5/8/82 | 5/9/82 |
| Test Period | 0753-1217 | 1301-1721 | 0818-1824 |

Sampling Data

| | | | |
|---|-------|-------|---------|
| Sampling Duration, minutes | 240.0 | 240.0 | 576.0 |
| Nozzle Diameter, inches | 0.253 | 0.250 | 0.253 |
| Barometric Pressure, inches mercury | 29.91 | 29.91 | 29.95 |
| Average Orifice Pressure Differential, inches water | 1.34 | 1.29 | 1.17 |
| Average Dry Gas Temperature at Meter, °F | 75. | 79. | 78. |
| Total Water Collected by Train, ml | 518.5 | 489.0 | 1,171.5 |
| Standard Volume of Water Vapor Collected, cubic feet | 24.4 | 23.0 | 55.1 |
| Dry Gas Meter Calibration Factor, dimensionless | 0.998 | 0.998 | 0.998 |
| Sample Volume at Meter Conditions, cubic feet | 138.9 | 138.8 | 318.8 |
| Sample Volume at Standard Conditions, cubic feet ¹ | 137.0 | 135.9 | 313.3 |

Gas Stream Composition

| | | | |
|---|-------|-------|-------|
| CO ₂ , percent by volume | 8.2 | 8.4 | 8.2 |
| O ₂ , percent by volume | 7.0 | 7.0 | 6.6 |
| CO, percent by volume | 0.0 | 0.0 | 0.0 |
| N ₂ , percent by volume | 84.8 | 84.6 | 85.2 |
| Moisture in Gas Stream, percent by volume | 15.1 | 14.5 | 15.0 |
| Mole Fraction of Dry Gas | 0.849 | 0.855 | 0.850 |
| Molecular Weight of Dry Gas | 29.6 | 29.7 | 29.6 |
| Molecular Weight of Wet Gas | 27.8 | 28.0 | 27.8 |

Gas Stream Velocity and Volumetric Flow

| | | | |
|---|---------|---------|---------|
| Static Pressure, inches water | - 0.60 | - 0.61 | - 0.63 |
| Absolute Pressure, inches mercury | 29.9 | 29.9 | 29.9 |
| Average Temperature, °F | 302. | 305. | 302. |
| Pitot Tube Calibration Coefficient, dimensionless | 0.84 | 0.84 | 0.84 |
| Total Number of Traverse Points | 48.0 | 48.0 | 48.0 |
| Velocity at Actual Conditions, feet/second | 44.3 | 44.6 | 42.6 |
| Stack/duct Cross-Sectional Area, square feet | 22.7 | 22.7 | 22.7 |
| Volumetric Flow, Wet Actual cubic feet/minute | 60,400. | 60,700. | 58,000. |
| Volumetric Flow, Dry Standard cubic feet/minute | 35,400. | 35,800. | 34,100. |

Percent Isokinetic

104.8 105.4 103.5

Unit/Process Operations Data

| | | | |
|---|-------|-------|-------|
| Fuel Firing Ratio, %Gas:Oil | 100:0 | 100:0 | 100:0 |
| Percent O ₂ Existing Boiler | 2.9 | 3.0 | 2.9 |
| Percent O ₂ at Test Location | 7.0 | 7.0 | 6.6 |
| Steam Load 103 lbs/hr | 138. | 141. | 138. |

¹ Standard Conditions = 68°F (20°C) and 29.92 inches (760 mm) mercury, dry basis.

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REFINERY A

SOURCE 2

Table A-26

SUMMARY OF PARTICULATE AND NO_x TEST RESULTSTest Data

| | 7 5/8/82 0753-1217 | 8 5/8/82 1301-1721 | 9 5/9/82 0818-1824 |
|--|--------------------------|--------------------------|--------------------------|
|--|--------------------------|--------------------------|--------------------------|

Gas Flow Volumes

| | | | |
|---|---------|---------|---------|
| Dry Standard Cubic Feet/Minute ⁽¹⁾ | 35,400. | 35,800. | 34,100. |
| Wet Actual Cubic Feet/Minute | 60,400. | 60,700. | 58,000. |

Particulate Analysis Report

| | | | |
|--|--------|--------|--------|
| Front-Half Acetone Wash Residue Wt., grams | 0.0131 | 0.0076 | 0.0074 |
| Front-Half Methylene Chloride Wash Residue Wt., grams | ----- | ----- | 0.0049 |
| Filter Catch Wt., grams | 0.0037 | 0.0035 | 0.0429 |
| Front-Half Catch Wt. Sub-total, grams | 0.0168 | 0.0111 | 0.0552 |
| Methylene Chloride Extraction of Impinger Contents/Wash Residue Wt., grams | ----- | ----- | 0.0009 |
| Impinger Contents/Wash Residue Wt., grams | 0.0138 | 0.0201 | 0.0699 |
| Back-Half Acetone Wash Residue Wt., grams | 0.0027 | 0.0031 | 0.0067 |
| Back-Half Methylene Chloride Wash Residue Wt., grams | ----- | ----- | 0.0256 |
| Back Half Catch Wt. Sub-total, grams | 0.0165 | 0.0232 | 0.1031 |
| Total Catch Weight, grams | 0.0333 | 0.0343 | 0.1583 |

Particulate ResultsFront-Half

| | | | |
|---|------|------|------|
| Concentration, grains/dry standard cubic foot, $\times 10^{-3}$ | 1.9 | 1.3 | 2.7 |
| Hass Emission Rate, pounds/hour | 0.57 | 0.39 | 0.80 |

Total

| | | | |
|---|-----|-----|-----|
| Concentration, grains/dry standard cubic foot, $\times 10^{-3}$ | 3.8 | 3.9 | 7.7 |
| Hass Emission Rate, pounds/hour | 1.1 | 1.2 | 2.3 |

NO_x Emissions, as NO₂⁽²⁾

| | | | |
|--|-----|------|-----|
| Concentration, Parts/million by Volume, dry basis | 76. | 102. | 69. |
| Concentration, Pounds/Dry Standard Cubic Foot $\times 10^{-6}$ | 9.0 | 12.2 | 8.2 |
| Hass Emission Rate, Pounds/Hour | 19. | 26. | 17. |

⁽¹⁾Standard Conditions = 68°F (20°C) and 29.92 inches Hg.⁽²⁾Results shown are averages of three (3) grab samples.

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REFINERY A

SOURCE 2

Table A-27

SUMMARY OF PARTICULATE TEST DATATest Data

| | 10 5/10/82 0850-1315 | 11 5/10/82 1410-1825 | 12 5/11/82 0813-1228 |
|--|----------------------------|----------------------------|----------------------------|
|--|----------------------------|----------------------------|----------------------------|

Sampling Data

| | | | |
|---|-------|-------|-------|
| Sampling Duration, minutes | 240.0 | 240.0 | 240.0 |
| Nozzle Diameter, inches | 0.250 | 0.250 | 0.250 |
| Barometric Pressure, inches mercury | 30.01 | 30.01 | 29.99 |
| Average Orifice Pressure Differential, inches water | 1.60 | 1.57 | 1.37 |
| Average Dry Gas Temperature at Meter, °F | 76. | 77. | 76. |
| Total Water Collected by Train, ml | 505.5 | 519.8 | 485.5 |
| Standard Volume of Water Vapor Collected, cubic feet | 23.8 | 24.5 | 22.9 |
| Dry Gas Meter Calibration Factor, dimensionless | 0.998 | 0.998 | 0.998 |
| Sample Volume at Meter Conditions, cubic feet | 159.3 | 157.6 | 146.9 |
| Sample Volume at Standard Conditions, cubic feet ¹ | 157.7 | 155.7 | 145.1 |

Gas Stream Composition

| | | | |
|---|-------|-------|-------|
| CO ₂ , percent by volume | 6.6 | 6.9 | 6.7 |
| O ₂ , percent by volume | 8.6 | 8.7 | 8.5 |
| CO, percent by volume | 0.0 | 0.0 | 0.0 |
| N ₂ , percent by volume | 84.8 | 84.4 | 84.8 |
| Moisture in Gas Stream, percent by volume | 13.1 | 13.6 | 13.6 |
| Mole Fraction of Dry Gas | 0.869 | 0.864 | 0.864 |
| Molecular Weight of Dry Gas | 29.4 | 29.4 | 29.4 |
| Molecular Weight of Wet Gas | 27.9 | 27.9 | 27.9 |

Gas Stream Velocity and Volumetric Flow

| | | | |
|---|---------|---------|---------|
| Static Pressure, inches water | - 0.64 | - 0.61 | - 0.67 |
| Absolute Pressure, inches mercury | 30.0 | 30.0 | 29.9 |
| Average Temperature, °F | 315. | 315. | 312. |
| Pitot Tube Calibration Coefficient, dimensionless | 0.84 | 0.84 | 0.84 |
| Total Number of Traverse Points | 48.0 | 48.0 | 48.0 |
| Velocity at Actual Conditions, feet/second | 51.8 | 50.9 | 47.5 |
| Stack/duct Cross-Sectional Area, square feet | 22.7 | 22.7 | 22.7 |
| Volumetric Flow, Wet Actual cubic feet/minute | 70,600. | 69,300. | 64,700. |
| Volumetric Flow, Dry Standard cubic feet/minute | 41,800. | 40,900. | 38,300. |

Percent Isokinetic

104.5 105.7 105.2

Unit/Process Operations Data

| | | | |
|---|-------|-------|-------|
| Fuel Firing Ratio, %Gas:Oil | 100:0 | 100:0 | 100:0 |
| Percent O ₂ Exiting Boiler | 4.8 | 4.6 | 4.6 |
| Percent O ₂ at Test Location | 8.6 | 8.7 | 8.5 |
| Steam Load 10 ³ lbs/hr | 146. | 142. | 138. |

¹Standard Conditions = 68°F (20°C) and 29.92 inches (760 mm) mercury, dry basis.

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REFINERY A

SOURCE 2

Table A-28

SUMMARY OF PARTICULATE AND NO_x TEST RESULTSTest Data

| | 10 5/10/82 0850-1315 | 11 5/10/82 1410-1825 | 12 5/11/82 0813-1228 |
|--|----------------------------|----------------------------|----------------------------|
|--|----------------------------|----------------------------|----------------------------|

Gas Flow Volumes

| | | | |
|---|---------|---------|---------|
| Dry Standard Cubic Feet/Minute ⁽¹⁾ | 41,800. | 40,900. | 38,300. |
| Wet Actual Cubic Feet/Minute | 70,600. | 69,300. | 64,700. |

Particulate Analysis Report

| | | | |
|--|--------|--------|--------|
| Front-Half Acetone Wash Residue Wt., grams | 0.0020 | 0.0037 | 0.0023 |
| Front-Half Methylene Chloride Wash Residue Wt., grams | ----- | ----- | 0.0054 |
| Filter Catch Wt., grams | 0.0047 | 0.0018 | 0.0034 |
| Front-Half Catch Wt. Sub-total, grams | 0.0067 | 0.0055 | 0.0111 |
| Methylene Chloride Extraction of Impinger Contents/Wash Residue Wt., grams | ----- | ----- | 0.0006 |
| Impinger Contents/Wash Residue Wt., grams | 0.0116 | 0.0147 | 0.0023 |
| Back-Half Acetone Wash Residue Wt., grams | 0.0001 | 0.0000 | 0.0002 |
| Back-Half Methylene Chloride Wash Residue Wt., grams | ----- | ----- | 0.0169 |
| Back Half Catch Wt. Sub-total, grams | 0.0117 | 0.0147 | 0.0200 |
| Total Catch Weight, grams | 0.0184 | 0.0202 | 0.0311 |

Particulate ResultsFront-Half

| | | | |
|---|------|------|------|
| Concentration, grains/dry standard cubic foot, $\times 10^{-3}$ | 0.7 | 0.5 | 1.2 |
| Mass Emission Rate, pounds/hour | 0.24 | 0.19 | 0.39 |

Total

| | | | |
|---|------|------|-----|
| Concentration, grains/dry standard cubic foot, $\times 10^{-3}$ | 1.8 | 2.0 | 3.3 |
| Mass Emission Rate, pounds/hour | 0.65 | 0.70 | 1.1 |

NO_x Emissions, as NO₂⁽²⁾

| | | | |
|--|------|------|------|
| Concentration, Parts/million by Volume, dry basis | 131. | 125. | 117. |
| Concentration, Pounds/Dry Standard Cubic Foot $\times 10^{-6}$ | 15.7 | 14.9 | 14.0 |
| Mass Emission Rate, Pounds/Hour | 39. | 37. | 32. |

⁽¹⁾Standard Conditions = 68°F (20°C) and 29.92 inches Hg.⁽²⁾Results shown are averages of three (3) grab samples.

AMERICAN PETROLEUM INSTITUTE

REFINERY A

SOURCE 2

Table A-29

SUMMARY OF PARTICULATE TEST DATATest Data

| | | |
|-----------------|-----------|-----------|
| Test Run Number | 13 | 14 |
| Test Date | 5/12/82 | 5/12/82 |
| Test Period | 0817-1230 | 1311-1723 |

Sampling Data

| | | |
|---|-------|-------|
| Sampling Duration, minutes | 240.0 | 240.0 |
| Nozzle Diameter, inches | 0.250 | 0.250 |
| Barometric Pressure, inches mercury | 29.95 | 29.95 |
| Average Orifice Pressure Differential, inches water | 1.43 | 1.48 |
| Average Dry Gas Temperature at Meter, °F | 81. | 79. |
| Total Water Collected by Train, ml | 430.0 | 443.0 |
| Standard Volume of Water Vapor Collected, cubic feet | 20.2 | 20.9 |
| Dry Gas Meter Calibration Factor, dimensionless | 0.998 | 0.998 |
| Sample Volume at Meter Conditions, cubic feet | 151.4 | 154.8 |
| Sample Volume at Standard Conditions, cubic feet ¹ | 148.0 | 152.1 |

Gas Stream Composition

| | | |
|---|-------|-------|
| CO ₂ , percent by volume | 8.0 | 7.6 |
| O ₂ , percent by volume | 8.8 | 9.0 |
| CO, percent by volume | 0.0 | 0.0 |
| N ₂ , percent by volume | 83.2 | 83.4 |
| Moisture in Gas Stream, percent by volume | 12.0 | 12.1 |
| Mole Fraction of Dry Gas | 0.880 | 0.879 |
| Molecular Weight of Dry Gas | 29.6 | 29.6 |
| Molecular Weight of Wet Gas | 28.2 | 28.2 |

Gas Stream Velocity and Volumetric Flow

| | | |
|---|---------|---------|
| Static Pressure, inches water | - 0.62 | - 0.61 |
| Absolute Pressure, inches mercury | 29.9 | 29.9 |
| Average Temperature, °F | 316. | 317. |
| Pitot Tube Calibration Coefficient, dimensionless | 0.84 | 0.84 |
| Total Number of Traverse Points | 48.0 | 48.0 |
| Velocity at Actual Conditions, feet/second | 48.8 | 49.9 |
| Stack/duct Cross-Sectional Area, square feet | 22.7 | 22.7 |
| Volumetric Flow, Wet Actual cubic feet/minute | 66,400. | 67,900. |
| Volumetric Flow, Dry Standard cubic feet/minute | 39,700. | 40,600. |

Percent Isokinetic

103.3 104.0

Unit/Process Operations Data

| | | |
|---|-------|-------|
| Fuel Firing Ratio, %Gas:%Oil | 68:32 | 70:30 |
| Percent O ₂ Exiting Boiler | 5.3 | 5.1 |
| Percent O ₂ at Test Location | 8.8 | 9.0 |
| Steam Load 10 ³ lbs/hr | 137. | 137. |

¹Standard Conditions = 68°F (20°C) and 29.92 inches (760 mm) mercury, dry basis.

AMERICAN PETROLEUM INSTITUTE

REFINERY A

SOURCE 2

Table A-30

SUMMARY OF PARTICULATE AND NO_x TEST RESULTSTest Data

| | | |
|-----------------|-----------|-----------|
| Test Run Number | 13 | 14 |
| Test Date | 5/12/82 | 5/12/82 |
| Test Time | 0817-1230 | 1311-1723 |

Gas Flow Volumes

| | | |
|---|---------|---------|
| Dry Standard Cubic Feet/Minute ⁽¹⁾ | 39,700. | 40,600. |
| Wet Actual Cubic Feet/Minute | 66,400. | 67,900. |

Particulate Analysis Report

| | | |
|--|--------|--------|
| Front-Half Acetone Wash Residue Wt., grams | 0.0055 | 0.0085 |
| Front-Half Hethylene Chloride Wash Residue Wt., grams | ----- | ----- |
| Filter Catch Wt., grams | 0.0285 | 0.0300 |
| Front-Half Catch Wt. Sub-total, grams | 0.0340 | 0.0385 |
| Hethylene Chloride Extraction of Impinger Contents/Wash Residue Wt., grams | ----- | ----- |
| Impinger Contents/Wash Residue Wt., grams | 0.0130 | 0.0422 |
| Back-Half Acetone Wash Residue Wt., grams | 0.0057 | 0.0028 |
| Back-Half Hethylene Chloride Wash Residue Wt., grams | ----- | ----- |
| Back Half Catch Wt. Sub-total, grams | 0.0187 | 0.0460 |
| Total Catch Weight, grams | 0.0527 | 0.0835 |

Particulate ResultsFront-Half

| | | |
|---|-----|-----|
| Concentration, grains/dry standard cubic foot, $\times 10^{-3}$ | 3.5 | 3.9 |
| Mass Emission Rate, pounds/hour | 1.2 | 1.4 |

Total

| | | |
|---|-----|-----|
| Concentration, grains/dry standard cubic foot, $\times 10^{-3}$ | 5.5 | 8.5 |
| Mass Emission Rate, pounds/hour | 1.9 | 2.9 |

NO_x Emissions, as NO₂⁽²⁾

| | | |
|--|------|------|
| Concentration, Parts/million by Volume, dry basis | 215. | 203. |
| Concentration, Pounds/Dry Standard Cubic Foot $\times 10^{-6}$ | 25.6 | 24.2 |
| Mass Emission Rate, Pounds/Hour | 61. | 59. |

⁽¹⁾Standard Conditions = 60°F (20°C) and 29.92 inches Hg.⁽²⁾Results shown are averages of three (3) grab samples.

AMERICAN PETROLEUM INSTITUTE

REFINERY A

SOURCE 2

Table A-31

SUMMARY OF PARTICULATE TEST DATATest Data

| | | |
|-----------------|-----------|-----------|
| Test Run Number | 15 | 16 |
| Test Date | 5/13/82 | 5/13/81 |
| Test Period | 0832-1246 | 1401-1832 |

Sampling Data

| | | |
|---|-------|-------|
| Sampling Duration, minutes | 240.0 | 240.0 |
| Nozzle Diameter, inches | 0.250 | 0.253 |
| Barometric Pressure, inches mercury | 29.98 | 29.98 |
| Average Orifice Pressure Differential, inches water | 1.42 | 1.44 |
| Average Dry Gas Temperature at Meter, °F | 78. | 79. |
| Total Water Collected by Train, ml | 414.0 | 429.0 |
| Standard Volume of Water Vapor Collected, cubic feet | 19.5 | 20.2 |
| Dry Gas Meter Calibration Factor, dimensionless | 0.998 | 0.998 |
| Sample Volume at Meter Conditions, cubic feet | 150.3 | 152.4 |
| Sample Volume at Standard Conditions, cubic feet ¹ | 147.9 | 149.8 |

Gas Stream Composition

| | | |
|---|-------|-------|
| CO ₂ , percent by volume | 7.2 | 7.4 |
| O ₂ , percent by volume | 9.6 | 9.8 |
| CO, percent by volume | 0.0 | 0.0 |
| N ₂ , percent by volume | 83.2 | 82.8 |
| Moisture in Gas Stream, percent by volume | 11.6 | 11.9 |
| Mole Fraction of Dry Gas | 0.884 | 0.881 |
| Molecular Weight of Dry Gas | 29.5 | 29.6 |
| Molecular Weight of Wet Gas | 28.2 | 28.2 |

Gas Stream Velocity and Volumetric Flow

| | | |
|---|---------|---------|
| Static Pressure, inches water | - 0.62 | - 0.67 |
| Absolute Pressure, inches mercury | 29.9 | 29.9 |
| Average Temperature, °F | 312. | 312. |
| Pitot Tube Calibration Coefficient, dimensionless | 0.84 | 0.84 |
| Total Number of Traverse Points | 48.0 | 48.0 |
| Velocity at Actual Conditions, feet/second | 48.9 | 49.3 |
| Stack/duct Cross-Sectional Area, square feet | 22.7 | 22.7 |
| Volumetric Flow, Wet Actual cubic feet/minute | 66,500. | 67,100. |
| Volumetric Flow, Dry Standard cubic feet/minute | 40,200. | 40,400. |

Percent Isokinetic

102.0 100.3

Unit/Process Operations Data

| | | |
|---|-------|-------|
| Fuel Firing Ratio, %Gas:%Oil | 75:25 | 74:26 |
| Percent O ₂ Exiting Boiler | 6.5 | 6.4 |
| Percent O ₂ at Test Location | 9.6 | 9.8 |
| Steam Load 10 ³ lbs/hr | 135. | 136. |

¹Standard Conditions = 68°F (20°C) and 29.92 inches (760 mm) mercury, dry basis.

AMERICAN PETROLEUM INSTITUTE

REFINERY A

SOURCE 2
Table A-32SUMMARY OF PARTICULATE AND NO_x TEST RESULTSTest Data

| | | |
|-----------------|-----------|-----------|
| Test Run Number | 15 | 16 |
| Test Date | 5/13/82 | 5/13/82 |
| Test Time | 0823-1246 | 1401-1832 |

Gas Flow Volumes

| | | |
|------------------------------------|---------|---------|
| Dry Standard Cubic Feet/Minute (1) | 40,200. | 40,400. |
| Wet Actual Cubic Feet/Minute | 66,500. | 67,100. |

Particulate Analysis Report

| | | |
|--|--------|--------|
| Front-Half Acetone Wash Residue Wt., grams | 0.0047 | 0.0135 |
| Front-Half Methylene Chloride Wash Residue Wt., grams | ----- | ----- |
| Filter Catch Wt., grams | 0.0273 | 0.0283 |
| Front-Half Catch Wt. Sub-total, grams | 0.0320 | 0.0418 |
| Methylene Chloride Extraction of Impinger Contents/Wash Residue Wt., grams | ----- | ----- |
| Impinger Contents/Wash Residue Wt., grams | 0.0310 | 0.0557 |
| Back-Half Acetone Wash Residue Wt., grams | 0.0042 | 0.0024 |
| Back-Half Methylene Chloride Wash Residue Wt., grams | ----- | ----- |
| Back Half Catch Wt. Sub-total, grams | 0.0352 | 0.0581 |
| Total Catch Weight, grams | 0.0672 | 0.0999 |

Particulate ResultsFront-Half

| | | |
|---|-----|-----|
| Concentration, grains/dry standard cubic foot, $\times 10^{-3}$ | 3.3 | 4.3 |
| Mass Emission Rate, pounds/hour | 1.2 | 1.5 |

Total

| | | |
|---|-----|------|
| Concentration, grains/dry standard cubic foot, $\times 10^{-3}$ | 7.0 | 10.3 |
| Mass Emission Rate, pounds/hour | 2.4 | 3.6 |

NO_x Emissions, as NO₂ (2)

| | | |
|--|------|------|
| Concentration, Parts/million by Volume, dry basis | 189. | 202. |
| Concentration, Pounds/Dry Standard Cubic Foot $\times 10^{-6}$ | 22.5 | 24.2 |
| Mass Emission Rate, Pounds/Hour | 54. | 59. |

(1) Standard Conditions = 68°F (20°C) and 29.92 inches Hg.
 (2) Results shown are averages of three (3) grab samples.

AMERICAN PETROLEUM INSTITUTE

REFINERY A

SOURCE 2

Table A-33

PARTICLE SIZE DISTRIBUTION *

| | | | |
|--|--------------|--|-------|
| Run: | Nine | Barometric Pressure(in. Hg) | 29.95 |
| Date: | 5/9/82 | Stack Temperature($^{\circ}$ F) | 302. |
| Traverse Point No. | Sampled: C-3 | Sample Time(min.) | 570. |
| Fuel Firing Ratio, %Gas:%Oil | 100:0 | Sample Volume(cf) | 346.1 |
| Percent O ₂ (existing boiler) | 2.9 | Moisture(%H ₂ O) | 15.0 |
| Percent O ₂ (at test location) | 6.6 | Meter Temperature($^{\circ}$ F) | 73. |
| Sample Flow Rate (at stack conditions): | 1.02 cfm | Flow Setting, Δ H(in. H ₂ O) | 1.35 |
| | | Nozzle Diameter(in.) | 0.252 |
| | | Static Pressure(in. H ₂ O) | -0.63 |
| | | Meter χ | 0.994 |
| | | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|--------------|-----------------------|-----------------------------------|---------------|
| 1 | 4.6 | 13.3 | 86.7 | 8.7 |
| 2 | 0.6 | 1.7 | 85. | 8.1 |
| 3 | 0.6 | 1.7 | 83.3 | 5.0 |
| 4 | 0.6 | 1.7 | 81.6 | 3.4 |
| 5 | 0.7 | 2.1 | 79.5 | 1.8 |
| 6 | 0.9 | 2.6 | 76.9 | 0.83 |
| 7 | 0.8 | 2.4 | 74.5 | 0.49 |
| 8 | 0.6 | 1.7 | 72.8 | 0.26 |
| Backup Filter | 25.2 | 72.8 | 0.0 | --- |
| TOTAL | 34.6 | --- | --- | --- |

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*Data plotted in Figure 4-3.

AMERICAN PETROLEUM INSTITUTE

REFINERY A

SOURCE 2

Table A-34

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|--------------|---|-------|
| Run: | Thirteen | Barometric Pressure(in. Hg) | 29.95 |
| Date: | 5/12/82 | Stack Temperature($^{\circ}$ F) | 316. |
| Traverse Point No. | Sampled: D-6 | Sample Time(min.) | 240. |
| Fuel Firing Ratio, %Gas:%oil | 68:32 | Sample Volume(cf) | 151. |
| Percent O ₂ (existing boiler) | 5.3 | Moisture(%H ₂ O) | 12.0 |
| Percent O ₂ (at test location) | 8.8 | Meter Temperature($^{\circ}$ F) | 77. |
| | | Flow Setting, ΔH (in. H ₂ O) | 1.45 |
| | | Nozzle Diameter(in.) | 0.250 |
| | | Static Pressure(in. H ₂ O) | -0.62 |
| | | Meter γ | 0.994 |
| Sample Flow Rate (at stack conditions): | 1.03 cfm | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|--------------|-----------------------|-----------------------------------|---------------|
| 1 | 6.9 | 20.7 | 79.3 | 8.7 |
| 2 | 0.5 | 1.5 | 77.8 | 8.1 |
| 3 | 0.7 | 2.1 | 75.7 | 5.0 |
| 4 | 0.9 | 2.7 | 73. | 3.4 |
| 5 | 2.1 | 6.3 | 66.7 | 1.8 |
| 6 | 1.6 | 4.8 | 61.9 | 0.82 |
| 7 | 1.1 | 3.3 | 58.6 | 0.49 |
| 8 | 1.3 | 3.9 | 54.7 | 0.26 |
| Backup Filter | 18.2 | 54.7 | 0.0 | --- |
| TOTAL | 33.3 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE

REFINERY A

SOURCE 2

Table A-35

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|--------------|--|-------|
| Run: | Fourteen | Barometric Pressure(in. Hg) | 29.95 |
| Date: | 5/12/82 | Stack Temperature($^{\circ}$ F) | 317. |
| Traverse Point No. | Sampled: D-6 | Sample Time(min.) | 240. |
| Fuel Firing Ratio, %Gas:%Oil | 70:30 | Sample Volume(cf) | 156.2 |
| Percent O ₂ (existing boiler) | 5.1 | Moisture(%H ₂ O) | 12.1 |
| Percent O ₂ (at test location) | 9.0 | Meter Temperature($^{\circ}$ F) | 73. |
| | | Flow Setting, Δ H(in. H ₂ O) | 1.45 |
| | | Nozzle Diameter(in.) | 0.252 |
| | | Static Pressure(in. H ₂ O) | -0.61 |
| | | Meter γ | 0.994 |
| Sample Flow Rate (at stack conditions): | 1.08 cfm | Sample Vac.(in. Hg) | 1.0 |

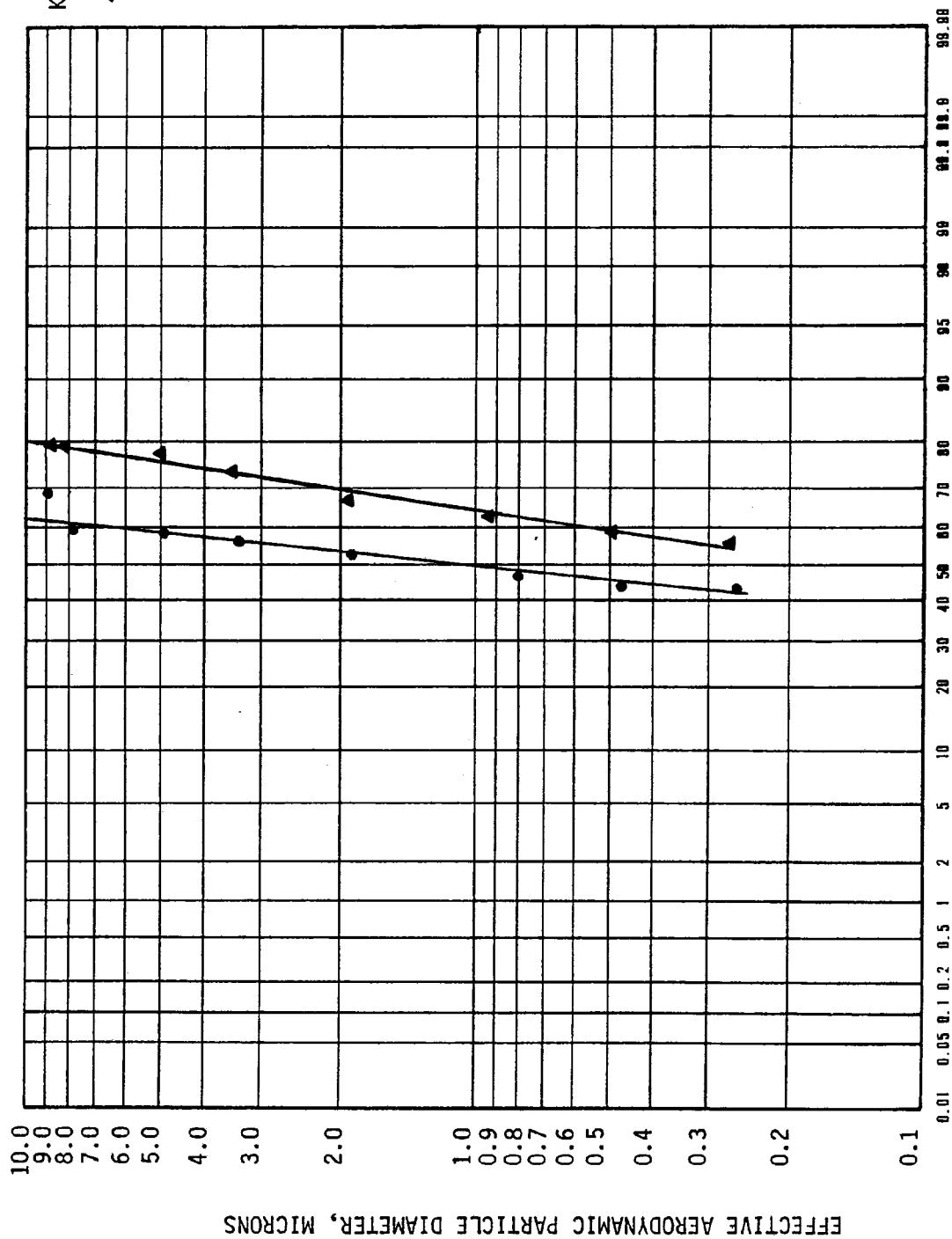
| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|-----------------------|-----------------------------------|---------------|
| 1 | 8.2 | 31.5 | 68.5 | 8.5 |
| 2 | 2.5 | 9.6 | 58.9 | 7.9 |
| 3 | 0.6 | 2.3 | 56.6 | 4.9 |
| 4 | 0.5 | 1.9 | 54.7 | 3.3 |
| 5 | 0.7 | 2.7 | 52. | 1.8 |
| 6 | 1.9 | 7.3 | 44.7 | 0.80 |
| 7 | 0.6 | 2.3 | 42.7 | 0.47 |
| 8 | 0.1 | 0.5 | 41.9 | 0.25 |
| Backup Filter | 10.9 | 41.9 | 0.0 | --- |
| TOTAL | 26.0 | --- | --- | --- |

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AMERICAN PETROLEUM INSTITUTE

REFINERY A SOURCE 2

PARTICLE SIZE DISTRIBUTION TEST RESULTS



A-38

CUMULATIVE PERCENTAGE
(% BY WEIGHT < DIAMETER)

FIGURE A-3

AMERICAN PETROLEUM INSTITUTE

REFINERY A

SOURCE 2

Table A-36

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|--------------|---|-------|
| Run: | Fifteen | Barometric Pressure(in. Hg) | 29.98 |
| Date: | 5/13/82 | Stack Temperature($^{\circ}$ F) | 312. |
| Traverse Point No. | Sampled: C-4 | Sample Time(min.) | 240. |
| Fuel Firing Ratio, %Gas:%Oil | 75:25 | Sample Volume(cf) | 160.5 |
| Percent O ₂ (existing boiler) | 6.5 | Moisture(%H ₂ O) | 11.6 |
| Percent O ₂ (at test location) | 9.6 | Meter Temperature($^{\circ}$ F) | 76. |
| | | Flow Setting, ΔH (in. H ₂ O) | 1.55 |
| | | Nozzle Diameter(in.) | 0.252 |
| | | Static Pressure(in. H ₂ O) | -0.62 |
| | | Meter χ | 0.994 |
| Sample Flow Rate (at stack conditions): | 1.07 cfm | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|--------------|-----------------------|-----------------------------------|---------------|
| 1 | 6.1 | 17.6 | 82.4 | 8.6 |
| 2 | 0.9 | 2.6 | 79.8 | 7.9 |
| 3 | 1.8 | 5.2 | 74.6 | 4.9 |
| 4 | 1.3 | 3.8 | 70.8 | 3.3 |
| 5 | 2.7 | 7.8 | 63. | 1.8 |
| 6 | 2.4 | 6.9 | 56.1 | 0.81 |
| 7 | 1.6 | 4.6 | 51.5 | 0.48 |
| 8 | 1.2 | 3.5 | 48.0 | 0.25 |
| Backup Filter | 16.7 | 48.1 | 0.0 | --- |
| TOTAL | 34.7 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE

REFINERY A

SOURCE 2

Table A-37

PARTICLE SIZE DISTRIBUTION

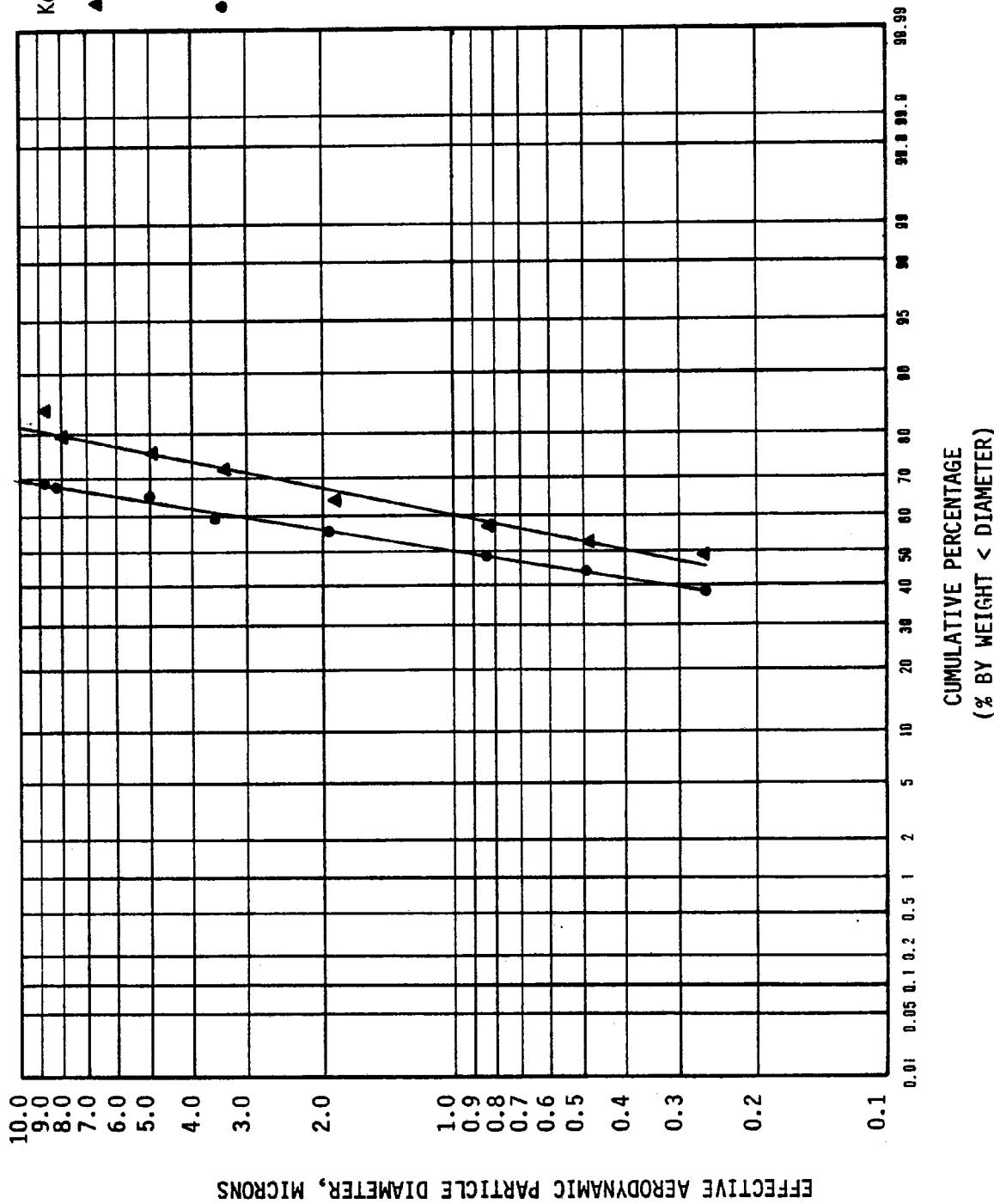
| | | | |
|--|--------------|--|-------|
| Run: | Sixteen | Barometric Pressure(in. Hg) | 29.98 |
| Date: | 5/13/82 | Stack Temperature($^{\circ}$ F) | 312. |
| Traverse Point No. | Sampled: C-5 | Sample Time(min.) | 240. |
| Fuel Firing Ratio, %Gas:%oil | 74:26 | Sample Volume(cf) | 149.8 |
| Percent O ₂ (existing boiler) | 6.4 | Moisture(%H ₂ O) | 11.9 |
| Percent O ₂ (at test location) | 9.8 | Meter Temperature($^{\circ}$ F) | 74. |
| Sample Flow Rate (at stack conditions): | 1.02 cfm | Flow Setting, Δ H(in. H ₂ O) | 1.45 |
| | | Nozzle Diameter(in.) | 0.252 |
| | | Static Pressure(in. H ₂ O) | -0.67 |
| | | Meter χ | 0.994 |
| | | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|--------------|-----------------------|-----------------------------------|---------------|
| 1 | 13.7 | 30.3 | 69.7 | 8.8 |
| 2 | 1.1 | 2.4 | 67.3 | 8.1 |
| 3 | 1.4 | 3.1 | 64.2 | 5.0 |
| 4 | 2.0 | 4.4 | 59.8 | 3.4 |
| 5 | 2.6 | 5.8 | 54. | 1.8 |
| 6 | 2.7 | 6.0 | 48. | 0.83 |
| 7 | 2.3 | 5.1 | 42.9 | 0.49 |
| 8 | 2.0 | 4.4 | 38.5 | 0.26 |
| Backup Filter | 17.4 | 38.5 | 0.0 | --- |
| TOTAL | 45.2 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE

REFINERY A SOURCE 2

PARTICLE SIZE DISTRIBUTION TEST RESULTS



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FIGURE A-4

AMERICAN PETROLEUM INSTITUTE

REFINERY A

SOURCE 2

Table A-38

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|----------|--|-------|
| Run: | One | Barometric Pressure(in. Hg) | 29.96 |
| Date: | 5/4/82 | Stack Temperature($^{\circ}$ F) | 315. |
| Traverse Point No. Sampled: | D-5 | Sample Time(min.) | 180. |
| Fuel Firing Ratio, %Gas:%Oil | 40:60 | Sample Volume(cf) | 114.4 |
| Percent O ₂ (existing boiler) | 5.5 | Moisture(%H ₂ O) | 10.5 |
| Percent O ₂ (at test location) | 8.7 | Meter Temperature($^{\circ}$ F) | 74. |
| Sample Flow Rate (at stack conditions): | 1.03 cfm | Flow Setting, Δ H(in. H ₂ O) | 1.50 |
| | | Nozzle Diameter(in.) | 0.252 |
| | | Static Pressure(in. H ₂ O) | -0.74 |
| | | Meter & | 0.994 |
| | | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|--------------------------|---|------------------|
| 1 | 14.6 | 25.5 | 74.5 | 8.7 |
| 2 | 1.4 | 2.4 | 72.1 | 8.1 |
| 3 | 1.9 | 3.3 | 68.8 | 5.0 |
| 4 | 2.6 | 4.5 | 64.3 | 4.0 |
| 5 | 2.8 | 4.9 | 59.4 | 1.8 |
| 6 | 2.9 | 5.1 | 54.3 | 0.83 |
| 7 | 2.6 | 4.5 | 49.8 | 0.49 |
| 8 | 2.5 | 4.4 | 45.4 | 0.26 |
| Backup Filter | 26.0 | 45.4 | 0.0 | --- |
| TOTAL | 57.3 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE

REFINERY A

SOURCE 2

Table A-39

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|----------|--|-------|
| Run: | Two | Barometric Pressure(in. Hg) | 30.07 |
| Date: | 5/5/82 | Stack Temperature($^{\circ}$ F) | 314. |
| Traverse Point No. Sampled: | C5 | Sample Time(min.) | 180. |
| Fuel Firing Ratio, %Gas:%oil | 40:60 | Sample Volume(cf) | 115.9 |
| Percent O ₂ (existing boiler) | 5.3 | Moisture(%H ₂ O) | 11.0 |
| Percent O ₂ (at test location) | 8.6 | Meter Temperature($^{\circ}$ F) | 70. |
| Sample Flow Rate (at stack conditions): | 1.05 cfm | Flow Setting, Δ H(in. H ₂ O) | 1.50 |
| | | Nozzle Diameter(in.) | 0.252 |
| | | Static Pressure(in. H ₂ O) | -0.69 |
| | | Meter χ | 0.994 |
| | | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|--------------------------|---|------------------|
| 1 | 11.1 | 28.8 | 71.2 | 8.6 |
| 2 | 2.2 | 5.7 | 65.5 | 8.0 |
| 3 | 1.2 | 3.1 | 62.4 | 5.0 |
| 4 | 2.2 | 5.7 | 56.7 | 3.3 |
| 5 | 2.2 | 5.7 | 51. | 1.8 |
| 6 | 1.9 | 4.9 | 46.1 | 0.81 |
| 7 | 2.0 | 5.2 | 40.9 | 0.48 |
| 8 | 1.5 | 3.9 | 37.0 | 0.25 |
| Backup Filter | 14.3 | 37.0 | 0.0 | --- |
| TOTAL | 38.6 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE

REFINERY A

SOURCE 2

Table A-40

PARTICLE SIZE DISTRIBUTION

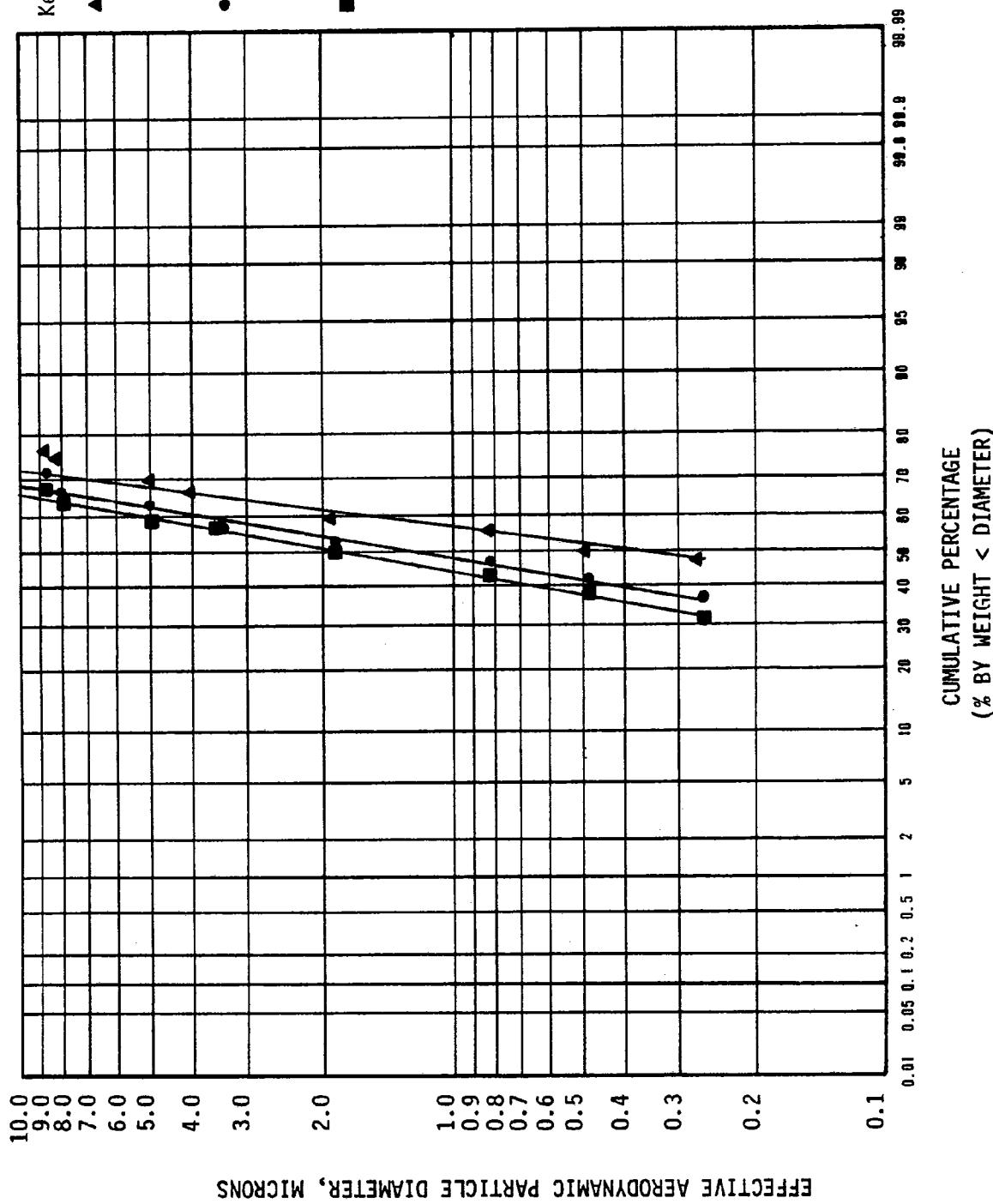
| | | | |
|--|----------|---|-------|
| Run: | Three | Barometric Pressure(in. Hg) | 30.07 |
| Date: | 5/5/82 | Stack Temperature($^{\circ}$ F) | 317. |
| Traverse Point No. Sampled: | D-6 | Sample Time(min.) | 200. |
| Fuel Firing Ratio, %Gas:%Oil | 40:60 | Sample Volume(cf) | 131.3 |
| Percent O ₂ (existing boiler) | 5.5 | Moisture(%H ₂ O) | 10.6 |
| Percent O ₂ (at test location) | 8.9 | Meter Temperature($^{\circ}$ F) | 77. |
| Sample Flow Rate (at stack conditions): | 1.06 cfm | Flow Setting, ΔH (in. H ₂ O) | 1.5 |
| | | Nozzle Diameter(in.) | 0.252 |
| | | Static Pressure(in. H ₂ O) | -0.59 |
| | | Meter γ | 0.994 |
| | | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|--------------|-----------------------|-----------------------------------|---------------|
| 1 | 14.9 | 34.7 | 65.3 | 8.6 |
| 2 | 1.0 | 2.3 | 63. | 7.9 |
| 3 | 1.8 | 4.2 | 58.8 | 5.0 |
| 4 | 1.6 | 3.7 | 55.1 | 3.4 |
| 5 | 2.2 | 5.1 | 50. | 1.8 |
| 6 | 3.2 | 7.6 | 42.4 | 0.81 |
| 7 | 2.2 | 5.1 | 37.3 | 0.48 |
| 8 | 2.9 | 6.8 | 30.5 | 0.25 |
| Backup Filter | 13.1 | 30.5 | 0.0 | --- |
| TOTAL | 42.9 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE

REFINERY A SOURCE 2

PARTICLE SIZE DISTRIBUTION TEST RESULTS



A-45

FIGURE A-5

AMERICAN PETROLEUM INSTITUTE

REFINERY A

SOURCE 2

Table A-41

PARTICLE SIZE DISTRIBUTION

| | | |
|---|---|-------|
| Run: Four | Barometric Pressure(in. Hg) | 30.04 |
| Date: 5/6/82 | Stack Temperature($^{\circ}$ F) | 318. |
| Traverse Point No. Sampled: C4 | Sample Time(min.) | 240. |
| Fuel Firing Ratio, %Gas:%Oil | Sample Volume(cf) | 154.4 |
| Percent O ₂ (existing boiler) | Moisture(%H ₂ O) | 10.4 |
| Percent O ₂ (at test location) | Meter Temperature($^{\circ}$ F) | 77. |
| 10.0 | Flow Setting, ΔH (in. H ₂ O) | 1.5 |
| | Nozzle Diameter(in.) | 0.252 |
| | Static Pressure(in. H ₂ O) | -0.69 |
| Sample Flow Rate (at stack conditions): 1.04 cfm | Meter χ | 0.994 |
| | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|--------------------------|---|------------------|
| 1 | 13.2 | 26.7 | 73.3 | 8.7 |
| 2 | 1.6 | 3.2 | 70.1 | 8.1 |
| 3 | 2.4 | 4.8 | 65.3 | 5.0 |
| 4 | 2.7 | 5.4 | 59.9 | 3.4 |
| 5 | 2.9 | 5.9 | 54. | 1.8 |
| 6 | 3.3 | 6.7 | 47.3 | 0.82 |
| 7 | 2.9 | 5.9 | 41.4 | 0.49 |
| 8 | 2.5 | 5.0 | 36.4 | 0.26 |
| Backup Filter | 18.0 | 36.4 | 0.0 | --- |
| TOTAL | 49.5 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE

REFINERY A

SOURCE 2

Table A-42

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|--------------|--|-------|
| Run: | Five | Barometric Pressure(in. Hg) | 29.93 |
| Date: | 5/7/82 | Stack Temperature($^{\circ}$ F) | 314. |
| Traverse Point No. | Sampled: D-4 | Sample Time(min.) | 200. |
| Fuel Firing Ratio, %Gas:%Oil | 40:60 | Sample Volume(cf) | 134.8 |
| Percent O ₂ (existing boiler) | 6.8 | Moisture(%H ₂ O) | 9.6 |
| Percent O ₂ (at test location) | 10.0 | Meter Temperature($^{\circ}$ F) | 76. |
| | | Flow Setting, Δ H(in. H ₂ O) | 1.6 |
| | | Nozzle Diameter(in.) | 0.252 |
| | | Static Pressure(in. H ₂ O) | -0.71 |
| | | Meter δ | 0.994 |
| Sample Flow Rate (at stack conditions): | 1.08 cfm | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|--------------|-----------------------|-----------------------------------|---------------|
| 1 | 13.3 | 25.2 | 74.8 | 8.5 |
| 2 | 1.0 | 1.9 | 72.9 | 7.9 |
| 3 | 0.7 | 1.3 | 71.6 | 4.9 |
| 4 | 0.9 | 1.7 | 69.9 | 3.3 |
| 5 | 2.4 | 4.5 | 65.4 | 1.8 |
| 6 | 2.8 | 5.3 | 60.1 | 0.80 |
| 7 | 2.1 | 4.0 | 56.1 | 0.47 |
| 8 | 1.3 | 2.5 | 53.6 | 0.25 |
| Backup Filter | 28.3 | 53.6 | 0.0 | --- |
| TOTAL | 52.8 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE

REFINERY A

SOURCE 2

Table A-43

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|--------------|--|-------|
| Run: | Six | Barometric Pressure(in. Hg) | 29.93 |
| Date: | 5/7/82 | Stack Temperature($^{\circ}$ F) | 319. |
| Traverse Point No. | Sampled: D-5 | Sample Time(min.) | 200. |
| Fuel Firing Ratio, %Gas:%Oil | 39:61 | Sample Volume(cf) | 136.7 |
| Percent O ₂ (existing boiler) | 6.8 | Moisture(%H ₂ O) | 9.5 |
| Percent O ₂ (at test location) | 10.0 | Meter Temperature($^{\circ}$ F) | 75. |
| Sample Flow Rate (at stack conditions): | 1.10 cfm | Flow Setting, Δ H(in. H ₂ O) | 1.7 |
| | | Nozzle Diameter(in.) | 0.252 |
| | | Static Pressure(in. H ₂ O) | -0.66 |
| | | Meter χ | 0.994 |
| | | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|--------------------------|---|------------------|
| 1 | 12.9 | 25.9 | 74.1 | 8.5 |
| 2 | 0.8 | 1.6 | 72.5 | 7.8 |
| 3 | 0.2 | 0.4 | 72.1 | 4.9 |
| 4 | 1.7 | 3.4 | 68.7 | 3.3 |
| 5 | 2.4 | 4.8 | 63.9 | 1.8 |
| 6 | 1.4 | 2.8 | 61.1 | 0.8 |
| 7 | 1.1 | 2.3 | 58.8 | 0.47 |
| 8 | 2.2 | 4.4 | 54.4 | 0.25 |
| Backup Filter | 27.1 | 54.4 | 0.0 | --- |
| TOTAL | 49.8 | --- | --- | --- |

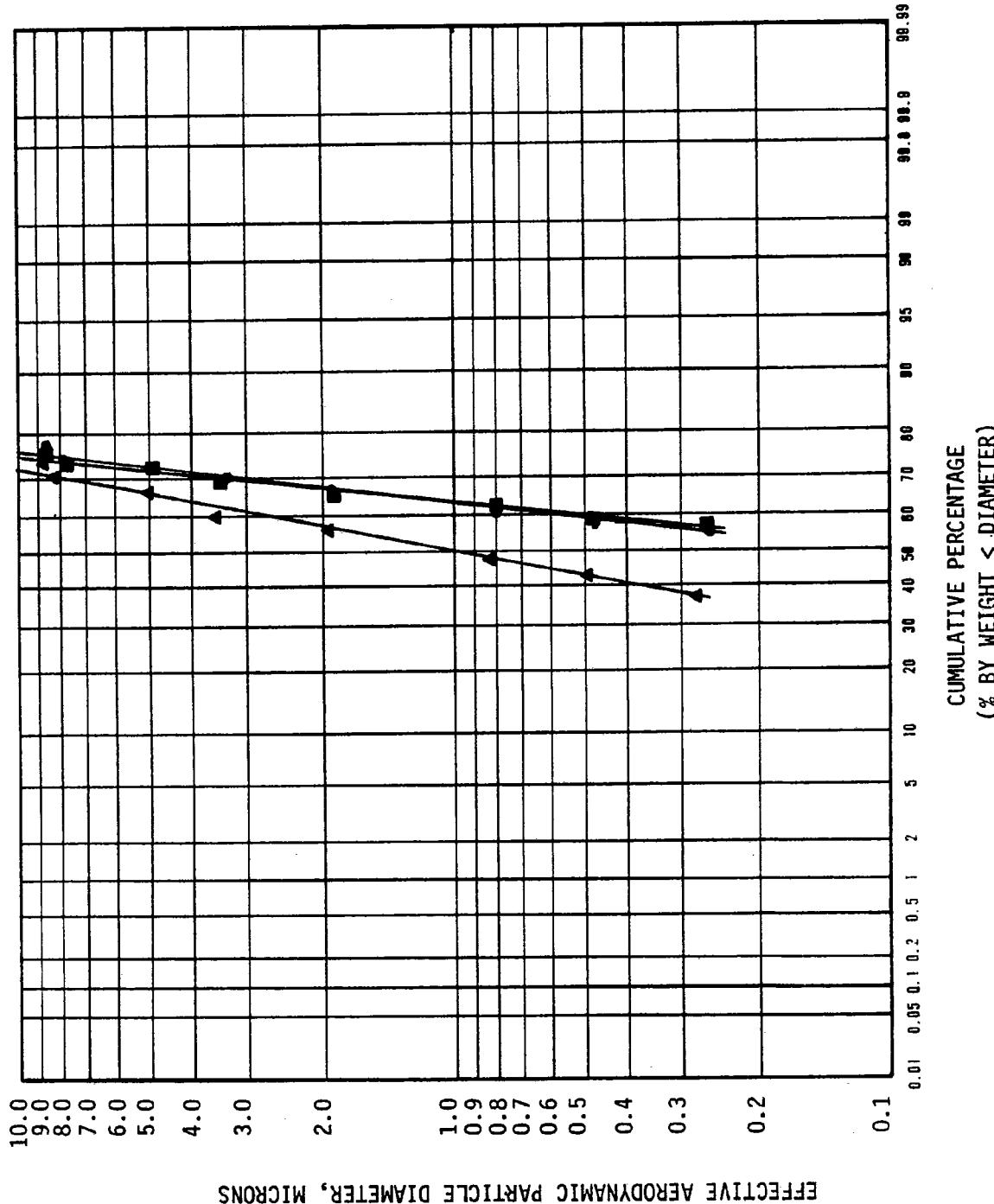
AMERICAN PETROLEUM INSTITUTE

REFINERY A SOURCE 2

PARTICLE SIZE DISTRIBUTION TEST RESULTS

Key:

- ▲ Test at 41% Gas : 59% Oil and 6.8% O₂ on 5/1/82.
- Test at 40% Gas : 60% Oil and 6.8% O₂ on 5/7/82.
- Test at 39% Gas : 61% Oil and 6.8% O₂ on 5/7/82.



A-49

AMERICAN PETROLEUM INSTITUTE

REFINERY A

SOURCE 2

Table A-44

RESULTS OF FUEL OIL COMPOSITE SAMPLE ANALYSIS
FOR TEST RUNS 1-6, 13-16; 5/4-13/82

| | |
|-------------------------|----------|
| Ash, % | 0.02 |
| Carbon, % | 87.0 |
| Hydrogen, % | 12.2 |
| Nitrogen, % | 0.30 |
| Oxygen, % | 0.26 |
| Sulfur, % | 0.22 |
| Density, lbs/gal. | 7.752 |
| Heating Value, BTU/lb. | 19,120. |
| Heating Value, BTU/gal. | 148,250. |
| Viscosity, SUS @ 100°F. | * |
| Viscosity, SUS @ 122°F. | * |
| Viscosity, SUS @ 210°F. | 158. |

Metals, ppm by weight

| | |
|----------|-------|
| Arsenic | < 0.2 |
| Barium | 1.9 |
| Cadmium | < 0.5 |
| Chromium | < 0.5 |
| Copper | 3.0 |
| Lead | < 0.5 |
| Mercury | 0.03 |
| Nickel | 21. |
| Selenium | 0.26 |
| Vanadium | < 0.5 |
| Zinc | 10. |

* The material was too viscous at this temperature to measure the Saybolt viscosity.

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REFINERY 8

SOURCE 2

Table A-45
SUMMARY OF PARTICULATE TEST DATATest Data

| Test Run Number | 1 | 2 | 3 |
|-----------------|-----------|-----------|-----------|
| Test Date | 12/11/81 | 12/12/81 | 12/12/81 |
| Test Period | 0904-1337 | 0756-1232 | 1324-1808 |

Sampling Data

| | | | |
|---|-------|-------|-------|
| Sampling Duration, minutes | 256.0 | 256.0 | 256.0 |
| Nozzle Diameter, inches | 0.180 | 0.180 | 0.180 |
| Barometric Pressure, inches mercury | 29.93 | 29.96 | 29.96 |
| Average Orifice Pressure Differential, inches water | 1.03 | 1.10 | 1.08 |
| Average Dry Gas Temperature at Meter, °F | 88. | 75. | 84. |
| Total Water Collected by Train, ml | 425.0 | 442.0 | 404.0 |
| Standard Volume of Water Vapor Collected, cubic feet | 20.0 | 20.8 | 19.0 |
| Dry Gas Meter Calibration Factor, dimensionless | 1.000 | 1.000 | 1.000 |
| Sample Volume at Meter Conditions, cubic feet | 141.0 | 145.1 | 146.0 |
| Sample Volume at Standard Conditions, cubic feet ¹ | 136.3 | 143.8 | 142.3 |

Gas Stream Composition

| | | | |
|---|-------|-------|-------|
| CO ₂ , percent by volume | 11.1 | 11.0 | 10.8 |
| O ₂ , percent by volume | 4.8 | 5.0 | 5.1 |
| CO, percent by volume | 0.0 | 0.0 | 0.0 |
| N ₂ , percent by volume | 84.1 | 84.0 | 84.1 |
| Moisture in Gas Stream, percent by volume | 12.8 | 12.6 | 11.8 |
| Mole Fraction of Dry Gas | 0.872 | 0.874 | 0.882 |
| Molecular Weight of Dry Gas | 30.0 | 30.0 | 29.9 |
| Molecular Weight of Wet Gas | 28.4 | 28.4 | 28.5 |

Gas Stream Velocity and Volumetric Flow

| | | | |
|---|---------|---------|---------|
| Static Pressure, inches water | -1.01 | -0.93 | -0.89 |
| Absolute Pressure, inches mercury | 29.9 | 29.9 | 29.9 |
| Average Temperature, °F | 481. | 489. | 493. |
| Pitot Tube Calibration Coefficient, dimensionless | 0.840 | 0.840 | 0.840 |
| Total Number of Traverse Points | 32.0 | 32.0 | 32.0 |
| Velocity at Actual Conditions, feet/second | 102.5 | 107.0 | 106.1 |
| Stack/duct Cross-Sectional Area, square feet | 41.3 | 41.3 | 41.3 |
| Volumetric Flow, Wet Actual cubic feet/minute | 254,000 | 265,000 | 263,000 |
| Volumetric Flow, Dry Standard cubic feet/minute | 124,000 | 129,000 | 128,000 |

Percent Isokinetic

100.4 101.9 101.2

Unit/Process Operations Data

| | | | |
|---|-------|-------|-------|
| Fuel Firing Ratio, % Gas: % Oil | 27:73 | 33:67 | 33:67 |
| % O ₂ at test location | 4.8 | 5.0 | 5.1 |
| Boiler Steam Production Rate, 10 ³ lb/hr | 371. | 370. | 370. |

¹Standard Conditions = 68°F (20°C) and 29.92 inches (760 mm) mercury, dry basis.

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REFINERY 8

SOURCE 2

Table A-46

SUMMARY OF PARTICULATE AND NO_x TEST RESULTSTest Data

| | | | |
|-----------------|-----------|-----------|-----------|
| Test Run Number | 1 | 2 | 3 |
| Test Date | 12/11/81 | 12/12/81 | 12/12/81 |
| Test Time | 0904-1337 | 0756-1232 | 1324-1808 |

Gas Flow Volumes

| | | | |
|---|----------|----------|----------|
| Dry Standard Cubic Feet/Minute ⁽¹⁾ | 124,000. | 129,000. | 128,000. |
| Wet Actual Cubic Feet/Minute | 254,000. | 265,000. | 263,000. |

Particulate Analysis Report

| | | | |
|--|--------|--------|--------|
| Front-Half Acetone Wash Residue Wt., grams | 0.0546 | 0.0449 | 0.0342 |
| Front-Half Methylene Chloride Wash Residue Wt., grams | ---- | ---- | 0.0001 |
| Filter Catch Wt., grams | 0.0965 | 0.0793 | 0.0691 |
| Front-Half Catch Wt. Sub-total, grams | 0.1511 | 0.1242 | 0.1034 |
| Methylene Chloride Extraction of Impinger Contents/Wash Residue wt., grams | ---- | ---- | 0.0005 |
| Impinger Contents/Wash Residue Wt., grams | 0.0144 | 0.0017 | 0.0063 |
| Back-Half Acetone Wash Residue Wt., grams | 0.0032 | 0.0003 | 0.0036 |
| Back-Half Methylene Chloride Wash Residue Wt., grams | ---- | ---- | 0.0116 |
| Back Half Catch Wt. Sub-total, grams | 0.0176 | 0.0020 | 0.0220 |
| Total Catch Weight, grams | 0.1687 | 0.1262 | 0.1254 |

Particulate ResultsFront-Half

| | | | |
|---|-------|-------|-------|
| Concentration, grains/dry standard cubic foot | 0.017 | 0.013 | 0.011 |
| Mass Emission Rate, pounds/hour | 18.2 | 14.7 | 12.3 |

Total

| | | | |
|---|-------|-------|-------|
| Concentration, grains/dry standard cubic foot | 0.019 | 0.014 | 0.014 |
| Mass Emission Rate, pounds/hour | 20.3 | 15.0 | 15.0 |

NO_x Emissions, as NO₂⁽²⁾

| | | | |
|--|------|------|------|
| Concentration, Parts/million by Volume, dry basis | 110. | 106. | 127. |
| Concentration, Pounds/Dry Standard Cubic Foot x 10 ⁻⁶ | 13.2 | 12.7 | 15.2 |
| Mass Emission Rate, Pounds/Hour | 98.0 | 98.1 | 117. |

⁽¹⁾Standard Conditions = 68°F (20°C) and 29.92 Inches Hg.⁽²⁾Results shown are averages of three (3) grab samples.

AMERICAN PETROLEUM INSTITUTE
REFINERY B
SOURCE 2
Table A-47
SUMMARY OF PARTICULATE TEST DATA

Test Data

| | 4 | 5 | 6 |
|-----------------|-----------|-----------|-----------|
| Test Run Number | 12/13/81 | 12/14/81 | 12/14/81 |
| Test Date | 0824-1259 | 0801-1141 | 1323-1658 |
| Test Period | | | |

Sampling Data

| | | | |
|---|-------|-------|-------|
| Sampling Duration, minutes | 256.0 | 200.0 | 200.0 |
| Nozzle Diameter, inches | 0.180 | 0.180 | 0.180 |
| Barometric Pressure, inches mercury | 30.03 | 30.05 | 30.05 |
| Average Orifice Pressure Differential, inches water | 1.32 | 1.34 | 1.36 |
| Average Dry Gas Temperature at Meter, °F | 84. | 80. | 78. |
| Total Water Collected by Train, ml | 399. | 318. | 318. |
| Standard Volume of Water Vapor Collected, cubic feet | 18.8 | 15.0 | 15.0 |
| Dry Gas Meter Calibration Factor, dimensionless | 1.000 | 1.000 | 1.000 |
| Sample Volume at Meter Conditions, cubic feet | 161.4 | 126.1 | 126.0 |
| Sample Volume at Standard Conditions, cubic feet ¹ | 157.8 | 124.3 | 124.5 |

Gas Stream Composition

| | | | |
|---|-------|-------|-------|
| CO ₂ , percent by volume | 9.7 | 9.8 | 9.8 |
| O ₂ , percent by volume | 6.7 | 6.7 | 6.6 |
| CO, percent by volume | 0.0 | 0.0 | 0.0 |
| N ₂ , percent by volume | 83.6 | 83.5 | 83.6 |
| Moisture in Gas Stream, percent by volume | 10.6 | 10.8 | 10.7 |
| Mole Fraction of Dry Gas | 0.894 | 0.893 | 0.893 |
| Molecular Weight of Dry Gas | 29.8 | 29.8 | 29.8 |
| Molecular Weight of Wet Gas | 28.6 | 28.6 | 28.6 |

Gas Stream Velocity and Volumetric Flow

| | | | |
|---|----------|----------|----------|
| Static Pressure, inches water | - 1.4 | - 0.99 | - 1.3 |
| Absolute Pressure, inches mercury | 29.9 | 30.0 | 30.0 |
| Average Temperature, °F | 517. | 505. | 505. |
| Pitot Tube Calibration Coefficient, dimensionless | 0.840 | 0.840 | 0.840 |
| Total Number of Traverse Points | 32.0 | 40.0 | 40.0 |
| Velocity at Actual Conditions, feet/second | 121.6 | 117.4 | 117.6 |
| Stack/duct Cross-Sectional Area, square feet | 41.3 | 41.3 | 41.3 |
| Volumetric Flow, Wet Actual cubic feet/minute | 301,000. | 291,000. | 291,000. |
| Volumetric Flow, Dry Standard cubic feet/minute | 146,000. | 142,000. | 142,000. |

Percent Isokinetic

| | | | |
|--|------|-------|-------|
| | 98.9 | 102.1 | 102.2 |
|--|------|-------|-------|

Unit/Process Operations Data

| | | | |
|---|-------|-------|-------|
| Fuel Firing Ratio, % Gas; % Oil | 31:69 | 27:73 | 27:73 |
| Percent O ₂ at test location | 6.7 | 6.7 | 6.6 |
| Boiler Steam Production Rate, 10 ³ lb/hr | 370. | 370. | 368. |

¹Standard Conditions = 60°F (20°C) and 29.92 inches (760 mm) mercury, dry basis.

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REFINERY B

SOURCE 2
Table A-48SUMMARY OF PARTICULATE AND NO_x TEST RESULTSTest Data

| | 4 12/13/81 0824-1259 | 5 12/14/81 0801-1141 | 6 12/14/81 1323-1658 |
|-----------------|----------------------------|----------------------------|----------------------------|
| Test Run Number | 4 | 5 | 6 |
| Test Date | 12/13/81 | 12/14/81 | 12/14/81 |
| Test Time | 0824-1259 | 0801-1141 | 1323-1658 |

Gas Flow Volumes

| Dry Standard Cubic Feet/Minute ⁽¹⁾ | 146,000. | 142,000. | 142,000. |
|---|----------|----------|----------|
| Wet Actual Cubic Feet/Minute | 301,000. | 291,000. | 291,000. |

Particulate Analysis Report

| | | | |
|--|--------|--------|--------|
| Front-Half Acetone Wash Residue Wt., grams | 0.0593 | 0.0553 | 0.0498 |
| Front-Half Methylene Chloride Wash Residue Wt., grams | ----- | ----- | 0.0002 |
| Filter Catch Wt., grams | 0.0735 | 0.0687 | 0.0660 |
| Front-Half Catch Wt. Sub-total, grams | 0.1328 | 0.1240 | 0.1160 |
| Methylene Chloride Extraction of Impinger Contents/Wash Residue wt., grams | ----- | ----- | 0.0006 |
| Impinger Contents/Wash Residue Wt., grams | 0.0003 | 0.0014 | 0.0024 |
| Back-Half Acetone Wash Residue Wt., grams | 0.0007 | 0.0018 | 0.0017 |
| Back-Half Methylene Chloride Wash Residue Wt., grams | ----- | ----- | 0.0043 |
| Back Half Catch Wt. Sub-total, grams | 0.0010 | 0.0032 | 0.0090 |
| Total Catch Weight, grams | 0.1338 | 0.1272 | 0.1250 |

Particulate ResultsFront-Half

| | | | |
|---|-------|-------|-------|
| Concentration, grains/dry standard cubic foot | 0.013 | 0.015 | 0.014 |
| Mass Emission Rate, pounds/hour | 16.2 | 18.8 | 17.5 |

Total

| | | | |
|---|-------|-------|-------|
| Concentration, grains/dry standard cubic foot | 0.013 | 0.016 | 0.015 |
| Mass Emission Rate, pounds/hour | 16.3 | 19.3 | 18.9 |

NO_x Emissions, as NO₂⁽²⁾

| | | | |
|--|------|------|------|
| Concentration, Parts/million by Volume, dry basis | 125. | 79.8 | 115. |
| Concentration, Pounds/Dry Standard Cubic Foot x 10 ⁻⁶ | 14.9 | 9.53 | 13.8 |
| Mass Emission Rate, Pounds/Hour | 131. | 81.2 | 118. |

(1) Standard Conditions = 68°F (20°C) and 29.92 inches Hg.

(2) Results shown are averages of three (3) grab samples.

AMERICAN PETROLEUM INSTITUTE

REFINERY 8

SOURCE 2

Table A-49

Test DataSUMMARY OF PARTICULATE TEST DATA

| Test Run Number | 7 | 8 | 9 |
|-----------------|-----------|-----------|-----------|
| Test Date | 12/15/81 | 12/16/81 | 12/16/81 |
| Test Period | 1051-1426 | 0811-1148 | 1340-1713 |

Sampling Data

| | 7 | 8 | 9 |
|---|-------|-------|-------|
| Sampling Duration, minutes | 200.0 | 200.0 | 200.0 |
| Nozzle Diameter, inches | 0.180 | 0.180 | 0.180 |
| Barometric Pressure, inches mercury | 30.14 | 30.08 | 30.08 |
| Average Orifice Pressure Differential, inches water | 1.28 | 1.36 | 1.36 |
| Average Dry Gas Temperature at Meter, °F | 96. | 96. | 86. |
| Total Water Collected by Train, ml | 260. | 287. | 290. |
| Standard Volume of Water Vapor Collected, cubic feet | 12.2 | 13.5 | 13.6 |
| Dry Gas Meter Calibration Factor, dimensionless | 1.000 | 1.000 | 1.000 |
| Sample Volume at Meter Conditions, cubic feet | 123.0 | 127.3 | 127.0 |
| Sample Volume at Standard Conditions, cubic feet ¹ | 118.1 | 122.1 | 124.0 |

Gas Stream Composition

| | 7 | 8 | 9 |
|---|-------|-------|-------|
| CO ₂ , percent by volume | 10.5 | 10.2 | 10.5 |
| O ₂ , percent by volume | 6.5 | 6.7 | 6.6 |
| CO, percent by volume | 0.0 | 0.0 | 0.0 |
| N ₂ , percent by volume | 83.0 | 83.1 | 82.9 |
| Moisture in Gas Stream, percent by volume | 9.4 | 10.0 | 9.9 |
| Mole Fraction of Dry Gas | 0.906 | 0.900 | 0.901 |
| Molecular Weight of Dry Gas | 29.9 | 29.9 | 30.0 |
| Molecular Weight of Wet Gas | 28.8 | 28.7 | 28.8 |

Gas Stream Velocity and Volumetric Flow

| | 7 | 8 | 9 |
|---|----------|----------|----------|
| Static Pressure, inches water | - 1.35 | - 1.33 | - 1.15 |
| Absolute Pressure, inches mercury | 30.0 | 30.0 | 30.0 |
| Average Temperature, °F | 498. | 501. | 499. |
| Pitot Tube Calibration Coefficient, dimensionless | 0.840 | 0.840 | 0.840 |
| Total Number of Traverse Points | 40.0 | 40.0 | 40.0 |
| Velocity at Actual Conditions, feet/second | 112.2 | 115.6 | 115.2 |
| Stack/duct Cross-Sectional Area, square feet | 41.3 | 41.3 | 41.3 |
| Volumetric Flow, Wet Actual cubic feet/minute | 278,000. | 286,000. | 285,000. |
| Volumetric Flow, Dry Standard cubic feet/minute | 139,000. | 142,000. | 142,000. |

Percent Isokinetic

99.0 100.5 102.1

Unit/Process Operations Data

| | 7 | 8 | 9 |
|---|-------|-------|-------|
| Fuel Firing Ratio, % Gas: % Oil | 0:100 | 0:100 | 0:100 |
| Percent O ₂ at test location | 6.5 | 6.7 | 6.6 |
| Boiler Steam Production Rate, 10 ³ lb/hr | 370. | 364. | 362. |

¹Standard Conditions = 68°F (20°C) and 29.92 inches (760 mm) mercury, dry basis.

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REFINERY B

SOURCE 2

Table A-50

SUMMARY OF PARTICULATE AND NO_x TEST RESULTSTest Data

| Test Run Number | 7 | 8 | 9 |
|-----------------|-----------|-----------|-----------|
| Test Date | 12/15/81 | 12/16/81 | 12/16/81 |
| Test Time | 1051-1426 | 0811-1148 | 1340-1713 |

Gas Flow Volumes

| Dry Standard Cubic Feet/Minute ⁽¹⁾ | 139,000. | 142,000. | 142,000. |
|---|----------|----------|----------|
| Wet Actual Cubic Feet/Minute | 278,000. | 286,000. | 285,000. |

Particulate Analysis Report

| | | | |
|--|--------|--------|--------|
| Front-Half Acetone Wash Residue Wt., grams | 0.0542 | 0.0628 | 0.0541 |
| Front-Half Methylene Chloride Wash Residue Wt., grams | ----- | ----- | 0.0010 |
| Filter Catch Wt., grams | 0.0732 | 0.0716 | 0.0712 |
| Front-Half Catch Wt. Sub-total, grams | 0.1274 | 0.1344 | 0.1263 |
| Methylene Chloride Extraction of Impinger Contents/Wash Residue wt., grams | ----- | ----- | 0.0004 |
| Impinger Contents/Wash Residue Wt., grams | 0.0056 | 0.0017 | 0.0021 |
| Back-Half Acetone Wash Residue Wt., grams | 0.0025 | 0.0024 | 0.0000 |
| Back-Half Methylene Chloride Wash Residue Wt., grams | ----- | ----- | 0.0029 |
| Back Half Catch Wt. Sub-total, grams | 0.0081 | 0.0041 | 0.0054 |
| Total Catch Weight, grams | 0.1355 | 0.1385 | 0.1317 |

Particulate ResultsFront-Half

| | | | |
|---|-------|-------|-------|
| Concentration, grains/dry standard cubic foot | 0.017 | 0.017 | 0.016 |
| Mass Emission Rate, pounds/hour | 19.9 | 20.7 | 19.1 |

Total

| | | | |
|---|-------|-------|-------|
| Concentration, grains/dry standard cubic foot | 0.018 | 0.018 | 0.016 |
| Mass Emission Rate, pounds/hour | 21.2 | 21.3 | 19.9 |

NO_x Emissions, as NO₂⁽²⁾

| | | | |
|--|------|------|------|
| Concentration, Parts/million by Volume, dry basis | 130. | 132. | 127. |
| Concentration, Pounds/Dry Standard Cubic Foot x 10 ⁻⁶ | 15.5 | 15.8 | 15.2 |
| Mass Emission Rate, Pounds/Hour | 130. | 135. | 129. |

⁽¹⁾Standard Conditions = 68°F (20°C) and 29.92 inches Hg.⁽²⁾Results shown are averages of three (3) grab samples.

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REFINERY 8

SOURCE 2

Table A-51

Test DataSUMMARY OF PARTICULATE TEST DATA

Test Run Number

10

11

12

Test Date

12/17/81

12/17/81

12/18/81

Test Period

0802-1148

1332-1704

0805-1224

Sampling Data

Sampling Duration, minutes

200.0

200.0

200.0

Nozzle Diameter, inches

0.180

0.180

0.180

Barometric Pressure, inches mercury

30.19

30.19

30.29

Average Orifice Pressure Differential, inches water

1.05

1.05

1.03

Average Dry Gas Temperature at Meter, °F

78.

83.

77.

Total Water Collected by Train, ml

275.

259.

259.

Standard Volume of Water Vapor Collected, cubic feet

12.9

12.2

12.2

Dry Gas Meter Calibration Factor, dimensionless

1.000

1.000

1.000

Sample Volume at Meter Conditions, cubic feet

111.3

111.5

108.1

Sample Volume at Standard Conditions, cubic feet¹

110.5

109.8

107.9

Gas Stream CompositionCO₂, percent by volume

11.9

11.8

11.9

O₂, percent by volume

4.9

5.0

4.7

CO, percent by volume

0.0

0.0

0.0

N₂, percent by volume

83.2

83.2

83.4

Moisture in Gas Stream, percent by volume

10.5

10.0

10.2

Mole Fraction of Dry Gas

0.895

0.900

0.898

Molecular Weight of Dry Gas

30.1

30.1

30.1

Molecular Weight of Wet Gas

28.8

28.9

28.9

Gas Stream Velocity and Volumetric Flow

Static Pressure, inches water

- 1.0

- 1.01

- 1.23

Absolute Pressure, inches mercury

30.1

30.1

30.2

Average Temperature, °F

485.

488.

486.

Pitot Tube Calibration Coefficient, dimensionless

0.840

0.840

0.840

Total Number of Traverse Points

40.0

40.0

40.0

Velocity at Actual Conditions, feet/second

102.9

103.4

102.0

Stack/duct Cross-Sectional Area, square feet

41.3

41.3

41.3

Volumetric Flow, Wet Actual cubic feet/minute

255,000.

256,000.

253,000.

Volumetric Flow, Dry Standard cubic feet/minute

128,000.

129,000.

128,000.

Percent Isokinetic

100.5

99.2

98.5

Unit/Process Operations Data

Fuel Firing Ratio, % Gas:% Oil

0:100

0:100

0:100

Percent O₂ at test location

4.9

5.0

4.7

Boiler Steam Production Rate, 10³ lb/hr.

370.

370.

370.

¹Standard Conditions = 68°F (20°C) and 29.92 inches (760 mm) mercury, dry basis.

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REFINERY 8

SOURCE 2

Table A-52

SUMMARY OF PARTICULATE AND NO_x TEST RESULTSTest Data

| | | | |
|-----------------|-----------|-----------|-----------|
| Test Run Number | 10 | 11 | 12 |
| Test Date | 12/17/81 | 12/17/81 | 12/18/81 |
| Test Time | 0802-1148 | 1332-1704 | 0850-1224 |

Gas Flow Volumes

| | | | |
|------------------------------------|----------|----------|----------|
| Dry Standard Cubic Feet/Minute (1) | 128,000. | 129,000. | 128,000. |
| Wet Actual Cubic Feet/Minute | 255,000. | 256,000. | 253,000. |

Particulate Analysis Report

| | | | |
|---|--------|--------|--------|
| Front-Half Acetone Wash Residue Wt., grams | 0.0582 | 0.0582 | 0.0292 |
| Front-Half Methylene Chloride Wash Residue Wt., grams | ----- | ----- | 0.0078 |
| Filter Catch Wt., grams | 0.0746 | 0.0784 | 0.0691 |
| Front-Half Catch Wt. Sub-total, grams | 0.1328 | 0.1366 | 0.1061 |
| Methylene Chloride Extraction of Impinger Contents/Wash Residue wt., grams----- | ----- | ----- | 0.0009 |
| Impinger Contents/Wash Residue Wt., grams | 0.0020 | 0.0011 | 0.0053 |
| Back-Half Acetone Wash Residue Wt., grams | 0.0013 | 0.0032 | 0.0000 |
| Back-Half Methylene Chloride Wash Residue Wt., grams | ----- | ----- | 0.0171 |
| Back Half Catch Wt. Sub-total, grams | 0.0033 | 0.0043 | 0.0233 |
| Total Catch Weight, grams | 0.1361 | 0.1409 | 0.1294 |

Particulate ResultsFront-Half

| | | | |
|---|-------|-------|-------|
| Concentration, grains/dry standard cubic foot | 0.019 | 0.019 | 0.015 |
| Mass Emission Rate, pounds/hour | 20.4 | 21.3 | 16.6 |

Total

| | | | |
|---|-------|-------|-------|
| Concentration, grains/dry standard cubic foot | 0.019 | 0.020 | 0.019 |
| Mass Emission Rate, pounds/hour | 20.9 | 21.9 | 20.3 |

NO_x Emissions, as NO₂ (2)

| | | | |
|--|------|------|------|
| Concentration, Parts/million by Volume, dry basis | 131. | 133. | 140. |
| Concentration, Pounds/Dry Standard Cubic Foot x 10 ⁻⁶ | 15.6 | 15.9 | 16.8 |
| Mass Emission Rate, Pounds/Hour | 121. | 123. | 129. |

(1) Standard Conditions = 68°F (20°C) and 29.92 inches Hg.

(2) Results shown are averages of three (3) grab samples.

AMERICAN PETROLEUM INSTITUTE

REFINERY B

SOURCE 2

Table A-53

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|----------|---|-------|
| Run: | One | Barometric Pressure(in. Hg) | 29.93 |
| Date: | 12/11/81 | Stack Temperature($^{\circ}$ F) | 481. |
| Traverse Point No. Sampled: | B-3 | Sample Time(min.) | 256 |
| Fuel Firing Ratio, %Gas:%Oil | 27:73 | Sample Volume(cf) | 141.3 |
| Percent O ₂ (at test location) | 4.8 | Moisture(%H ₂ O) | 12.8 |
| | | Meter Temperature($^{\circ}$ F) | 97. |
| | | Flow Setting, ΔH (in. H ₂ O) | 1.10 |
| | | Nozzle Diameter(in.) | 0.185 |
| | | Static Pressure(in. H ₂ O) | -1.01 |
| | | Meter γ | 0.990 |
| Sample Flow Rate (at stack conditions): | 1.07 cfm | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|--------------------------|---|------------------|
| 1 | 8.8 | 8.2 | 91.8 | 9.2 |
| 2 | 1.1 | 1.0 | 90.8 | 8.5 |
| 3 | 3.6 | 3.3 | 87.5 | 5.3 |
| 4 | 1.9 | 1.8 | 85.7 | 3.6 |
| 5 | 2.2 | 2.0 | 83.7 | 1.9 |
| 6 | 4.1 | 3.8 | 79.9 | 0.85 |
| 7 | 3.5 | 3.2 | 76.7 | 0.50 |
| 8 | 4.6 | 4.3 | 72.4 | 0.25 |
| Backup Filter | 78.2 | 72.4 | 0.0 | --- |
| TOTAL | 108.0 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE

REFINERY B

SOURCE 2

Table A-54

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|----------|---|-------|
| Run: | Two | Barometric Pressure(in. Hg) | 29.96 |
| Date: | 12/12/81 | Stack Temperature(⁰ F) | 488. |
| Traverse Point No. Sampled: | B-3; D-3 | Sample Time(min.) | 210. |
| Fuel Firing Ratio, %Gas:%Oil | 33:67 | Sample Volume(cf) | 114.9 |
| Percent O ₂ (at test location) | 5.0 | Moisture(%H ₂ O) | 12.6 |
| | | Meter Temperature(⁰ F) | 85. |
| | | Flow Setting, ΔH (in. H ₂ O) | 1.10 |
| | | Nozzle Diameter(in.) | 0.180 |
| | | Static Pressure(in. H ₂ O) | -0.93 |
| | | Meter χ | 0.990 |
| Sample Flow Rate (at stack conditions): | 1.08 cfm | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|--------------------------|---|------------------|
| 1 | 17.9 | 32.3 | 67.7 | 9.1 |
| 2 | 0.4 | 0.7 | 67.0 | 8.4 |
| 3 | 0.6 | 1.1 | 65.9 | 5.2 |
| 4 | 0.5 | 0.9 | 65.0 | 3.5 |
| 5 | 0.6 | 1.1 | 63.9 | 1.9 |
| 6 | 0.4 | 0.7 | 63.2 | 0.84 |
| 7 | 1.8 | 3.3 | 59.9 | 0.49 |
| 8 | 2.0 | 3.6 | 56.3 | 0.25 |
| Backup Filter | 31.2 | 56.3 | 0.0 | --- |
| TOTAL | 55.4 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE

REFINERY B

SOURCE 2

Table A-55

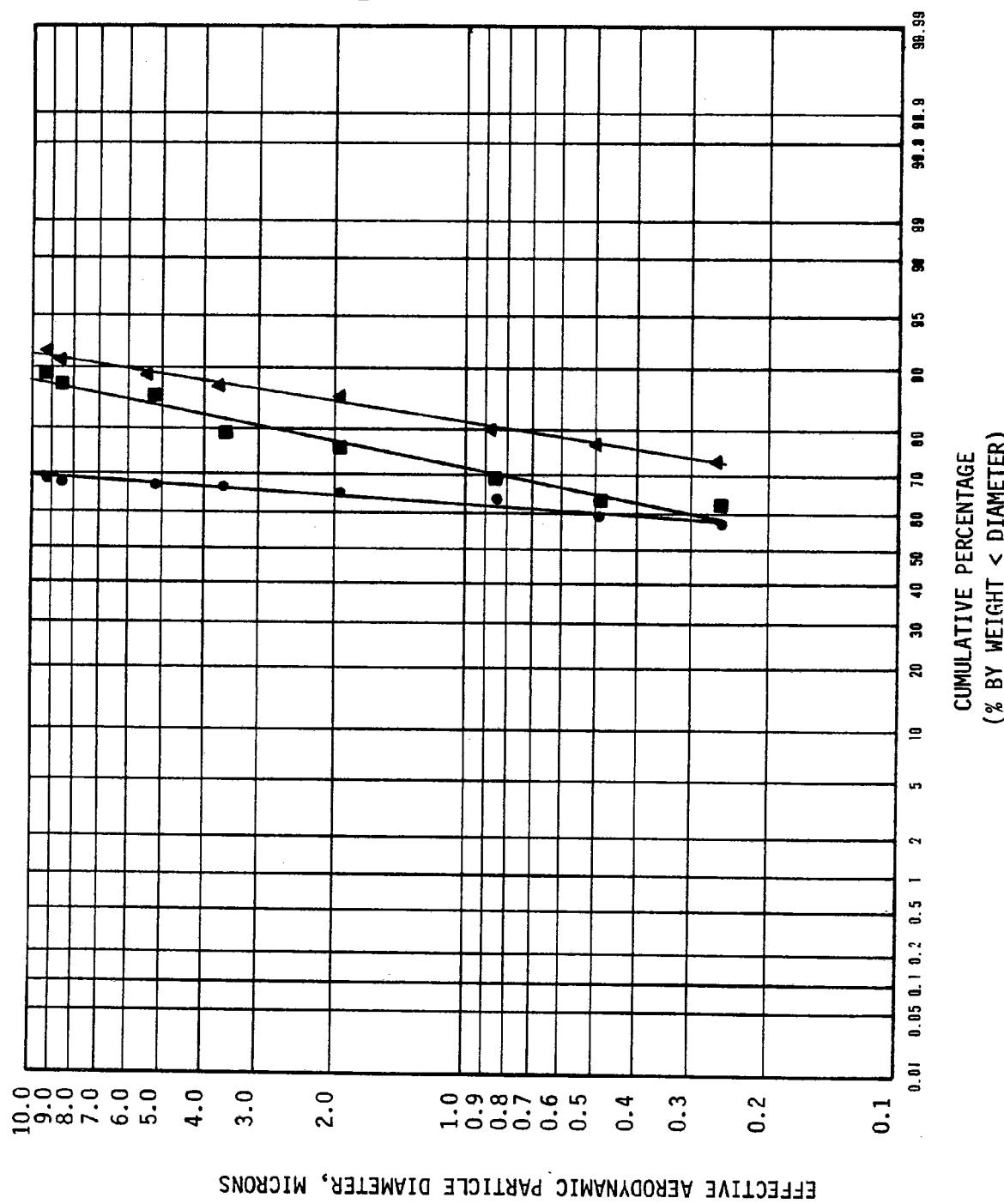
PARTICLE SIZE DISTRIBUTION

| | | | |
|--|----------|--|-------|
| Run: | Three | Barometric Pressure(in. Hg) | 29.96 |
| Date: | 12/12/81 | Stack Temperature($^{\circ}$ F) | 493. |
| Traverse Point No. Sampled: | B-3;D-3 | Sample Time(min.) | 210. |
| Fuel Firing Ratio, %Gas:%Oil | 33:67 | Sample Volume(cf) | 113.6 |
| Percent O ₂ (at test location) | 5.1 | Moisture(%H ₂ O) | 11.8 |
| Sample Flow Rate (at stack conditions): | 1.10 cfm | Meter Temperature($^{\circ}$ F) | 70. |
| | | Flow Setting, Δ H(in. H ₂ O) | 1.10 |
| | | Nozzle Diameter(in.) | 0.180 |
| | | Static Pressure(in. H ₂ O) | -0.89 |
| | | Meter χ | 0.990 |
| | | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|--------------------------|---|------------------|
| 1 | 5.6 | 11.9 | 88.1 | 9.1 |
| 2 | 1.0 | 2.1 | 86.0 | 8.4 |
| 3 | 1.0 | 2.1 | 83.9 | 5.2 |
| 4 | 2.3 | 4.9 | 79.0 | 3.5 |
| 5 | 2.1 | 4.5 | 74.5 | 1.9 |
| 6 | 2.4 | 5.1 | 69.4 | 0.84 |
| 7 | 2.9 | 6.1 | 63.3 | 0.49 |
| 8 | 0.7 | 1.5 | 61.8 | 0.25 |
| Backup Filter | 29.1 | 61.8 | 0.0 | --- |
| TOTAL | 47.1 | --- | --- | --- |

A-61

PARTICLE SIZE DISTRIBUTION TEST RESULTS



A-62

FIGURE A-7

AMERICAN PETROLEUM INSTITUTE

REFINERY B

SOURCE 2

Table A-56

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|----------|---|-------|
| Run: | Four | Barometric Pressure(in. Hg) | 30.03 |
| Date: | 12/13/81 | Stack Temperature($^{\circ}$ F) | 517. |
| Traverse Point No. Sampled: | B-3; D-3 | Sample Time(min.) | 210. |
| Fuel Firing Ratio, %Gas:%Oil | 31:69 | Sample Volume(cf) | 120.5 |
| Percent O ₂ (at test location) | 6.7 | Moisture(%H ₂ O) | 10.6 |
| | | Meter Temperature($^{\circ}$ F) | 76. |
| | | Flow Setting, ΔH (in. H ₂ O) | 1.25 |
| | | Nozzle Diameter(in.) | 0.180 |
| | | Static Pressure(in. H ₂ O) | -1.38 |
| | | Meter γ | 0.99 |
| Sample Flow Rate (at stack conditions): | 1.17 cfm | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|--------------------------|---|------------------|
| 1 | 23.2 | 26.4 | 73.6 | 8.9 |
| 2 | 2.7 | 3.1 | 70.5 | 8.2 |
| 3 | 5.1 | 5.8 | 64.7 | 5.1 |
| 4 | 4.8 | 5.5 | 59.2 | 3.4 |
| 5 | 5.5 | 6.3 | 52.9 | 1.8 |
| 6 | 5.7 | 6.5 | 46.4 | 0.81 |
| 7 | 6.1 | 6.9 | 39.5 | 0.47 |
| 8 | 5.9 | 6.7 | 32.8 | 0.24 |
| Backup Filter | 28.8 | 32.8 | 0.0 | --- |
| TOTAL | 87.8 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE

REFINERY B

SOURCE 2

Table A-57

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|----------|---|-------|
| Run: | Five | Barometric Pressure(in. Hg) | 30.05 |
| Date: | 12/14/81 | Stack Temperature($^{\circ}$ F) | 505. |
| Traverse Point No. Sampled: | B-3; D-3 | Sample Time(min.) | 210. |
| Fuel Firing Ratio, %Gas:%Oil | 27:73 | Sample Volume(cf) | 121.4 |
| Percent O ₂ (at test location) | 6.7 | Moisture(%H ₂ O) | 10.7 |
| | | Meter Temperature($^{\circ}$ F) | 60. |
| | | Flow Setting, ΔH (in. H ₂ O) | 1.30 |
| | | Nozzle Diameter(in.) | 0.180 |
| | | Static Pressure(in. H ₂ O) | -0.99 |
| | | Meter γ | 0.99 |
| Sample Flow Rate (at stack conditions): | 1.20 cfm | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|-----------------------|-----------------------------------|---------------|
| 1 | 30.9 | 36.1 | 63.9 | 8.7 |
| 2 | 2.0 | 2.3 | 61.6 | 8.1 |
| 3 | 3.5 | 4.1 | 57.5 | 5.0 |
| 4 | 4.1 | 4.8 | 52.7 | 3.4 |
| 5 | 4.4 | 5.2 | 47.5 | 1.8 |
| 6 | 4.8 | 5.6 | 41.9 | 0.79 |
| 7 | 4.5 | 5.3 | 36.6 | 0.46 |
| 8 | 3.0 | 3.5 | 33.1 | 0.23 |
| Backup Filter | 28.3 | 33.1 | 0.0 | --- |
| TOTAL | 85.5 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE

REFINERY B

SOURCE 2

Table A-58

PARTICLE SIZE DISTRIBUTION

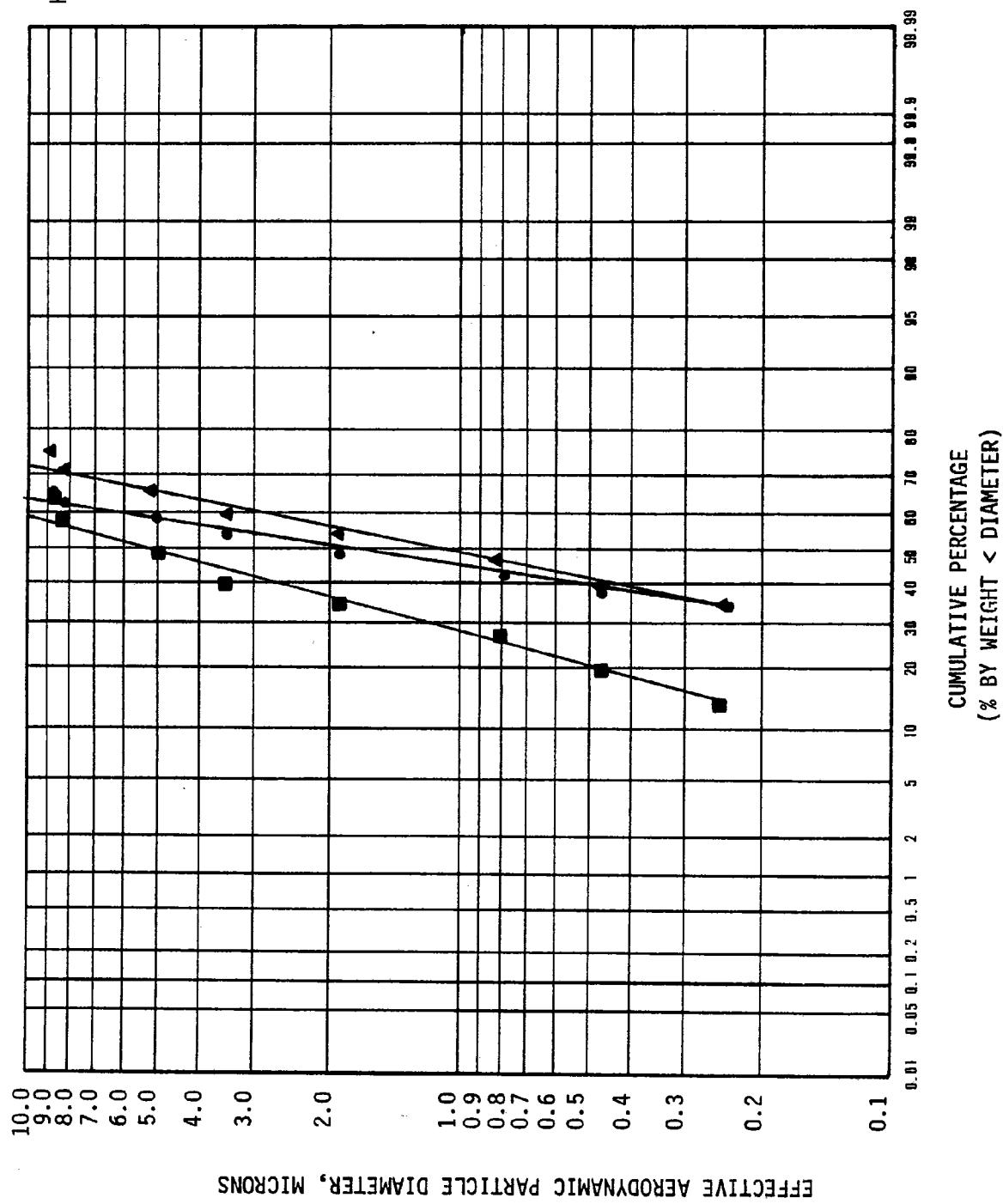
| | | | |
|--|----------|---|-------|
| Run: | Six | Barometric Pressure(in. Hg) | 30.05 |
| Date: | 12/14/81 | Stack Temperature($^{\circ}$ F) | 505. |
| Traverse Point No. Sampled: | B-3: D-3 | Sample Time(min.) | 150. |
| Fuel Firing Ratio, %Gas:%Oil | 27:73 | Sample Volume(cf) | 86.1 |
| Percent O ₂ (at test location) | 6.6 | Moisture(%H ₂ O) | 10.7 |
| | | Meter Temperature($^{\circ}$ F) | 59. |
| | | Flow Setting, ΔH (in. H ₂ O) | 1.3 |
| | | Nozzle Diameter(in.) | 0.180 |
| | | Static Pressure(in. H ₂ O) | -1.30 |
| | | Meter γ | 0.99 |
| Sample Flow Rate (at stack conditions): | 1.19 cfm | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|--------------------------|---|------------------|
| 1 | 22.1 | 37.7 | 62.3 | 8.7 |
| 2 | 3.3 | 5.6 | 56.7 | 8.1 |
| 3 | 5.0 | 8.5 | 48.2 | 5.0 |
| 4 | 4.8 | 8.2 | 40.0 | 3.4 |
| 5 | 4.0 | 6.8 | 33.2 | 1.8 |
| 6 | 4.4 | 7.5 | 25.7 | 0.80 |
| 7 | 3.8 | 6.5 | 19.2 | 0.46 |
| 8 | 3.5 | 6.0 | 13.2 | 0.24 |
| Backup Filter | 7.7 | 13.2 | 0.0 | --- |
| TOTAL | 58.6 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE

REFINERY B SOURCE 2

PARTICLE SIZE DISTRIBUTION TEST RESULTS



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FIGURE A-8

AMERICAN PETROLEUM INSTITUTE

REFINERY B

SOURCE 2

Table A-59

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|----------|---|-------|
| Run: | Ten | Barometric Pressure(in. Hg) | 30.19 |
| Date: | 12/17/81 | Stack Temperature($^{\circ}$ F) | 485. |
| Traverse Point No. Sampled: | B-3 | Sample Time(min.) | 120. |
| Fuel Firing Ratio, %Gas:%Oil | 0:100 | Sample Volume(cf) | 66.0 |
| Percent O ₂ (at test location) | 4.9 | Moisture(%H ₂ O) | 10.5 |
| | | Meter Temperature($^{\circ}$ F) | 62. |
| | | Flow Setting, ΔH (in. H ₂ O) | 1.20 |
| | | Nozzle Diameter(in.) | 0.180 |
| | | Static Pressure(in. H ₂ O) | -1.0 |
| | | Meter γ | 0.99 |
| Sample Flow Rate (at stack conditions): | 1.11 cfm | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|-----------------------|-----------------------------------|---------------|
| 1 | 24.2 | 18.7 | 81.3 | 9.0 |
| 2 | 11.0 | 8.5 | 72.8 | 8.3 |
| 3 | 12.7 | 9.8 | 63.0 | 5.2 |
| 4 | 11.5 | 8.9 | 54.1 | 3.5 |
| 5 | 11.5 | 8.9 | 45.2 | 1.8 |
| 6 | 10.7 | 8.2 | 37.0 | 0.83 |
| 7 | 10.9 | 8.4 | 28.6 | 0.49 |
| 8 | 9.6 | 7.4 | 21.2 | 0.25 |
| Backup Filter | 27.5 | 21.2 | 0.0 | --- |
| TOTAL | 129.6 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE

REFINERY B

SOURCE 2

Table A-60

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|--------------|--|-------|
| Run: | Eleven | Barometric Pressure(in. Hg) | 30.20 |
| Date: | 12/17/81 | Stack Temperature($^{\circ}$ F) | 488. |
| Traverse Point No. | Sampled: D-3 | Sample Time(min.) | 120. |
| Fuel Firing Ratio, %Gas:%Oil | 0:100 | Sample Volume(cf) | 65.4 |
| Percent O ₂ (at test location) | 5.0 | Moisture(%H ₂ O) | 10.0 |
| | | Meter Temperature($^{\circ}$ F) | 72. |
| | | Flow Setting, Δ H(in. H ₂ O) | 1.10 |
| | | Nozzle Diameter(in.) | 0.180 |
| | | Static Pressure(in. H ₂ O) | -1.01 |
| | | Meter χ | 0.99 |
| Sample Flow Rate (at stack conditions): | 1.07 cfm | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|-----------------------|-----------------------------------|---------------|
| 1 | 8.0 | 14.3 | 85.7 | 9.2 |
| 2 | 0.9 | 1.6 | 84.1 | 8.5 |
| 3 | 3.3 | 5.9 | 78.2 | 5.3 |
| 4 | 3.0 | 5.4 | 72.8 | 3.5 |
| 5 | 2.3 | 4.1 | 68.7 | 1.9 |
| 6 | 2.9 | 5.2 | 63.5 | 0.85 |
| 7 | 1.7 | 3.0 | 60.5 | 0.49 |
| 8 | 2.2 | 3.9 | 56.6 | 0.25 |
| Backup Filter | 31.7 | 56.6 | --- | --- |
| TOTAL | 56.0 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE

REFINERY B

SOURCE 2

Table A-61

PARTICLE SIZE DISTRIBUTION

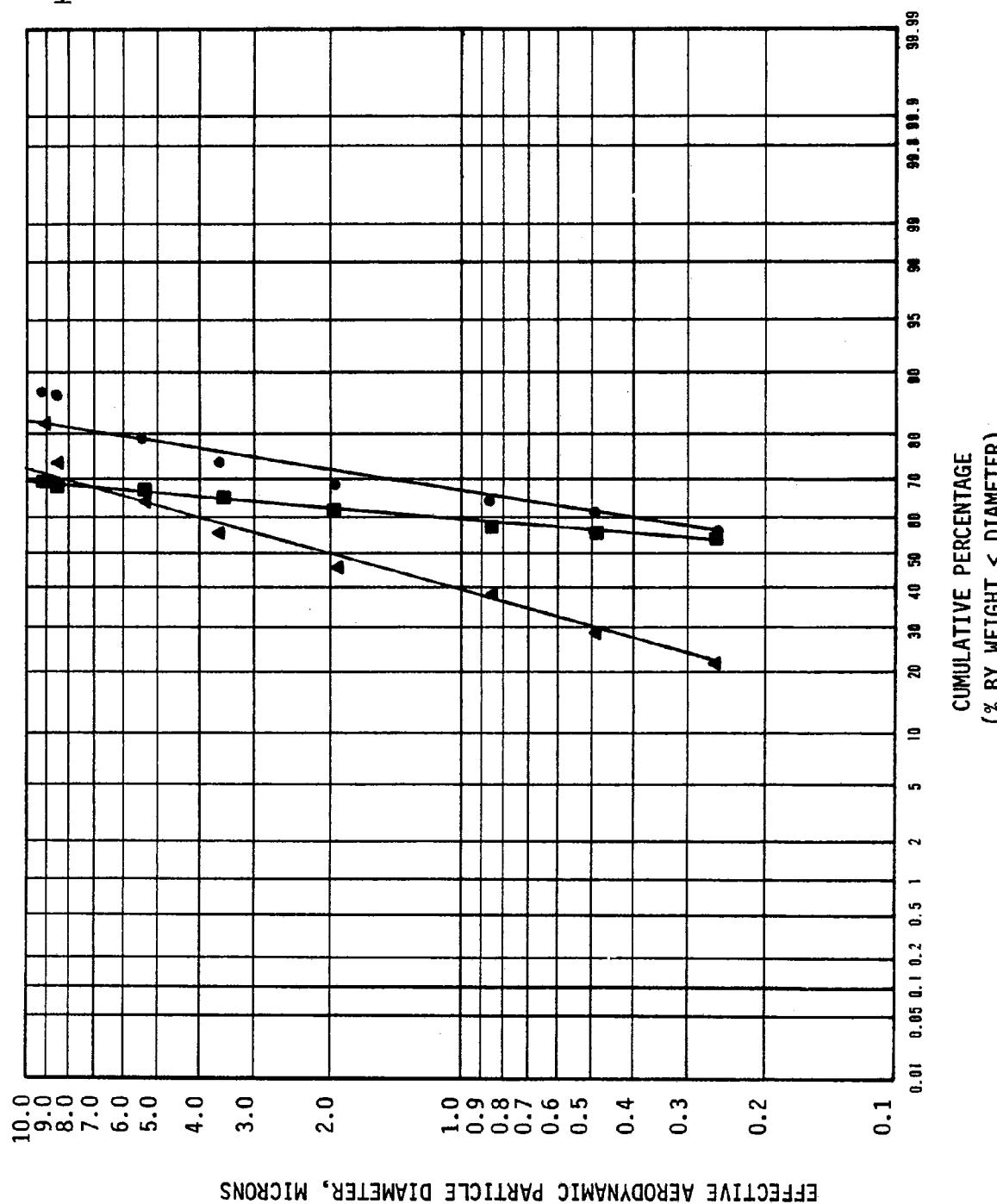
| | | | |
|--|----------|---|-------|
| Run: | Twelve | Barometric Pressure(in. Hg) | 30.29 |
| Date: | 12/18/81 | Stack Temperature($^{\circ}$ F) | 486. |
| Traverse Point No. Sampled: | B-3: D-3 | Sample Time(min.) | 120. |
| Fuel Firing Ratio, %Gas:%Oil | 0:100 | Sample Volume(cf) | 64.6 |
| Percent O ₂ (at test location) | 4.7 | Moisture(%H ₂ O) | 10.2 |
| | | Meter Temperature($^{\circ}$ F) | 64.6 |
| | | Flow Setting, ΔH (in. H ₂ O) | 1.10 |
| | | Nozzle Diameter(in.) | 0.180 |
| | | Static Pressure(in. H ₂ O) | -1.23 |
| | | Meter γ | 0.99 |
| Sample Flow Rate (at stack conditions): | 1.08 cfm | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|--------------------------|---|------------------|
| 1 | 13.4 | 30.6 | 69.4 | 9.1 |
| 2 | 0.9 | 2.1 | 67.3 | 8.5 |
| 3 | 0.7 | 1.6 | 65.7 | 5.3 |
| 4 | 0.8 | 1.8 | 63.9 | 3.5 |
| 5 | 1.3 | 3.0 | 60.9 | 1.9 |
| 6 | 1.7 | 3.9 | 57.0 | 0.85 |
| 7 | 1.2 | 2.7 | 54.3 | 0.49 |
| 8 | 0.8 | 1.8 | 52.5 | 0.25 |
| Backup Filter | 23.0 | 52.5 | 0.0 | --- |
| TOTAL | 43.8 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE

REFINERY B SOURCE 2

PARTICLE SIZE DISTRIBUTION TEST RESULTS



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AMERICAN PETROLEUM INSTITUTE

REFINERY B

SOURCE 2

Table A-62

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|----------|--|-------|
| Run: | Seven | Barometric Pressure(in. Hg) | 30.14 |
| Date: | 12/15/81 | Stack Temperature($^{\circ}$ F) | 498. |
| Traverse Point No. Sampled: | D-3 | Sample Time(min.) | 120. |
| Fuel Firing Ratio, %Gas:%Oil | 0:100 | Sample Volume(cf) | 68.9 |
| Percent O ₂ (at test location) | 6.5 | Moisture(%H ₂ O) | 9.4 |
| | | Meter Temperature($^{\circ}$ F) | 73. |
| | | Flow Setting, Δ H(in. H ₂ O) | 1.30 |
| Sample Flow Rate (at stack conditions): | 1.20 cfm | Nozzle Diameter(in.) | 0.180 |
| | | Static Pressure(in. H ₂ O) | -1.35 |
| | | Meter γ | 0.99 |
| | | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|-----------------------|-----------------------------------|---------------|
| 1 | 15.3 | 22.3 | 77.7 | 8.7 |
| 2 | 1.5 | 2.2 | 75.5 | 8.0 |
| 3 | 3.8 | 5.5 | 70.0 | 5.0 |
| 4 | 2.7 | 3.9 | 66.1 | 3.4 |
| 5 | 3.0 | 4.4 | 61.7 | 1.8 |
| 6 | 5.2 | 7.6 | 54.1 | 0.80 |
| 7 | 6.3 | 9.2 | 44.9 | 0.46 |
| 8 | 4.6 | 6.7 | 38.2 | 0.23 |
| Backup Filter | 26.2 | 38.2 | 0.0 | --- |
| TOTAL | 68.6 | --- | --- | --- |

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AMERICAN PETROLEUM INSTITUTE

REFINERY B

SOURCE 2

Table A-63

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|--------------|--|-------|
| Run: | Eight | Barometric Pressure(in. Hg) | 30.08 |
| Date: | 12/16/81 | Stack Temperature($^{\circ}$ F) | 501. |
| Traverse Point No. | Sampled: B-3 | Sample Time(min.) | 120. |
| Fuel Firing Ratio, %Gas:%Oil | 0:100 | Sample Volume(cf) | 71.1 |
| Percent O ₂ (at test location) | 6.7 | Moisture(%H ₂ O) | 10.0 |
| | | Meter Temperature($^{\circ}$ F) | 92. |
| | | Flow Setting, Δ H(in. H ₂ O) | 1.35 |
| | | Nozzle Diameter(in.) | 0.180 |
| | | Static Pressure(in. H ₂ O) | -1.33 |
| | | Meter γ | 0.99 |
| Sample Flow Rate (at stack conditions): | 1.14 cfm | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|--------------------------|---|------------------|
| 1 | 27.4 | 31.4 | 68.6 | 8.9 |
| 2 | 2.0 | 2.3 | 66.3 | 8.2 |
| 3 | 4.1 | 4.7 | 61.6 | 5.1 |
| 4 | 3.2 | 3.7 | 57.9 | 3.4 |
| 5 | 3.5 | 4.0 | 53.9 | 1.8 |
| 6 | 3.6 | 4.1 | 49.8 | 0.82 |
| 7 | 7.9 | 9.0 | 40.8 | 0.48 |
| 8 | 4.2 | 4.8 | 36.0 | 0.24 |
| Backup Filter | 31.4 | 36.0 | 0.0 | --- |
| TOTAL | 87.3 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE

REFINERY 8

SOURCE 2

Table A-64

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|--------------|---|-------|
| Run: | Nine | Barometric Pressure(in. Hg) | 30.08 |
| Date: | 12/16/81 | Stack Temperature($^{\circ}$ F) | 499. |
| Traverse Point No. | Sampled: D-3 | Sample Time(min.) | 120. |
| Fuel Firing Ratio, %Gas:%Oil | 0:100 | Sample Volume(cf) | 72.2 |
| Percent O ₂ (at test location) | 6.6 | Moisture(%H ₂ O) | 9.9 |
| | | Meter Temperature($^{\circ}$ F) | 93. |
| | | Flow Setting, ΔH (in. H ₂ O) | 1.35 |
| | | Nozzle Diameter(in.) | 0.180 |
| | | Static Pressure(in. H ₂ O) | -1.15 |
| | | Meter γ | 0.99 |
| Sample Flow Rate (at stack conditions): | 1.15 cfm | Sample Vac.(in. Hg) | 1.0 |

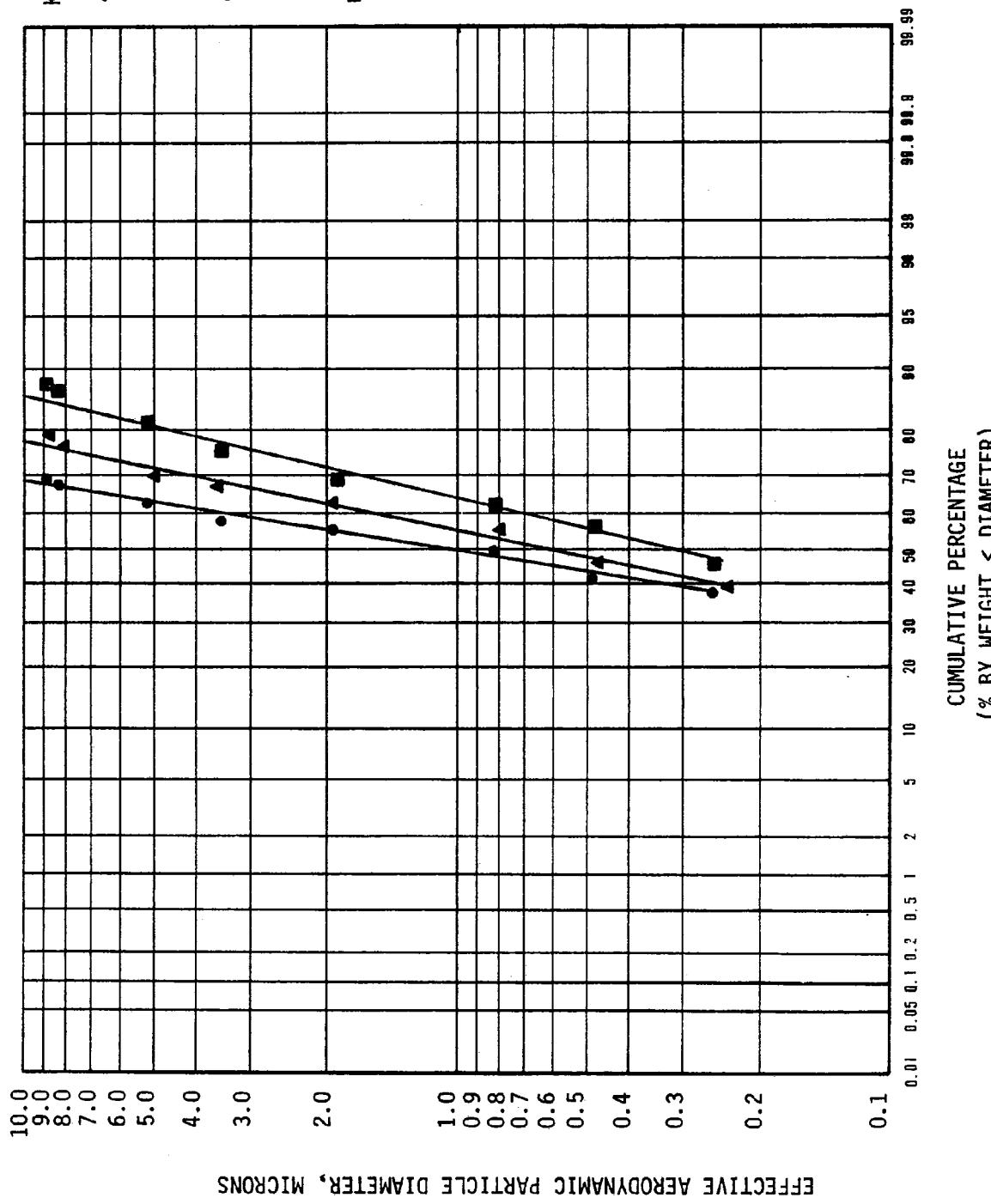
| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|-----------------------|-----------------------------------|---------------|
| 1 | 7.9 | 14.0 | 86.0 | 8.9 |
| 2 | 0.8 | 1.4 | 84.6 | 8.2 |
| 3 | 2.1 | 3.7 | 80.9 | 5.1 |
| 4 | 3.7 | 6.6 | 74.3 | 3.4 |
| 5 | 3.3 | 5.9 | 68.4 | 1.8 |
| 6 | 3.7 | 6.6 | 61.8 | 0.81 |
| 7 | 3.7 | 6.6 | 55.2 | 0.47 |
| 8 | 5.5 | 9.8 | 45.4 | 0.24 |
| Backup Filter | 25.6 | 45.4 | 0.0 | --- |
| TOTAL | 56.3 | --- | --- | --- |

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AMERICAN PETROLEUM INSTITUTE

REFINERY B SOURCE 2

PARTICLE SIZE DISTRIBUTION TEST RESULTS



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AMERICAN PETROLEUM INSTITUTE

REFINERY B

SOURCE 2

Table A-65

RESULTS OF FUEL OIL COMPOSITE SAMPLE ANALYSES
FOR TEST RUNS 1-12, 12/11-18/81

| | |
|--------------------------|----------|
| Ash, % | 0.03 |
| Carbon, % | 86.8 |
| Hydrogen, % | 11.3 |
| Nitrogen, % | 0.22 |
| Oxygen, % | 0.87 |
| Sulfur, % | 0.73 |
| Density, lbs/gal | 7.951 |
| Heating Value, BTU/lb. | 18,750. |
| Heating Value, BTU/gal. | 149,100. |
| Viscosity, SFS at 122°F. | 81.6 |

Metals, ppm by weight

| | |
|----------|-------|
| Arsenic | < 0.2 |
| Barium | 0.7 |
| Cadmium | < 0.5 |
| Chromium | 0.7 |
| Copper | 1.5 |
| Lead | 5.4 |
| Mercury | 0.05 |
| Nickel | 11.0 |
| Selenium | < 0.1 |
| Vanadium | 2.1 |
| Zinc | 6.7 |

AMERICAN PETROLEUM INSTITUTE
REFINERY C
SOURCE 1
Table A-66
SUMMARY OF PARTICULATE TEST DATA

Test Data

| Test Run Number | ¹ 2/17/82 | ² 2/18/82 | ³ 2/19/82 |
|-----------------|-------------------------|-------------------------|-------------------------|
| Test Date | 1005-1421 | 0908-1458 | 0937-1400 |
| Test Period | | | |

Sampling Data

| | | | |
|---|-------|-------|-------|
| Sampling Duration, minutes | 240.0 | 200.0 | 200.0 |
| Nozzle Diameter, inches | 0.253 | 0.253 | 0.253 |
| Barometric Pressure, inches mercury | 30.12 | 30.28 | 29.95 |
| Average Orifice Pressure Differential, inches water | 1.55 | 1.62 | 1.61 |
| Average Dry Gas Temperature at Meter, °F | 61. | 70. | 75. |
| Total Water Collected by Train, ml | 315.5 | 251.0 | 252.0 |
| Standard Volume of Water Vapor Collected, cubic feet | 14.9 | 11.8 | 11.9 |
| Dry Gas Meter Calibration Factor, dimensionless | 1.005 | 1.005 | 1.005 |
| Sample Volume at Meter Conditions, cubic feet | 136.3 | 120.8 | 122.2 |
| Sample Volume at Standard Conditions, cubic feet ¹ | 140.2 | 122.9 | 121.8 |

Gas Stream Composition

| | | | |
|---|-------|-------|-------|
| CO ₂ , percent by volume | 9.8 | 9.4 | 10.0 |
| O ₂ , percent by volume | 7.2 | 7.5 | 7.2 |
| CO, percent by volume | 0.0 | 0.0 | 0.0 |
| H ₂ , percent by volume | 83.0 | 83.1 | 82.8 |
| Moisture in Gas Stream, percent by volume | 9.6 | 8.8 | 8.9 |
| Mole Fraction of Dry Gas | 0.904 | 0.912 | 0.911 |
| Molecular Weight of Dry Gas | 29.9 | 29.8 | 29.9 |
| Molecular Weight of Wet Gas | 28.7 | 28.8 | 28.8 |

Gas Stream Velocity and Volumetric Flow

| | | | |
|---|---------|---------|---------|
| Static Pressure, inches water | - 0.33 | - 0.28 | - 0.32 |
| Absolute Pressure, inches mercury | 30.1 | 30.3 | 29.9 |
| Average Temperature, °F | 349. | 359. | 364. |
| Pitot Tube Calibration Coefficient, dimensionless | 0.84 | 0.84 | 0.84 |
| Total Number of Traverse Points | 40.0 | 40.0 | 40.0 |
| Velocity at Actual Conditions, feet/second | 46.6 | 49.1 | 49.8 |
| Stack/duct Cross-Sectional Area, square feet | 28.3 | 28.3 | 28.3 |
| Volumetric Flow, Wet Actual cubic feet/minute | 79,100. | 83,400. | 84,500. |
| Volumetric Flow, Dry Standard cubic feet/minute | 48,900. | 49,600. | 49,300. |

Percent Isokinetic

| | | | |
|--------------------|-------|-------|-------|
| Percent Isokinetic | 100.8 | 100.3 | 100.0 |
|--------------------|-------|-------|-------|

Unit/Process Operations Data

| | | | |
|--|-------|-------|-------|
| Fuel Firing Ratio, %Gas:Oil | 0:100 | 0:100 | 0:100 |
| Percent O ₂ Exiting Boiler | 3.5 | 4.0 | 3.5 |
| Percent O ₂ at Test Location | 7.2 | 7.5 | 7.2 |
| Boiler Steam Production Rate, 10 ³ lb/hr. | 103. | 105. | 103. |

¹Standard Conditions = 68°F (20°C) and 29.92 inches (760 mm) mercury, dry basis.

AMERICAN PETROLEUM INSTITUTE

REFINERY C

SOURCE 1

Table A-67

SUMMARY OF PARTICULATE AND NO_x TEST RESULTSTest Data

| | 1 2/17/82 1005-1421 | 2 2/18/82 0908-1458 | 3 2/19/82 0937-1400 |
|--|---------------------------|---------------------------|---------------------------|
|--|---------------------------|---------------------------|---------------------------|

Gas Flow Volumes

| | | | |
|---|---------|---------|---------|
| Dry Standard Cubic Feet/Minute ⁽¹⁾ | 46,900. | 49,600. | 49,300. |
| Wet Actual Cubic Feet/Minute | 79,100. | 83,400. | 84,500. |

Particulate Analysis Report

| | | | |
|--|--------|--------|--------|
| Front-Half Acetone Wash Residue Wt., grams | 0.0709 | 0.1039 | 0.0889 |
| Front-Half Methylene Chloride Wash Residue Wt., grams | ----- | ----- | 0.0001 |
| Filter Catch Wt., grams | 0.1163 | 0.1370 | 0.1241 |
| Front-Half Catch Wt. Sub-total, grams | 0.1872 | 0.2409 | 0.2131 |
| Methylene Chloride Extraction of Impinger Contents/Wash Residue wt., grams | ----- | ----- | 0.0000 |
| Impinger Contents/Wash Residue Wt., grams | 0.0566 | 0.0103 | 0.0799 |
| Back-Half Acetone Wash Residue Wt., grams | 0.0022 | 0.0012 | 0.0019 |
| Back-Half Methylene Chloride Wash Residue Wt., grams | ----- | ----- | 0.0036 |
| Back Half Catch Wt. Sub-total, grams | 0.0588 | 0.0115 | 0.0854 |
| Total Catch Weight, grams | 0.2460 | 0.2524 | 0.2985 |

Particulate Results

| | | | |
|---|-------|-------|-------|
| <u>Front-Half</u> | | | |
| Concentration, grains/dry standard cubic foot | 0.021 | 0.030 | 0.027 |
| Mass Emission Rate, pounds/hour | 8.29 | 12.9 | 11.4 |

Total

| | | | |
|---|-------|-------|-------|
| Concentration, grains/dry standard cubic foot | 0.027 | 0.032 | 0.038 |
| Mass Emission Rate, pounds/hour | 10.9 | 13.5 | 16.0 |

NO_x Emissions, as NO₂⁽²⁾

| | | | |
|--|------|------|------|
| Concentration, Parts/million by Volume, dry basis | 157. | 123. | 191. |
| Concentration, Pounds/Dry Standard Cubic Foot x 10 ⁻⁶ | 19. | 15. | 23. |
| Mass Emission Rate, Pounds/Hour | 53. | 44. | 67. |

(1) Standard Conditions = 68°F (20°C) and 29.92 inches Hg.

(2) Results shown are averages of three (3) grab samples.

AMERICAN PETROLEUM INSTITUTE

REFINERY C

SOURCE I

Table A-68

SUMMARY OF PARTICULATE TEST DATATest Data

| Test Run Number | 4 | 5 | 6 |
|-----------------|-----------|-----------|-----------|
| Test Date | 2/22/82 | 2/22/82 | 2/23/82 |
| Test Period | 0855-1246 | 1313-1640 | 0929-1311 |

Sampling Data

| | | | |
|---|-------|-------|-------|
| Sampling Duration, minutes | 200.0 | 200.0 | 200.0 |
| Nozzle Diameter, inches | 0.253 | 0.253 | 0.253 |
| Barometric Pressure, inches mercury | 29.80 | 29.80 | 30.07 |
| Average Orifice Pressure Differential, inches water | 1.15 | 1.13 | 1.22 |
| Average Dry Gas Temperature at Meter, °F | 59. | 61. | 73. |
| Total Water Collected by Train, ml | 198.0 | 210.0 | 211.0 |
| Standard Volume of Water Vapor Collected, cubic feet | 9.3 | 9.9 | 9.9 |
| Dry Gas Meter Calibration Factor, dimensionless | 1.005 | 1.005 | 1.005 |
| Sample Volume at Meter Conditions, cubic feet | 110.4 | 108.8 | 112.8 |
| Sample Volume at Standard Conditions, cubic feet ¹ | 112.6 | 110.8 | 113.3 |

Gas Stream Composition

| | | | |
|---|-------|-------|-------|
| CO ₂ , percent by volume | 8.1 | 8.5 | 8.3 |
| O ₂ , percent by volume | 9.7 | 9.5 | 9.6 |
| CO, percent by volume | 0.0 | 0.0 | 0.0 |
| H ₂ , percent by volume | 82.2 | 82.0 | 82.1 |
| Moisture in Gas Stream, percent by volume | 7.6 | 8.2 | 8.1 |
| Mole Fraction of Dry Gas | 0.924 | 0.918 | 0.919 |
| Molecular Weight of Dry Gas | 29.7 | 29.7 | 29.7 |
| Molecular Weight of Wet Gas | 28.9 | 28.7 | 28.8 |

Gas Stream Velocity and Volumetric Flow

| | | | |
|---|---------|---------|---------|
| Static Pressure, inches water | - 0.28 | - 0.31 | - 0.42 |
| Absolute Pressure, inches mercury | 29.8 | 29.8 | 30.0 |
| Average Temperature, °F | 372. | 373. | 377. |
| Pitot Tube Calibration Coefficient, dimensionless | 0.84 | 0.84 | 0.84 |
| Total Number of Traverse Points | 40.0 | 40.0 | 40.0 |
| Velocity at Actual Conditions, feet/second | 45.5 | 45.0 | 45.5 |
| Stack/duct Cross-Sectional Area, square feet | 28.3 | 28.3 | 28.3 |
| Volumetric Flow, Wet Actual cubic feet/minute | 77,100. | 76,300. | 77,200. |
| Volumetric Flow, Dry Standard cubic feet/minute | 45,000. | 44,200. | 45,000. |

Percent Isokinetic

| | | |
|-------|-------|-------|
| 101.4 | 101.5 | 102.0 |
|-------|-------|-------|

Unit/Process Operations Data

| | | | |
|--|-------|-------|-------|
| Fuel Firing Ratio, %Gas:%Oil | 0:100 | 0:100 | 0:100 |
| Percent O ₂ Existing Boiler | 5.4 | 5.4 | 5.5 |
| Percent O ₂ at Test Location | 9.7 | 9.5 | 9.6 |
| Boiler Steam Production Rate, 10 ³ lb/hr. | 100. | 100. | 95. |

¹Standard Conditions = 60°F (20°C) and 29.92 inches (760 mm) mercury, dry basis.

AMERICAN PETROLEUM INSTITUTE

REFINERY C

SOURCE 1

Table A-69

SUMMARY OF PARTICULATE AND NO_x TEST RESULTSTest Data

| | | | |
|-----------------|-----------|-----------|-----------|
| Test Run Number | 4 | 5 | 6 |
| Test Date | 2/22/82 | 2/22/82 | 2/23/82 |
| Test Time | 0855-1246 | 1313-1640 | 0949-1311 |

Gas Flow Volumes

| | | | |
|------------------------------------|---------|---------|---------|
| Dry Standard Cubic Feet/Minute (1) | 45,000. | 44,200. | 45,000. |
| Wet Actual Cubic Feet/Minute | 77,100. | 76,300. | 77,200. |

Particulate Analysis Report

| | | | |
|--|--------|--------|--------|
| Front-Half Acetone Wash Residue Wt., grams | 0.0704 | 0.1027 | 0.1040 |
| Front-Half Methylene Chloride Wash Residue Wt., grams | ---- | ---- | 0.0002 |
| Filter Catch Wt., grams | 0.2057 | 0.1782 | 0.1200 |
| Front-Half Catch Wt. Sub-total, grams | 0.2761 | 0.2809 | 0.2242 |
| Methylene Chloride Extraction of Impinger Contents/Wash Residue wt., grams | ---- | ---- | 0.0000 |
| Impinger Contents/Wash Residue Wt., grams | 0.0190 | 0.0591 | 0.0210 |
| Back-Half Acetone Wash Residue Wt., grams | 0.0022 | 0.0013 | 0.0006 |
| Back-Half Methylene Chloride Wash Residue Wt., grams | ---- | ---- | 0.0038 |
| Back Half Catch Wt. Sub-total, grams | 0.0212 | 0.0704 | 0.0254 |
| Total Catch Weight, grams | 0.2973 | 0.3513 | 0.2496 |

Particulate ResultsFront-Half

| | | | |
|---|-------|-------|-------|
| Concentration, grains/dry standard cubic foot | 0.038 | 0.039 | 0.031 |
| Mass Emission Rate, pounds/hour | 14.6 | 14.8 | 11.8 |

Total

| | | | |
|---|-------|-------|-------|
| Concentration, grains/dry standard cubic foot | 0.041 | 0.049 | 0.034 |
| Mass Emission Rate, pounds/hour | 15.7 | 18.5 | 13.1 |

NO_x Emissions, as NO₂ (2)

| | | | |
|--|------|------|------|
| Concentration, Parts/million by Volume, dry basis -6 | 170. | 162. | 158. |
| Concentration, Pounds/Dry Standard Cubic Foot x 10 ⁻⁶ | 20. | 19. | 19. |
| Mass Emission Rate, Pounds/Hour | 55. | 51. | 51. |

(1) Standard Conditions = 68°F (20°C) and 29.92 inches Hg.

(2) Results shown are averages of three (3) grab samples.

AMERICAN PETROLEUM INSTITUTE

REFINERY C

SOURCE 1

Table A-70

SUMMARY OF PARTICULATE TEST DATATest Data

| Test Run Number | 7 | 8 | 9 |
|-----------------|-----------|-----------|-----------|
| Test Date | 3/3/82 | 3/4/82 | 3/4/82 |
| Test Period | 0910-1556 | 0937-1315 | 1429-1718 |

Sampling Data

| | | | |
|---|-------|-------|-------|
| Sampling Duration, minutes | 400.0 | 200.0 | 160.0 |
| Nozzle Diameter, inches | 0.253 | 0.253 | 0.253 |
| Absolute Pressure, inches mercury | 30.14 | 30.24 | 30.26 |
| Average Orifice Pressure Differential, inches water | 1.46 | 1.45 | 1.38 |
| Average Dry Gas Temperature at Meter, °F | 61. | 63. | 72. |
| Total Water Collected by Train, ml | 523.0 | 274.0 | 209.0 |
| Standard Volume of Water Vapor Collected, cubic feet | 24.6 | 12.9 | 9.8 |
| Dry Gas Meter Calibration Factor, dimensionless | 1.005 | 1.005 | 1.005 |
| Sample Volume at Meter Conditions, cubic feet ¹ | 232.3 | 115.7 | 91.7 |
| Sample Volume at Standard Conditions, cubic feet ¹ | 239.0 | 119.0 | 92.8 |

Gas Stream Composition

| | | | |
|---|-------|-------|-------|
| CO ₂ , percent by volume | 7.4 | 7.5 | 7.4 |
| O ₂ , percent by volume | 9.2 | 9.1 | 9.1 |
| CO, percent by volume | 0.0 | 0.0 | 0.0 |
| H ₂ , percent by volume | 83.4 | 83.4 | 83.5 |
| Moisture in Gas Stream, percent by volume | 9.3 | 9.8 | 9.6 |
| Molar Fraction of Dry Gas | 0.907 | 0.902 | 0.904 |
| Molecular Weight of Dry Gas | 29.6 | 29.6 | 29.6 |
| Molecular Weight of Wet Gas | 28.5 | 28.4 | 28.4 |

Gas Stream Velocity and Volumetric Flow

| | | | |
|---|---------|---------|---------|
| Static Pressure, inches water | - 0.41 | - 0.35 | - 0.50 |
| Absolute Pressure, inches mercury | 30.1 | 30.2 | 30.2 |
| Average Temperature, °F | 366. | 368. | 369. |
| Pitot Tube Calibration Coefficient, dimensionless | 0.84 | 0.84 | 0.84 |
| Total Number of Traverse Points | 40.0 | 40.0 | 40.0 |
| Velocity at Actual Conditions, feet/second | 47.4 | 47.0 | 46.2 |
| Stack/duct Cross-Sectional Area, square feet | 28.3 | 28.3 | 28.3 |
| Volumetric Flow, Wet Actual cubic feet/minute | 80,500. | 79,700. | 78,300. |
| Volumetric Flow, Dry Standard cubic feet/minute | 46,900. | 46,300. | 45,500. |

Percent Isokinetic

| | | |
|-------|-------|-------|
| 103.1 | 104.0 | 103.1 |
|-------|-------|-------|

Unit/Process Operations Data

| | | | |
|--|-------|-------|-------|
| Fuel Firing Ratio, % Gas : % Oil | 47:53 | 36:64 | 48:52 |
| Percent O ₂ Exiting Boiler | 5.5 | 5.4 | 5.4 |
| Percent O ₂ at test location | 9.2 | 9.1 | 9.1 |
| Boiler Steam Production Rate, 10 ³ lb/hr. | 97. | 100. | 100. |

¹Standard Conditions = 68°F (20°C) and 29.92 inches (760 mm) mercury, dry basis.

AMERICAN PETROLEUM INSTITUTE

REFINERY-C

SOURCE 1

Table A-71

SUMMARY OF PARTICULATE AND NO_x TEST RESULTSTest Data

| | 7 | 8 | 9 |
|-----------------|-----------|-----------|-----------|
| Test Run Number | 3/3/82 | 3/4/82 | 3/4/82 |
| Test Date | 0910-1556 | 0937-1315 | 1429-1718 |
| Test Time | | | |

Gas Flow Volumes

| (1) | | | |
|--------------------------------|---------|---------|---------|
| Dry Standard Cubic Feet/Minute | 46,900. | 46,300. | 45,500. |
| Wet Actual Cubic Feet/Minute | 80,500. | 79,700. | 78,300. |

Particulate Analysis Report

| | | | |
|--|--------|--------|--------|
| Front-Half Acetone Wash Residue Wt., grams | 0.2267 | 0.1127 | 0.0832 |
| Front-Half Methylene Chloride Wash Residue Wt., grams | --- | --- | 0.0041 |
| Filter Catch Wt., grams | 0.2444 | 0.1759 | 0.1250 |
| Front-Half Catch Wt. Sub-total, grams | 0.4711 | 0.2886 | 0.2123 |
| Methylene Chloride Extraction of Impinger Contents/Wash Residue wt., grams | --- | --- | 0.0131 |
| Impinger Contents/Wash Residue Wt., grams | 0.0087 | 0.0355 | 0.0056 |
| Back-Half Acetone Wash Residue Wt., grams | 0.0013 | 0.0026 | 0.0013 |
| Back-Half Methylene Chloride Wash Residue Wt., grams | --- | --- | 0.0071 |
| Back Half Catch Wt. Sub-total, grams | 0.0100 | 0.0381 | 0.0271 |
| Total Catch Weight, grams | 0.4811 | 0.3267 | 0.2394 |

Particulate ResultsFront-Half

| | | | |
|--|-------|-------|-------|
| Concentration, grains/dry standard cubic foot, | 0.030 | 0.037 | 0.035 |
| Mass Emission Rate, pounds/hour | 12.2 | 14.9 | 13.8 |

Total

| | | | |
|--|-------|-------|-------|
| Concentration, grains/dry standard cubic foot, | 0.031 | 0.042 | 0.040 |
| Mass Emission Rate, pounds/hour | 12.5 | 16.8 | 15.5 |

NO_x Emissions, as NO₂ (2)

| | | | |
|--|------|------|------|
| Concentration, Parts/million by Volume, dry basis | 134. | 121. | 118. |
| Concentration, Pounds/Dry Standard Cubic Foot $\times 10^{-6}$ | 16. | 14. | 14. |
| Mass Emission Rate, Pounds/Hour | 45. | 40. | 39. |

(1) Standard Conditions = 68°F (20°C) and 29.92 inches Hg.

(2) Results shown are averages of three (3) grab samples.

AMERICAN PETROLEUM INSTITUTE
REFINERY C
SOURCE 1
Table A-72
SUMMARY OF PARTICULATE TEST DATA

Test Data

| | | | |
|-----------------|--------------------------|--------------------------|--------------------------|
| Test Run Number | ¹⁰ 3/22/82 | ¹¹ 3/23/82 | ¹² 3/23/82 |
| Test Date | 1007-1340 | 0900-1230 | 1430-1757 |
| Test Period | | | |

Sampling Data

| | | | |
|---|-------|-------|-------|
| Sampling Duration, minutes | 200.0 | 200.0 | 200.0 |
| Nozzle Diameter, inches | 0.253 | 0.253 | 0.253 |
| Barometric Pressure, inches mercury | 30.10 | 30.03 | 30.03 |
| Average Orifice Pressure Differential, inches water | 1.18 | 1.39 | 1.40 |
| Average Dry Gas Temperature at Meter, °F | 72. | 78. | 88. |
| Total Water Collected by Train, ml | 225.0 | 227.0 | 226.0 |
| Standard Volume of Water Vapor Collected, cubic feet | 10.6 | 10.7 | 10.6 |
| Dry Gas Meter Calibration Factor, dimensionless | 1.005 | 1.005 | 1.005 |
| Sample Volume at Meter Conditions, cubic feet ¹ | 114.3 | 120.2 | 121.4 |
| Sample Volume at Standard Conditions, cubic feet ¹ | 115.1 | 119.4 | 118.5 |

Gas Stream Composition

| | | | |
|---|-------|-------|-------|
| CO ₂ , percent by volume | 7.4 | 7.4 | 7.8 |
| O ₂ , percent by volume | 10.5 | 10.2 | 9.7 |
| CO, percent by volume | 0.0 | 0.0 | 0.0 |
| H ₂ , percent by volume | 82.1 | 82.4 | 82.5 |
| Moisture in Gas Stream, percent by volume | 8.4 | 8.2 | 8.2 |
| Pilot Tube Fraction of Dry Gas | 0.916 | 0.918 | 0.918 |
| Molecular Weight of Dry Gas | 29.6 | 29.6 | 29.6 |
| Molecular Weight of Wet Gas | 28.6 | 28.6 | 28.7 |

Gas Stream Velocity and Volumetric Flow

| | | | |
|---|---------|---------|---------|
| Static Pressure, inches water | ~ 0.25 | ~ 0.32 | ~ 0.27 |
| Absolute Pressure, inches mercury | 30.1 | 30.0 | 30.0 |
| Average Temperature, °F | 370. | 363. | 361. |
| Pilot Tube Calibration Coefficient, dimensionless | 0.84 | 0.84 | 0.84 |
| Total Number of Traverse Points | 40.0 | 40.0 | 40.0 |
| Velocity at Actual Conditions, feet/second | 45.3 | 47.7 | 48.4 |
| Stack/duct Cross-Sectional Area, square feet | 28.3 | 28.3 | 28.3 |
| Volumetric Flow, Wet Actual cubic feet/minute | 76,900. | 80,800. | 82,100. |
| Volumetric Flow, Dry Standard cubic feet/minute | 45,000. | 47,000. | 48,600. |

Percent Isokinetic

| | | | |
|--------------------|-------|-------|------|
| Percent Isokinetic | 103.5 | 101.2 | 98.8 |
|--------------------|-------|-------|------|

Unit/Process Operations Data

| | | | |
|--|-------|-------|-------|
| Fuel Firing Ratio, % Gas : % Oil | 43:57 | 33:67 | 35:65 |
| Percent O ₂ Exiting Boiler | 6.4 | 6.6 | 6.5 |
| Percent O ₂ at test location | 10.5 | 10.2 | 9.7 |
| Boiler Steam Production Rate, 10 ³ lb/hr. | 96. | 95. | 94. |

¹Standard Conditions = 60°F (20°C) and 29.92 inches (760 mm) mercury, dry basis.

AMERICAN PETROLEUM INSTITUTE

REFINERY C

SOURCE 1

Table A-73

SUMMARY OF PARTICULATE AND NO_x TEST RESULTSTest Data

| | | | |
|-----------------|-----------|-----------|-----------|
| Test Run Number | 10 | 11 | 12 |
| Test Date | 3/22/82 | 3/23/82 | 3/23/82 |
| Test Time | 1007-1341 | 0900-1230 | 1430-1757 |

Gas Flow Volumes

| | | | |
|---|---------|---------|---------|
| Dry Standard Cubic Feet/Minute ⁽¹⁾ | 45,000. | 47,800. | 48,600. |
| Wet Actual Cubic Feet/Minute | 76,900. | 80,800. | 82,100. |

Particulate Analysis Report

| | | | |
|--|--------|--------|--------|
| Front-Half Acetone Wash Residue Wt., grams | 0.1121 | 0.0978 | 0.0927 |
| Front-Half Methylene Chloride Wash Residue Wt., grams | --- | --- | 0.0019 |
| Filter Catch Wt., grams | 0.1432 | 0.1123 | 0.1256 |
| Front-Half Catch Wt. Sub-total, grams | 0.2553 | 0.2101 | 0.2202 |
| Methylene Chloride Extraction of Impinger Contents/Wash Residue wt., grams | --- | --- | 0.0029 |
| Impinger Contents/Wash Residue Wt., grams | 0.0019 | 0.0035 | 0.0049 |
| Back-Half Acetone Wash Residue Wt., grams | 0.0006 | 0.0007 | 0.0011 |
| Back-Half Methylene Chloride Wash Residue Wt., grams | --- | --- | 0.0093 |
| Back Half Catch Wt. Sub-total, grams | 0.0025 | 0.0042 | 0.0182 |
| Total Catch Weight, grams | 0.2578 | 0.2143 | 0.2384 |

Particulate ResultsFront-Half

| | | | |
|--|-------|-------|-------|
| Concentration, grains/dry standard cubic foot, | 0.034 | 0.027 | 0.029 |
| Mass Emission Rate, pounds/hour | 13.2 | 11.1 | 12.0 |

Total

| | | | |
|--|-------|-------|-------|
| Concentration, grains/dry standard cubic foot, | 0.035 | 0.028 | 0.031 |
| Mass Emission Rate, pounds/hour | 13.3 | 11.3 | 13.0 |

NO_x Emissions, as NO₂⁽²⁾

| | | | |
|--|------|------|------|
| Concentration, Parts/million by Volume, dry basis -6 | 130. | 127. | 109. |
| Concentration, Pounds/Dry Standard Cubic Foot x 10 ⁻⁶ | 16. | 15. | 13. |
| Mass Emission Rate, Pounds/Hour | 42. | 43. | 38. |

(1) Standard Conditions = 68°F (20°C) and 29.92 inches Hg.

(2) Results shown are averages of three (3) grab samples.

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REFINERY C

SOURCE 1

Table A-74

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|-----------|---|-------|
| Run: | Seven | Barometric Pressure(in. Hg) | 30.14 |
| Date: | 3/3/82 | Stack Temperature($^{\circ}$ F) | 366. |
| Traverse Point No. Sampled: | X-10; Y-8 | Sample Time(min.) | 200. |
| Fuel Firing Ratio, %Gas:%Oil | 47:53 | Sample Volume(cf) | 117.1 |
| Percent O ₂ (existing boiler) | 5.5 | Moisture(%H ₂ O) | 9.3 |
| Percent O ₂ (at test location) | 9.2 | Meter Temperature($^{\circ}$ F) | 62. |
| Sample Flow Rate (at stack conditions): | 1.03 cfm | Flow Setting, ΔH (in. H ₂ O) | 1.25 |
| | | Nozzle Diameter(in.) | 0.253 |
| | | Static Pressure(in. H ₂ O) | -0.41 |
| | | Meter χ | 1.002 |
| | | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|--------------------------|---|------------------|
| 1 | 45.5 | 41.7 | 58.3 | 8.9 |
| 2 | 5.4 | 4.9 | 53.4 | 8.3 |
| 3 | 5.3 | 4.9 | 48.5 | 5.2 |
| 4 | 6.5 | 5.9 | 42.6 | 3.5 |
| 5 | 6.3 | 5.8 | 36.8 | 1.8 |
| 6 | 6.1 | 5.6 | 31.2 | 0.84 |
| 7 | 3.7 | 3.4 | 27.8 | 0.50 |
| 8 | 3.8 | 3.5 | 24.3 | 0.26 |
| Backup Filter | 26.5 | 24.3 | 0.0 | --- |
| TOTAL | 109.1 | --- | --- | --- |

A-84

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REFINERY C

SOURCE 1

Table A-75

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|-----------|---|-------|
| Run: | Eight | Barometric Pressure(in. Hg) | 30.24 |
| Date: | 3/4/82 | Stack Temperature($^{\circ}$ F) | 368. |
| Traverse Point No. Sampled: | X-10; Y-8 | Sample Time(min.) | 200. |
| Fuel Firing Ratio, %Gas:%Oil | 36:64 | Sample Volume(cf) | 116.4 |
| Percent O ₂ (existing boiler) | 5.4 | Moisture(%H ₂ O) | 9.8 |
| Percent O ₂ (at test location) | 9.1 | Meter Temperature($^{\circ}$ F) | 69. |
| | | Flow Setting, ΔH (in. H ₂ O) | 1.25 |
| | | Nozzle Diameter(in.) | 0.252 |
| | | Static Pressure(in. H ₂ O) | -0.35 |
| | | Meter χ | 1.002 |
| Sample Flow Rate (at stack conditions): | 1.02 cfm | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|--------------|-----------------------|-----------------------------------|---------------|
| 1 | 27.2 | 22.1 | 77.9 | 9.0 |
| 2 | 6.1 | 5.0 | 72.9 | 8.3 |
| 3 | 8.5 | 6.9 | 66.0 | 5.2 |
| 4 | 9.5 | 7.7 | 58.3 | 3.5 |
| 5 | 7.9 | 6.4 | 51.9 | 1.9 |
| 6 | 7.7 | 6.3 | 45.6 | 0.85 |
| 7 | 4.4 | 3.6 | 42.0 | 0.50 |
| 8 | 4.7 | 3.8 | 38.0 | 0.26 |
| Backup Filter | 46.9 | 38.2 | 0.0 | --- |
| TOTAL | 122.9 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE

REFINERY C

SOURCE 1

Table A-76

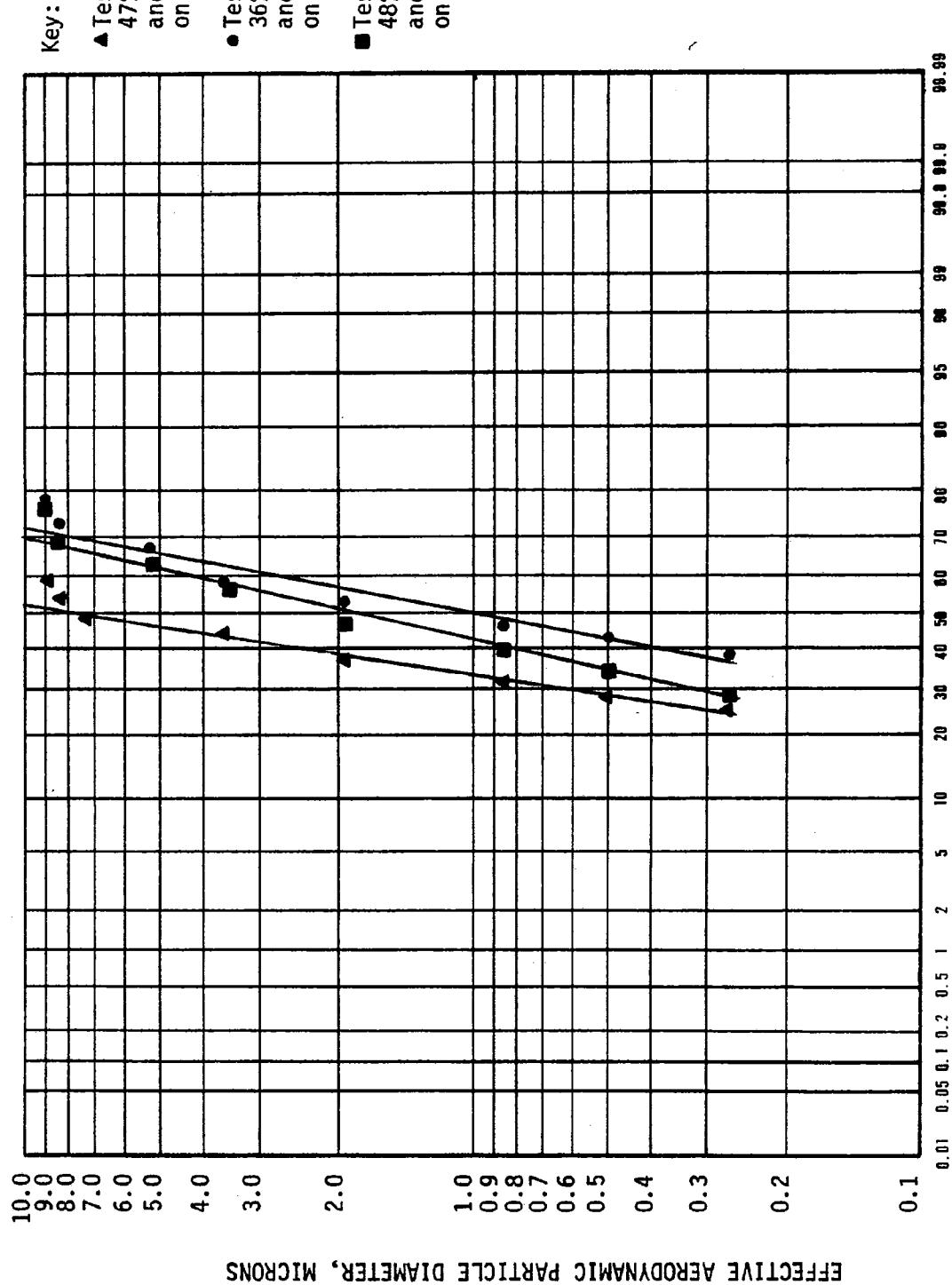
PARTICLE SIZE DISTRIBUTION

| | | | |
|--|----------|---|-------|
| Run: | Nine | Barometric Pressure(in. Hg) | 30.24 |
| Date: | 3/4/82 | Stack Temperature($^{\circ}$ F) | 369. |
| Traverse Point No. Sampled: | X-10:Y-8 | Sample Time(min.) | 160. |
| Fuel Firing Ratio, %Gas:%oil | 48:52 | Sample Volume(cf) | 94.7 |
| Percent O ₂ (existing boiler) | 5.4 | Moisture(%H ₂ O) | 9.6 |
| Percent O ₂ (at test location) | 9.1 | Meter Temperature($^{\circ}$ F) | 74. |
| Sample Flow Rate (at stack conditions): | 1.02 cfm | Flow Setting, ΔH (in. H ₂ O) | 1.25 |
| | | Nozzle Diameter(in.) | 0.252 |
| | | Static Pressure(in. H ₂ O) | -0.5 |
| | | Meter χ | 1.002 |
| | | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|--------------------------|---|------------------|
| 1 | 18.2 | 24.7 | 75.3 | 9.0 |
| 2 | 5.0 | 6.8 | 68.5 | 8.3 |
| 3 | 4.6 | 6.2 | 62.3 | 5.2 |
| 4 | 5.2 | 7.1 | 55.2 | 3.5 |
| 5 | 6.2 | 8.4 | 46.8 | 1.9 |
| 6 | 5.7 | 7.7 | 39.1 | 0.84 |
| 7 | 4.7 | 6.4 | 32.7 | 0.50 |
| 8 | 3.9 | 5.3 | 27.4 | 0.26 |
| Backup Filter | 20.2 | 27.4 | 0.0 | --- |
| TOTAL | 73.7 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE
REFINERY C SOURCE 1

PARTICLE SIZE DISTRIBUTION TEST RESULTS



A-87

FIGURE A-11

AMERICAN PETROLEUM INSTITUTE

REFINERY C

SOURCE 1

Table A-77

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|----------|---|-------|
| Run: | Ten | Barometric Pressure(in. Hg) | 30.10 |
| Date: | 3/22/82 | Stack Temperature($^{\circ}$ F) | 370. |
| Traverse Point No. Sampled: | X-10:Y-8 | Sample Time(min.) | 200. |
| Fuel Firing Ratio, %Gas:%Oil | 43:57 | Sample Volume(cf) | 120.6 |
| Percent O ₂ (existing boiler) | 6.4 | Moisture(%H ₂ O) | 8.5 |
| Percent O ₂ (at test location) | 10.5 | Meter Temperature($^{\circ}$ F) | 78. |
| Sample Flow Rate (at stack conditions): | 1.02 cfm | Flow Setting, ΔH (in. H ₂ O) | 1.25 |
| | | Nozzle Diameter(in.) | 0.253 |
| | | Static Pressure(in. H ₂ O) | -0.25 |
| | | Meter γ | 1.002 |
| | | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|-----------------------|-----------------------------------|---------------|
| 1 | 17.3 | 29.2 | 70.8 | 9.0 |
| 2 | 0.9 | 1.5 | 69.3 | 8.3 |
| 3 | 2.0 | 3.4 | 65.9 | 5.2 |
| 4 | 2.5 | 4.2 | 61.7 | 3.5 |
| 5 | 4.4 | 7.4 | 54.3 | 1.9 |
| 6 | 3.4 | 5.7 | 48.6 | 0.84 |
| 7 | 0.6 | 1.0 | 47.6 | 0.50 |
| 8 | 0.9 | 1.5 | 46.1 | 0.26 |
| Backup Filter | 27.3 | 46.1 | 0.0 | --- |
| TOTAL | 59.3 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE
REFINERY C
SOURCE 1
Table A-78

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|------------|---|-------|
| Run: | Eleven | Barometric Pressure(in. Hg) | 30.03 |
| Date: | 3/23/82 | Stack Temperature($^{\circ}$ F) | 363. |
| Traverse Point No. Sampled: | X-11; Y-10 | Sample Time(min.) | 200. |
| Fuel Firing Ratio, %Gas:%Oil | 33:67 | Sample Volume(cf) | 119.3 |
| Percent O ₂ (existing boiler) | 6.6 | Moisture(%H ₂ O) | 8.2 |
| Percent O ₂ (at test location) | 10.2 | Meter Temperature($^{\circ}$ F) | 82. |
| Sample Flow Rate (at stack conditions): | 0.992 cfm | Flow Setting, ΔH (in. H ₂ O) | 1.2 |
| | | Nozzle Diameter(in.) | 0.252 |
| | | Static Pressure(in. H ₂ O) | -0.32 |
| | | Meter γ | 1.002 |
| | | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|-----------------------|-----------------------------------|---------------|
| 1 | 10.0 | 17.3 | 82.7 | 9.1 |
| 2 | 2.1 | 3.6 | 79.1 | 8.4 |
| 3 | 1.7 | 3.0 | 76.1 | 5.2 |
| 4 | 2.8 | 4.9 | 71.2 | 3.5 |
| 5 | 3.9 | 6.7 | 64.5 | 1.9 |
| 6 | 4.7 | 8.1 | 56.4 | 0.86 |
| 7 | 1.9 | 3.3 | 53.1 | 0.51 |
| 8 | 1.0 | 1.7 | 51.4 | 0.27 |
| Backup Filter | 29.7 | 51.4 | 0.0 | --- |
| TOTAL | 57.8 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE

REFINERY C

SOURCE 1

Table A-79

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|-----------|---|-------|
| Run: | Twelve | Barometric Pressure(in. Hg) | 30.03 |
| Date: | 3/23/82 | Stack Temperature($^{\circ}$ F) | 361. |
| Traverse Point No. Sampled: | X-11;Y-12 | Sample Time(min.) | 200. |
| Fuel Firing Ratio, %Gas:%Oil | 35:65 | Sample Volume(cf) | 120.1 |
| Percent O ₂ (existing boiler) | 6.5 | Moisture(%H ₂ O) | 8.3 |
| Percent O ₂ (at test location) | 9.7 | Meter Temperature($^{\circ}$ F) | 87. |
| Sample Flow Rate (at stack conditions): | 0.99 cfm | Flow Setting, ΔH (in. H ₂ O) | 1.2 |
| | | Nozzle Diameter(in.) | 0.253 |
| | | Static Pressure(in. H ₂ O) | -0.27 |
| | | Meter χ | 1.002 |
| | | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|--------------------------|---|------------------|
| 1 | 8.2 | 14.6 | 85.4 | 9.1 |
| 2 | 1.5 | 2.7 | 82.7 | 8.4 |
| 3 | 1.8 | 3.2 | 79.5 | 5.3 |
| 4 | 2.4 | 4.3 | 75.2 | 3.5 |
| 5 | 3.7 | 6.6 | 68.6 | 1.9 |
| 6 | 5.2 | 9.2 | 59.4 | 0.86 |
| 7 | 1.9 | 3.4 | 56.0 | 0.51 |
| 8 | 1.3 | 2.3 | 53.7 | 0.27 |
| Backup Filter | 30.3 | 53.7 | 0.0 | --- |
| TOTAL | 56.3 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE
 REFINERY C SOURCE 1
 PARTICLE SIZE DISTRIBUTION TEST RESULTS

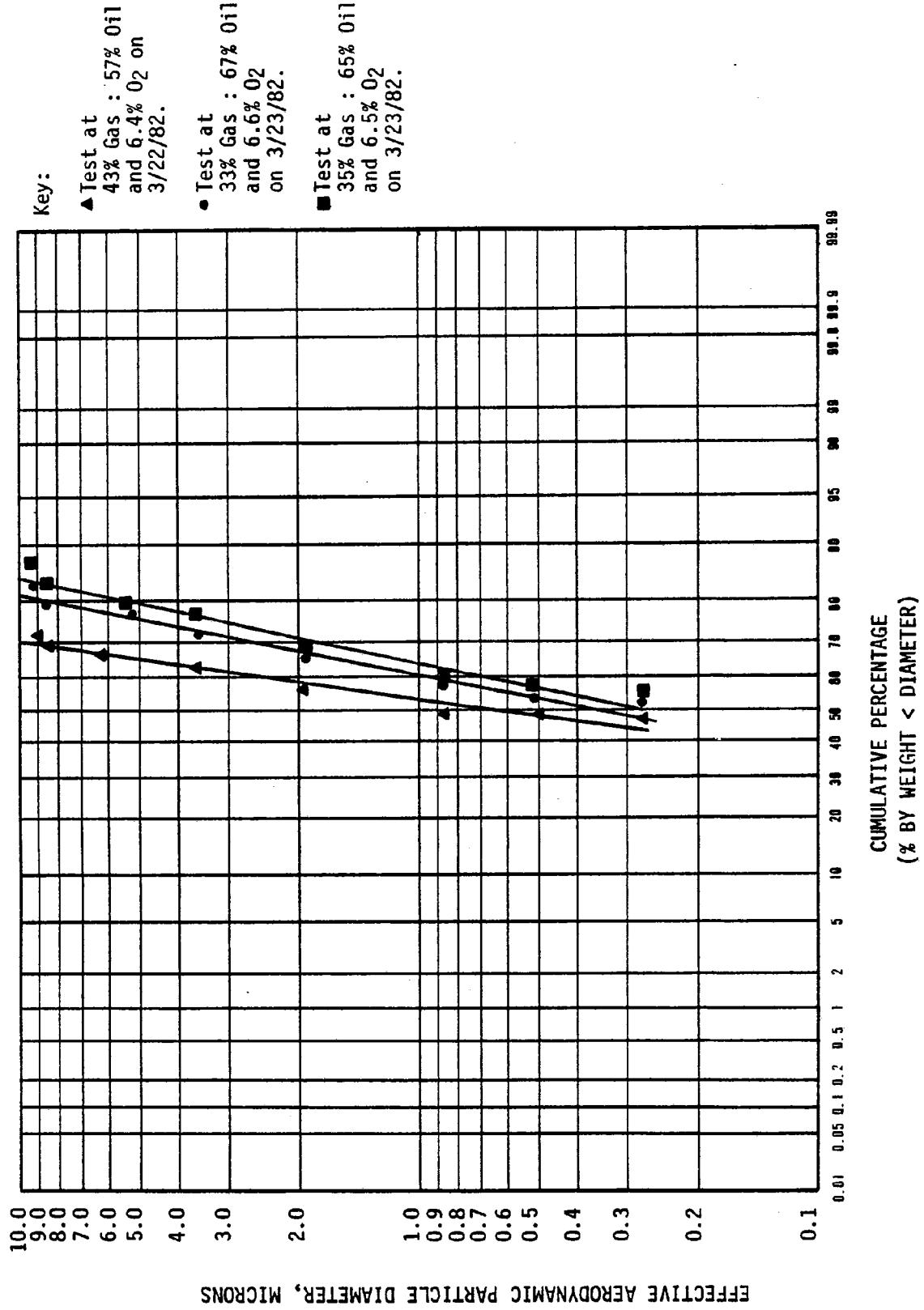


FIGURE A-12

AMERICAN PETROLEUM INSTITUTE

REFINERY C

SOURCE 1

Table A-80

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|------------|---|-------|
| Run: | One | Barometric Pressure(in. Hg) | 30.12 |
| Date: | 2/17/82 | Stack Temperature($^{\circ}$ F) | 349. |
| Traverse Point No. Sampled: | Y-13/ X-11 | Sample Time(min.) | 240. |
| Fuel Firing Ratio, %Gas:%Oil | 0:100 | Sample Volume(cf) | 146.0 |
| Percent O ₂ (existing boiler) | 3.5 | Moisture(%H ₂ O) | 9.6 |
| Percent O ₂ (at test location) | 7.2 | Meter Temperature($^{\circ}$ F) | 48. |
| Sample Flow Rate (at stack conditions): | 1.08 cfm | Flow Setting, ΔH (in. H ₂ O) | 1.40 |
| | | Nozzle Diameter(in.) | 0.252 |
| | | Static Pressure(in. H ₂ O) | -0.33 |
| | | Meter γ | 1.002 |
| | | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|--------------------------|---|------------------|
| 1 | 10.1 | 14.7 | 85.3 | 8.7 |
| 2 | 2.3 | 3.4 | 81.9 | 8.0 |
| 3 | 3.4 | 5.0 | 76.9 | 5.0 |
| 4 | 4.5 | 6.6 | 70.3 | 3.4 |
| 5 | 6.3 | 9.2 | 61.1 | 1.8 |
| 6 | 6.7 | 9.8 | 51.3 | 0.81 |
| 7 | 5.3 | 7.7 | 43.6 | 0.48 |
| 8 | 4.8 | 7.0 | 36.6 | 0.25 |
| Backup Filter | 25.1 | 36.6 | 0.0 | --- |
| TOTAL | 68.5 | --- | --- | --- |

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AMERICAN PETROLEUM INSTITUTE

REFINERY C

SOURCE 1

Table A-81

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|------------|--|-------|
| Run: | Two | Barometric Pressure(in. Hg) | 30.28 |
| Date: | 2/18/82 | Stack Temperature($^{\circ}$ F) | 359. |
| Traverse Point No. Sampled: | Y-11; X-11 | Sample Time(min.) | 200. |
| Fuel Firing Ratio, %Gas:%Oil | 0:100 | Sample Volume(cf) | 115.2 |
| Percent O ₂ (existing boiler) | 4.0 | Moisture(%H ₂ O) | 8.8 |
| Percent O ₂ (at test location) | 7.5 | Meter Temperature($^{\circ}$ F) | 55. |
| Sample Flow Rate (at stack conditions): | 1.01 cfm | Flow Setting, Δ H(in. H ₂ O) | 1.25 |
| | | Nozzle Diameter(in.) | 0.252 |
| | | Static Pressure(in. H ₂ O) | -0.28 |
| | | Meter χ | 1.002 |
| | | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|--------------|-----------------------|-----------------------------------|---------------|
| 1 | 8.1 | 14.8 | 85.2 | 9.0 |
| 2 | 3.6 | 6.6 | 78.6 | 8.3 |
| 3 | 3.8 | 6.9 | 71.7 | 5.2 |
| 4 | 4.4 | 8.0 | 63.7 | 3.5 |
| 5 | 5.3 | 9.7 | 54.0 | 1.9 |
| 6 | 5.8 | 10.6 | 43.4 | 0.85 |
| 7 | 3.8 | 6.9 | 36.5 | 0.50 |
| 8 | 2.5 | 4.6 | 31.9 | 0.26 |
| Backup Filter | 17.5 | 31.9 | 0.0 | --- |
| TOTAL | 54.8 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE

REFINERY C

SOURCE 1

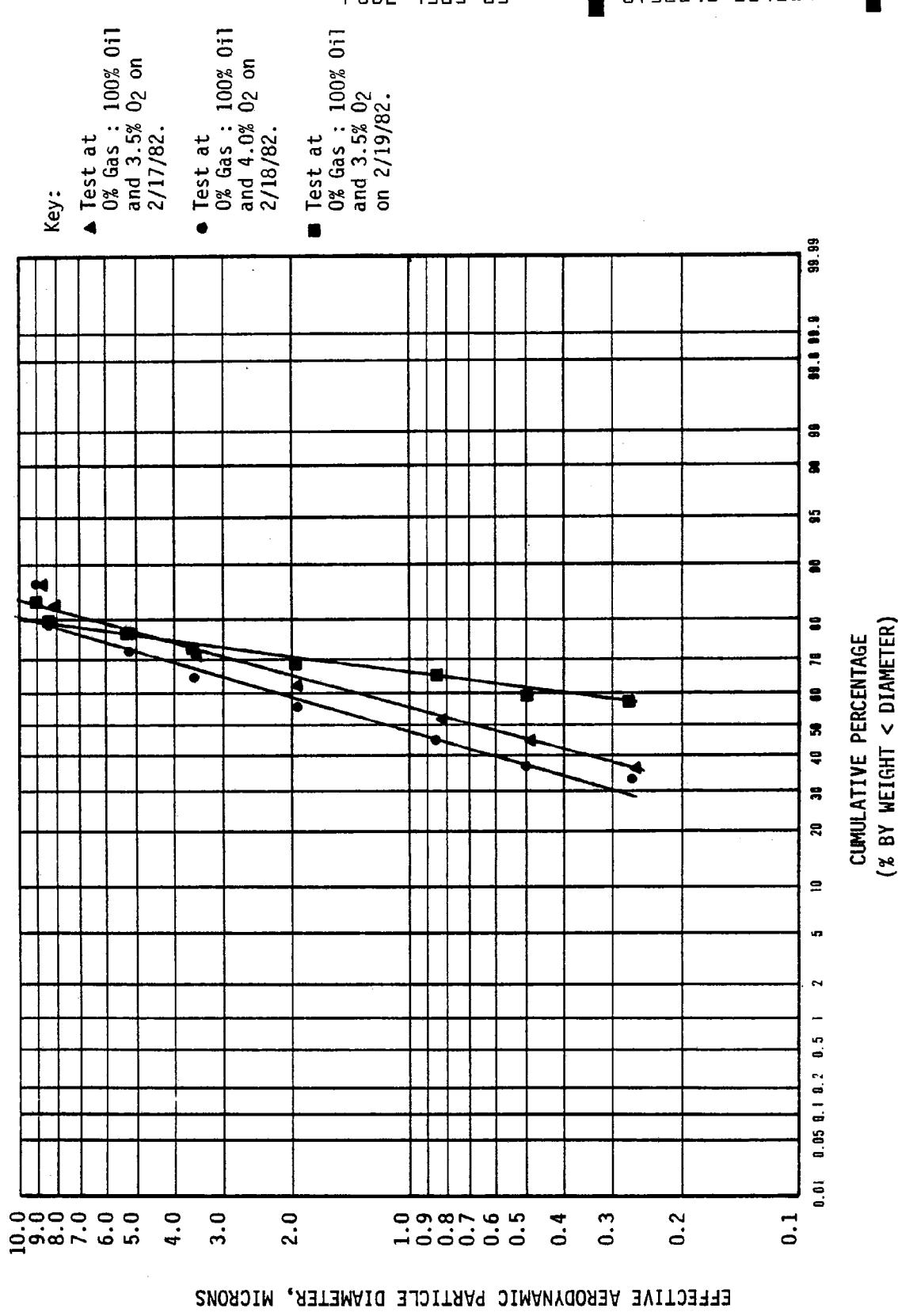
Table A-82

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|-----------|---|-------|
| Run: | Three | Barometric Pressure(in. Hg) | 29.95 |
| Date: | 2/19/82 | Stack Temperature($^{\circ}$ F) | 364. |
| Traverse Point No. Sampled: | Y-11;X-11 | Sample Time(min.) | 200. |
| Fuel Firing Ratio, %Gas:%Oil | 0:100 | Sample Volume(cf) | 118.3 |
| Percent O ₂ (existing boiler) | 3.5 | Moisture(%H ₂ O) | 8.9 |
| Percent O ₂ (at test location) | 7.2 | Meter Temperature($^{\circ}$ F) | 6.7 |
| | | Flow Setting, ΔH (in. H ₂ O) | 1.25 |
| Sample Flow Rate (at stack conditions): | 1.02 cfm | Nozzle Diameter(in.) | 0.252 |
| | | Static Pressure(in. H ₂ O) | -0.32 |
| | | Meter δ | 1.002 |
| | | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|-----------------------|-----------------------------------|---------------|
| 1 | 10.5 | 16.7 | 83.3 | 9.0 |
| 2 | 2.6 | 4.1 | 79.2 | 8.3 |
| 3 | 2.8 | 4.5 | 74.7 | 5.2 |
| 4 | 1.6 | 2.5 | 72.2 | 3.5 |
| 5 | 2.1 | 3.3 | 68.9 | 1.9 |
| 6 | 3.0 | 4.8 | 64.1 | 0.84 |
| 7 | 3.1 | 4.9 | 59.2 | 0.50 |
| 8 | 1.9 | 3.0 | 56.2 | 0.26 |
| Backup Filter | 35.3 | 56.2 | 0.0 | --- |
| TOTAL | 62.9 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE
 REFINERY C SOURCE 1
 PARTICLE SIZE DISTRIBUTION TEST RESULTS



A-95

FIGURE A-13

AMERICAN PETROLEUM INSTITUTE

REFINERY C

SOURCE 1

Table A-83

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|---------------------|--|-------|
| Run: | Four | Barometric Pressure(in. Hg) | 29.80 |
| Date: | 2/22/82 | Stack Temperature($^{\circ}$ F) | 372 |
| Traverse Point No. | Sampled: Y-11; X-11 | Sample Time(min.) | 200 |
| Fuel Firing Ratio, %Gas:%Oil | 0:100 | Sample Volume(cf) | 117.4 |
| Percent O ₂ (existing boiler) | 5.4 | Moisture(%H ₂ O) | 7.6 |
| Percent O ₂ (at test location) | 9.7 | Meter Temperature($^{\circ}$ F) | 55. |
| Sample Flow Rate (at stack conditions): | 1.03 cfm | Flow Setting, Δ H(in. H ₂ O) | 1.25 |
| | | Nozzle Diameter(in.) | 0.252 |
| | | Static Pressure(in. H ₂ O) | -0.28 |
| | | Meter γ | 1.002 |
| | | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|--------------------------|---|------------------|
| 1 | 9.2 | 13.4 | 86.6 | 8.9 |
| 2 | 1.5 | 2.2 | 84.4 | 8.3 |
| 3 | 2.0 | 2.9 | 81.5 | 5.2 |
| 4 | 2.0 | 2.9 | 78.6 | 3.5 |
| 5 | 2.7 | 3.9 | 74.7 | 1.8 |
| 6 | 3.6 | 5.2 | 69.5 | 0.84 |
| 7 | 3.4 | 4.9 | 64.6 | 0.49 |
| 8 | 2.2 | 3.2 | 61.4 | 0.26 |
| Backup Filter | 42.2 | 61.4 | 0.0 | --- |
| TOTAL | 68.8 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE

REFINERY C

SOURCE 1

Table A-84

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|------------|---|-------|
| Run: | Five | Barometric Pressure(in. Hg) | 29.80 |
| Date: | 2/22/82 | Stack Temperature($^{\circ}$ F) | 373. |
| Traverse Point No. Sampled: | X-10; Y-11 | Sample Time(min.) | 200. |
| Fuel Firing Ratio, %Gas:%Oil | 0:100 | Sample Volume(cf) | 116.9 |
| Percent O ₂ (existing boiler) | 5.4 | Moisture(%H ₂ O) | 8.2 |
| Percent O ₂ (at test location) | 9.5 | Meter Temperature($^{\circ}$ F) | 59. |
| Sample Flow Rate (at stack conditions): | 1.03 cfm | Flow Setting, ΔH (in. H ₂ O) | 1.25 |
| | | Nozzle Diameter(in.) | 0.255 |
| | | Static Pressure(in. H ₂ O) | -0.31 |
| | | Meter γ | 1.002 |
| | | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|-----------------------|-----------------------------------|---------------|
| 1 | 15.2 | 20.6 | 79.4 | 9.0 |
| 2 | 2.6 | 3.5 | 75.9 | 8.3 |
| 3 | 2.3 | 3.1 | 72.8 | 5.2 |
| 4 | 3.9 | 5.3 | 67.5 | 3.5 |
| 5 | 5.0 | 6.8 | 60.7 | 1.8 |
| 6 | 5.6 | 7.6 | 53.1 | 0.84 |
| 7 | 4.4 | 5.9 | 47.2 | 0.49 |
| 8 | 5.2 | 7.0 | 40.2 | 0.26 |
| Backup Filter | 29.7 | 40.2 | 0.0 | --- |
| TOTAL | 73.9 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE

REFINERY C

SOURCE 1

Table A-85

PARTICLE SIZE DISTRIBUTION

| | | | |
|--|-----------|---|-------|
| Run: | Six | Barometric Pressure(in. Hg) | 30.07 |
| Date: | 2/23/82 | Stack Temperature($^{\circ}$ F) | 377. |
| Traverse Point No. Sampled: | Y-10:X-11 | Sample Time(min.) | 200. |
| Fuel Firing Ratio, %Gas:%oil | 0:100 | Sample Volume(cf) | 112.8 |
| Percent O ₂ (existing boiler) | 5.5 | Moisture(%H ₂ O) | 8.1 |
| Percent O ₂ (at test location) | 9.6 | Meter Temperature($^{\circ}$ F) | 76. |
| Sample Flow Rate (at stack conditions): | 1.02 cfm | Flow Setting, ΔH (in. H ₂ O) | 1.25 |
| | | Nozzle Diameter(in.) | 0.252 |
| | | Static Pressure(in. H ₂ O) | -0.42 |
| | | Meter γ | 1.002 |
| | | Sample Vac.(in. Hg) | 1.0 |

| Plate No. | Net Wt. (mg) | Percent in Size Range | Cumulative Percent Less Than Dia. | EAD (microns) |
|---------------|-----------------|--------------------------|---|------------------|
| 1 | 8.8 | 17.0 | 83.0 | 9.0 |
| 2 | 1.8 | 3.5 | 79.5 | 8.4 |
| 3 | 2.3 | 4.4 | 75.1 | 5.2 |
| 4 | 2.5 | 4.8 | 70.3 | 3.5 |
| 5 | 3.1 | 6.0 | 64.3 | 1.9 |
| 6 | 4.7 | 9.1 | 55.2 | 0.85 |
| 7 | 3.3 | 6.4 | 48.8 | 0.50 |
| 8 | 2.3 | 4.4 | 44.4 | 0.26 |
| Backup Filter | 23.0 | 44.4 | 0.0 | --- |
| TOTAL | 51.8 | --- | --- | --- |

AMERICAN PETROLEUM INSTITUTE

REFINERY C SOURCE 1

PARTICLE SIZE DISTRIBUTION TEST RESULTS

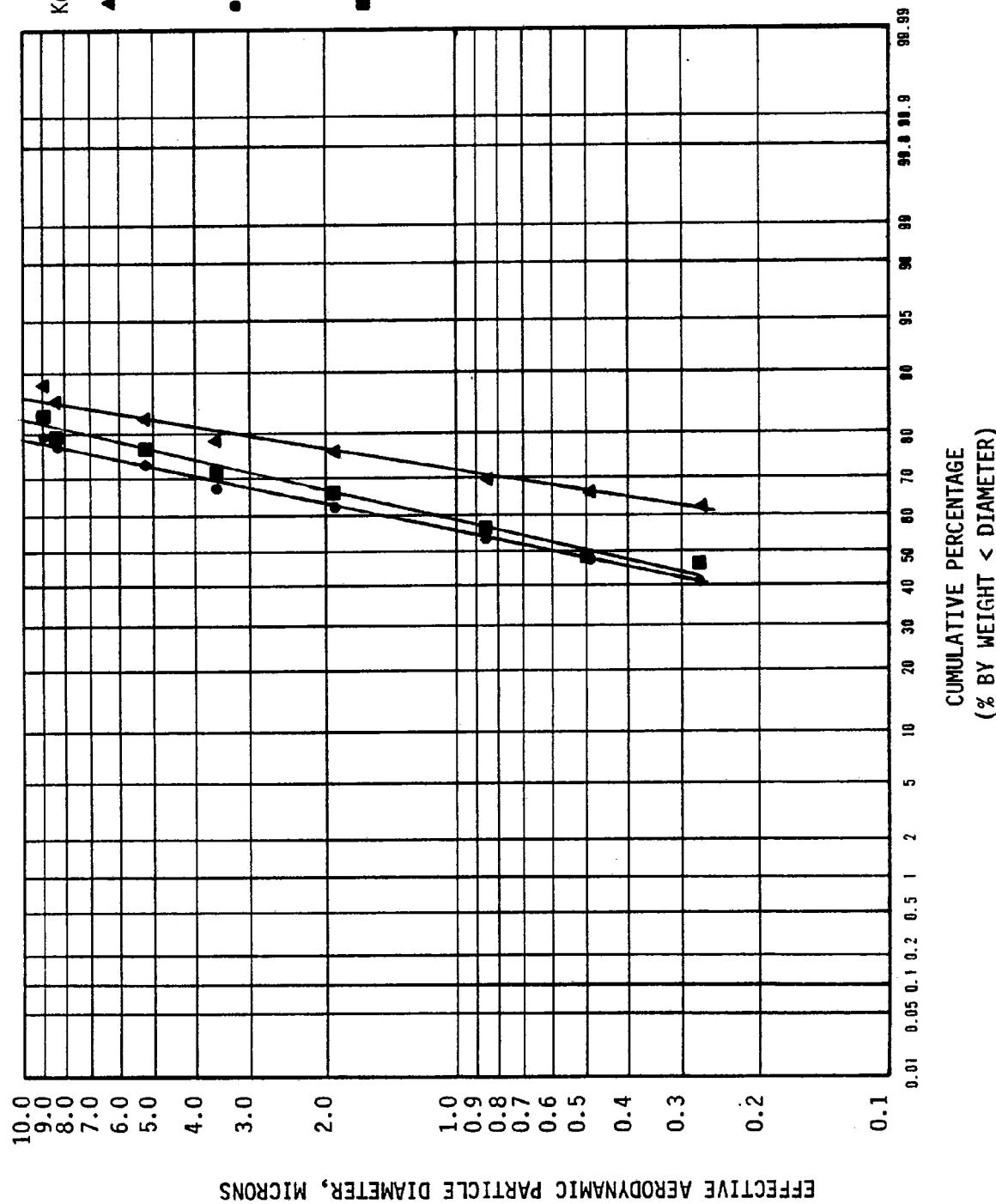


FIGURE A-14

AMERICAN PETROLEUM INSTITUTE

REFINERY C

SOURCE 1

Table A-86

RESULTS OF FUEL OIL COMPOSITE SAMPLE ANALYSES
FOR TEST RUNS 1-12, 2/17-23/1982

| | |
|-------------------------|----------|
| Ash, % | 0.02 |
| Carbon, % | 86.8 |
| Hydrogen, % | 11.2 |
| Nitrogen, % | 0.18 |
| Oxygen, % | 0.61 |
| Sulfur, % | 1.19 |
| Density, lbs/gal | 8.027 |
| Heating Value, BTU/lb. | 18,610. |
| Heating Value, BTU/gal. | 149,400. |
| Viscosity, SFS @ 122°F. | 45.0 |

Metals, ppm by weight

| | |
|----------|-------|
| Arsenic | < 0.2 |
| Barium | 0.75 |
| Cadmium | < 0.5 |
| Chromium | < 0.5 |
| Copper | < 0.5 |
| Lead | < 0.5 |
| Mercury | 0.067 |
| Nickel | 11.0 |
| Selenium | 0.49 |
| Vanadium | 31.0 |
| Zinc | 1.7 |

A-100

PUBL 4365-83

0732290 0042305 6

APPENDIX B

DESCRIPTIONS OF UNITS TESTED

DESCRIPTIONS OF UNITS TESTED

Five sources (2 heaters and 3 boilers) were surveyed under this contract. Descriptions of the units and schematics of the test points are contained in this Appendix.

Process HeatersRefinery A - Source 1

This source is an atmospheric crude heater installed in 1978 by Foster Wheeler. It is 1 of 2 furnaces used to supply heat to a crude unit before atmospheric distillation.

It has a maximum gross fired duty of 315×10^6 BTU/hr; fuel ratios can be varied from 0 to 100% gas or oil.

It is a side-fired horizontal radiant tube furnace. Low pressure steam is produced in the convection section.

A schematic of the test site showing traverse point locations is presented in Figure B-1.

AMERICAN PETROLEUM INSTITUTE
REFINERY A
SOURCE 1 (FURNACE)

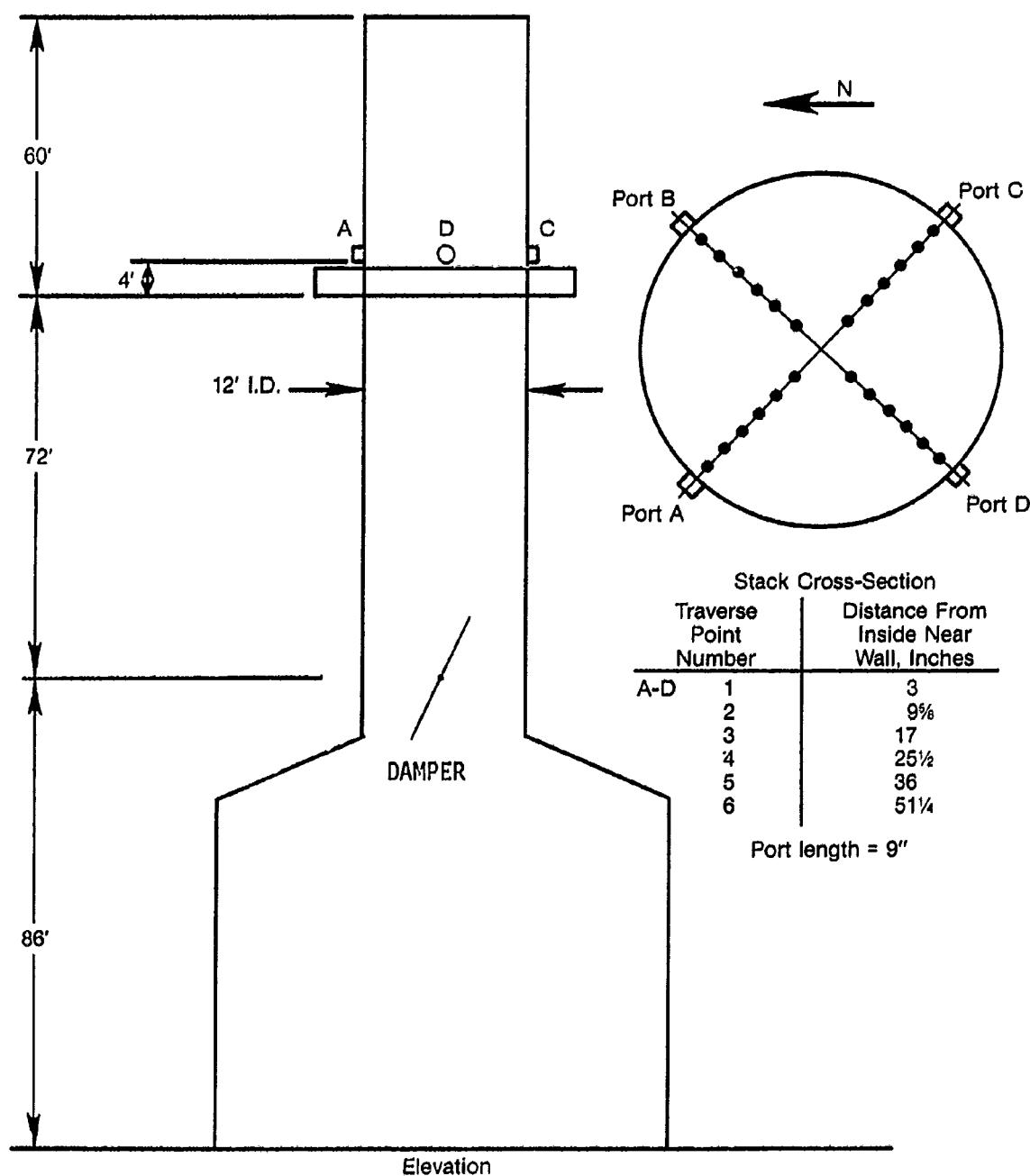


FIGURE B-1 TEST POINT SCHEMATIC

B-2

Refinery B - Source 1

This source, constructed in 1978, is a hydrotreating unit furnace normally used for desulfurization of diesel distillate. Unit processing capacity is 25,000 BPOD with a maximum fired duty of 60.1×10^6 BTU/hr. Heat is supplied by firing plant fuel gas only.

The unit may be divided into three sections, namely:

1. Make-up Hydrogen Section
2. Reactor Section
3. Fractionation Section

1. Make-up Hydrogen Section

Make-up hydrogen is supplied from existing high pressure and low pressure hydrogen systems to the unit. Two 100 percent capacity reciprocating machines are provided to compress the make-up gas from either hydrogen system to the suction pressure of a recycle compressor.

2. Reactor Section

The Reaction Section consists of the reactor, heat exchangers, fired heater, coolers, a high pressure separator and centrifugal recycle gas compressor.

Unit charge is supplied cold from offsite tankage. Charge is pumped through a feed solids separator, then through feed/effluent exchangers. The hot oil is then routed through a feed heater.

Recycle gas from the discharge of the recycle compressor exchanges heat with reactor effluent and then combines with the hot charge. Effluent flow leaving the reactor is split between the feed/effluent and gas/effluent exchangers. After exchange, the combined effluent flows to an effluent air cooler where condensate and corrosion inhibitors are injected into the inlet piping. Separation of hydrogen rich gas and rerun tower feed occurs in the HP Separator.

Bleed gas from the HP Separator is released to the high pressure hydrogen system and recycle gas enters the compressor K0 drum for recompression by a recycle gas compressor.

Make up gas feed into the effluent air cooler inlet is obtained from either or both the plant high and low pressure hydrogen systems.

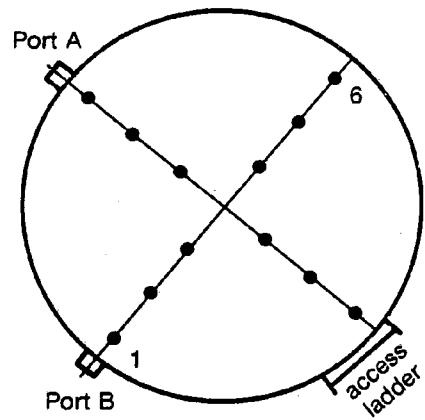
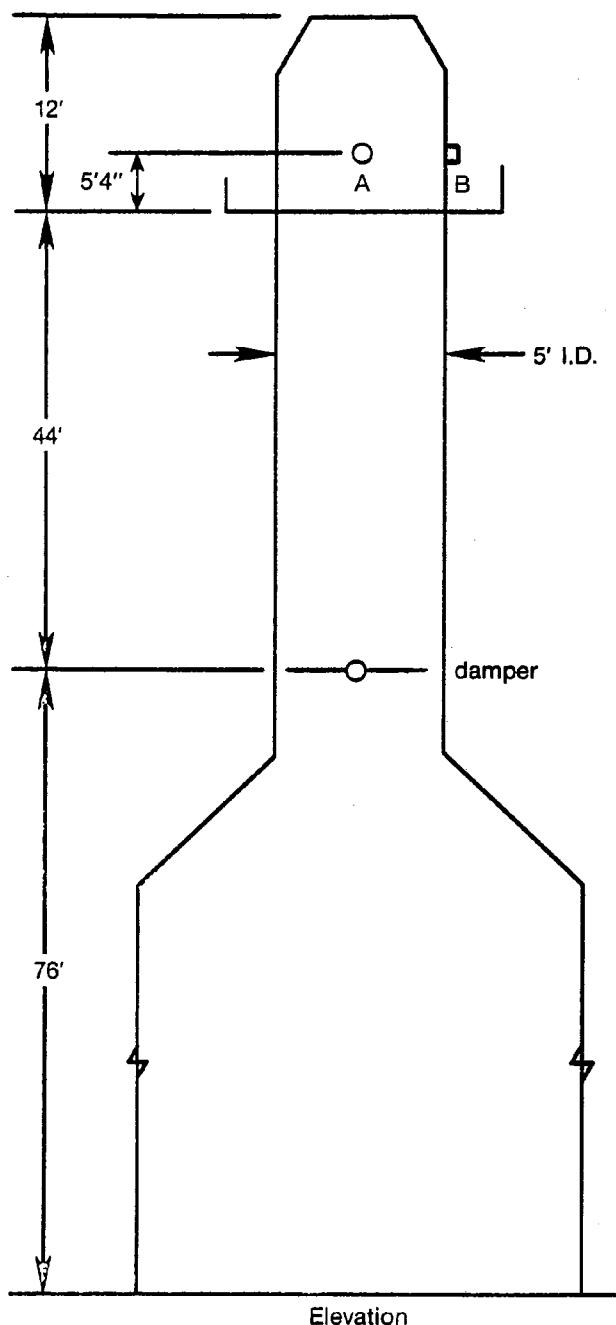
3. Fractionation Section

The stripping and fractionation of the reaction product liquid is accomplished in a routine manner in a rerun tower with a fired heater reboiler.

Off gas from the rerun tower is MEA-scrubbed for H₂S removal, compressed and routed offsite for further treating.

A schematic of the test point is presented in Figure B-2.

**AMERICAN PETROLEUM INSTITUTE
REFINERY B
SOURCE 1 (HEATER - DIESEL CHARGE)**



| Stack Cross-Section | |
|-----------------------|--|
| Traverse Point Number | Distance From Inside Near Wall, Inches |
| 1 | 2 $\frac{5}{8}$ |
| 2 | 8 $\frac{3}{4}$ |
| 3 | 17 $\frac{3}{4}$ |
| 4 | 42 $\frac{1}{4}$ |
| 5 | 51 $\frac{1}{4}$ |
| 6 | 57 $\frac{3}{8}$ |

Port length = 8"

FIGURE B-2 TEST POINT SCHEMATIC

BoilersRefinery A - Source 2

This source is a Riley Stoker utility boiler constructed in 1948. The boiler generates high pressure steam for refinery use.

It has a maximum gross fired duty of 215×10^6 BTU/hr; fuel ratios can be varied from 0 to 100% refinery fuel gas or oil.

It is a balanced draft, end horizontal fired boiler with vertical section radiant tubes and horizontal section convection tubes. It has a combustion air preheater.

A test point schematic is presented in Figure B-3.

AMERICAN PETROLEUM INSTITUTE
REFINERY A
SOURCE 2 (BOILER)

| Traverse Point Number | Distance From Inside Near Wall, Inches |
|-----------------------|--|
| 1 | 2 $\frac{5}{8}$ |
| 2 | 8 |
| 3 | 13 $\frac{3}{8}$ |
| 4 | 18 $\frac{1}{4}$ |
| 5 | 24 $\frac{1}{8}$ |
| 6 | 29 $\frac{1}{2}$ |
| 7 | 34 $\frac{7}{8}$ |
| 8 | 40 $\frac{1}{4}$ |

Port Length = 6"

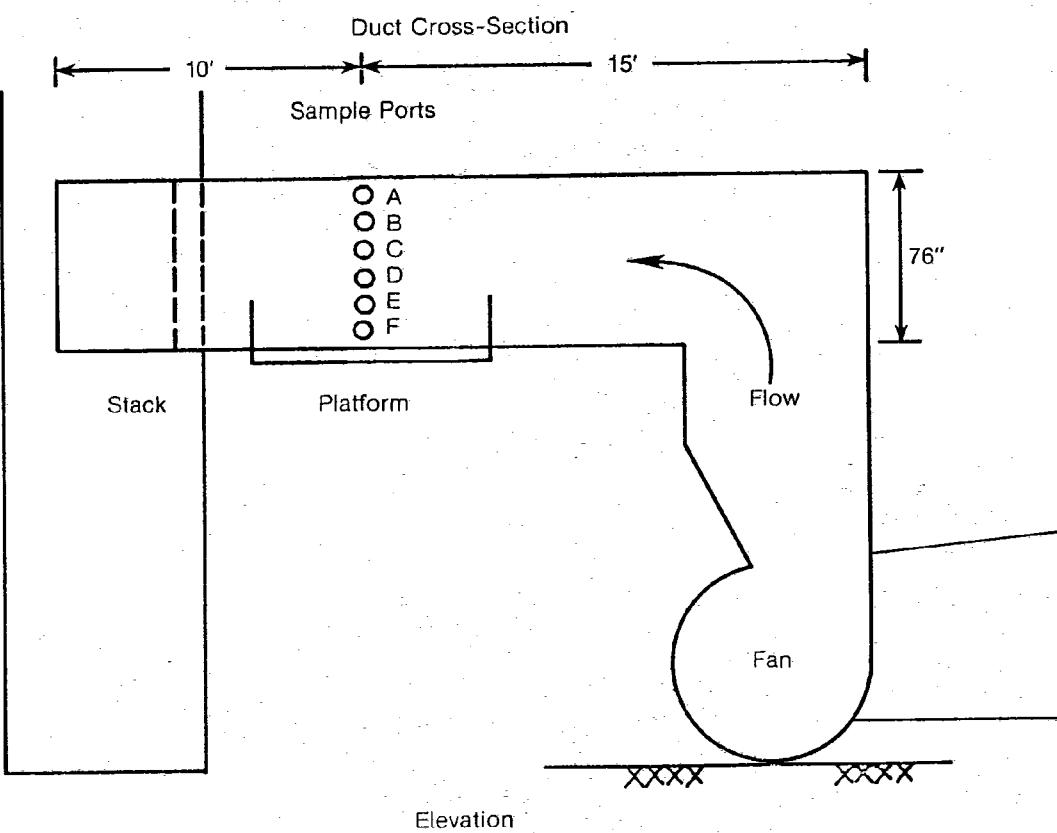
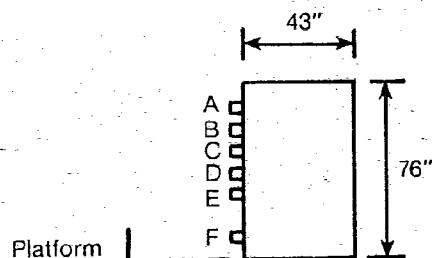


FIGURE B-3

TEST POINT SCHEMATIC

Refinery B - Source 2

Basically, in this process, water is fed into a generator, and by application of heat, evaporated continuously into steam. The heat is supplied by firing No. 6 fuel oil and/or process fuel gas. The steam generator is of a natural circulation water tube type design built in 1978.

Its steam production capacity is $440. \times 10^3$ lbs/hr. at a maximum heat rating of 576.1×10^6 BTU/hr. Its fuel firing ratio is infinitely adjustable but is currently limited by the availability of process fuel gas to about 30% gas. The unit is normally operated on oil using gas as a float.

Water is initially introduced into the economizer section for preheat, then flows into the boiler section. The boiler section consists of a steam drum, mud drum, boiler tubes and water wall tubes. Water enters the boiler section via the steam drum, then, by natural circulation, the fluid flows from the steam drum through the boiler and water wall tubes to the mud drum and back to the steam drum. During this natural circulation period, the water is evaporated into steam. The saturated steam is collected in the top half of the steam drum, then flows to the superheater section of the steam generator. The superheater raises the temperature of the steam above its saturation point. In order to maintain adequate superheated steam temperature, a steam attemperation control is utilized. This control passes a portion of the superheated steam through a heat exchanger placed in the mud drum of the boiler section where a portion of the steam is cooled close to saturation temperature and is then returned to the superheater outlet header. The cooled steam mixes with the superheated steam so that the temperature of the mixture reaches the design final steam temperature.

See Figure B-4 for a schematic of the test point.

**AMERICAN PETROLEUM INSTITUTE
REFINERY B
SOURCE 2 (BOILER)**

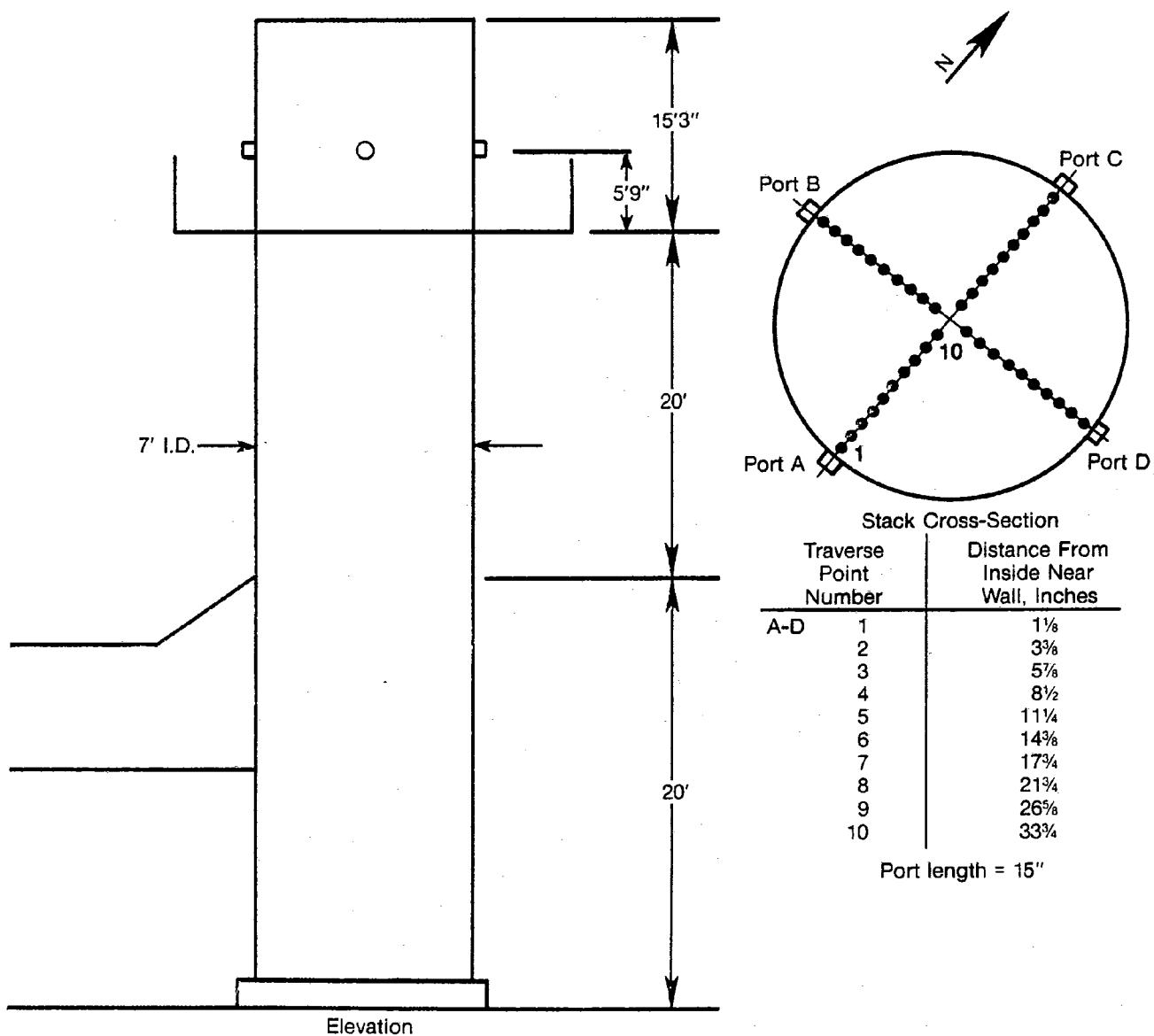


FIGURE B-4 TEST POINT SCHEMATIC
B-9

Refinery C - Source 1

This boiler was designed by Babcock and Wilcox and constructed in 1942. It is a balanced draft unit with a maximum steam rating of 125,000 lb/hr at 750°F and 700 psig. The boiler can be fired by either oil or gas using a series of four conventional tip burners for oil or four B and W ring type burners for gas. The fire box dimensions are 21' high by 16' wide and 21' deep. The boiler is equipped with a heat exchanger air heater. Its design efficiency is 86%. Maximum design rating is 200×10^6 Btu/hr.

A schematic of the test site showing port and traverse point locations is presented in Figure B-5.

**AMERICAN PETROLEUM INSTITUTE
REFINERY C
SOURCE 1 (BOILER)**

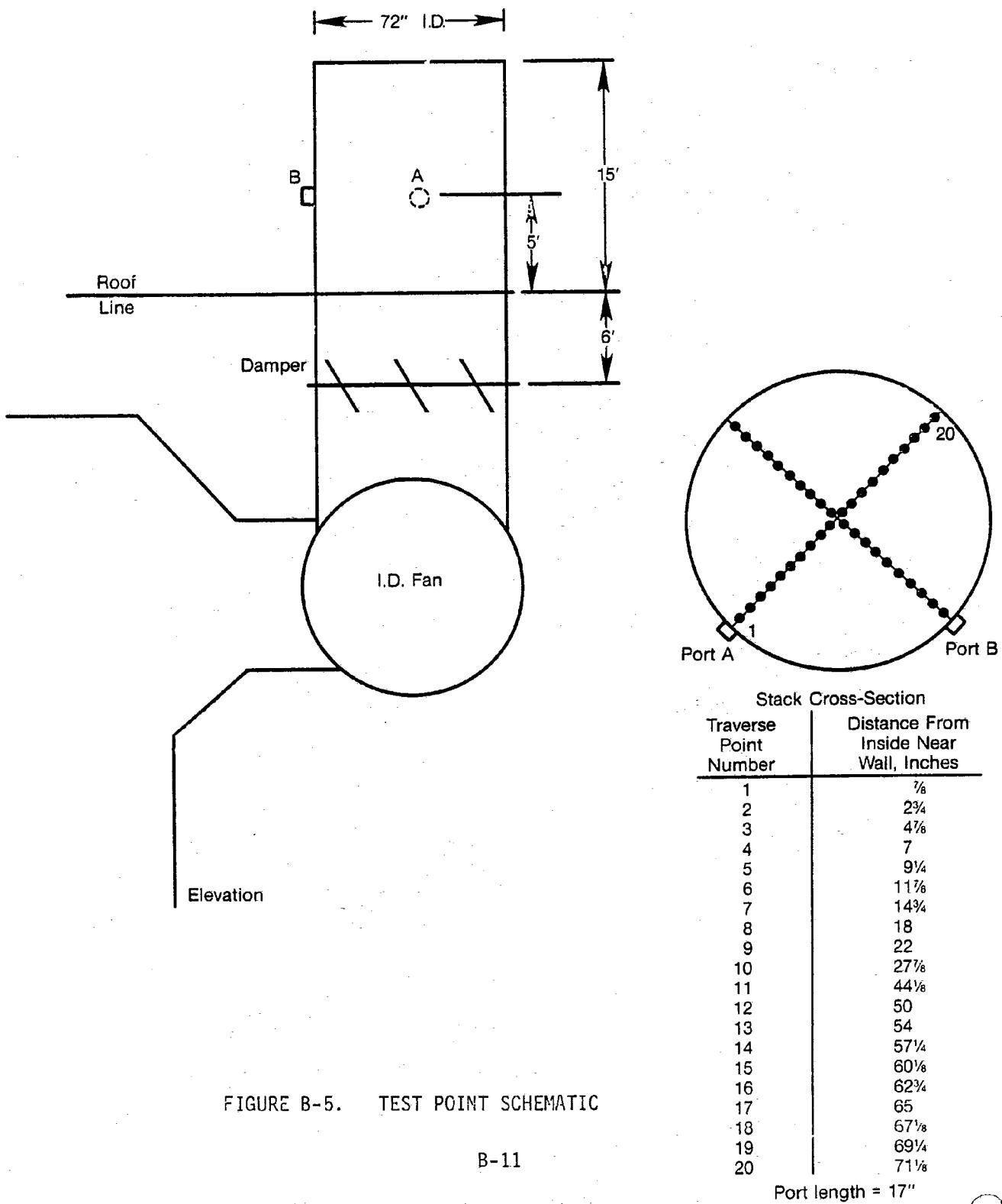


FIGURE B-5. TEST POINT SCHEMATIC

B-11

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APPENDIX C

TESTING AND ANALYSIS EQUIPMENT AND PROCEDURES

TESTING AND ANALYSIS EQUIPMENT AND PROCEDURES

Particulate Measurement and Procedures

Test Equipment

The test train utilized for particulate sampling at all boiler and heater sources was the standard EPA Method 5 train (see Figure C-1).

A stainless steel nozzle was attached to a heated ($\sim 250^{\circ}\text{F}$) borosilicate probe which was connected directly to a borosilicate filter holder containing a 9-cm Reeve Angel 934 AH glass fiber filter. The filter holder was maintained at approximately 250°F in a heated chamber, and was connected by a rigid borosilicate connector to the first of four Greenburg-Smith impingers. Each of the first two impingers contained 100 ml of distilled water, the third was dry, and the final impinger contained 200 gm of dry preweighed silica gel. The first, third, and fourth impingers were modified Greenburg-Smith types; the second was of the standard design. All impingers were maintained in a crushed ice bath. An RAC or Nutech control console with vacuum pump, dry gas meter, a calibrated orifice, and inclined manometers completed the sampling train. Flue gas temperature was measured by means of a Type K thermocouple connected to a calibrated direct readout pyrometer. The thermocouple sensor was positioned adjacent to the sampling nozzle.

Flue gas velocity was measured using a calibrated "S" type pitot tube (provided with extensions) fastened alongside the sampling probe. Gas stream composition (carbon dioxide, oxygen, and carbon monoxide content), was determined utilizing an Orsat apparatus to analyze grab samples of the flue gases. Orsat analyses were performed at each port in conjunction with each particulate test set.

Preliminary Test Procedures

Preliminary test data were obtained at each sampling location. Duct geometry measurements were recorded, and traverse point distances calculated. A preliminary velocity traverse was performed at each site utilizing a calibrated S-type pitot tube and a Dwyer inclined manometer to determine velocity profiles. A check for the presence or absence of cyclonic flow was conducted at each site prior to formal testing. Flue gas temperatures were observed with a calibrated direct readout pyrometer equipped with a chromel-alumel thermocouple. Water vapor content was estimated from previous experience or determined through an EPA Method 4 moisture test. Preliminary test data were used for nozzle sizing and nomograph set-up for isokinetic sampling procedures.

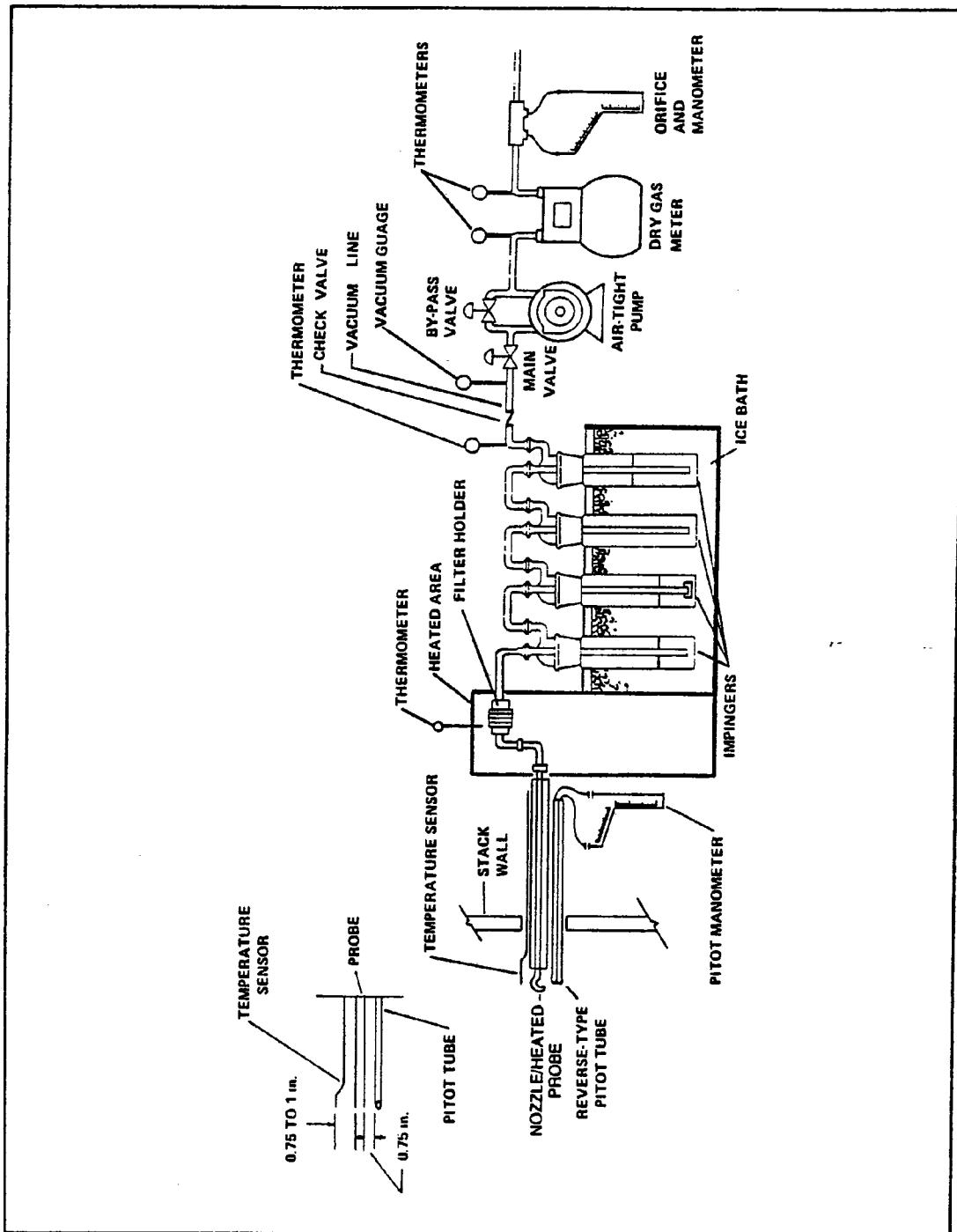


FIGURE C-1 PARTICULATE SAMPLING TRAIN-EPA METHOD 5

C-2

Calibration of sampling nozzles, pitot tubes, metering systems, thermocouples/pyrometers, and temperature gauges was performed as specified in Section 5 of EPA Method 5 test procedures.

Prior to formal sampling, the oxygen content of the flue gas stream was determined using an Orsat apparatus. The Orsat O₂ readings were compared to those recorded by the continuous monitoring instrumentation. This cross check was conducted to determine the accuracy of the continuous O₂ monitors and to determine if any in-leakage of ambient air was occurring between the boiler or heater exit and the sampling location.

Particulate Test Procedures

During the sampling program triplicate EPA Method 5 particulate test runs were conducted at each unit operating condition. An exception occurred for Refinery A Source 2 where duplicate tests were run for 2 of the 6 operating conditions studied. The third test of these 2 sets could not be performed due to a boiler outage. The number of test sets performed on each unit (2 to 6) was dependent on the fuel firing capabilities of the source.

During particulate sampling, gas stream velocities were measured by inserting a calibrated S-type pitot tube into the gas stream adjacent to the sampling nozzle. The velocity pressure differential was observed immediately after positioning the nozzle at each point, and the sampling rate was adjusted to maintain isokineticity. Flue gas temperature was monitored at each point with a pyrometer and thermocouple. Temperature readings of the filter box, final impinger, and inlet and outlet of the dry test meter were also recorded. See Figure C-1 for a schematic of the EPA Method 5 particulate sampling train.

Leak checks were performed on the equipment according to EPA Method 5 instructions, prior to and after each run and/or component change.

Testing duration for particulate sampling was dependent on the units fuel firing ratio, oxygen level and particulate loading for each test set condition.

Control room operating data, plus fuel samples for each source, were collected during each test run.

Sample Recovery Procedures

One of two sample recovery procedures were employed depending upon the analysis required following the gravimetric step.

Particulate Sample Recovery for Analysis Types 1 and 2

During each test set (a total of 3 runs), particulate sample recovery procedures for sample analysis types one and two were identical and are described below.

At the conclusion of each test, the sampling trains were dismantled, openings sealed, and the components transported to the field laboratory.

A consistent procedure was employed for sample recovery:

1. The glass fiber filter(s) was removed from its holder with tweezers and placed in its original container (petri dish), along with any loose particulate and filter fragments (sample 1).
2. The probe and nozzle were separated and the internal particulate rinsed with acetone into a borosilicate container while brushing a minimum of three times. Particulate adhering to the brush was rinsed with acetone into the same container. The front-half of the filter holder, and connecting glassware were rinsed with acetone while brushing a minimum of three times. The rinses were added to the container, and the container was then sealed with a Teflon-lined cap (sample 2).
3. The total liquid contents of impingers 1, 2, and 3 was measured and placed in a borosilicate container fitted with a Teflon-lined closure (sample 3). Also included in this sample was a distilled water rinse of the impingers and connectors.
4. Components from the aforementioned step were acetone washed into a separate borosilicate container fitted with a Teflon-lined lid (sample 4).
5. The silica gel was removed from the last impinger, immediately weighed, and the weight gain recorded.
6. Samples of acetone and distilled water were retained for blank analysis.

Particulate Sample Recovery for Analysis Type 3

The third particulate test sample per set of 3, designated for Analysis Type 3, was recovered in the manner described below.

At the conclusion of each test, the sampling trains were dismantled, openings sealed, and the components transported to the field laboratory.

A consistent procedure was employed for sample recovery:

1. The glass fiber filter(s) was removed from its holder with tweezers and placed in its original container (petri dish), along with any loose particulate and filter fragments (sample 1).
2. The probe and nozzle were separated and the internal particulate rinsed with acetone into a borosilicate container while brushing a minimum of three times. Particulate adhering to the brush was rinsed with acetone into the same container. The front-half of the filter holder, and connecting glassware were rinsed with acetone while brushing a minimum of three times. The rinses were added to the container and the container was then sealed with a Teflon-lined cap (sample 2).
3. Sampling train components in the aforementioned step were rinsed with methylene chloride and brushed in like manner into another borosilicate container with a Teflon-lined lid (sample 3).
4. The total liquid contents of impingers 1, 2, and 3 was measured and placed in a borosilicate container fitted with a Teflon-lined closure (sample 4). Also included in this sample was a distilled water rinse of the impingers and connectors.
5. The impingers and connectors were acetone washed into a separate borosilicate container fitted with a Teflon-lined lid (sample 5).
6. Components from the aforementioned step were methylene chloride washed into a separate borosilicate container fitted with a Teflon-lined lid (sample 6).
7. The silica gel was removed from the last impinger, immediately weighed, and the weight gain recorded.
8. Samples of acetone, methylene chloride, and distilled water were retained for blank analysis.

Sample Analysis Procedures

Analysis Type 1 (filterable and total particulate plus heavy metals content).

The particulate analysis proceeded as shown in Figure C-2 and as described below.

1. The filters (sample 1) and any loose fragments were desiccated for 24 hours and weighed to the nearest 0.1 milligram to a constant weight.
2. The front-half acetone wash samples (sample 2) were evaporated at ambient temperature and pressure in tared beakers, and desiccated to constant weight to the nearest 0.1 mg.
3. The back-half water wash samples (sample 3) and a distilled water blank were evaporated to dryness at $105^{\circ}\text{C} \pm 5^{\circ}\text{C}$ in tared beakers, cooled, then desiccated to constant 0.1 mg weight.
4. The back-half acetone wash samples (sample 4) and a blank were evaporated at ambient temperature and pressure in tared beakers, then desiccated to constant 0.1 mg weight.

After completion of the gravimetric particulate analysis the resultant "front-half" and "back-half" residues were combined then solubilized in acid/peroxide and analyzed for heavy metals content using inductively coupled plasma (ICP) spectrophotometry. (Perkin Elmer Model 5000).

Analysis Type 2 (filterable and total particulate plus nitrate, sulfate, and elemental analysis).

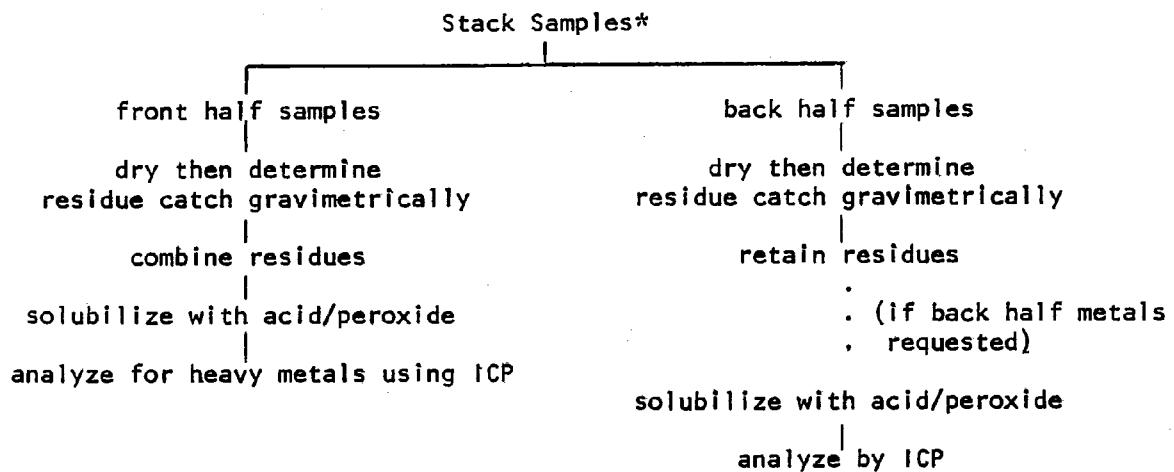
The sample analysis scheme is indicated in Figure C-3.

Since nitrate, sulfate, and elemental analysis of the particulate residues were planned, the particulate sample residues were split prior to gravimetric analysis. The procedures followed for gravimetric Analysis Type 2 samples are identical to those described under Analysis Type 1.

After completion of the gravimetric particulate analyses, one split sample was analyzed for nitrate and sulfate content using a Perkin-Elmer Series 2 High Performance Liquid Chromatograph equipped with a Vydac conductivity detector. The total carbon, hydrogen and nitrogen content of the remaining split sample was determined using a Perkin-Elmer Model 240-B Elemental analyzer.

Analysis Type 3 (filterable and total particulate plus extractable organics).

An analysis tree is shown in Figure C-4.



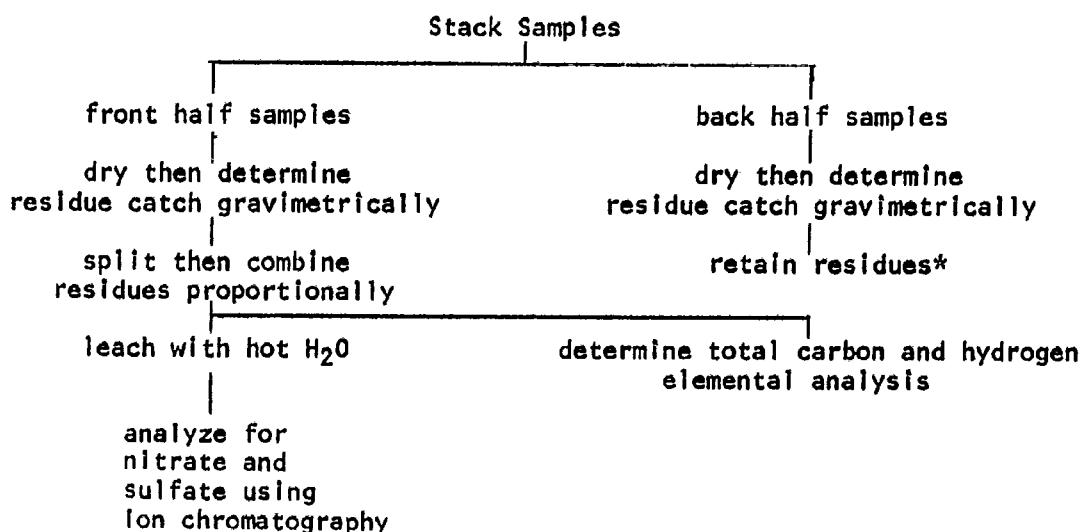
*Front half samples:

1. Acetone wash of nozzle, probe, and front half filter holder.
2. Filter catch.

Back half samples:

1. Impinger contents and water wash.
2. Acetone wash of impingers and connectors.

FIGURE C-2. ANALYSIS TREE FOR ANALYSIS TYPE 1



*Back half analysis if requested would follow that described for front half starting at the splitting step.

FIGURE C-3. ANALYSIS TREE FOR ANALYSIS TYPE 2

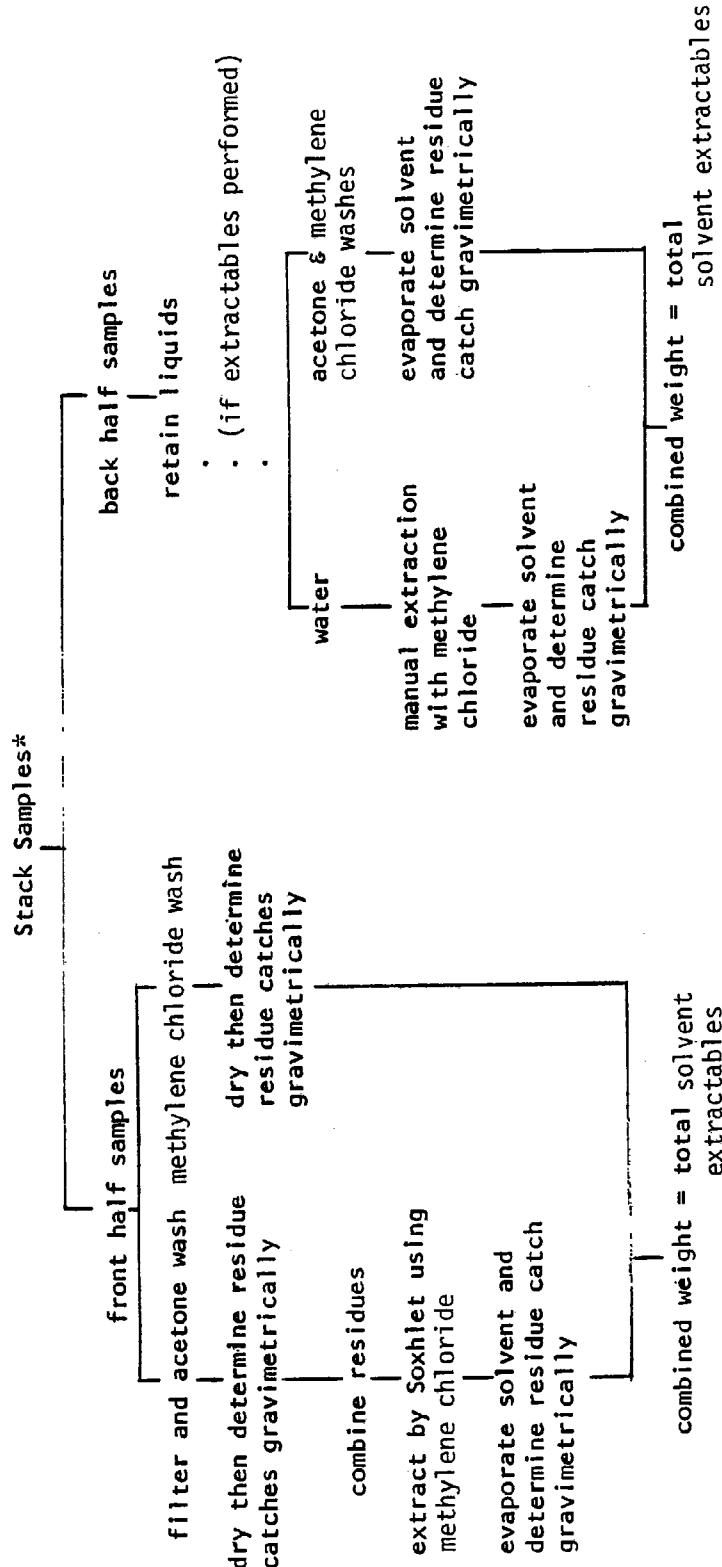


FIGURE C-4. ANALYSIS TREE FOR ANALYSIS TYPE 3

The particulate determination for Analysis Type 3 proceeded as follows.

1. The filters (sample 1) and any loose fragments were desiccated for 24 hours and weighed to the nearest 0.1 mg to a constant weight.
2. The front-half acetone and methylene chloride samples (samples 2 and 3) were evaporated at ambient temperature and pressure in tared beakers, and desiccated to constant weight to the nearest 0.1 mg.
3. The back-half impinger contents (sample 4) and wash were extracted with 75 mls of methylene chloride. The methylene chloride extract was then evaporated at ambient temperature and pressure in a tared beaker and desiccated to constant weight to the nearest 0.1 mg. The extracted impinger contents and wash were evaporated to dryness at 105°C in a tared beaker, cooled, then desiccated to constant 0.1 mg weight.
4. The back-half acetone and methylene chloride rinses (samples 5 and 6) plus blanks were evaporated at ambient temperature and pressure in tared beakers, and desiccated to constant weight to the nearest 0.1 mg.

After completion of the gravimetric particulate analyses, the "front-half" residues were combined, then methylene chloride extracted in a Soxhlet apparatus to determine solvent extractables.

Particle Size Distribution Measurement and Procedures

Test Equipment

The equipment utilized for particle size distribution measurements was an eight-stage Andersen Mark III Cascade Impactor. A stainless steel nozzle was connected directly to a preimpactor followed by an 8-stage Andersen Mark III Cascade Impactor which separated the particles according to their effective aerodynamic particle diameter. A solid Reeve Angel 934 AH glass fiber filter was used to capture any particles that passed through the impactor substrates to permit the measurement of total particulate. The filter holder was maintained at stack temperature, and was attached to a probe. Vacuum tubing joined the probe to the first of four Greenburg-Smith impingers which were included in the train to condense the moisture in the gas stream. All impingers were maintained in a crushed ice bath. An RAC or Nutech control console with vacuum pump, dry gas meter, a calibrated orifice, and inclined manometers completed the sampling train. See Figure C-5 for a schematic of the particle sizing apparatus.

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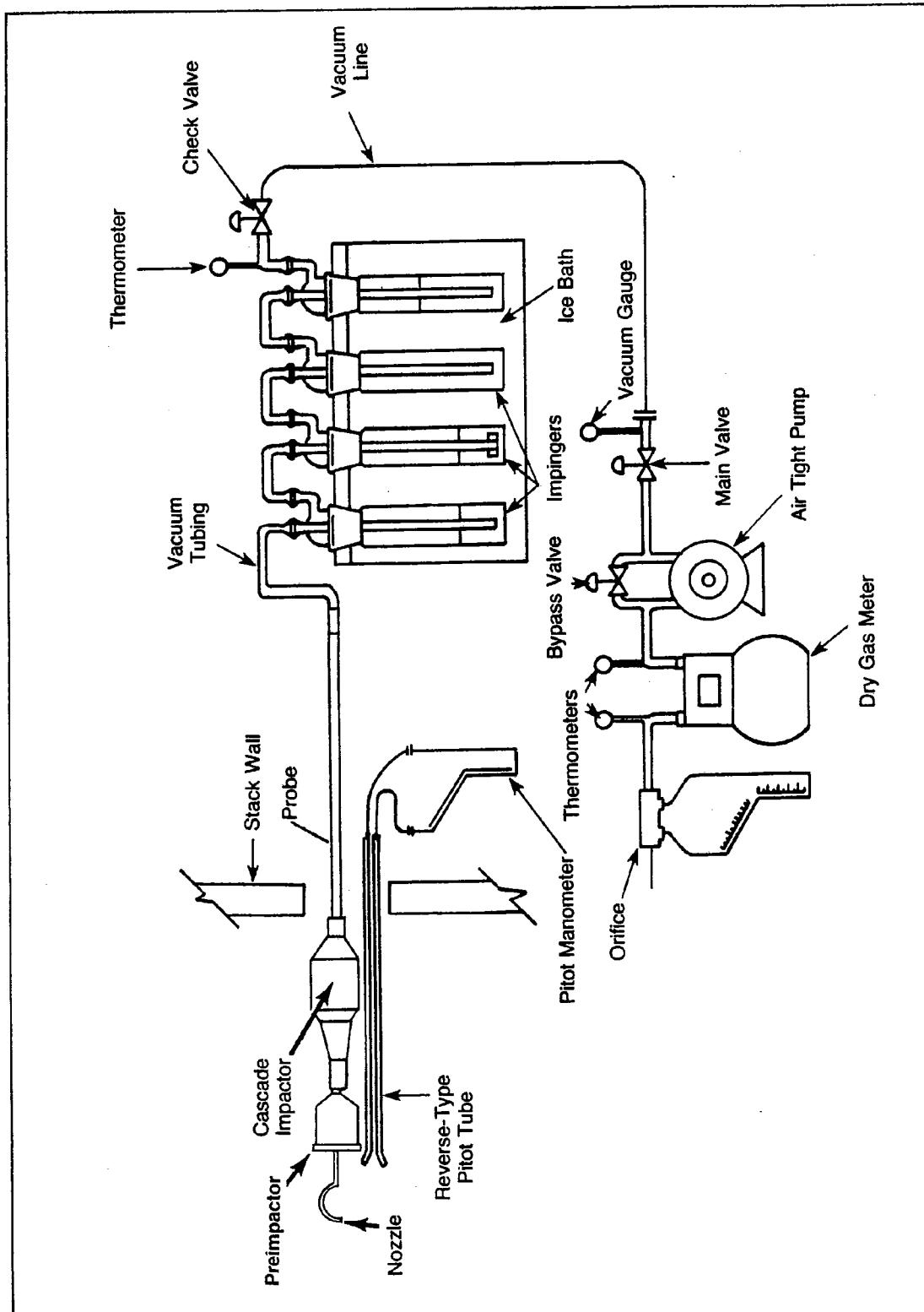


FIGURE C-5. PARTICLE SIZE DISTRIBUTION SAMPLING APPARATUS --
ANDERSEN 2000, INC.

Particle Size Distribution Test Procedures

During particle size distribution testing, gas stream velocities were measured by inserting a calibrated S-type pitot tube into the gas stream adjacent to the sampling nozzle. A point or points of average velocity were selected from preliminary test data and rechecked prior to formal sampling. The apparatus was positioned at a point or points of average gas stream velocity during each test. A constant isokinetic sampling rate was maintained for the duration of each test. Test length was dependent on particulate loading. During each test, sampling rates were monitored. Temperature readings at the final impinger and inlet and outlet of the dry test chamber were also recorded. All particle size distribution tests were run in conjunction with particulate tests except for the last 2 runs at Refinery A Source 1 which were performed independently.

Sample Recovery Procedures

At the conclusion of each test, the sampling trains were dismantled, openings sealed, and the components transported to the field laboratory.

A consistent procedure was employed for sample recovery.

1. The cascade impactor substrates and any loose fragments were carefully removed from their support plates with tweezers and placed in individual containers (petri dishes) for shipment to the Weston laboratories.
2. An acetone rinse of the nozzle, preimpactor, and cone of the impactor was performed.
3. Samples of acetone were retained for blank analysis.

Sample Analysis Procedures

The particle size distribution analysis proceeded as follows.

1. The cascade impactor substrates, back-up filters, and any loose fragments were desiccated for 24 hours, and weighed to the nearest 0.1 mg to constant weight.
2. Each acetone rinse sample and blank was evaporated at ambient temperature and pressure in a tared beaker, then desiccated to constant weight to the nearest 0.1 mg.

NO_x Measurement and Procedures

Test Equipment

The test train utilized for NO_x sampling was a standard EPA Method 7 Train (see Figure C-6).

A heated borosilicate gas sampling probe containing a glass wool filter was connected to a 2-liter borosilicate round-bottom boiling flask in a foam encasement. The flask was fitted with a glass 3-way valve. A mercury U-tube manometer was connected to the sample flask and to the vacuum pump of a Nutech control console by rubber vacuum tubing. Another 3-way valve was placed between the manometer and pump, and was connected to a squeeze bulb. The bulb was used to purge the sampling probe of extraneous gases prior to sample collection.

NO_x Test Procedures

During each particulate test run a series of three EPA Method 7 NO_x grab samples were obtained from the gas stream.

The heated probe was positioned near the center of the stack. The flask was evacuated to a pressure of less than three inches of mercury absolute. Flask temperature and pressure were recorded. After purging the probe with stack gas, the 3-way valve was positioned to allow a sample to enter the flask for fifteen seconds.

Sample Recovery Procedures

A consistent procedure for sample recovery was maintained throughout the test program.

After sitting for a minimum of sixteen hours, the flask and contents were shaken for two minutes. The final absolute flask temperatures and pressures were obtained and recorded and the flask contents were transferred to a leak-free polyethylene bottle. After the flask was rinsed twice with 5 ml portions of deionized distilled water and the rinses added to the bottle, the pH of the sample was adjusted to 9-12 by dropwise addition of sodium hydroxide (1N). The container was sealed, labeled, and the height of the liquid level marked. The samples, including a blank, were transported to the Weston Laboratories for analysis.

Sample Analysis Procedures

The samples were analyzed for oxides of nitrogen, except nitrous oxide, using the colorimetric phenoldisulfonic acid procedure described in EPA Method 7.

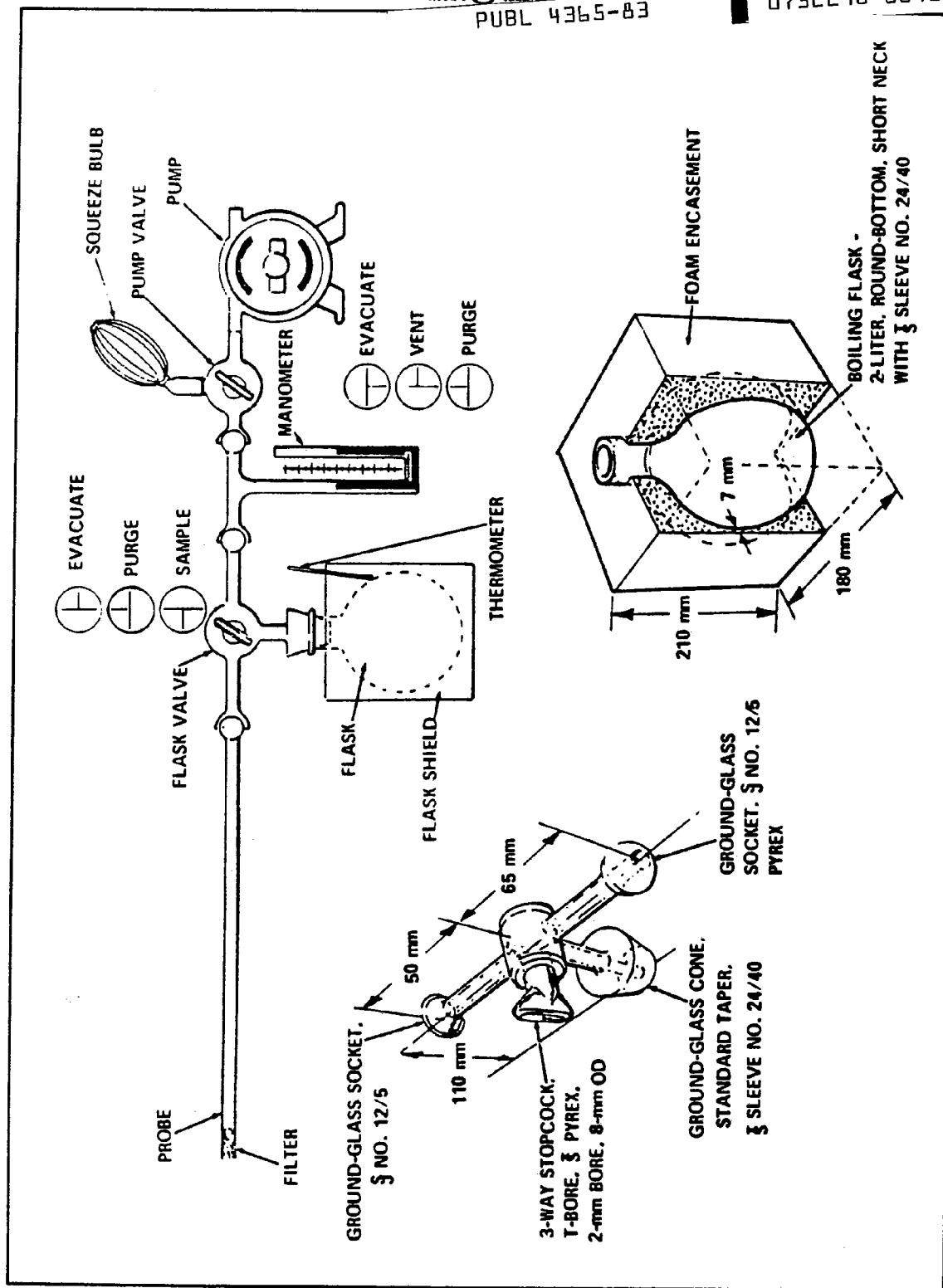


FIGURE C-6. NO. SAMPLING TRAIN
EPA METHOD 7

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APPENDIX D

WESTON PROJECT PARTICIPANTS



PROJECT PARTICIPANTS

The following Weston employees participated in this project.

| | |
|--|---------------------------|
| Peter J. Marks Vice President and Project Director Laboratory Services | econENVIRONomics Division |
| Barry L. Jackson Project Manager Air Quality Testing Services | econENVIRONomics Division |
| Jeffrey D. O'Neill Project Scientist | econENVIRONomics Division |
| Paul Meeter Assistant Project Scientist | econENVIRONomics Division |
| Thomas Davis Project Technician | econENVIRONomics Division |
| James S. Smith, Ph.D. Director Analytical Laboratory | econENVIRONomics Division |
| Dianne S. Therry Quality Assurance Coordinator | econENVIRONomics Division |
| Bruce Maglietto Chemist | econENVIRONomics Division |
| Kim Burke Chemist | econENVIRONomics Division |
| Ken Seace Chemist | econENVIRONomics Division |
| Nancy Robertson Senior Laboratory Technician | econENVIRONomics Division |
| Bruce Wood Instrument Maintenance Technician | econENVIRONomics Division |
| Marie Nadeau Technical Support | econENVIRONomics Division |