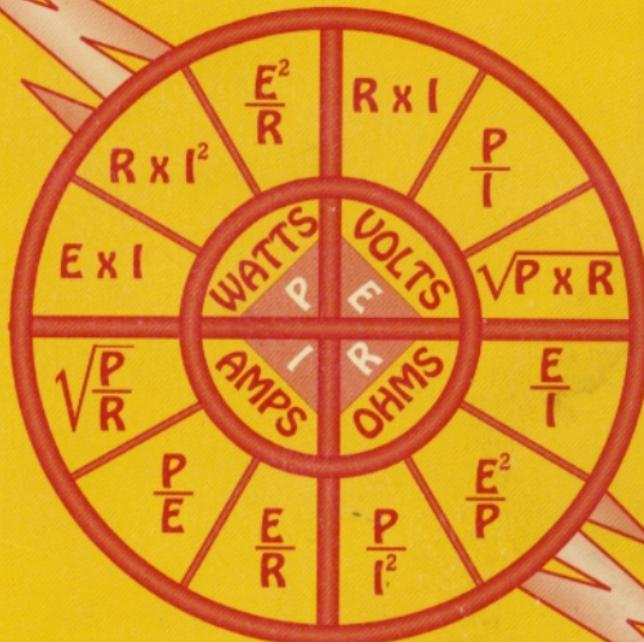


UGLY'S™ ELECTRICAL REFERENCES



REVISED 2005 EDITION

BY
GEORGE V. HART

EDITED BY
WILLIAM C. BUCHANAN



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UGLY'S™ ELECTRICAL REFERENCES

by
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and
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Editor

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OHM'S LAW

The rate of the flow of the current is equal to electromotive force divided by resistance.

I = Intensity of Current = Amperes

E = Electromotive Force = Volts

R = Resistance = Ohms

P = Power = Watts

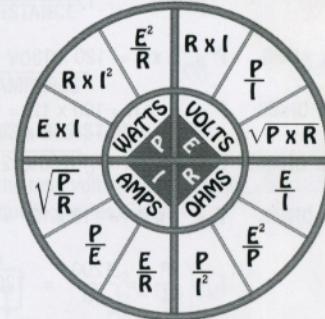
The three basic Ohm's law formulas are:

$$I = \frac{E}{R}$$

$$R = \frac{E}{I}$$

$$E = I \times R$$

Below is a chart containing the formulas related to Ohm's law. To use the chart, from the center circle, select the value you need to find, I (Amps), R (Ohms), E (Volts) or P (Watts). Then select the formula containing the values you know from the corresponding chart quadrant.



Example:

An electric appliance is rated at 1200 Watts, and is connected to 120 Volts. How much current will it draw?

$$\text{Amperes} = \frac{\text{Watts}}{\text{Volts}} \quad I = \frac{P}{E} \quad I = \frac{1200}{120} = 10 \text{ A}$$

What is the Resistance of the same appliance?

$$\text{Ohms} = \frac{\text{Volts}}{\text{Amperes}} \quad R = \frac{E}{I} \quad R = \frac{120}{10} = 12 \Omega$$

OHM'S LAW

In the preceding example, we know the following values:

$$I = \text{amps} = 10$$

$$R = \text{ohms} = 12\Omega$$

$$E = \text{volts} = 120$$

$$P = \text{watts} = 1200$$

We can now see how the twelve formulas in the Ohm's Law chart can be applied.

$$\text{AMPS} = \sqrt{\frac{\text{WATTS}}{\text{OHMS}}}$$

$$I = \sqrt{\frac{P}{R}} = \sqrt{\frac{1200}{12}} = \sqrt{100} = 10\text{A}$$

$$\text{AMPS} = \frac{\text{WATTS}}{\text{VOLTS}}$$

$$I = \frac{P}{E} = \frac{1200}{120} = 10\text{A}$$

$$\text{AMPS} = \frac{\text{VOLTS}}{\text{OHMS}}$$

$$I = \frac{E}{R} = \frac{120}{12} = 10\text{A}$$

$$\text{WATTS} = \frac{\text{VOLTS}^2}{\text{OHMS}}$$

$$P = \frac{E^2}{R} = \frac{120^2}{12} = \frac{14,400}{12} = 1200\text{W}$$

$$\text{WATTS} = \text{VOLTS} \times \text{AMPS} \quad P = E \times I = 120 \times 10 = 1200\text{W}$$

$$\text{WATTS} = \text{AMPS}^2 \times \text{OHMS} \quad P = I^2 \times R = 100 \times 12 = 1200\text{W}$$

$$\text{VOLTS} = \sqrt{\text{WATTS} \times \text{OHMS}} \quad E = \sqrt{P \times R} = \sqrt{1200 \times 12} = \sqrt{14,400} = 120\text{V}$$

$$\text{VOLTS} = \text{AMPS} \times \text{OHMS} \quad E = I \times R = 10 \times 12 = 120\text{V}$$

$$\text{VOLTS} = \frac{\text{WATTS}}{\text{AMPS}} \quad E = \frac{P}{I} = \frac{1200}{10} = 120\text{V}$$

$$\text{OHMS} = \frac{\text{VOLTS}^2}{\text{WATTS}} \quad R = \frac{E^2}{P} = \frac{120^2}{1,200} = \frac{14,400}{1,200} = 12\Omega$$

$$\text{OHMS} = \frac{\text{WATTS}}{\text{AMPS}^2} \quad R = \frac{P}{I^2} = \frac{1200}{100} = 12\Omega$$

$$\text{OHMS} = \frac{\text{VOLTS}}{\text{AMPS}} \quad R = \frac{E}{I} = \frac{120}{10} = 12\Omega$$

SERIES CIRCUITS

A SERIES CIRCUIT is a circuit that has only one path through which the electrons may flow.

RULE 1: The total current in a series circuit is equal to the current in any other part of the circuit.

$$\text{TOTAL CURRENT } I_T = I_1 = I_2 = I_3, \text{ etc.}$$

RULE 2: The total voltage in a series circuit is equal to the sum of the voltages across all parts of the circuit.

$$\text{TOTAL VOLTAGE } E_T = E_1 + E_2 + E_3, \text{ etc.}$$

RULE 3: The total resistance of a series circuit is equal to the sum of the resistances of all the parts of the circuit

$$\text{TOTAL RESISTANCE } R_T = R_1 + R_2 + R_3, \text{ etc.}$$

FORMULAS FROM OHM'S LAW

$$\text{AMPERES} = \frac{\text{VOLTS}}{\text{RESISTANCE}}$$

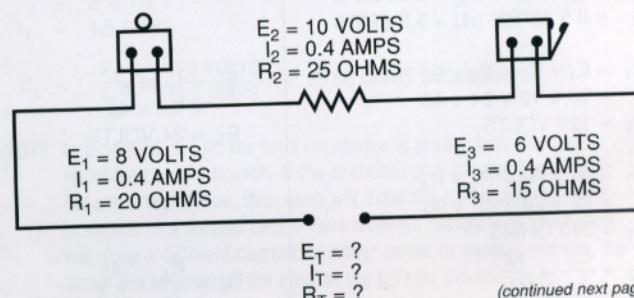
$$\text{OR} \quad I = \frac{E}{R}$$

$$\text{RESISTANCE} = \frac{\text{VOLTS}}{\text{AMPERES}}$$

$$\text{OR} \quad R = \frac{E}{I}$$

$$\text{VOLTS} = \text{AMPERES} \times \text{RESISTANCE} \quad \text{OR} \quad E = I \times R$$

EXAMPLE: Find the total voltage, total current, and total resistance of the following series circuit.



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SERIES CIRCUITS

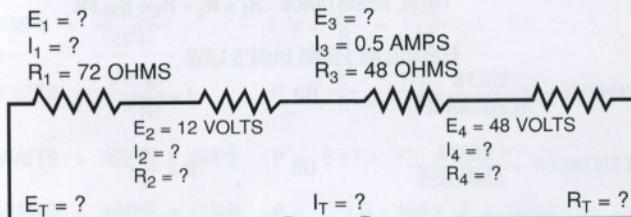
$$\begin{aligned} E_T &= E_1 + E_2 + E_3 \\ &= 8 + 10 + 6 \\ E_T &= 24 \text{ VOLTS} \end{aligned}$$

$$\begin{aligned} I_T &= I_1 = I_2 = I_3 \\ &= 0.4 = 0.4 = 0.4 \\ I_T &= 0.4 \text{ AMPS} \end{aligned}$$

$$\begin{aligned} R_T &= R_1 + R_2 + R_3 \\ &= 20 + 25 + 15 \\ R_T &= 60 \text{ OHMS} \end{aligned}$$

EXAMPLE: Find E_T , E_1 , E_3 , I_T , I_1 , I_2 , I_4 , R_T , R_2 , AND R_4 .

Remember that the total current in a series circuit is equal to the current in any other part of the circuit.



$$\begin{aligned} I_T &= I_1 = I_2 = I_3 = I_4 \\ I_T &= I_1 = I_2 = 0.5 = I_4 \\ 0.5 &= 0.5 = 0.5 = 0.5 = 0.5 \\ I_T &= 0.5 \text{ AMPERS} \quad I_2 = 0.5 \text{ AMPERS} \\ I_1 &= 0.5 \text{ AMPERS} \quad I_4 = 0.5 \text{ AMPERS} \end{aligned}$$

$$\begin{aligned} E_T &= E_1 + E_2 + E_3 + E_4 \\ &= 36 + 12 + 24 + 48 \\ E_T &= 120 \text{ VOLTS} \end{aligned}$$

$$\begin{aligned} R_T &= R_1 + R_2 + R_3 + R_4 \\ &= 72 + 24 + 48 + 96 \end{aligned}$$

$$R_T = 240 \text{ OHMS}$$

$$\begin{aligned} R_2 &= \frac{E_2}{I_2} = \frac{12}{0.5} \\ R_2 &= 24 \text{ OHMS} \end{aligned}$$

$$\begin{aligned} E_1 &= I_1 \times R_1 \\ &= 0.5 \times 72 \\ E_1 &= 36 \text{ VOLTS} \end{aligned}$$

$$\begin{aligned} E_3 &= I_3 \times R_3 \\ &= 0.5 \times 48 \\ E_3 &= 24 \text{ VOLTS} \end{aligned}$$

$$\begin{aligned} R_4 &= \frac{E_4}{I_4} = \frac{48}{0.5} \\ R_4 &= 96 \text{ OHMS} \end{aligned}$$

PARALLEL CIRCUITS

A PARALLEL CIRCUIT is a circuit that has more than one path through which the electrons may flow.

RULE 1: The total current in a parallel circuit is equal to the sum of the currents in all the branches of the circuit.

$$\text{TOTAL CURRENT } I_T = I_1 + I_2 + I_3, \text{ etc.}$$

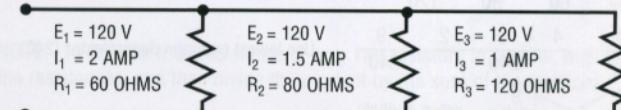
RULE 2: The total voltage across any branch in parallel is equal to the voltage across any other branch and is also equal to the total voltage.

$$\text{TOTAL VOLTAGE } E_T = E_1 = E_2 = E_3, \text{ etc.}$$

RULE 3: The total resistance of a parallel circuit is found by applying OHM'S LAW to the total values of the circuit.

$$\text{TOTAL RESISTANCE} = \frac{\text{TOTAL VOLTAGE}}{\text{TOTAL AMPERES}} \quad \text{OR} \quad R_T = \frac{E_T}{I_T}$$

Example: Find the total current, total voltage, and total resistance of the following parallel circuit.



$$\begin{aligned} I_T &= I_1 + I_2 + I_3 \\ &= 2 + 1.5 + 1 \\ I_T &= 4.5 \text{ AMPERS} \end{aligned} \quad \begin{aligned} E_T &= E_1 = E_2 = E_3 \\ &= 120 = 120 = 120 \\ E_T &= 120 \text{ VOLTS} \end{aligned}$$

$$R_T = \frac{E_T}{I_T} = \frac{120 \text{ VOLTS}}{4.5 \text{ AMPERS}} = 26.66 \text{ OHMS RESISTANCE}$$

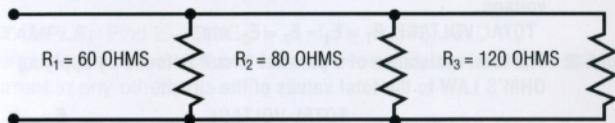
NOTE: In a parallel circuit, the total resistance is always less than the resistance of any branch. If the branches of a parallel circuit have the same resistance, then each will draw the same current. If the branches of a parallel circuit have different resistances, then each will draw a different current. In either series or parallel circuits, the larger the resistance, the smaller the current drawn.

PARALLEL CIRCUITS

To determine the total resistance in a parallel circuit when the total current and total voltage are unknown:

$$\frac{1}{\text{TOTAL RESISTANCE}} = \frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3} \quad \text{AND ETC.}$$

EXAMPLE: Find the total resistance of the following circuit:



$$\frac{1}{R_T} = \frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3}$$

$$\frac{1}{R_T} = \frac{1}{60} + \frac{1}{80} + \frac{1}{120}$$

$$\frac{1}{R_T} = \frac{4 + 3 + 2}{240} = \frac{9}{240} \quad \text{Use lowest common denominator (240).}$$

$$\frac{1}{R_T} = \frac{9}{240} \quad \text{cross multiply.}$$

$$9 \times R_T = 1 \times 240 \quad \text{or} \quad 9R_T = 240$$

divide both sides of the equation by 9

$$R_T = 26.66 \text{ OHMS RESISTANCE}$$

NOTE: The total resistance of a number of EQUAL resistors in parallel is equal to the resistance of one resistor divided by the number of resistors.

$$\text{TOTAL RESISTANCE} = \frac{\text{RESISTANCE OF ONE RESISTOR}}{\text{NUMBER OF RESISTORS IN CIRCUIT}}$$

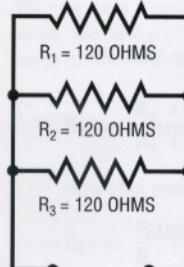
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PARALLEL CIRCUITS

FORMULA:

$$R_T = \frac{R}{N}$$

EXAMPLE: Find the total resistance



There are three resistors in parallel. Each has a value of 120 OHMS resistance. According to the formula, if we divide the resistance of any one of the resistors by three, we will obtain the total resistance of the circuit.

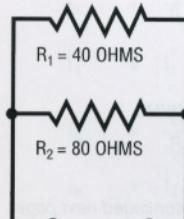
$$R_T = \frac{R}{N} \quad \text{OR} \quad R_T = \frac{120}{3}$$

$$\text{TOTAL RESISTANCE} = 40 \text{ OHMS.}$$

NOTE: To find the total resistance of only two resistors in parallel, multiply the resistances, and then divide the product by the sum of the resistors.

$$\text{FORMULA: TOTAL RESISTANCE} = \frac{R_1 \times R_2}{R_1 + R_2}$$

EXAMPLE:



$$R_T = \frac{R_1 \times R_2}{R_1 + R_2}$$

$$= \frac{40 \times 80}{40 + 80}$$

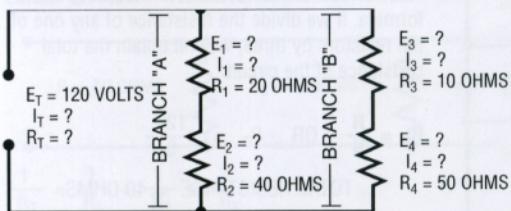
$$R_T = \frac{3200}{120} = 26.66 \text{ OHMS}$$

COMBINATION CIRCUITS

In combination circuits, we combine series circuits with parallel circuits. Combination circuits make it possible to obtain the different voltages of series circuits, and the different currents of parallel circuits.

EXAMPLE 1. PARALLEL-SERIES CIRCUIT:

Solve for all missing values.



TO SOLVE:

- Find the total resistance of each branch. Both branches are simple series circuits, so

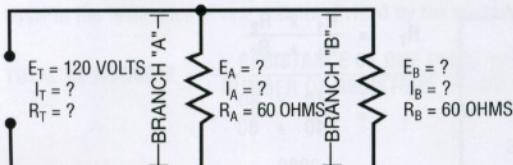
$$R_1 + R_2 = R_A$$

20 + 40 = 60 OHMS total resistance of branch "A"

$$R_3 + R_4 = R_B$$

10 + 50 = 60 OHMS total resistance of branch "B"

- Re-draw the circuit, combining resistors ($R_1 + R_2$) and ($R_3 + R_4$) so that each branch will have only one resistor.



(continued next page)

COMBINATION CIRCUITS

NOTE: We now have a simple parallel circuit, so

$$\begin{aligned} E_T &= E_A &= E_B \\ 120 \text{ V} &= 120 \text{ V} &= 120 \text{ V} \end{aligned}$$

We now have a parallel circuit with only two resistors, and they are of equal value. We have a choice of three different formulas that can be used to solve for the total resistance of the circuit.

$$(1) \quad R_T = \frac{R_A \times R_B}{R_A + R_B} = \frac{60 \times 60}{60 + 60} = \frac{3600}{120} = 30 \text{ OHMS}$$

- When the resistors of a parallel circuit are of equal value,

$$R_T = \frac{R}{N} = \frac{60}{2} = 30 \text{ OHMS} \quad \text{OR}$$

$$(3) \quad \frac{1}{R_T} = \frac{1}{R_A} + \frac{1}{R_B} = \frac{1}{60} + \frac{1}{60} = \frac{2}{60} = \frac{1}{30}$$

$$\frac{1}{R_T} = \frac{1}{30} \quad \text{OR} \quad 1 \times R_T = 1 \times 30 \quad \text{OR} \quad R_T = 30 \text{ OHMS}$$

- We know the values of E_T , R_T , E_A , R_A , E_B , R_B , R_1 , R_2 , R_3 , and R_4 . Next we will solve for I_T , I_A , I_B , I_1 , I_2 , I_3 , and I_4 .

$$I_T = \frac{E_T}{R_T} \quad \text{OR} \quad \frac{120}{30} = 4 \quad I_T = 4 \text{ AMPS}$$

$$I_A = \frac{E_A}{R_A} \quad \text{OR} \quad \frac{120}{60} = 2 \quad I_A = 2 \text{ AMPS}$$

$$I_A = I_1 = I_2 \quad \text{OR} \quad 2 = 2 = 2 \quad I_1 = 2 \text{ AMPS}$$

$$I_B = \frac{E_B}{R_B} = \frac{120}{60} = 2 \quad I_B = 2 \text{ AMPS}$$

$$I_B = I_3 = I_4 \quad \text{OR} \quad 2 = 2 = 2 \quad I_3 = 2 \text{ AMPS} \\ I_4 = 2 \text{ AMPS}$$

(continued next page)

COMBINATION CIRCUITS

4. We know that resistors #1 and #2 of branch "A" are in series. We know too that resistors #3 and #4 of branch "B" are in series. We have determined that the total current of branch "A" is 2 AMPS, and the total current of branch "B" is 2 AMPS. By using the series formula, we can solve for the current of each branch.

BRANCH "A"

$$\begin{aligned} I_A &= I_1 = I_2 \\ 2 &= 2 = 2 \\ I_1 &= 2 \text{ AMPS} \\ I_2 &= 2 \text{ AMPS} \end{aligned}$$

BRANCH "B"

$$\begin{aligned} I_B &= I_3 = I_4 \\ 2 &= 2 = 2 \\ I_3 &= 2 \text{ AMPS} \\ I_4 &= 2 \text{ AMPS} \end{aligned}$$

5. We were given the resistance values of all resistors.

$R_1 = 20 \text{ OHMS}$, $R_2 = 40 \text{ OHMS}$, $R_3 = 10 \text{ OHMS}$, and $R_4 = 50 \text{ OHMS}$. By using OHM'S Law, we can determine the voltage drop across each resistor.

$$\begin{aligned} E_1 &= R_1 \times I_1 \\ &= 20 \times 2 \\ E_1 &= 40 \text{ VOLTS} \end{aligned}$$

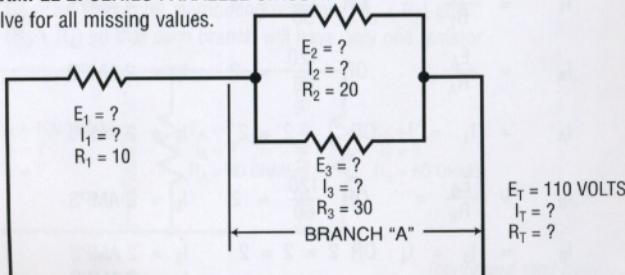
$$\begin{aligned} E_2 &= R_2 \times I_2 \\ &= 40 \times 2 \\ E_2 &= 80 \text{ VOLTS} \end{aligned}$$

$$\begin{aligned} E_3 &= R_3 \times I_3 \\ &= 10 \times 2 \\ E_3 &= 20 \text{ VOLTS} \end{aligned}$$

$$\begin{aligned} E_4 &= R_4 \times I_4 \\ &= 50 \times 2 \\ E_4 &= 100 \text{ VOLTS} \end{aligned}$$

EXAMPLE 2: SERIES PARALLEL CIRCUIT.

Solve for all missing values.



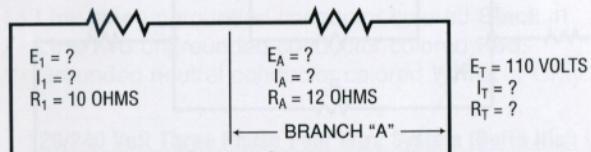
COMBINATION CIRCUITS

To solve:

1. We can see that resistors #2 and #3 are in parallel, and combined they are branch "A". When there are only two resistors, we use the following formula:

$$R_A = \frac{R_2 \times R_3}{R_2 + R_3} \text{ OR } \frac{20 \times 30}{20 + 30} \text{ OR } \frac{600}{50} \text{ OR } 12 \text{ OHMS}$$

2. We can now re-draw our circuit as a simple series circuit.



3. In a series circuit,
 $R_T = R_1 + R_A$ OR $R_T = 10 + 12$ OR 22 OHMS
 By using OHM'S Law,
 $I_T = \frac{E_T}{R_T} = \frac{110}{22} = 5 \text{ AMPS}$

In a series circuit,
 $I_T = I_1 = I_A$ or $I_T = 5 \text{ AMPS}$, $I_1 = 5 \text{ AMPS}$, and $I_A = 5 \text{ AMPS}$

By using OHM'S Law,
 $E_1 = I_1 \times R_1 = 5 \times 10 = 50 \text{ VOLTS}$
 $E_T - E_1 = E_A$ or $110 - 50 = 60 \text{ VOLTS} = E_A$

In a parallel circuit,
 $E_A = E_2 = E_3$ or $E_A = 60 \text{ VOLTS}$
 $E_2 = 60 \text{ VOLTS}$, and $E_3 = 60 \text{ VOLTS}$

By using OHM'S Law,
 $I_2 = \frac{E_2}{R_2} = \frac{60}{20} = 3 \text{ AMPS}$
 $I_3 = \frac{E_3}{R_3} = \frac{60}{30} = 2 \text{ AMPS}$

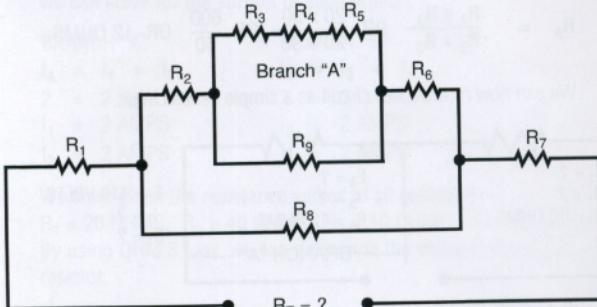
COMBINATION CIRCUITS

PROBLEM:

Solve for total resistance.

Re-draw circuit as many times as necessary.

Correct answer is 100 OHMS.



$$R_T = ?$$

GIVEN VALUES:

$$R_1 = 15 \text{ OHMS}$$

$$R_2 = 35 \text{ OHMS}$$

$$R_3 = 50 \text{ OHMS}$$

$$R_4 = 40 \text{ OHMS}$$

$$R_5 = 30 \text{ OHMS}$$

$$R_6 = 25 \text{ OHMS}$$

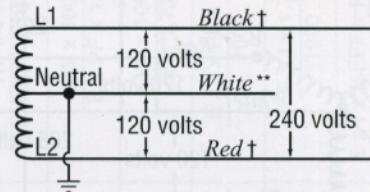
$$R_7 = 10 \text{ OHMS}$$

$$R_8 = 300 \text{ OHMS}$$

$$R_9 = 60 \text{ OHMS}$$

COMMON ELECTRICAL DISTRIBUTION SYSTEMS

120/240 Volt Single Phase Three Wire System

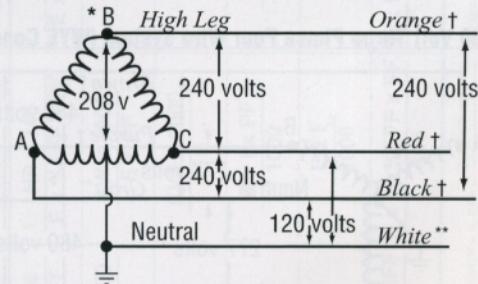


† • Line one ungrounded conductor colored **Black**.

† • Line two ungrounded conductor colored **Red**.

** Grounded neutral conductor colored **White** or Gray.

120/240 Volt Three Phase Four Wire System (Delta High Leg)



† • A phase ungrounded conductor colored **Black**.

†* • B phase ungrounded conductor colored **Orange** or tagged (High Leg). (Caution - 208V Orange to White)

† • C phase ungrounded conductor colored **Red**.

** • Grounded conductor colored **White** or Gray. (Center tap)

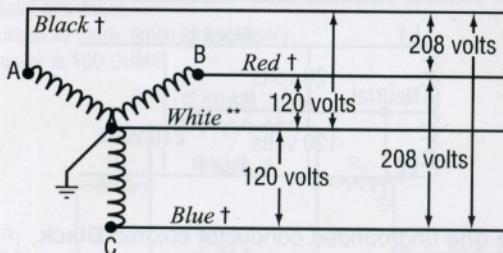
** Grounded conductors are required to be white or gray or three white stripes. See NEC 200.6A.

* B phase of high leg delta must be Orange or tagged.

† Ungrounded conductor colors may be other than shown; see local ordinances or specifications.

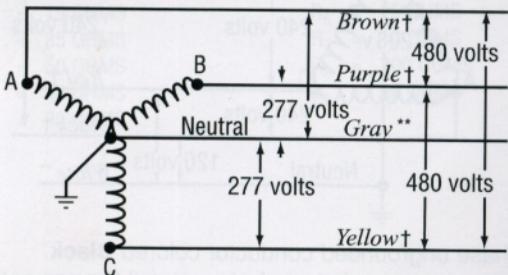
COMMON ELECTRICAL DISTRIBUTION SYSTEMS

120/208 Volt Three Phase Four Wire System (WYE Connected)



- † A phase ungrounded conductor colored **Black**.
- † B phase ungrounded conductor colored **Red**.
- † C phase ungrounded conductor colored **Blue**.
- ** Grounded neutral conductor colored **White** or **Gray**.

277/480 Volt Three Phase Four Wire System (WYE Connected)



- † A phase ungrounded conductor colored **Brown**.
- † B phase ungrounded conductor colored **Purple**.
- † C phase ungrounded conductor colored **Yellow**.
- ** Grounded neutral conductor colored **Gray**.

^{**} Grounded conductors are required to be white or gray or three white stripes. See NEC 200.6A.
^{*B} Phase of high leg delta must be Orange or tagged.
[†] Ungrounded conductor colors may be other than shown; see local ordinances or specifications.

ELECTRICAL FORMULAS FOR CALCULATING AMPERES, HORSEPOWER, KILOWATTS AND KVA

| TO FIND | ALTERNATING CURRENT | | |
|---|--|--|--|
| | DIRECT CURRENT | SINGLE PHASE | TWO PHASE-FOUR WIRE |
| AMPERES WHEN "HP" IS KNOWN | $\frac{HP \times 746}{E \times \%EFF}$ | $\frac{HP \times 746}{E \times \%EFF \times PF}$ | $\frac{HP \times 746}{E \times \%EFF \times PF \times 1.73}$ |
| AMPERES WHEN "KW" IS KNOWN | $\frac{KW \times 1000}{E \times PF}$ | $\frac{KW \times 1000}{E \times PF \times 2}$ | $\frac{KW \times 1000}{E \times PF \times 1.73}$ |
| AMPERES WHEN "KVA" IS KNOWN | $\frac{KVA \times 1000}{E \times 2}$ | $\frac{KVA \times 1000}{E \times 2}$ | $\frac{KVA \times 1000}{E \times 1.73}$ |
| KILOWATTS (True Power) | $\frac{E \times I}{1000}$ | $\frac{E \times I \times PF \times 2}{1000}$ | $\frac{E \times I \times PF \times 1.73}{1000}$ |
| KILOVOLT-AMPERES "KVA" (Apparent Power) | $\frac{E \times I \times \%EFF}{746}$ | $\frac{E \times I \times \%EFF \times PF}{746}$ | $\frac{E \times I \times \%EFF \times PF \times 2}{746}$ |
| HORSEPOWER | $\frac{E \times I \times \%EFF}{746}$ | $\frac{E \times I \times \%EFF \times PF}{746}$ | $\frac{E \times I \times \%EFF \times PF \times 1.73}{746}$ |

$$\text{PERCENT EFFICIENCY} = \%EFF = \frac{\text{OUTPUT (WATTS)}}{\text{INPUT (WATTS)}}$$

$$\text{POWER FACTOR} = PF = \frac{\text{POWER USED (WATTS)}}{\text{APPARENT POWER}} = \frac{KW}{KVA}$$

NOTE: DIRECT CURRENT FORMULAS DO NOT USE (PF, 2, OR 1.73)
 SINGLE PHASE FORMULAS DO NOT USE (2 OR 1.73)
 TWO PHASE - FOUR WIRE FORMULAS DO NOT USE (1.73)
 THREE PHASE FORMULAS DO NOT USE (2)

TO FIND AMPERES

DIRECT CURRENT:

A. When HORSEPOWER is known:

$$\text{AMPERES} = \frac{\text{HORSEPOWER} \times 746}{\text{VOLTS} \times \text{EFFICIENCY}} \quad \text{or} \quad I = \frac{\text{HP} \times 746}{E \times \% \text{EFF}}$$

What current will a travel-trailer toilet draw when equipped with a 12-volt, 1/8 HP motor, having a 96% efficiency rating?

$$I = \frac{\text{HP} \times 746}{E \times \% \text{EFF}} = \frac{746 \times 1/8}{12 \times 0.96} = \frac{93.25}{11.52} = 8.09 \text{ AMPS}$$

B. When KILOWATTS are known:

$$\text{AMPERES} = \frac{\text{KILOWATTS} \times 1000}{\text{VOLTS}} \quad \text{or} \quad I = \frac{\text{KW} \times 1000}{E}$$

A 75 KW, 240 Volt, direct current generator is used to power a variable-speed conveyor belt at a rock crushing plant. Determine the current.

$$I = \frac{\text{KW} \times 1000}{E} = \frac{75 \times 1000}{240} = 312.5 \text{ AMPS}$$

SINGLE PHASE:

A. When WATTS, VOLTS, AND POWER FACTOR are known:

$$\text{AMPERES} = \frac{\text{WATTS}}{\text{VOLTS} \times \text{POWER FACTOR}} \quad \text{or} \quad I = \frac{P}{E \times PF}$$

Determine the current when a circuit has a 1500 watt load, a power-factor of 86%, and operates from a single-phase 230 volt source.

$$I = \frac{1500}{230 \times 0.86} = \frac{1500}{197.8} = 7.58 \text{ AMPS}$$

TO FIND AMPERES

SINGLE PHASE:

B. When HORSEPOWER is known:

$$\text{AMPERES} = \frac{\text{HORSEPOWER} \times 746}{\text{VOLTS} \times \text{EFFICIENCY} \times \text{POWER-FACTOR}}$$

Determine the amp-load of a single-phase, 1/2 HP, 115 volt motor. The motor has an efficiency rating of 92%, and a power-factor of 80%.

$$I = \frac{\text{HP} \times 746}{E \times \% \text{EFF} \times PF} = \frac{1/2 \times 746}{115 \times 0.92 \times 0.80} = \frac{373}{84.64}$$

$$I = 4.4 \text{ AMPS}$$

C. When KILOWATTS are known:

$$\text{AMPERES} = \frac{\text{KILOWATTS} \times 1000}{\text{VOLTS} \times \text{POWER-FACTOR}} \quad \text{or} \quad I = \frac{\text{KW} \times 1000}{E \times PF}$$

A 230 Volt single-phase circuit has a 12KW power load, and operates at 84% power-factor. Determine the current.

$$I = \frac{\text{KW} \times 1000}{E \times PF} = \frac{12 \times 1000}{230 \times 0.84} = \frac{12,000}{193.2} = 62 \text{ AMPS}$$

D. When KILOVOLT-AMPERE is known:

$$\text{AMPERES} = \frac{\text{KILOVOLT-AMPERE} \times 1000}{\text{VOLTS}} \quad \text{or} \quad I = \frac{\text{KVA} \times 1000}{E}$$

A 115 volt, 2 KVA, single-phase generator operating at full load will deliver 17.4 AMPERES. (Prove.)

$$I = \frac{2 \times 1000}{115} = \frac{2000}{115} = 17.4 \text{ AMPS}$$

REMEMBER:

By definition, amperes is the rate of the flow of the current.

TO FIND AMPERES

THREE PHASE:

A. When WATTS, VOLTS, AND POWER FACTOR are known:

$$\text{AMPERES} = \frac{\text{WATTS}}{\text{VOLTS} \times \text{POWER-FACTOR} \times 1.73}$$

$$\text{or } I = \frac{P}{E \times PF \times 1.73}$$

Determine the current when a circuit has a 1500 watt load, a power factor of 86%, and operates from a three-phase, 230 volt source.

$$I = \frac{P}{E \times PF \times 1.73} = \frac{1500}{230 \times 0.86 \times 1.73} = \frac{1500}{342.2}$$

$$I = 4.4 \text{ AMPS}$$

B. When HORSEPOWER is known:

$$\text{AMPERES} = \frac{\text{HORSEPOWER} \times 746}{\text{VOLTS} \times \text{EFFICIENCY} \times \text{POWER-FACTOR} \times 1.73}$$

$$\text{or } I = \frac{HP \times 746}{E \times \%EFF \times PF \times 1.73}$$

Determine the amp-load of a three-phase, 1/2 HP, 230 volt motor. The motor has an efficiency rating of 92%, and a power-factor of 80%.

$$I = \frac{HP \times 746}{E \times \%EFF \times PF \times 1.73} = \frac{1/2 \times 746}{230 \times .92 \times .80 \times 1.73}$$

$$= \frac{373}{293} = 1.27 \text{ AMPS}$$

TO FIND AMPERES

THREE PHASE:

C. When KILOWATTS are known:

$$\text{AMPERES} = \frac{\text{KILOWATTS} \times 1000}{\text{VOLTS} \times \text{POWER-FACTOR} \times 1.73}$$

$$\text{or } I = \frac{KW \times 1000}{E \times PF \times 1.73}$$

A 230 volt, three-phase circuit, has a 12KW power load, and operates at 84% power-factor. Determine the current.

$$I = \frac{KW \times 1000}{E \times PF \times 1.73} = \frac{12,000}{230 \times 0.84 \times 1.73} = \frac{12,000}{334.24}$$

$$I = 36 \text{ AMPS}$$

D. When KILOVOLT-AMPERE is known:

$$\text{AMPERES} = \frac{\text{KILOVOLT-AMPERE} \times 1000}{E \times 1.73} = \frac{\text{KVA} \times 1000}{E \times 1.73}$$

A 230 Volt, 4 KVA, three-phase generator operating at full load will deliver 10 AMPERES. (Prove.)

$$I = \frac{\text{KVA} \times 1000}{E \times 1.73} = \frac{4 \times 1000}{230 \times 1.73} = \frac{4000}{397.9}$$

$$I = 10 \text{ AMPS}$$

NOTE: To better understand the preceding formulas:

1. TWO-PHASE CURRENT $\times 2$ = SINGLE-PHASE CURRENT.
2. THREE-PHASE CURRENT $\times 1.73$ = SINGLE-PHASE CURRENT
3. THE CURRENT IN THE COMMON CONDUCTOR OF A TWO-PHASE (THREE WIRE) CIRCUIT IS 141% GREATER THAN EITHER OF THE OTHER TWO CONDUCTORS OF THAT CIRCUIT.

TO FIND HORSEPOWER

DIRECT CURRENT:

$$\text{HORSEPOWER} = \frac{\text{VOLTS} \times \text{AMPERES} \times \text{EFFICIENCY}}{746}$$

A 12 volt motor draws a current of 8.09 amperes, and has an efficiency rating of 96%. Determine the horsepower.

$$\text{HP} = \frac{E \times I \times \% \text{EFF}}{746} = \frac{12 \times 8.09 \times 0.96}{746} = \frac{93.19}{746}$$

$$\text{HP} = 0.1249 = 1/8 \text{ HP}$$

SINGLE-PHASE:

$$\text{HP} = \frac{\text{VOLTS} \times \text{AMPERES} \times \text{EFFICIENCY} \times \text{POWER FACTOR}}{746}$$

A single-phase, 115 volt (AC) motor has an efficiency rating of 92%, and a power-factor of 80%. Determine the horsepower if the amp-load is 4.4 amperes.

$$\text{HP} = \frac{E \times I \times \% \text{EFF} \times \text{PF}}{746} = \frac{115 \times 4.4 \times 0.92 \times 0.80}{746}$$

$$\text{HP} = \frac{372.416}{746} = 0.4992 = 1/2 \text{ HP}$$

TWO-PHASE:

$$\text{HP} = \frac{\text{VOLTS} \times \text{AMPERES} \times \text{EFFICIENCY} \times \text{POWER FACTOR} \times 2}{746}$$

Determine the horsepower of a two-phase, 230 volt (AC) motor. The motor has an efficiency rating of 92%, a power-factor of 80%, and an amp-load of 1.1 amperes.

$$\text{HP} = \frac{E \times I \times \% \text{EFF} \times \text{PF} \times 2}{746} = \frac{230 \times 1.1 \times 0.92 \times 0.8 \times 2}{746}$$

$$\text{HP} = \frac{372.416}{746} = 0.4992 = 1/2 \text{ HP}$$

TO FIND HORSEPOWER

THREE-PHASE:

$$\text{HP} = \frac{\text{VOLTS} \times \text{AMPERES} \times \text{EFFICIENCY} \times \text{POWER FACTOR} \times 1.73}{746}$$

A three-phase, 460 volt motor draws a current of 52 amperes. The motor has an efficiency rating of 94%, and a power factor of 80%. Determine the horsepower.

$$\text{HP} = \frac{E \times I \times \% \text{EFF} \times \text{PF} \times 1.73}{746} = \frac{460 \times 52 \times 0.94 \times 0.80 \times 1.73}{746}$$

$$\text{HP} = 41.7 \text{ HP}$$

TO FIND WATTS

The electrical power in any part of a circuit is equal to the current in that part multiplied by the voltage across that part of the circuit.

A watt is the power used when one volt causes one ampere to flow in a circuit.

One horsepower is the amount of energy required to lift 33,000 pounds, one foot, in one minute. The electrical equivalent of one horsepower is 745.6 watts. One watt is the amount of energy required to lift 44.26 pounds, one foot, in one minute. Watts is power, and power is the amount of work done in a given time.

When VOLTS AND AMPERES are known:

$$\text{POWER (WATTS)} = \text{VOLTS} \times \text{AMPERES}$$

A 120 volt AC circuit draws a current of 5 amperes. Determine the power consumption.

$$P = E \times I = 120 \times 5 = 600 \text{ WATTS}$$

We can now determine the resistance of this circuit.

$$\text{POWER} = \text{RESISTANCE} \times (\text{AMPERES})^2$$

$$P = R \times I^2 \quad \text{or} \quad 600 = R \times 25 \quad \text{divide both sides of equation by 25}$$

$$\frac{600}{25} = R \quad \text{or} \quad R = 24 \text{ OHMS}$$

or

$$\text{POWER} = \frac{(\text{VOLTS})^2}{\text{RESISTANCE}} \quad \text{or} \quad P = \frac{E^2}{R} \quad \text{or} \quad 600 = \frac{120^2}{R}$$

$$R \times 600 = 120^2 \quad \text{or} \quad R = \frac{14,400}{600} = 24 \text{ OHMS}$$

NOTE: REFER TO THE FORMULAS OF THE OHM'S LAW CHART ON PAGE 1

TO FIND KILOWATTS

DIRECT CURRENT:

$$\text{KILOWATTS} = \frac{\text{VOLTS} \times \text{AMPERES}}{1000}$$

A 120 volt (DC) motor draws a current of 40 amperes. Determine the kilowatts.

$$KW = \frac{E \times I}{1000} = \frac{120 \times 40}{1000} = \frac{4800}{1000} = 4.8 \text{ KW}$$

SINGLE-PHASE:

$$\text{KILOWATTS} = \frac{\text{VOLTS} \times \text{AMPERES} \times \text{POWER FACTOR}}{1000}$$

A single-phase, 115 volt (AC) motor draws a current of 20 amperes, and has a power-factor rating of 86%. Determine the kilowatts.

$$KW = \frac{E \times I \times PF}{1000} = \frac{115 \times 20 \times 0.86}{1000} = \frac{1978}{1000} = 1.978 = 2 \text{ KW}$$

TWO-PHASE:

$$\text{KILOWATTS} = \frac{\text{VOLTS} \times \text{AMPERES} \times \text{POWER FACTOR} \times 2}{1000}$$

A two-phase, 230 volt (AC) motor with a power-factor of 92%, draws a current of 55 amperes. Determine the kilowatts.

$$KW = \frac{E \times I \times PF \times 2}{1000} = \frac{230 \times 55 \times 0.92 \times 2}{1000}$$

$$KW = \frac{23,276}{1000} = 23.276 = 23 \text{ KW}$$

TO FIND KILOWATTS

THREE-PHASE:

$$\text{KILOWATTS} = \frac{\text{VOLTS} \times \text{AMPERES} \times \text{POWER FACTOR} \times 1.73}{1000}$$

A three-phase, 460 volt (AC) motor draws a current of 52 amperes, and has a power-factor rating of 80%. Determine the kilowatts.

$$\begin{aligned}\text{KW} &= \frac{E \times I \times \text{PF} \times 1.73}{1000} = \frac{460 \times 52 \times 0.80 \times 1.73}{1000} \\ &= \frac{33,105}{1000} = 33.105 = 33\text{KW}\end{aligned}$$

KIRCHHOFF'S LAWS

FIRST LAW (CURRENT):

THE SUM OF THE CURRENTS ARRIVING AT ANY POINT IN A CIRCUIT MUST EQUAL THE SUM OF THE CURRENTS LEAVING THAT POINT.

SECOND LAW (VOLTAGE):

THE TOTAL VOLTAGE APPLIED TO ANY CLOSED CIRCUIT PATH IS ALWAYS EQUAL TO THE SUM OF THE VOLTAGE DROPS IN THAT PATH.

OR

THE ALGEBRAIC SUM OF ALL THE VOLTAGES ENCOUNTERED IN ANY LOOP EQUALS ZERO.

TO FIND KILOVOLT-AMPERES

SINGLE-PHASE:

$$\text{KILOVOLT-AMPERES} = \frac{\text{VOLTS} \times \text{AMPERES}}{1000}$$

A single-phase, 240 volt generator delivers 41.66 amperes at full load. Determine the kilovolt-amperes rating.

$$\text{KVA} = \frac{E \times I}{1000} = \frac{240 \times 41.66}{1000} = \frac{10,000}{1000} = 10 \text{ KVA}$$

TWO-PHASE:

$$\text{KILOVOLT-AMPERES} = \frac{\text{VOLTS} \times \text{AMPERES} \times 2}{1000}$$

A two-phase, 230 volt generator delivers 55 amperes. Determine the kilovolt-amperes.

$$\begin{aligned}\text{KVA} &= \frac{E \times I \times 2}{1000} = \frac{230 \times 55 \times 2}{1000} = \frac{25,300}{1000} \\ &= 25.3 = 25 \text{ KVA}\end{aligned}$$

THREE-PHASE:

$$\text{KILOVOLT-AMPERES} = \frac{\text{VOLTS} \times \text{AMPERES} \times 1.73}{1000}$$

A three-phase, 460 volt generator delivers 52 amperes. Determine the kilovolt-amperes rating.

$$\begin{aligned}\text{KVA} &= \frac{E \times I \times 1.73}{1000} = \frac{460 \times 52 \times 1.73}{1000} = \frac{41,382}{1000} \\ &= 41.382 = 41 \text{ KVA}\end{aligned}$$

NOTE: KVA = APPARENT POWER = POWER BEFORE USED, SUCH AS THE RATING OF A TRANSFORMER.

TO FIND CAPACITANCE

CAPACITANCE (C):

$$C = \frac{Q}{E} \text{ or } \text{CAPACITANCE} = \frac{\text{COULOMBS}}{\text{VOLTS}}$$

Capacitance is the property of a circuit or body that permits it to store an electrical charge equal to the accumulated charge divided by the voltage. Expressed in farads.

A. To determine the total capacity of capacitors, and/or condensers connected in series.

$$\frac{1}{C_T} = \frac{1}{C_1} + \frac{1}{C_2} + \frac{1}{C_3} + \frac{1}{C_4}$$

Determine the total capacity of four each, 12 microfarad capacitors connected in series.

$$\frac{1}{C_T} = \frac{1}{C_1} + \frac{1}{C_2} + \frac{1}{C_3} + \frac{1}{C_4}$$

$$= \frac{1}{12} + \frac{1}{12} + \frac{1}{12} + \frac{1}{12} = \frac{4}{12}$$

$$\frac{1}{C_T} = \frac{4}{12} \text{ or } C_T \times 4 = 12 \text{ or } C_T = \frac{12}{4} = 3 \text{ microfarads}$$

B. To determine the total capacity of capacitors, and/or condensers connected in parallel.

$$C_T = C_1 + C_2 + C_3 + C_4$$

Determine the total capacity of four each, 12 microfarad capacitors connected in parallel.

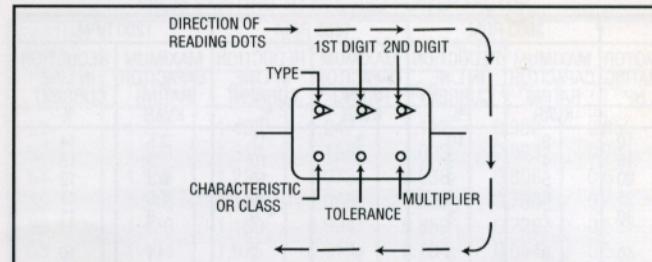
$$C_T = C_1 + C_2 + C_3 + C_4$$

$$C_T = 12 + 12 + 12 + 12 = 48 \text{ microfarads}$$

A farad is the unit of capacitance of a condenser that retains one coulomb of charge with one volt difference of potential.

1 Farad = 1,000,000 Microfarads

6-DOT COLOR CODE FOR MICA AND MOLDED PAPER CAPACITORS



| TYPE | COLOR | 1ST DIGIT | 2ND DIGIT | MULTIPLIER | TOLERANCE (%) | CHARACTERISTIC OR CLASS |
|--------------|--------|-----------|-----------|---------------|---------------|--|
| JAN, MICA | BLACK | 0 | 0 | 1 | ± 1 | APPLIES TO TEMPERATURE COEFFICIENT OR METHODS OF TESTING |
| | BROWN | 1 | 1 | 10 | ± 2 | |
| | RED | 2 | 2 | 100 | ± 3 | |
| | ORANGE | 3 | 3 | 1,000 | ± 4 | |
| | YELLOW | 4 | 4 | 10,000 | ± 5 | |
| | GREEN | 5 | 5 | 100,000 | ± 6 | |
| | BLUE | 6 | 6 | 1,000,000 | ± 7 | |
| | VIOLET | 7 | 7 | 10,000,000 | ± 8 | |
| | GRAY | 8 | 8 | 100,000,000 | ± 9 | |
| ETA, MICA | WHITE | 9 | 9 | 1,000,000,000 | .1 | |
| MOLDED PAPER | GOLD | | | | .01 | ± 10 |
| | SILVER | | | | | ± 20 |
| | BODY | | | | | |

**MAXIMUM PERMISSIBLE CAPACITOR KVAR FOR USE WITH
OPEN-TYPE THREE-PHASE SIXTY-CYCLE INDUCTION MOTORS**

| MOTOR RATING HP | 3600 RPM | | 1800 RPM | | 1200 RPM | |
|-----------------------|--|--------------------------------------|--|--------------------------------------|--|--------------------------------------|
| | MAXIMUM CAPACITOR RATING KVAR | REDUCTION IN LINE CURRENT % | MAXIMUM CAPACITOR RATING KVAR | REDUCTION IN LINE CURRENT % | MAXIMUM CAPACITOR RATING KVAR | REDUCTION IN LINE CURRENT % |
| 10 | 3 | 10 | 3 | 11 | 3.5 | 14 |
| 15 | 4 | 9 | 4 | 10 | 5 | 13 |
| 20 | 5 | 9 | 5 | 10 | 6.5 | 12 |
| 25 | 6 | 9 | 6 | 10 | 7.5 | 11 |
| 30 | 7 | 8 | 7 | 9 | 9 | 11 |
| 40 | 9 | 8 | 9 | 9 | 11 | 10 |
| 50 | 12 | 8 | 11 | 9 | 13 | 10 |
| 60 | 14 | 8 | 14 | 8 | 15 | 10 |
| 75 | 17 | 8 | 16 | 8 | 18 | 10 |
| 100 | 22 | 8 | 21 | 8 | 25 | 9 |
| 125 | 27 | 8 | 26 | 8 | 30 | 9 |
| 150 | 32.5 | 8 | 30 | 8 | 35 | 9 |
| 200 | 40 | 8 | 37.5 | 8 | 42.5 | 9 |

| MOTOR RATING HP | 900 RPM | | 720 RPM | | 600 RPM | |
|-----------------------|--|--------------------------------------|--|--------------------------------------|--|--------------------------------------|
| | MAXIMUM CAPACITOR RATING KVAR | REDUCTION IN LINE CURRENT % | MAXIMUM CAPACITOR RATING KVAR | REDUCTION IN LINE CURRENT % | MAXIMUM CAPACITOR RATING KVAR | REDUCTION IN LINE CURRENT % |
| 10 | 5 | 21 | 6.5 | 27 | 7.5 | 31 |
| 15 | 6.5 | 18 | 8 | 23 | 9.5 | 27 |
| 20 | 7.5 | 16 | 9 | 21 | 12 | 25 |
| 25 | 9 | 15 | 11 | 20 | 14 | 23 |
| 30 | 10 | 14 | 12 | 18 | 16 | 22 |
| 40 | 12 | 13 | 15 | 16 | 20 | 20 |
| 50 | 15 | 12 | 19 | 15 | 24 | 19 |
| 60 | 18 | 11 | 22 | 15 | 27 | 19 |
| 75 | 21 | 10 | 26 | 14 | 32.5 | 18 |
| 100 | 27 | 10 | 32.5 | 13 | 40 | 17 |
| 125 | 32.5 | 10 | 40 | 13 | 47.5 | 16 |
| 150 | 37.5 | 10 | 47.5 | 12 | 52.5 | 15 |
| 200 | 47.5 | 10 | 60 | 12 | 65 | 14 |

NOTE: If capacitors of a lower rating than the values given in the table are used, the percentage reduction in line current given in the table should be reduced proportionately.

POWER-FACTOR CORRECTION

TABLE VALUES x KW OF CAPACITORS NEEDED TO CORRECT
FROM EXISTING TO DESIRED POWER FACTOR

| EXISTING POWER FACTOR % | CORRECTED POWER FACTOR | | | | | |
|----------------------------------|------------------------|-------|-------|-------|-------|-------|
| | 100% | 95% | 90% | 85% | 80% | 75% |
| 50 | 1.732 | 1.403 | 1.247 | 1.112 | 0.982 | 0.850 |
| 52 | 1.643 | 1.314 | 1.158 | 1.023 | 0.893 | 0.761 |
| 54 | 1.558 | 1.229 | 1.073 | 0.938 | 0.808 | 0.676 |
| 55 | 1.518 | 1.189 | 1.033 | 0.898 | 0.768 | 0.636 |
| 56 | 1.479 | 1.150 | 0.994 | 0.859 | 0.729 | 0.597 |
| 58 | 1.404 | 1.075 | 0.919 | 0.784 | 0.654 | 0.522 |
| 60 | 1.333 | 1.004 | 0.848 | 0.713 | 0.583 | 0.451 |
| 62 | 1.265 | 0.936 | 0.780 | 0.645 | 0.515 | 0.383 |
| 64 | 1.201 | 0.872 | 0.716 | 0.581 | 0.451 | 0.319 |
| 65 | 1.168 | 0.839 | 0.683 | 0.548 | 0.418 | 0.286 |
| 66 | 1.139 | 0.810 | 0.654 | 0.519 | 0.389 | 0.257 |
| 68 | 1.078 | 0.749 | 0.593 | 0.458 | 0.328 | 0.196 |
| 70 | 1.020 | 0.691 | 0.535 | 0.400 | 0.270 | 0.138 |
| 72 | 0.964 | 0.635 | 0.479 | 0.344 | 0.214 | 0.082 |
| 74 | 0.909 | 0.580 | 0.424 | 0.289 | 0.159 | 0.027 |
| 75 | 0.882 | 0.553 | 0.397 | 0.262 | 0.132 | |
| 76 | 0.855 | 0.526 | 0.370 | 0.235 | 0.105 | |
| 78 | 0.802 | 0.473 | 0.317 | 0.182 | 0.052 | |
| 80 | 0.750 | 0.421 | 0.265 | 0.130 | | |
| 82 | 0.698 | 0.369 | 0.213 | 0.078 | | |
| 84 | 0.646 | 0.317 | 0.161 | | | |
| 85 | 0.620 | 0.291 | 0.135 | | | |
| 86 | 0.594 | 0.265 | 0.109 | | | |
| 88 | 0.540 | 0.211 | 0.055 | | | |
| 90 | 0.485 | 0.156 | | | | |
| 92 | 0.426 | 0.097 | | | | |
| 94 | 0.363 | 0.034 | | | | |
| 95 | 0.329 | | | | | |

TYPICAL PROBLEM: With a load of 500 KW at 70% power factor, it is desired to find the KVA of capacitors required to correct the power factor to 85%

SOLUTION: From the table, select the multiplying factor 0.400 corresponding to the existing 70%, and the corrected 85% power factor.
 $0.400 \times 500 = 200$ KVA of capacitors required.

POWER FACTOR AND EFFICIENCY EXAMPLE

A squirrel cage induction motor is rated 10 horsepower, 208 volt, three phase and has a nameplate rating of 27.79 amperes. A wattmeter reading indicates 8 kilowatts of consumed (true) power. Calculate apparent power (KVA), power factor, efficiency, internal losses and size the capacitor in kilo-volts reactive (KVAR) needed to correct the power factor to unity (100%).

Apparent input power: kilovolt-amperes (KVA)

$$\text{KVA} = (E \times I \times 1.73) / 1000 = (208 \times 27.79 \times 1.73) / 1000 = 10 \text{ KVA}$$

Power factor (PF) = ratio of true power (KW) to apparent power (KVA).

$$\text{Kilo-watts} / \text{kilo-volt-amperes} = 8\text{KW}/10 \text{ KVA} = .8 = 80\% \text{ Power Factor}$$

80% of the 10-KVA apparent power input performs work.

Motor output in kilowatts = 10 horsepower x 746 watts = 7460 watts = **7.46 KW**.

$$\text{Efficiency} = \text{watts out/watts in} = 7.46 \text{ KW} / 8\text{KW} = .9325 = 93.25\% \text{ Efficiency.}$$

Internal losses (heat, friction, hysteresis) = 8KW - 7.46 KW = **.54 KW** (540 watts)

Kilovolt-amperes reactive (KVAR) (Power stored in motor magnetic field)

$$\text{KVAR} = \sqrt{\text{KVA}^2 - \text{KW}^2} = \sqrt{10\text{KVA}^2 - 8\text{KW}^2} = \sqrt{100-64} = \sqrt{36} = 6 \text{ KVAR}$$

The size capacitor needed to equal the motor's stored reactive power is 6 KVAR. (A capacitor stores reactive power in its electrostatic field).

The power source must supply the current to perform work and maintain the motor's magnetic field. Before power factor correction, this was 27.79 amperes.

The motor magnetizing current after power factor correction is supplied by circulation of current between the motor and the electrostatic field of the capacitor and is no longer supplied by power source after initial start up.

The motor feeder current after correction to 100% will equal the amount required by the input watts in this case $(8 \text{ KW} \times 1000) / (208 \text{ volts} \times 1.73) = 22.23 \text{ amps}$

- kilo = 1000 example: 1000 watts = 1 kilowatt

- inductive loads (motors, coils) have lagging currents and capacitive loads have leading currents.

- inductance and capacitance have opposite effects in a circuit and can cancel each other

TO FIND INDUCTANCE

INDUCTANCE (L):

Inductance is the production of magnetization of electrification in a body by the proximity of a magnetic field or electric charge, or of the electric current in a conductor by the variation of the magnetic field in its vicinity. Expressed in Henrys.

A. To find the total inductance of coils connected in series.

$$L_T = L_1 + L_2 + L_3 + L_4$$

Determine the total inductance of four coils connected in series.
Each coil has an inductance of four Henrys.

$$L_T = L_1 + L_2 + L_3 + L_4$$

$$= 4 + 4 + 4 + 4 = 16 \text{ Henrys}$$

B. To find the total inductance of coils connected in parallel.

$$\frac{1}{L_T} = \frac{1}{L_1} + \frac{1}{L_2} + \frac{1}{L_3} + \frac{1}{L_4}$$

Determine the total inductance of four coils connected in parallel.
Each coil has an inductance of four Henrys.

$$\frac{1}{L_T} = \frac{1}{L_1} + \frac{1}{L_2} + \frac{1}{L_3} + \frac{1}{L_4}$$

$$\frac{1}{L_T} = \frac{1}{4} + \frac{1}{4} + \frac{1}{4} + \frac{1}{4}$$

$$\frac{1}{L_T} = \frac{4}{4} \text{ OR } L_T \times 4 = 1 \times 4 \text{ OR } L_T = \frac{4}{4} = 1 \text{ Henry}$$

An induction coil is a device, consisting of two concentric coils and an interrupter, that changes a low steady voltage into a high intermittent alternating voltage by electromagnetic induction. Most often used as a spark coil.

TO FIND IMPEDANCE

IMPEDANCE (Z):

Impedance is the total opposition to an alternating current presented by a circuit. Expressed in OHMS.

A. When VOLTS AND AMPERES are known:

$$\text{IMPEDANCE} = \frac{\text{VOLTS}}{\text{AMPERES}} \quad \text{OR} \quad Z = \frac{E}{I}$$

Determine the impedance of a 120 volt A-C circuit that draws a current of four amperes.

$$Z = \frac{E}{I} = \frac{120}{4} = 30 \text{ OHMS}$$

B. When RESISTANCE AND REACTANCE are known:

$$Z = \sqrt{\text{RESISTANCE}^2 + \text{REACTANCE}^2} = \sqrt{R^2 + X^2}$$

Determine the impedance of an A-C circuit when the resistance is 6 OHMS, and the reactance is 8 OHMS.

$$Z = \sqrt{R^2 + X^2} = \sqrt{36 + 64} = \sqrt{100} = 10 \text{ OHMS}$$

C. When RESISTANCE, INDUCTIVE REACTANCE, AND CAPACITIVE REACTANCE are known:

$$Z = \sqrt{R^2 + (X_L - X_C)^2}$$

Determine the impedance of an A-C circuit which has a resistance of 6 OHMS, an inductive reactance of 18 OHMS, and a capacitive reactance of 10 OHMS.

$$\begin{aligned} Z &= \sqrt{R^2 + (X_L - X_C)^2} \\ &= \sqrt{6^2 + (18 - 10)^2} = \sqrt{6^2 + (8)^2} \\ &= \sqrt{36 + 64} = \sqrt{100} = 10 \text{ OHMS} \end{aligned}$$

TO FIND REACTANCE

REACTANCE (X):

Reactance in a circuit is the opposition to an alternating current caused by inductance and capacitance, equal to the difference between capacitive and inductive reactance. Expressed in OHMS.

A. INDUCTIVE REACTANCE X_L

Inductive reactance is that element of reactance in a circuit caused by self-inductance.

$$X_L = 2 \times 3.1416 \times \text{FREQUENCY} \times \text{INDUCTANCE}$$

$$= 6.28 \times F \times L$$

Determine the reactance of a four-Henry coil on a 60 cycle, A-C circuit.

$$X_L = 6.28 \times F \times L = 6.28 \times 60 \times 4 = 1507 \text{ OHMS}$$

B. CAPACITIVE REACTANCE X_C

Capacitive reactance is that element of reactance in a circuit caused by capacitance.

$$X_C = \frac{1}{2 \times 3.1416 \times \text{FREQUENCY} \times \text{CAPACITANCE}}$$

$$= \frac{1}{6.28 \times F \times C}$$

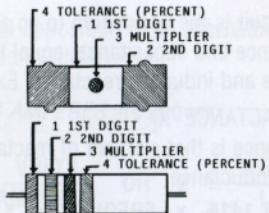
Determine the reactance of a four microfarad condenser on a 60 cycle, A-C circuit.

$$X_C = \frac{1}{6.28 \times F \times C} = \frac{1}{6.28 \times 60 \times .000004}$$

$$= \frac{1}{0.0015072} = 663 \text{ OHMS}$$

A HENRY is a unit of inductance, equal to the inductance of a circuit in which the variation of a current at the rate of one ampere per second induces an electromotive force of one volt.

RESISTOR COLOR CODE



| COLOR | 1ST DIGIT | 2ND DIGIT | MULTIPLIER | TOLERANCE (%) |
|----------|-----------|-----------|---------------|---------------|
| BLACK | 0 | 0 | 1 | |
| BROWN | 1 | 1 | 10 | |
| RED | 2 | 2 | 100 | |
| ORANGE | 3 | 3 | 1,000 | |
| YELLOW | 4 | 4 | 10,000 | |
| GREEN | 5 | 5 | 100,000 | |
| BLUE | 6 | 6 | 1,000,000 | |
| VIOLET | 7 | 7 | 10,000,000 | |
| GRAY | 8 | 8 | 100,000,000 | |
| WHITE | 9 | 9 | 1,000,000,000 | |
| GOLD | | | .1 | ± 5% |
| SILVER | | | .01 | ± 10% |
| NO COLOR | | | | ± 20% |

RUNNING OVERLOAD UNITS

| KIND OF MOTOR | SUPPLY SYSTEM | NUMBER & LOCATION OF OVER-LOAD UNITS, SUCH AS TRIP COILS OR RELAYS |
|------------------|--|--|
| 1-Phase ac or dc | 2-wire, 1-phase ac or dc, ungrounded | 1 in either conductor |
| 1-Phase ac or dc | 2-wire, 1-phase ac or dc, one conductor ungrounded | 1 in ungrounded conductor |
| 1-Phase ac or dc | 3-wire, 1-phase ac or dc, grounded neutral | 1 in either ungrounded conductor |
| 1-Phase ac | any 3-phase | 1 in ungrounded conductor |
| 2-Phase ac | 3-wire, 2-phase ac, ungrounded | 2, one in each phase |
| 2-Phase ac | 3-wire, 2-phase ac, one conductor grounded | 2 in ungrounded conductors |
| 2-Phase ac | 4-wire, 2-phase ac, grounded or ungrounded | 2, one per phase in ungrounded conductors |
| 2-Phase ac | 5-wire, 2-phase ac, grounded neutral or ungrounded | 2, one per phase in any ungrounded phase wire |
| 3-Phase ac | any 3-phase | 3, one in each phase* |

* Exception: Where protected by other approved means.

MOTOR BRANCH - CIRCUIT PROTECTIVE DEVICES MAXIMUM RATING OR SETTING

| Type of Motor | Percent of Full-Load Current | | | |
|--|------------------------------|---------------------------------|----------------------------|------------------------|
| | Nontime Delay Fuse* | Dual Element (Time-Delay) Fuse* | Instantaneous Trip Breaker | Inverse Time Breaker** |
| Single-phase motors | 300 | 175 | 800 | 250 |
| AC polyphase motors other than wound-rotor | | | | |
| Squirrel Cage: | | | | |
| Other than Design B | 300 | 175 | 800 | 250 |
| Design B | 300 | 175 | 1100 | 250 |
| Synchronous *** | 300 | 175 | 800 | 250 |
| Wound rotor | 150 | 150 | 800 | 150 |
| Direct-current (constant voltage) | 150 | 150 | 250 | 150 |

For certain exceptions to the values specified, see Sections 430-52 - 430-54.

* The values in the Nontime Delay Fuse column apply to Time-Delay Class CC fuses.

** The values given in the last column also cover the ratings of nonadjustable inverse time types of circuit breakers that may be modified as in Section 430-52.

*** Synchronous motors of the low-torque, low speed type (usually 450 rpm or lower), such as are used to drive reciprocating compressors, pumps, etc., that start unloaded, do not require a fuse rating or circuit-breaker setting in excess of 200% of full-load current.

FULL-LOAD CURRENT IN AMPERES
DIRECT CURRENT MOTORS

| HP | 90V | 120V | 180V | 240V | 500V | 550V |
|-------|------|------|------|------|------|------|
| 1/4 | 4.0 | 3.1 | 2.0 | 1.6 | - | - |
| 1/3 | 5.2 | 4.1 | 2.6 | 2.0 | - | - |
| 1/2 | 6.8 | 5.4 | 3.4 | 2.7 | - | - |
| 3/4 | 9.6 | 7.6 | 4.8 | 3.8 | - | - |
| 1 | 12.2 | 9.5 | 6.1 | 4.7 | - | - |
| 1-1/2 | - | 13.2 | 8.3 | 6.6 | - | - |
| 2 | - | 17 | 10.8 | 8.5 | - | - |
| 3 | - | 25 | 16 | 12.2 | - | - |
| 5 | - | 40 | 27 | 20 | - | - |
| 7-1/2 | - | 58 | - | 29 | 13.6 | 12.2 |
| 10 | - | 76 | - | 38 | 18 | 16 |
| 15 | - | - | - | 55 | 27 | 24 |
| 20 | - | - | - | 72 | 34 | 31 |
| 25 | - | - | - | 89 | 43 | 38 |
| 30 | - | - | - | 106 | 51 | 46 |
| 40 | - | - | - | 140 | 67 | 61 |
| 50 | - | - | - | 173 | 83 | 75 |
| 60 | - | - | - | 206 | 99 | 90 |
| 75 | - | - | - | 255 | 123 | 111 |
| 100 | - | - | - | 341 | 164 | 148 |
| 125 | - | - | - | 425 | 205 | 185 |
| 150 | - | - | - | 506 | 246 | 222 |
| 200 | - | - | - | 675 | 330 | 294 |

These values of full-load currents* are for motors running at base speed.

* These are average dc quantities.

DIRECT CURRENT MOTORS

TERMINAL MARKINGS:

Terminal markings are used to tag terminals to which connections are to be made from outside circuits.

Facing the end opposite the drive (commutator end) the standard direction of shaft rotation is counter-clockwise.

A-1 and A-2 indicate armature leads.

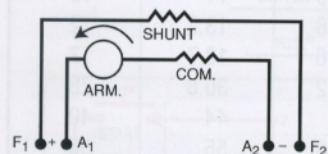
S-1 and S-2 indicate series-field leads.

F-1 and F-2 indicate shunt-field leads.



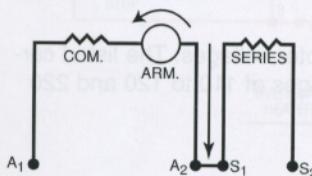
SHUNT WOUND MOTORS

To change rotation, reverse either armature leads or shunt leads. Do not reverse both armature and shunt leads.



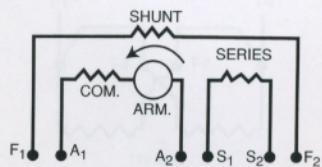
SERIES WOUND MOTORS

To change rotation, reverse either armature leads or series leads. Do not reverse both armature and series leads.



COMPOUND WOUND MOTORS

To change rotation, reverse either armature leads or both the series and shunt leads. Do not reverse all three sets of leads.



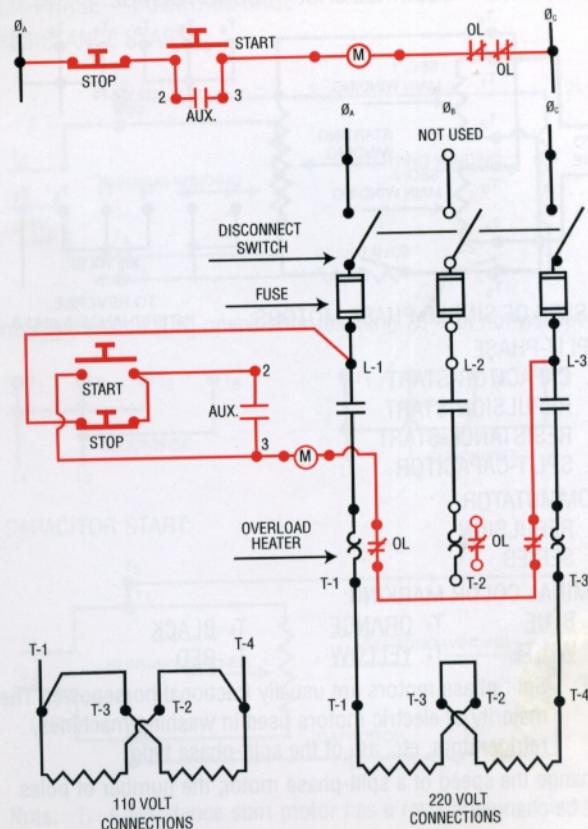
Note: Standard rotation for D.C. Generator is clockwise.

**FULL-LOAD CURRENT IN AMPERES
SINGLE-PHASE ALTERNATING CURRENT MOTORS**

| HP | 115V | 200V | 208V | 230V |
|-------|------|------|------|------|
| 1/6 | 4.4 | 2.5 | 2.4 | 2.2 |
| 1/4 | 5.8 | 3.3 | 3.2 | 2.9 |
| 1/3 | 7.2 | 4.1 | 4.0 | 3.6 |
| 1/2 | 9.8 | 5.6 | 5.4 | 4.9 |
| 3/4 | 13.8 | 7.9 | 7.6 | 6.9 |
| 1 | 16 | 9.2 | 8.8 | 8.0 |
| 1-1/2 | 20 | 11.5 | 11 | 10 |
| 2 | 24 | 13.8 | 13.2 | 12 |
| 3 | 34 | 19.6 | 18.7 | 17 |
| 5 | 56 | 32.2 | 30.8 | 28 |
| 7-1/2 | 80 | 46 | 44 | 40 |
| 10 | 100 | 57.5 | 55 | 50 |

The voltages listed are rated motor voltages. The listed currents are for system voltage ranges of 110 to 120 and 220 to 240.

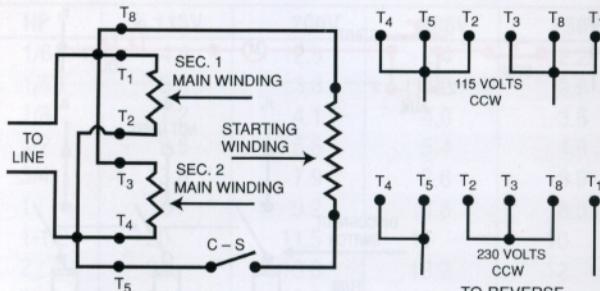
SINGLE-PHASE USING STANDARD THREE-PHASE STARTER



(M) = MOTOR STARTER COIL

SINGLE PHASE MOTORS

SPLIT-PHASE---SQUIRREL CAGE---DUAL-VOLTAGE



CLASSES OF SINGLE-PHASE MOTORS:

1. SPLIT-PHASE

- A. CAPACITOR-START
- B. REPULSION-START
- C. RESISTANCE-START
- D. SPLIT-CAPACITOR

2. COMMUTATOR

- A. REPULSION
- B. SERIES

TERMINAL COLOR MARKING:

| | | |
|----------------------|-----------------------|----------------------|
| T ₁ BLUE | T ₃ ORANGE | T ₅ BLACK |
| T ₂ WHITE | T ₄ YELLOW | T ₆ RED |

NOTE: Split-phase motors are usually fractional horsepower. The majority of electric motors used in washing machines, refrigerators, etc. are of the split-phase type.

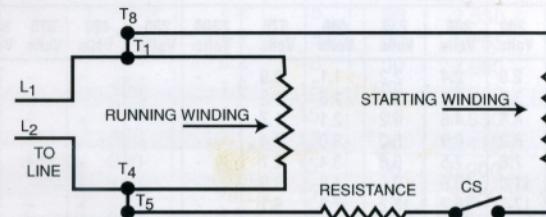
To change the speed of a split-phase motor, the number of poles must be changed.

1. Addition of running winding
2. Two starting windings, and two running windings
3. Consequent pole connections

SINGLE PHASE MOTORS

SPLIT-PHASE---SQUIRREL CAGE

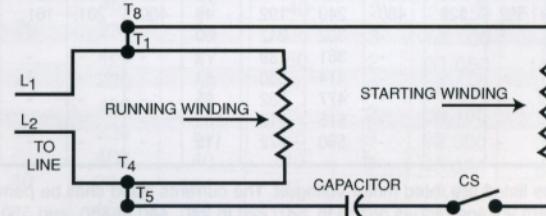
A. RESISTANCE START:



Centrifugal switch (CS) opens after reaching 75% of normal speed.



B. CAPACITOR START:



Note: 1. A resistance start motor has a resistance connected in series with the starting winding.

2. The capacitor start motor is employed where a high starting torque is required.

**FULL-LOAD CURRENT
THREE-PHASE ALTERNATING CURRENT MOTORS**

| HP | Induction Type Squirrel-Cage and Wound-Rotor Amperes | | | | | | Synchronous Type Unity Power Factor* Amperes | | | | | |
|-------|--|--------------|--------------|--------------|--------------|--------------|--|--------------|--------------|--------------|---------------|--|
| | 115 Volts | 200 Volts | 208 Volts | 230 Volts | 460 Volts | 575 Volts | 2300 Volts | 230 Volts | 460 Volts | 575 Volts | 2300 Volts | |
| 1/2 | 4.4 | 2.5 | 2.4 | 2.2 | 1.1 | 0.9 | - | - | - | - | - | |
| 3/4 | 6.4 | 3.7 | 3.5 | 3.2 | 1.6 | 1.3 | - | - | - | - | - | |
| 1 | 8.4 | 4.8 | 4.6 | 4.2 | 2.1 | 1.7 | - | - | - | - | - | |
| 1 1/2 | 12.0 | 6.9 | 6.6 | 6.0 | 3.0 | 2.4 | - | - | - | - | - | |
| 2 | 13.6 | 7.8 | 7.5 | 6.8 | 3.4 | 2.7 | - | - | - | - | - | |
| 3 | - | 11.0 | 10.6 | 9.6 | 4.8 | 3.9 | - | - | - | - | - | |
| 5 | - | 17.5 | 16.7 | 15.2 | 7.6 | 6.1 | - | - | - | - | - | |
| 7 1/2 | - | 25.3 | 24.2 | 22 | 11 | 9 | - | - | - | - | - | |
| 10 | - | 32.2 | 30.8 | 28 | 14 | 11 | - | - | - | - | - | |
| 15 | - | 48.3 | 46.2 | 42 | 21 | 17 | - | - | - | - | - | |
| 20 | - | 62.1 | 59.4 | 54 | 27 | 22 | - | - | - | - | - | |
| 25 | - | 78.2 | 74.8 | 68 | 34 | 27 | - | 53 | 26 | 21 | - | |
| 30 | - | 92 | 88 | 80 | 40 | 32 | - | 63 | 32 | 26 | - | |
| 40 | - | 120 | 114 | 104 | 52 | 41 | - | 83 | 41 | 33 | - | |
| 50 | - | 150 | 143 | 130 | 65 | 52 | - | 104 | 52 | 42 | - | |
| 60 | - | 177 | 169 | 154 | 77 | 62 | 16 | 123 | 61 | 49 | 12 | |
| 75 | - | 221 | 211 | 192 | 96 | 77 | 20 | 155 | 78 | 62 | 15 | |
| 100 | - | 285 | 273 | 248 | 124 | 99 | 26 | 202 | 101 | 81 | 20 | |
| 125 | - | 359 | 343 | 312 | 156 | 125 | 31 | 253 | 126 | 101 | 25 | |
| 150 | - | 414 | 396 | 360 | 180 | 144 | 37 | 302 | 151 | 121 | 30 | |
| 200 | - | 552 | 528 | 480 | 240 | 192 | 49 | 400 | 201 | 161 | 40 | |
| 250 | - | - | - | - | 302 | 242 | 60 | - | - | - | - | |
| 300 | - | - | - | - | 361 | 289 | 72 | - | - | - | - | |
| 350 | - | - | - | - | 414 | 336 | 83 | - | - | - | - | |
| 400 | - | - | - | - | 477 | 382 | 95 | - | - | - | - | |
| 450 | - | - | - | - | 515 | 412 | 103 | - | - | - | - | |
| 500 | - | - | - | - | 590 | 472 | 118 | - | - | - | - | |

The voltages listed are rated motor voltages. The currents listed shall be permitted for system voltage ranges of 110 to 120, 220 to 240, 440 to 480, and 550-600 volts.

* For 90 and 80 percent power factor, the above figures shall be multiplied by 1.1 and 1.25 respectively.

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**FULL-LOAD CURRENT AND OTHER DATA
THREE PHASE A.C. MOTORS**

| MOTOR HORSEPOWER | MOTOR AMPERE | SIZE BREAKER | SIZE STARTER | HEATER AMPERE ** | SIZE WIRE | SIZE CONDUIT |
|---------------------|-----------------|-----------------|-----------------|------------------------|--------------|--------------------|
| 1/2 | 230V | 2.2 | 15 | 00 | 2.530 | 12 ^{3/4"} |
| | 460 | 1.1 | 15 | 00 | 1.265 | 12 ^{3/4"} |
| 3/4 | 230 | 3.2 | 15 | 00 | 3.680 | 12 ^{3/4"} |
| | 460 | 1.6 | 15 | 00 | 1.840 | 12 ^{3/4"} |
| 1 | 230 | 4.2 | 15 | 00 | 4.830 | 12 ^{3/4"} |
| | 460 | 2.1 | 15 | 00 | 2.415 | 12 ^{3/4"} |
| 1 1/2 | 230 | 6.0 | 15 | 00 | 6.900 | 12 ^{3/4"} |
| | 460 | 3.0 | 15 | 00 | 3.450 | 12 ^{3/4"} |
| 2 | 230 | 6.8 | 15 | 0 | 7.820 | 12 ^{3/4"} |
| | 460 | 3.4 | 15 | 00 | 3.910 | 12 ^{3/4"} |
| 3 | 230 | 9.6 | 20 | 0 | 11.040 | 12 ^{3/4"} |
| | 460 | 4.8 | 15 | 0 | 5.520 | 12 ^{3/4"} |
| 5 | 230 | 15.2 | 30 | 1 | 17.480 | 12 ^{3/4"} |
| | 460 | 7.6 | 15 | 0 | 8.740 | 12 ^{3/4"} |
| 7 1/2 | 230 | 22 | 45 | 1 | 25.300 | 10 ^{3/4"} |
| | 460 | 11 | 20 | 1 | 12.650 | 12 ^{3/4"} |
| 10 | 230 | 28 | 60 | 2 | 32.200 | 10 ^{3/4"} |
| | 460 | 14 | 30 | 1 | 16.100 | 12 ^{3/4"} |
| 15 | 230 | 42 | 70 | 2 | 48.300 | 6 1 |
| | 460 | 21 | 40 | 2 | 24.150 | 10 ^{3/4"} |
| 20 | 230 | 54 | 100 | 3 | 62.100 | 4 1 |
| | 460 | 27 | 50 | 2 | 31.050 | 10 ^{3/4"} |
| 25 | 230 | 68 | 100 | 3 | 78.200 | 4 ^{1 1/2} |
| | 460 | 34 | 50 | 2 | 39.100 | 8 1 |
| 30 | 230 | 80 | 125 | 3 | 92.000 | 3 ^{1 1/2} |
| | 460 | 40 | 70 | 3 | 46.000 | 8 1 |
| 40 | 230 | 104 | 175 | 4 | 119.600 | 1 ^{1 1/2} |
| | 460 | 52 | 100 | 3 | 59.800 | 6 1 |
| 50 | 230 | 130 | 200 | 4 | 149.500 | 00 2 |
| | 460 | 65 | 150 | 3 | 74.750 | 4 ^{1 1/2} |

* Overcurrent device may have to be increased due to starting current and load conditions. See NEC 430-52, Table 430-52. Wire size based on 75°C terminations and 75°C insulation.

** Overload heater must be based on motor nameplate & sized per NEC 430-32.

*** Conduit size based on Rigid Metal Conduit with some spare capacity. For minimum size & other conduit types, see NEC Appendix C, or UGLY'S pages 83 - 103.

**FULL-LOAD CURRENT AND OTHER DATA
THREE PHASE A.C. MOTORS**

| MOTOR HORSEPOWER | MOTOR AMPERE | SIZE BREAKER | SIZE STARTER | HEATER AMPERE ** | SIZE WIRE | SIZE CONDUIT |
|------------------|--------------|--------------|--------------|------------------|------------------|------------------------------|
| 60 | 230V 460 | 154 77 | 250 200 | 5 4 | 177.10 88.55 | 000 3 |
| 75 | 230 460 | 192 96 | 300 200 | 5 4 | 220.80 110.40 | 250 _{kcmil} 1 |
| 100 | 230 460 | 248 124 | 400 200 | 5 4 | 285.20 142.60 | 350 _{kcmil} 2/0 |
| 125 | 230 460 | 312 156 | 500 250 | 6 5 | 358.80 179.40 | 600 _{kcmil} 000 |
| 150 | 230 460 | 360 180 | 600 300 | 6 5 | 414.00 207.00 | 700 _{kcmil} 0000 |

NOTE:

1. Wire & conduit size will vary depending on type of insulation & termination listing.
2. The preceding calculations apply to induction type, squirrel-cage, and wound-rotor motors only.
3. The voltages listed are rated motor voltages; corresponding nominal system voltages are 220V to 240V, and 440V to 480V.
4. Hertz: Preferred terminology for cycles per second.
5. Form coil: Coil made with rectangular or square wire.
6. Mash coil: Coil made with round wire.
7. Slip: Percentage difference between synchronous and operating speeds.
8. Synchronous speed: Maximum speed for A.C. motors or $(\text{Frequency} \times 120) / \text{Poles}$.
9. Full load speed: Speed at which rated horsepower is developed.
10. Poles: Number of magnetic poles set up inside the motor by the placement and connection of the windings.

** Overload heater must be based on motor nameplate & sized per NEC 430-32.

GENERAL MOTOR RULES

- Use Full Load Current from Tables instead of nameplate.
- Branch Circuit Conductors - Use 125% of Full Load Current to find conductor size.
- Branch Circuit OCP Size - Use percentages given in Tables for Full Load Current. (UGLY'S page 35)
- Feeder Conductor Size - 125% of largest motor and sum of the rest.
- Feeder OCP - Use largest OCP plus rest of Full Load Currents

**MOTOR BRANCH CIRCUIT AND FEEDER EXAMPLE
GENERAL MOTOR APPLICATIONS**

Branch Circuit Conductors: Use Full Load Three Phase Currents; From Table UGLY'S Page 42 or 2005 NEC Table 430.250, 50 HP 480 volt three phase motor design B, 75 degree terminations = 65 Amperes
125% of Full Load Current (NEC 430.22(A)) (UGLY'S page 44)
125% of 65 A = **81.25 Amperes** Conductor Selection Ampacity

Branch Circuit Over Current Device: NEC 430.52 (C1)
(Branch Circuit Short Circuit and Ground Fault Protection)
Use percentages given in UGLY'S Page 35 or 2005 NEC 430.52 for Type of circuit breaker or fuse used.

50 HP 480 V 3 Ph Motor = 65 Amperes from UGLY'S Page 42.
Nontime Fuse = 300% from UGLY'S Page 35.
300% of 65A = 195 A. NEC 430.52(C1)(EX1) Next size allowed
NEC 240.6A = **200 Ampere Fuse**.

Feeder Connectors: For 50 HP and 30 HP 480 Volt Three phase design B motors on same feeder

Use 125% of largest full load current and 100% of rest. (NEC 430.24)
50 HP 480 V 3 Ph Motor = 65A; 30 HP 480 V 3 Ph Motor = 40A
(125% of 65A) + 40A = **121.25 A** Conductor Selection Ampacity

Feeder Overcurrent Device: (NEC 430.62(A))

(Feeder short circuit and ground fault protection)
Use largest over current protection device plus full load currents of the rest of the motors.

50 HP = 200 A fuse (65 FLC)
30 HP = 125 A fuse (40 FLC)

200 A fuse + 40 A (FLC) = 240 A. Do not exceed this value on feeder. Go down to a **225 A** fuse.

LOCKED ROTOR CODE LETTERS

| Code Letter | Kilovolt-Ampere per Horsepower with Locked Rotor | Code Letter | Kilovolt-Ampere per Horsepower with Locked Rotor |
|-------------|--|-------------|--|
| A | 0 - 3.14 | L | 9.0 - 9.99 |
| B | 3.15 - 3.54 | M | 10.0 - 11.19 |
| C | 3.55 - 3.99 | N | 11.2 - 12.49 |
| D | 4.0 - 4.49 | P | 12.5 - 13.99 |
| E | 4.5 - 4.99 | R | 14.0 - 15.99 |
| F | 5.0 - 5.59 | S | 16.0 - 17.99 |
| G | 5.6 - 6.29 | T | 18.0 - 19.99 |
| H | 6.3 - 7.09 | U | 20.0 - 22.39 |
| J | 7.1 - 7.99 | V | 22.4 and up |
| K | 8.0 - 8.99 | | |

The National Electrical Code® requires that all alternating current motors rated 1/2 horsepower or more (except for polyphase wound rotor motors) must have code letters on their nameplates indicating motor input with locked rotor (in kilovolt-amperes per horsepower). If you know the horsepower and voltage rating of a motor and its "Locked KVA per Horsepower" (from above table), you can calculate the locked rotor current using the following formulas.

Single Phase Motors:

$$\text{Locked Rotor Current} = \frac{\text{HP} \times \text{KVA}_{\text{hp}} \times 1000}{E}$$

Three Phase Motors:

$$\text{Locked Rotor Current} = \frac{\text{HP} \times \text{KVA}_{\text{hp}} \times 1000}{E \times 1.73}$$

Example: What is the maximum locked rotor current for a 480 volt 25 horsepower code letter F motor?
(from the above table, code letter F = 5.59 KVA_{hp})

$$I = \frac{\text{HP} \times \text{KVA}_{\text{hp}} \times 1000}{E \times 1.73} = \frac{25 \times 5.59 \times 1000}{480 \times 1.73} = 168.29 \text{ Amperes}$$

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MAXIMUM MOTOR LOCKED ROTOR CURRENT in AMPERES, SINGLE PHASE *

| HP | 115V | 208V | 230V | HP | 115V | 208V | 230V |
|-------|------|------|------|-------|------|------|------|
| 1/2 | 58.8 | 32.5 | 29.4 | 3 | 204 | 113 | 102 |
| 3/4 | 82.8 | 45.8 | 41.4 | 5 | 336 | 186 | 168 |
| 1 | 96 | 53 | 48 | 7-1/2 | 480 | 265 | 240 |
| 1-1/2 | 120 | 66 | 60 | 10 | 600 | 332 | 300 |
| 2 | 144 | 80 | 72 | | | | |

MAXIMUM MOTOR LOCKED ROTOR CURRENT in AMPERES, TWO & THREE PHASE, DESIGN B, C AND D **

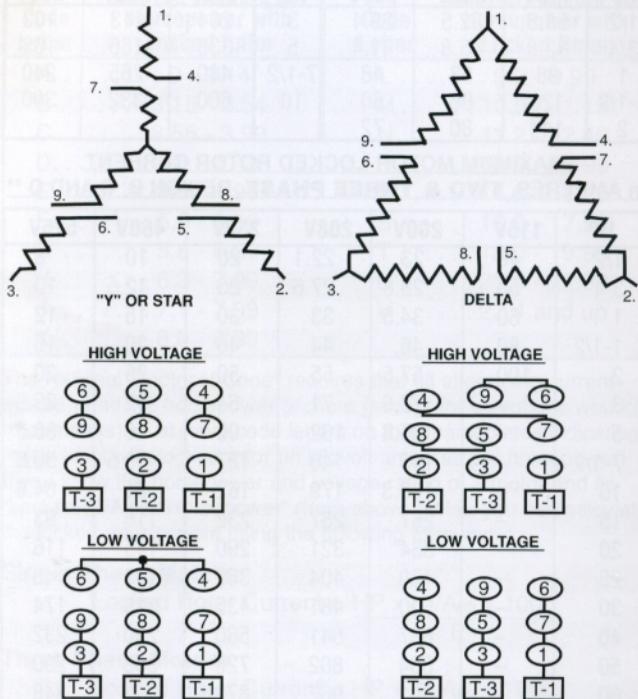
| HP | 115V | 200V | 208V | 230V | 460V | 575V |
|-------|------|-------|------|------|------|------|
| 1/2 | 40 | 23 | 22.1 | 20 | 10 | 8 |
| 3/4 | 50 | 28.8 | 27.6 | 25 | 12.5 | 10 |
| 1 | 60 | 34.5 | 33 | 30 | 15 | 12 |
| 1-1/2 | 80 | 46 | 44 | 40 | 20 | 16 |
| 2 | 100 | 57.5 | 55 | 50 | 25 | 20 |
| 3 | - | 73.6 | 71 | 64 | 32 | 25.6 |
| 5 | - | 105.8 | 102 | 92 | 46 | 36.8 |
| 7-1/2 | - | 146 | 140 | 127 | 63.5 | 50.8 |
| 10 | - | 186.3 | 179 | 162 | 81 | 64.8 |
| 15 | - | 267 | 257 | 232 | 116 | 93 |
| 20 | - | 334 | 321 | 290 | 145 | 116 |
| 25 | - | 420 | 404 | 365 | 183 | 146 |
| 30 | - | 500 | 481 | 435 | 218 | 174 |
| 40 | - | 667 | 641 | 580 | 290 | 232 |
| 50 | - | 834 | 802 | 725 | 363 | 290 |
| 60 | - | 1001 | 962 | 870 | 435 | 348 |
| 75 | - | 1248 | 1200 | 1085 | 543 | 434 |
| 100 | - | 1668 | 1603 | 1450 | 725 | 580 |
| 125 | - | 2087 | 2007 | 1815 | 908 | 726 |
| 150 | - | 2496 | 2400 | 2170 | 1085 | 868 |
| 200 | - | 3335 | 3207 | 2900 | 1450 | 1160 |

* Conversion Table for Selection of Disconnecting Means and Controllers as Determined from Horsepower and Voltage Rating. For use only with 430.110, 440.12, 440.41 and 455.8(C).

** Conversion Table for Selection of Disconnecting Means and Controllers as Determined from Horsepower and Voltage Rating and Design Letter. For use only with 430.110, 440.12, 440.41 and 455.8(C).

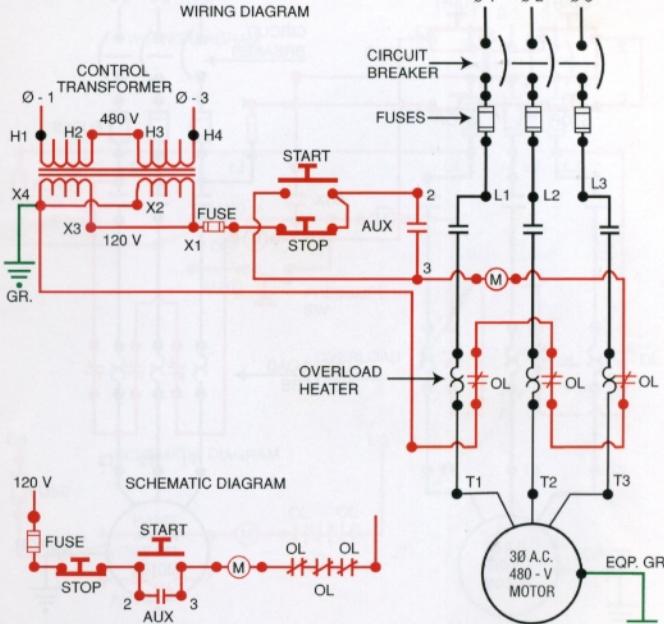
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THREE PHASE A.C. MOTOR WINDINGS AND CONNECTIONS



- Note:
1. The most important part of any motor is the name plate. Check the data given on the plate before making the connections.
 2. To change rotation direction of 3 phase motor, swap any 2 T-leads.

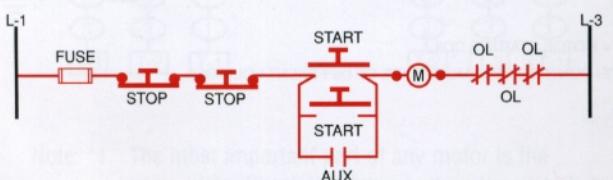
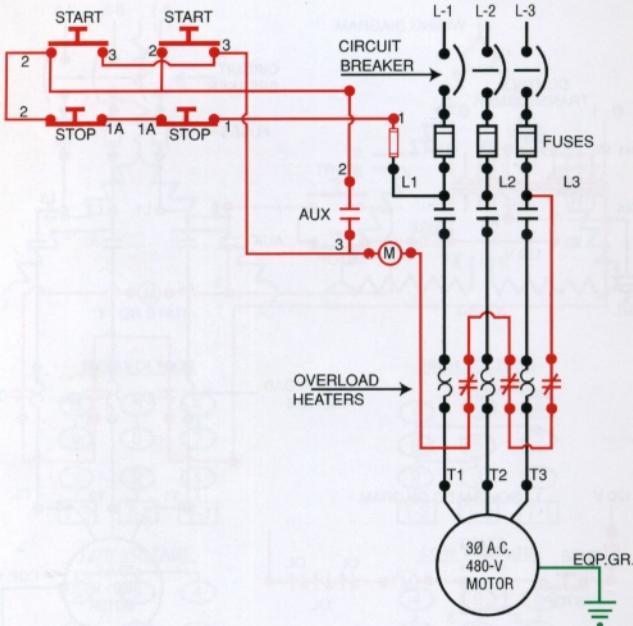
THREE WIRE STOP-START STATION



(M) = MOTOR STARTER COIL

NOTE: CONTROLS AND MOTOR ARE OF DIFFERENT VOLTAGES.

TWO THREE WIRE STOP-START STATIONS



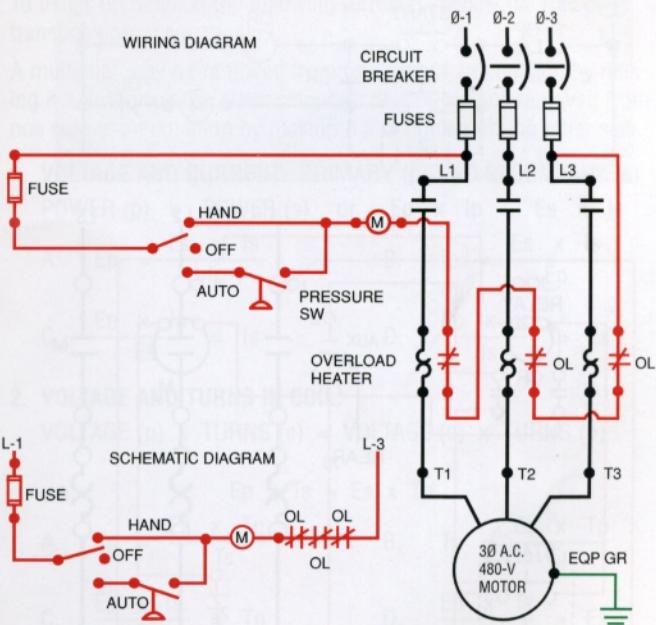
(M) = MOTOR STARTER COIL

Note: Controls and motor are of the same voltage.

If Low Voltage controls are used, see UGLY'S page 49 for control transformer connections.

HAND OFF AUTOMATIC CONTROL

WIRING DIAGRAM

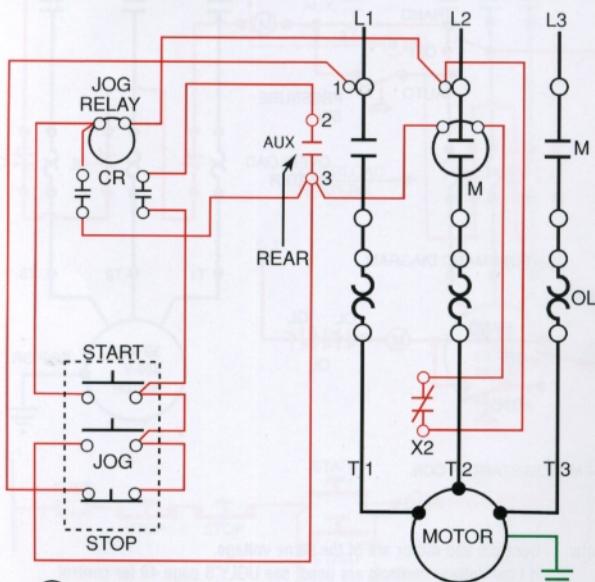
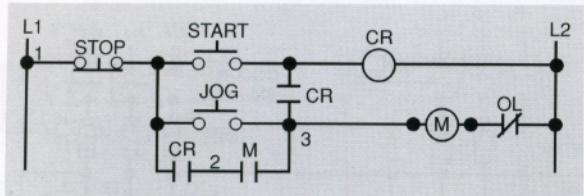


(M) = MOTOR STARTER COIL

Note: Controls and motor are of the same voltage.

If Low Voltage controls are used, see UGLY'S page 49 for control transformer connections.

JOGGING WITH CONTROL RELAY



Jogging circuits are used when machines must be operated momentarily for inching (as in set-up or maintenance). The jog circuit allows the starter to be energized only as long as the jog button is depressed.

TRANSFORMER CALCULATIONS

To better understand the following formulas, review the rule of transposition in equations.

A multiplier may be removed from one side of an equation by making it a divisor on the other side; or a divisor may be removed from one side of an equation by making it a multiplier on the other side.

1. VOLTAGE AND CURRENT: PRIMARY (p) AND SECONDARY (s)

$$\text{POWER (p)} = \text{POWER (s)} \quad \text{or} \quad E_p \times I_p = E_s \times I_s$$

$$A. \quad E_p = \frac{E_s \times I_s}{I_p} \qquad B. \quad I_p = \frac{E_s \times I_s}{E_p}$$

$$C. \quad \frac{E_p \times I_p}{E_s} = I_s \qquad D. \quad \frac{E_p \times I_p}{I_s} = E_s$$

2. VOLTAGE AND TURNS IN COIL:

$$\text{VOLTAGE (p)} \times \text{TURNS (s)} = \text{VOLTAGE (s)} \times \text{TURNS (p)} \\ \text{or} \\ E_p \times T_s = E_s \times T_p$$

$$A. \quad E_p = \frac{E_s \times T_p}{T_s} \qquad B. \quad T_s = \frac{E_s \times T_p}{E_p}$$

$$C. \quad \frac{E_p \times T_s}{E_s} = T_p \qquad D. \quad \frac{E_p \times T_s}{T_p} = E_s$$

3. AMPERES AND TURNS IN COIL:

$$\text{AMPERES (p)} \times \text{TURNS (p)} = \text{AMPERES (s)} \times \text{TURNS (s)} \\ \text{or} \\ I_p \times T_p = I_s \times T_s$$

$$A. \quad I_p = \frac{I_s \times T_s}{T_p} \qquad B. \quad T_p = \frac{I_s \times T_s}{I_p}$$

$$C. \quad \frac{I_p \times T_p}{I_s} = T_s \qquad D. \quad \frac{I_p \times T_p}{T_s} = I_s$$

VOLTAGE DROP CALCULATIONS INDUCTANCE NEGIGIBLE

- Vd = Voltage Drop
I = Current in Conductor (Amperes)
L = One-way Length of Circuit (Ft.)
Cm = Cross Section Area of Conductor (Circular Mils) (page 72)
K = Resistance in ohms of one circular mil foot of conductor

K = 12.9 for Copper Conductors @75°C

K = 21.2 for Aluminum Conductors @75°C

NOTE: K value changes with temperature.
See NEC chapter 9, Table 8, Notes

* SINGLE PHASE CIRCUITS:

$$Vd = \frac{2K \times L \times I}{Cm} \quad \text{or} \quad Cm = \frac{2K \times L \times I}{Vd}$$

* THREE PHASE CIRCUITS:

$$Vd = \frac{1.73K \times L \times I}{Cm} \quad \text{or} \quad Cm = \frac{1.73K \times L \times I}{Vd}$$

* Note: Always check ampacity tables to insure conductors' ampacity is equal to load after voltage drop calculation.

Refer to UGLY'S pages 72 - 78 for conductor size, type & ampacity.
See UGLY'S page 55 for example.

VOLTAGE DROP CALCULATIONS EXAMPLES

SINGLE PHASE VOLTAGE DROP

What is the voltage drop of a 240 volt single phase circuit consisting of #8 THWN copper conductors feeding a 30 ampere load that is 150 feet in length?

Voltage Drop Formula - See UGLY'S page 54

$$Vd = \frac{2K \times L \times I}{Cm} = \frac{2 \times 12.9 \times 150 \times 30}{16,510} = \frac{116,100}{16,510} = 7 \text{ Volts}$$

Percentage voltage drop = 7 volts/240 volts = .029 = **2.9%**
Voltage at load = 240 volts - 7 volts = **233** volts

THREE PHASE VOLTAGE DROP

What is the voltage drop of a 480 volt three phase circuit consisting of 250 kcmil THWN copper conductors that supply a 250 ampere load that is 500 feet from the source?

Voltage Drop Formula - See UGLY'S page 54
250 kcmil = 250,000 circular mils

$$Vd = \frac{1.73K \times L \times I}{Cm} = \frac{1.73 \times 12.9 \times 500 \times 250}{250,000} = \frac{2,789,625}{250,000} = 11 \text{ Volts}$$

Percentage voltage drop = 11 volts/480 volts = .0229 = **2.29%**
Voltage at load = 480 volts - 11 volts = **469** volts

Note: Always check ampacity tables for conductors selected

Refer to UGLY'S pages 72 - 78 for conductor size, type & ampacity.

ALTERNATE VOLTAGE DROP CALCULATIONS

(Courtesy of Cooper Bussmann)

How to figure volt loss (drop):

Multiply the **Distance** (length in feet of one wire) by the **Current** (expressed in amperes) by the **Multiplier** shown in Table A (see next page) for the kind of current and the size of wire to be used, by one over the number of conductors per phase. Then place a decimal point in front of the last 6 digits.

This results in the volt loss to be expected on that circuit.

Example: No. 6 copper wire in 180 feet of iron conduit - 3 phase, 40 amp. load at 80% power factor.

Multiply feet by amperes: $180 \times 40 = 7200$

Multiply this number by the multiplier from Table A for No. 6 wire, three phase at 80% power factor. $7200 \times .745 = 5364000$.

$$\text{Multiply by } \frac{1}{\#/\text{phase}} \quad 5364000 \times \frac{1}{1} = 5364000$$

Place the decimal point 6 places to the left. 5.364 volts expected volt loss.

(For a 240 volt circuit, the % voltage drop is $\frac{5.364}{240} \times 100$ or 2.23%).

This table takes into consideration reactance on AC circuits as well as resistance of the wire. Remember on short runs to verify that the size and type of wire indicated has sufficient ampere capacity.

How to select size of wire:

Multiply the **Distance** (length in feet of one wire) by the **Current** (expressed in amperes), by one over the number of conductors per phase.

Divide that figure into the permissible **Volt Loss** multiplied by 1,000,000.

In Table A, look in the column applying to the type of current and power factor for the figure nearest to, but not above your result. Then follow that row to the left and this is the wire size needed.

Example:

Copper in 180 feet of iron conduit - 3 phase, 40 amp. load at 80% power factor - volt loss from local code equals 5.5 volts.

$$\text{Multiply feet by amperes by } \frac{1}{\#/\text{phase}} : \quad 180 \times 40 \times \frac{1}{1} = 7200$$

$$\text{Divide (permissible volt loss multiplied by } 1,000,000) \quad \frac{5.5 \times 1,000,000}{7200} = 764$$

From Table A, select the number from the 3 phase, 80% power factor column that is nearest, but not greater than 764. This number is 745, indicating the size or wire needed is No.6.

TABLE A
MULTIPLIER FOR VOLTAGE DROP CALCULATIONS - STEEL CONDUIT

| WIRE SIZE | AMPACITY TYPE T,TW | TYPE RH, THHN, (60°C WIRE) | TYPE RHH, THHN, XHHW (90°C WIRE) | DIRECT CURRENT | THREE PHASE (60 CYCLE, LAGGING POWER FACTOR) | | | SINGLE PHASE (60 CYCLE, LAGGING POWER FACTOR) | 60% 100% 90% 80% 70% | 60% 100% 90% 80% 70% | 60% 100% 90% 80% 70% | |
|-----------|--------------------------|--|---|-------------------|---|------|------|--|----------------------------------|----------------------------------|----------------------------------|------|
| | | | | | 100% | 90% | 80% | | | | | |
| 14 | 20 | 25 | 6140 | 5369 | 4887 | 4371 | 3848 | 3322 | 6200 | 5643 | 5047 | 4444 |
| 12 | 25 | 30 | 3860 | 3464 | 3169 | 2841 | 2508 | 2172 | 4000 | 3659 | 3281 | 2897 |
| 10 | 35 | 40 | 2420 | 2078 | 1918 | 1728 | 1532 | 1334 | 2400 | 2214 | 1995 | 1769 |
| 8 | 40 | 50 | 1528 | 1350 | 1264 | 1148 | 1026 | 900 | 1560 | 1460 | 1326 | 1184 |
| 6 | 55 | 65 | 982 | 848 | 812 | 745 | 673 | 597 | 980 | 937 | 860 | 777 |
| 4 | 70 | 85 | 616 | 536 | 528 | 491 | 450 | 405 | 620 | 610 | 563 | 519 |
| 3 | 85 | 100 | 490 | 433 | 434 | 407 | 376 | 341 | 500 | 501 | 470 | 434 |
| 2 | 95 | 115 | 388 | 346 | 354 | 336 | 312 | 286 | 400 | 398 | 361 | 331 |
| 1 | 110 | 130 | 308 | 277 | 292 | 280 | 264 | 245 | 320 | 337 | 324 | 305 |
| 0 | 125 | 150 | 244 | 207 | 228 | 223 | 213 | 200 | 240 | 263 | 258 | 246 |
| 00 | 145 | 175 | 195 | 173 | 196 | 194 | 188 | 178 | 227 | 224 | 217 | 206 |
| 000 | 165 | 200 | 225 | 153 | 136 | 162 | 163 | 160 | 154 | 158 | 187 | 184 |
| 0000 | 195 | 230 | 260 | 122 | 109 | 136 | 140 | 139 | 136 | 126 | 157 | 161 |
| 250 | 215 | 255 | 290 | 103 | 93 | 123 | 128 | 129 | 108 | 142 | 148 | 148 |
| 300 | 245 | 320 | 386 | 77 | 108 | 115 | 117 | 117 | 90 | 125 | 133 | 135 |
| 350 | 260 | 350 | 73 | 67 | 98 | 106 | 109 | 109 | 78 | 113 | 122 | 126 |
| 400 | 280 | 380 | 64 | 60 | 91 | 99 | 103 | 104 | 70 | 105 | 114 | 118 |
| 500 | 320 | 430 | 52 | 50 | 81 | 90 | 94 | 96 | 58 | 94 | 104 | 111 |
| 600 | 355 | 420 | 475 | 43 | 75 | 84 | 89 | 92 | 50 | 86 | 97 | 103 |
| 750 | 400 | 475 | 535 | 34 | 36 | 68 | 78 | 84 | 42 | 79 | 91 | 97 |
| 1000 | 455 | 545 | 615 | 26 | 31 | 62 | 72 | 78 | 36 | 84 | 90 | 95 |

SHORT CIRCUIT CALCULATION

(Courtesy of Cooper Bussmann)

Basic Short-Circuit Calculation Procedure:

- Determine transformer full-load amperes from either:
 - Name plate
 - Formula:

$$3\text{Ø transf. } I_{L.L.} = \frac{KVA \times 1000}{E_{L-L} \times 1.732}$$

$$1\text{Ø transf. } I_{L.L.} = \frac{KVA \times 1000}{E_{L-L}}$$

- Find transformer multiplier.

$$\text{Multiplier} = \frac{100}{*\%Z_{trans}}$$

- Determine transformer let-thru short-circuit current.**

$$I_{S.C.} = I_{L.L.} \times \text{Multiplier}$$

- Calculate "f" factor.

$$3\text{Ø faults } f = \frac{1.732 \times L \times I_{3Ø}}{C \times E_{L-L}}$$

$$10 \text{ line-to-line (L-L) faults } f = \frac{2 \times L \times I_{L-L}}{C \times E_{L-L}}$$

on 1Ø Center Tapped Transformer

$$10 \text{ line-to-neutral (L-N) faults on 1Ø Center Tapped Transformer } f = \frac{2 \times L \times I_{L-N}}{C \times E_{L-N}}^{***}$$

L = length (feet) of conductor to the fault

C = constant from Table C (page 60) for conductors & busway. For parallel runs, multiply C values by the number of conductors per phase.

I = available short-circuit current in amperes at beginning of circuit.

- Calculate "M" (multiplier) $M = \frac{1}{1 + f}$

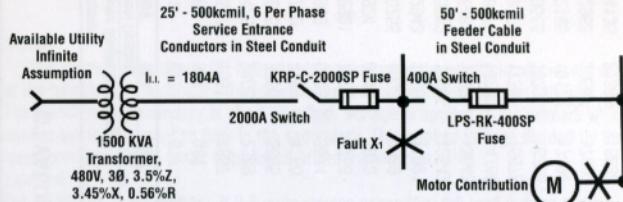
- Calculate the available short-circuit symmetrical RMS current at the point of fault.

$$I_{S.C. \text{ sym RMS}} = I_{S.C.} \times M$$

(Continued - next page)

SHORT CIRCUIT CALCULATION (continued)

(Courtesy of Cooper Bussmann)



Example - Short-Circuit Calculation:

(FAULT #1)

- $I_{L.L.} = \frac{KVA \times 1000}{E_{L-L} \times 1.732} = \frac{1500 \times 1000}{480 \times 1.732} = 1804 \text{ A}$

- $\text{Multiplier} = \frac{100}{*\%Z_{trans}} = \frac{100}{3.5} = 28.57$

- $I_{S.C.} = 1804 \times 28.57 = 51,540 \text{ A}$

- $f = \frac{1.732 \times L \times I_{3Ø}}{C \times E_{L-L}} = \frac{1.73 \times 25 \times 51,540}{6 \times 22,185 \times 480} = 0.0349$

- $M = \frac{1}{1 + f} = \frac{1}{1 + .0349} = .9663$

- $I_{S.C. \text{ sym RMS}} = I_{S.C.} \times M = 51,540 \times .9663 = 49,803 \text{ A}$

$I_{S.C. \text{ motor contrib}} = 4 \times 1,804 = 7,216 \text{ A}$

$I_{\text{total S.C. sym RMS}} = 49,803 + 7,216 = 57,019 \text{ A}$

(FAULT #2)

- Use $I_{S.C. \text{ sym RMS}}$ @ Fault X₁ to calculate "f"

$$f = \frac{1.73 \times 50 \times 49,803}{22,185 \times 480} = 0.4050$$

- $M = \frac{1}{1 + .4050} = .7117$

- $I_{S.C. \text{ sym RMS}} = 49,803 \times .7117 = 35,445 \text{ A}$

$I_{\text{sym motor contrib}} = 4 \times 1,804 = 7,216 \text{ A}$

$I_{\text{total S.C. sym RMS}} = 35,445 + 7,216 = 42,661 \text{ A}$

(Continued - next page)

SHORT-CIRCUIT CALCULATION (continued)

(Courtesy of Cooper Bussmann)

NOTES:

- * Transformer impedance (Z) helps to determine what the short circuit current will be at the transformer secondary. Transformer impedance is determined as follows: The transformer secondary is short circuited. Voltage is applied to the primary which causes full load current to flow in the secondary. This applied voltage divided by the rated primary voltage is the impedance of the transformer.

Example:

For a 480 volt rated primary, if 9.6 volts causes secondary full load current to flow through the shorted secondary, the transformer impedance is $9.6 \div 480 = .02 = 2\%Z$. In addition, U.L. listed transformers 25KVA and larger have a $\pm 10\%$ impedance tolerance. Short circuit amperes can be affected by this tolerance.

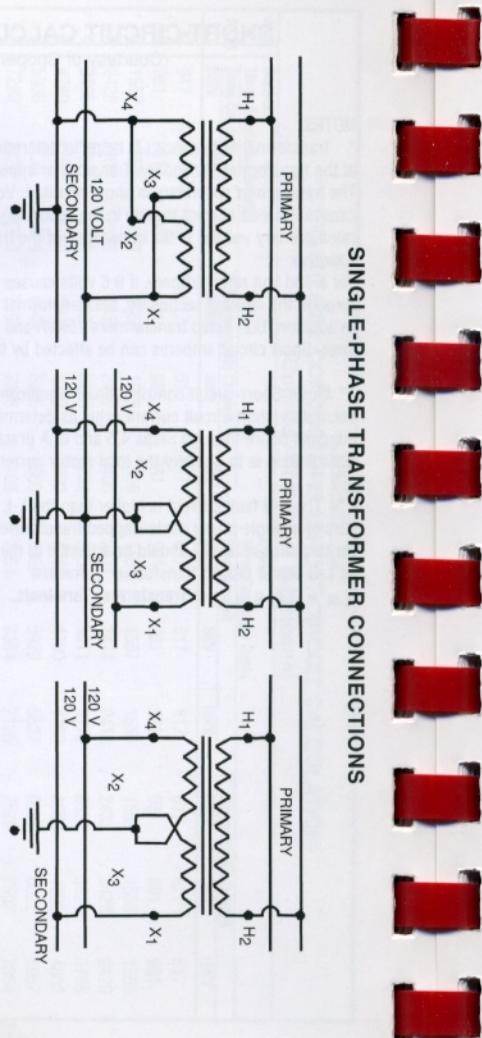
** Motor Short-circuit contribution, if significant, may be added to the transformer secondary short-circuit current value as determined in Step 3. Proceed with this adjusted figure through Steps 4,5 and 6. A practical estimate of motor short-circuit contribution is to multiply the total motor current in amperes by 4.

*** The L-N fault current is higher than the L-L fault current at the secondary terminals of a single-phase center-tapped transformer. The short-circuit current available (I) for this case in Step 4 should be adjusted at the transformer terminals as follows:
At L-N center tapped transformer terminals,
 $I_{L-N} = 1.5 \times I_{L-L}$ at Transformer Terminals.

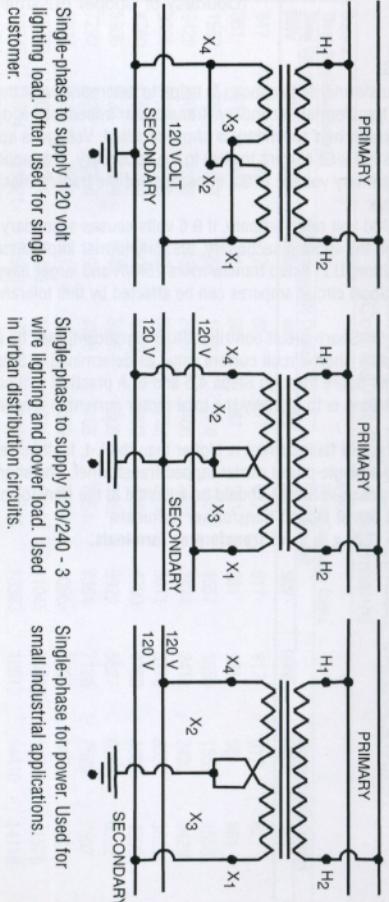
TABLE "C"
"C" VALUES for CONDUCTORS (SHORT-CIRCUIT CALCULATION)
(Courtesy of Cooper Bussmann)

| AWG or MCM | Copper Three Single Conductors | | Nonmagnetic Conduit | | Copper Three Conductor Cable | | Nonmagnetic Conduit | |
|------------------|-----------------------------------|-------|---------------------|-------|---------------------------------|-------|---------------------|-------|
| | 600V 5KV | 15KV | 600V 5KV | 15KV | 600V 5KV | 15KV | 600V 5KV | 15KV |
| 12 | 617 | 617 | 617 | 617 | 617 | 617 | 617 | 617 |
| 10 | 981 | 981 | 981 | 981 | 981 | 981 | 981 | 981 |
| 8 | 1557 | 1551 | 1557 | 1558 | 1555 | 1558 | 1557 | 1559 |
| 6 | 2425 | 2406 | 2389 | 2430 | 2417 | 2406 | 2424 | 2414 |
| 4 | 3806 | 3750 | 3695 | 3825 | 3789 | 3752 | 3830 | 3811 |
| 3 | 4760 | 4760 | 4760 | 4802 | 4802 | 4760 | 4790 | 4760 |
| 2 | 5906 | 5736 | 5574 | 6044 | 5926 | 5809 | 5989 | 5929 |
| 1 | 7292 | 7029 | 6758 | 7493 | 7306 | 7108 | 7454 | 7364 |
| 10 | 8924 | 8543 | 7973 | 9317 | 9033 | 8590 | 9209 | 9086 |
| 20 | 10755 | 10661 | 9389 | 11423 | 10877 | 10318 | 11244 | 11045 |
| 30 | 12843 | 11804 | 11021 | 13923 | 13048 | 12360 | 13656 | 13333 |
| 40 | 15082 | 13605 | 12542 | 16673 | 15351 | 14347 | 16391 | 15890 |
| 50 | 16483 | 14924 | 13643 | 18593 | 17102 | 15865 | 18310 | 17850 |
| 60 | 18176 | 16282 | 14768 | 20867 | 18975 | 17408 | 20617 | 20051 |
| 750 | 19703 | 17385 | 15678 | 22736 | 20526 | 18672 | 22646 | 21914 |
| 400 | 20565 | 18235 | 16365 | 24296 | 21786 | 19731 | 24253 | 23371 |
| 500 | 22185 | 19172 | 17492 | 26706 | 23277 | 21329 | 26880 | 25449 |
| 600 | 22965 | 20567 | 17962 | 28033 | 25203 | 22097 | 28752 | 27974 |
| 750 | 24136 | 18888 | 18888 | 28303 | 25430 | 22690 | 31050 | 30024 |
| 1000 | 25259 | 19923 | 19923 | 31490 | 33864 | 32688 | 329320 | 37197 |

BUCK AND BOOST TRANSFORMER CONNECTIONS



SINGLE-PHASE TRANSFORMER CONNECTIONS



SINGLE Ø TRANSFORMER CIRCUIT

A transformer is a stationary induction device for transferring electrical energy from one circuit to another without change of frequency. A transformer consists of two coils or windings wound upon a magnetic core of soft iron laminations, and insulated from one another.

THREE PHASE CONNECTIONS

WYE (STAR)

Voltage from "A", "B", or "C" to Neutral = $E_{\text{PHASE}} (E_p)$

Voltage between A-B, B-C, or C-A = $E_{\text{LINE}} (E_L)$

$I_L = I_p$, if balanced.

If unbalanced,

$$I_N = \sqrt{I_A^2 + I_B^2 + I_C^2 - (I_A \times I_B) - (I_B \times I_C) - (I_C \times I_A)}$$

$$E_L = E_p \times 1.73$$

$$E_p = E_L \div 1.73$$

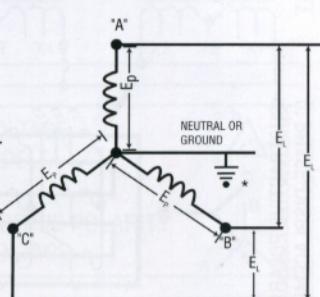
(True Power)

Power =

$$I_L \times E_L \times 1.73 \times \text{Power Factor} (\cosine)$$

(Apparent Power)

$$\text{Voltamperes} = I_L \times E_L \times 1.73$$



DELTA

$E_{\text{LINE}} (E_L) = E_{\text{PHASE}} (E_p)$

$$I_{\text{LINE}} = I_p \times 1.73$$

$$I_{\text{PHASE}} = I_L \div 1.73$$

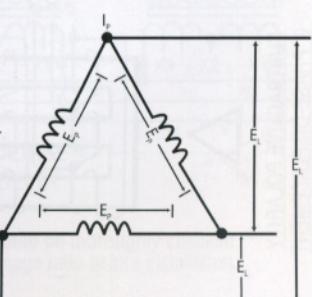
(True Power)

Power =

$$I_L \times E_L \times 1.73 \times \text{Power Factor} (\cosine)$$

(Apparent Power)

$$\text{Voltamperes} = I_L \times E_L \times 1.73$$



* Neutral could be ungrounded

Also see NEC A250 System Grounding Requirements

| THREE-PHASE TRANSFORMERS VOLTAGE (LINE TO LINE) | | | | | | FULL LOAD CURRENTS | | | | | | SINGLE-PHASE TRANSFORMERS VOLTAGE | | | | | |
|--|---------|---------|--------|--------|--------|--------------------|--------|--------|--------|-------|-------|--------------------------------------|---------|---------|---------|---------|------|
| KVA | 208 | 240 | 480 | 2400 | 4160 | KVA | 120 | 208 | 240 | 480 | 2400 | KVA | 120 | 208 | 240 | 480 | 2400 |
| 3 | 8.3 | 7.2 | .72 | .72 | .416 | 1 | 8.33 | 4.81 | 4.17 | 2.08 | .42 | 6 | 16.7 | 14.4 | 14.4 | 12.5 | 1.25 |
| 9 | 25.0 | 21.7 | 10.8 | 2.17 | 1.25 | 3 | 25.0 | 14.4 | 12.5 | 6.25 | 1.25 | 15 | 41.6 | 36.1 | 18.0 | 10.4 | 2.08 |
| 30 | 83.3 | 72.2 | 36.1 | 7.2 | 2.08 | 7.5 | 62.5 | 36.1 | 31.3 | 15.6 | 3.13 | 45 | 124.9 | 108.3 | 54.1 | 41.7 | 4.17 |
| 75 | 208.2 | 180.4 | 90.2 | 18.0 | 10.4 | 15 | 125.0 | 72.1 | 62.5 | 31.3 | 6.25 | 100 | 277.6 | 240.6 | 120.3 | 24.1 | 2.08 |
| 150 | 416.4 | 360.9 | 180.4 | 36.1 | 20.8 | 50 | 416.7 | 240.4 | 208.3 | 104.2 | 20.8 | 225 | 624.6 | 541.3 | 270.6 | 54.1 | 4.17 |
| 300 | 832.7 | 721.7 | 360.9 | 72.2 | 41.6 | 100 | 833.3 | 480.8 | 416.7 | 208.3 | 41.7 | 500 | 1387.9 | 1202.8 | 601.4 | 120.3 | 2.08 |
| 500 | 1387.9 | 1202.8 | 601.4 | 120.3 | 69.4 | 125 | 1041.7 | 601.0 | 520.8 | 260.4 | 52.1 | 750 | 2081.9 | 1804.3 | 902.1 | 180.4 | 2.08 |
| 1000 | 2775.8 | 2405.7 | 1202.8 | 240.5 | 104.1 | 167.5 | 1395.8 | 805.3 | 697.9 | 349.0 | 69.8 | 1500 | 4163.7 | 3608.3 | 1804.3 | 360.9 | 2.08 |
| 1500 | 4163.7 | 3608.3 | 1804.3 | 360.9 | 208.2 | 250 | 2083.3 | 1201.9 | 1041.7 | 520.8 | 104.2 | 2000 | 5551.6 | 4811.4 | 2405.7 | 481.1 | 2.08 |
| 2500 | 6999.5 | 6014.2 | 3007.1 | 601.4 | 347.0 | 500 | 2750.0 | 1601.7 | 1387.5 | 693.8 | 138.8 | 5000 | 13879.0 | 12028.5 | 6014.2 | 12028.8 | 2.08 |
| 7500 | 20818.5 | 18042.7 | 9021.4 | 1804.3 | 1040.9 | 4166.7 | 2403.8 | 2083.3 | 1041.7 | 520.8 | 104.2 | 10000 | 27758.0 | 24057.0 | 12028.5 | 2405.7 | 2.08 |

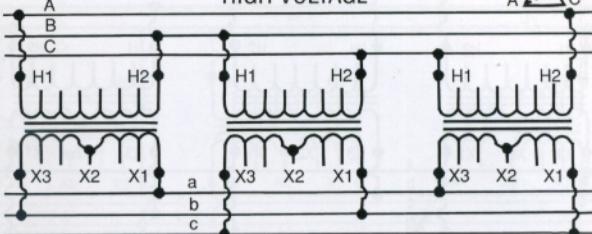
$$I = \frac{KVA \times 1000}{E \times 1.73} \quad \text{or} \quad KVA = \frac{E \times I \times 1.73}{1000}$$

$$I = \frac{KVA \times 1000}{E} \quad \text{or} \quad KVA = \frac{E \times I}{1000}$$

TRANSFORMER CONNECTIONS

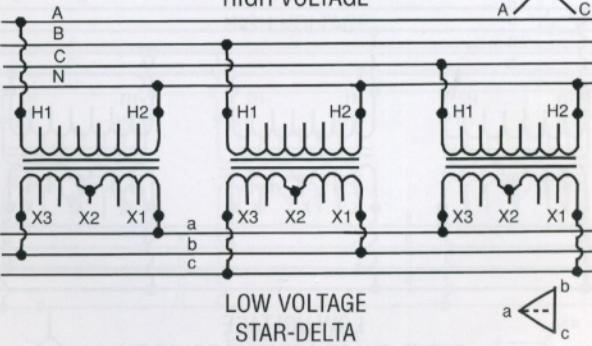
SERIES CONNECTIONS OF LOW VOLTAGE WINDINGS

THREE-PHASE ADDITIVE POLARITY HIGH VOLTAGE



LOW VOLTAGE
DELTA-DELTA

THREE-PHASE ADDITIVE POLARITY HIGH VOLTAGE

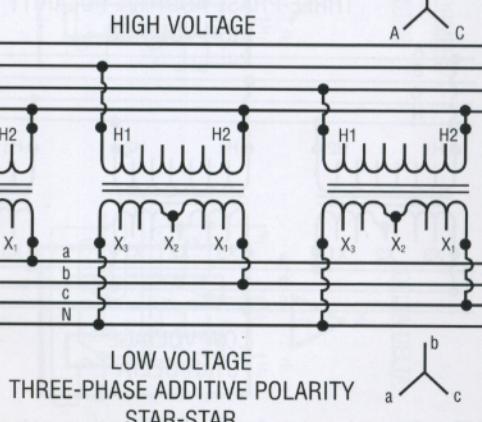
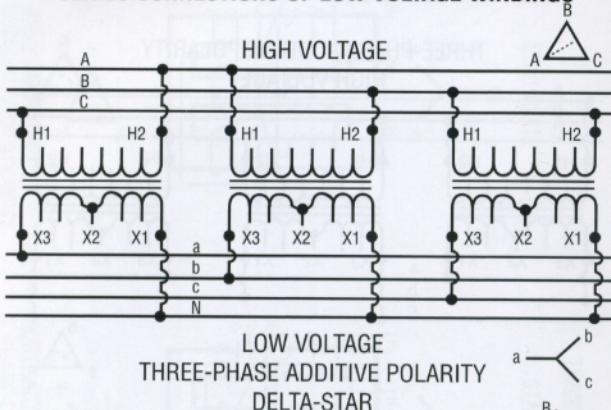


LOW VOLTAGE
STAR-DELTA

NOTE: Single-phase transformers should be thoroughly checked for impedance, polarity, and voltage ratio before installation.

TRANSFORMER CONNECTIONS

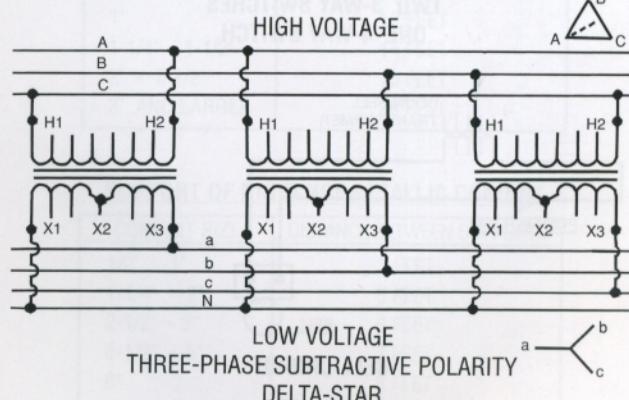
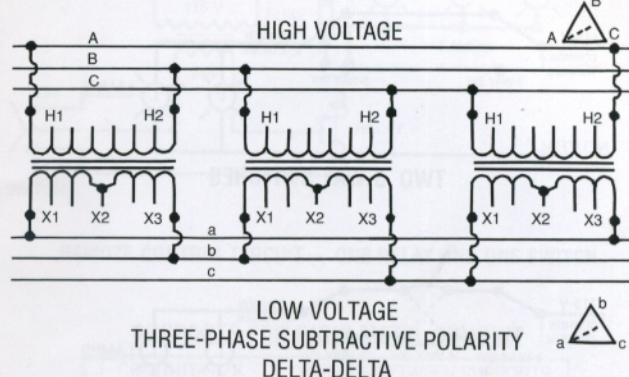
SERIES CONNECTIONS OF LOW VOLTAGE WINDINGS



NOTE: For additive polarity the H-1 and the X-1 bushings are diagonally opposite each other.

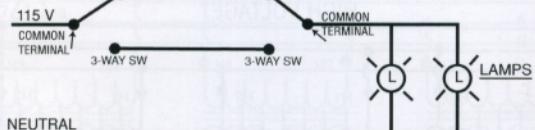
TRANSFORMER CONNECTIONS

SERIES CONNECTIONS OF LOW VOLTAGE WINDINGS

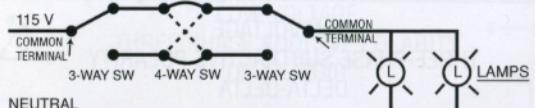


NOTE: For subtractive polarity the H-1 and the X-1 bushings are directly opposite each other.

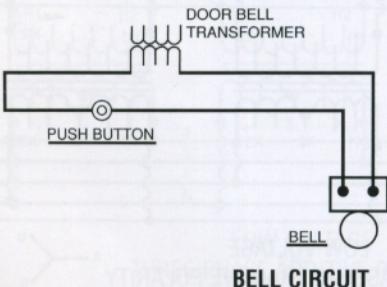
MISCELLANEOUS WIRING DIAGRAMS



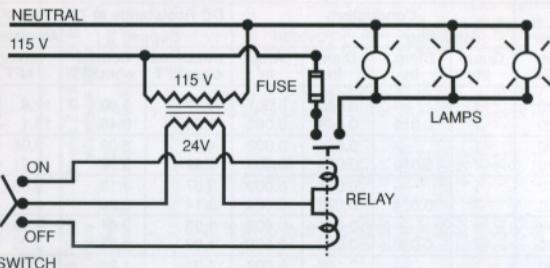
TWO 3-WAY SWITCHES



**TWO 3-WAY SWITCHES
ONE 4-WAY SWITCH**



MISCELLANEOUS WIRING DIAGRAMS



REMOTE CONTROL CIRCUIT - ONE RELAY AND ONE SWITCH

SUPPORTS FOR RIGID METAL CONDUIT

| CONDUIT SIZE | DISTANCE BETWEEN SUPPORTS |
|-----------------|---------------------------|
| 1/2" - 3/4" | 10 FEET |
| 1" | 12 FEET |
| 1-1/4" - 1-1/2" | 14 FEET |
| 2" - 2-1/2" | 16 FEET |
| 3" AND LARGER | 20 FEET |

SUPPORT OF RIGID NONMETALLIC CONDUIT

| CONDUIT SIZE | DISTANCE BETWEEN SUPPORTS |
|--------------|---------------------------|
| 1/2" - 1" | 3 FEET |
| 1-1/4" - 2" | 5 FEET |
| 2-1/2" - 3" | 6 FEET |
| 3-1/2" - 5" | 7 FEET |
| 6" | 8 FEET |

For SI units: (Supports) one foot = 0.3048 meter

CONDUCTOR PROPERTIES

| Size AWG/ kcmil | Area Cir. Mils | Conductors | | | DC Resistance at 75°C (167°F) | | | |
|-----------------------|----------------------|------------|--------------|--------------|-------------------------------|---------------------|-------------------|--------|
| | | Stranding | | Overall | Copper | | Aluminum | |
| | | Quantity | Diam. In. | Diam. In. | Area In ² | Uncoated ohm/kFT | Coated ohm/kFT | |
| 18 | 1620 | 1 | ---- | 0.040 | 0.001 | 7.77 | 8.08 | 12.8 |
| 18 | 1620 | 7 | 0.015 | 0.046 | 0.002 | 7.95 | 8.45 | 13.1 |
| 16 | 2580 | 1 | ---- | 0.051 | 0.002 | 4.89 | 5.08 | 8.05 |
| 16 | 2580 | 7 | 0.019 | 0.058 | 0.003 | 4.99 | 5.29 | 8.21 |
| 14 | 4110 | 1 | ---- | 0.064 | 0.003 | 3.07 | 3.19 | 5.06 |
| 14 | 4110 | 7 | 0.024 | 0.073 | 0.004 | 3.14 | 3.26 | 5.17 |
| 12 | 6530 | 1 | ---- | 0.081 | 0.005 | 1.93 | 2.01 | 3.18 |
| 12 | 6530 | 7 | 0.030 | 0.092 | 0.006 | 1.98 | 2.05 | 3.25 |
| 10 | 10380 | 1 | ---- | 0.102 | 0.008 | 1.21 | 1.26 | 2.00 |
| 10 | 10380 | 7 | 0.038 | 0.116 | 0.011 | 1.24 | 1.29 | 2.04 |
| 8 | 16510 | 1 | ---- | 0.128 | 0.013 | 0.764 | 0.786 | 1.26 |
| 8 | 16510 | 7 | 0.049 | 0.146 | 0.017 | 0.778 | 0.809 | 1.28 |
| 6 | 26240 | 7 | 0.061 | 0.184 | 0.027 | 0.491 | 0.510 | 0.808 |
| 4 | 41740 | 7 | 0.077 | 0.232 | 0.042 | 0.308 | 0.321 | 0.508 |
| 3 | 52620 | 7 | 0.087 | 0.260 | 0.053 | 0.245 | 0.254 | 0.403 |
| 2 | 66360 | 7 | 0.097 | 0.292 | 0.067 | 0.194 | 0.201 | 0.319 |
| 1 | 83690 | 19 | 0.066 | 0.332 | 0.087 | 0.154 | 0.160 | 0.253 |
| 1/0 | 105600 | 19 | 0.074 | 0.372 | 0.109 | 0.122 | 0.127 | 0.201 |
| 2/0 | 133100 | 19 | 0.084 | 0.418 | 0.137 | 0.0967 | 0.101 | 0.159 |
| 3/0 | 167800 | 19 | 0.094 | 0.470 | 0.173 | 0.0766 | 0.0797 | 0.126 |
| 4/0 | 211600 | 19 | 0.106 | 0.528 | 0.219 | 0.0608 | 0.0626 | 0.100 |
| 250 | ----- | 37 | 0.082 | 0.575 | 0.260 | 0.0515 | 0.0535 | 0.0847 |
| 300 | ----- | 37 | 0.090 | 0.630 | 0.312 | 0.0429 | 0.0446 | 0.0707 |
| 350 | ----- | 37 | 0.097 | 0.681 | 0.364 | 0.0367 | 0.0382 | 0.0605 |
| 400 | ----- | 37 | 0.104 | 0.728 | 0.416 | 0.0321 | 0.0331 | 0.0529 |
| 500 | ----- | 37 | 0.116 | 0.813 | 0.519 | 0.0258 | 0.0265 | 0.0424 |
| 600 | ----- | 61 | 0.099 | 0.893 | 0.626 | 0.0214 | 0.0223 | 0.0353 |
| 700 | ----- | 61 | 0.107 | 0.964 | 0.730 | 0.0184 | 0.0189 | 0.0303 |
| 750 | ----- | 61 | 0.111 | 0.998 | 0.782 | 0.0171 | 0.0176 | 0.0282 |
| 800 | ----- | 61 | 0.114 | 1.030 | 0.834 | 0.0161 | 0.0166 | 0.0265 |
| 900 | ----- | 61 | 0.122 | 1.094 | 0.940 | 0.0143 | 0.0147 | 0.0235 |
| 1000 | ----- | 61 | 0.128 | 1.152 | 1.042 | 0.0129 | 0.0132 | 0.0212 |
| 1250 | ----- | 91 | 0.117 | 1.289 | 1.305 | 0.0103 | 0.0106 | 0.0169 |
| 1500 | ----- | 91 | 0.128 | 1.412 | 1.566 | 0.00858 | 0.00883 | 0.0141 |
| 1750 | ----- | 127 | 0.117 | 1.526 | 1.829 | 0.00735 | 0.00756 | 0.0121 |
| 2000 | ----- | 127 | 0.126 | 1.632 | 2.092 | 0.00643 | 0.00662 | 0.0106 |

These resistance values are valid ONLY for the parameters as given. Using conductors having coated strands, different stranding type, and, especially, other temperatures changes the resistance.

Formula for temperature change: $R_t = R_75 [1 + \alpha_{t-75}]$ where $\alpha_{Cu} = 0.00323$, $\alpha_{Al} = 0.00330$ at 75°C.

See NEC Chapter 9, Table 8. See Ugly's page 127 - 135 for metric conversions.

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AC Resistance and Reactance for 600 Volt Cables, 3-Phase, 60 Hz, 75°C (167°F) –

Three Single Conductors in Conduit

| Size AWG/ kcmil | X (Reactance) for All Wires | AC Resistance for Uncoated Copper Wires | | | AC Resistance for Aluminum Wires | | | Effective Z at 0.85 PF for Uncoated Copper Wires | Effective Z at 0.85 PF for Aluminum Wires |
|-----------------------|--------------------------------|--|--------------------------|----------------|-------------------------------------|----------------|----------------|---|--|
| | | PVC, Al. Conduit | PVC, Steel Conduit | Al. Conduit | PVC, Steel Conduit | Al. Conduit | Al. Conduit | | |
| 14 | 0.058 | 0.073 | 3.1 | 3.1 | — | — | 2.7 | 2.7 | — |
| 12 | 0.054 | 0.068 | 2.0 | 2.0 | 3.2 | 3.2 | 1.7 | 2.8 | 2.8 |
| 10 | 0.050 | 0.063 | 1.2 | 1.2 | 2.0 | 2.0 | 1.1 | 1.8 | 1.8 |
| 8 | 0.052 | 0.065 | 0.78 | 0.78 | 1.3 | 1.3 | 0.69 | 0.70 | 1.1 |
| 6 | 0.051 | 0.064 | 0.49 | 0.49 | 0.81 | 0.81 | 0.45 | 0.45 | 0.72 |
| 4 | 0.048 | 0.060 | 0.31 | 0.31 | 0.51 | 0.51 | 0.29 | 0.29 | 0.46 |
| 3 | 0.047 | 0.059 | 0.25 | 0.25 | 0.40 | 0.40 | 0.23 | 0.24 | 0.37 |
| 2 | 0.045 | 0.057 | 0.19 | 0.20 | 0.32 | 0.32 | 0.19 | 0.20 | 0.30 |
| 1 | 0.046 | 0.057 | 0.15 | 0.16 | 0.25 | 0.25 | 0.16 | 0.16 | 0.24 |
| 1/0 | 0.044 | 0.055 | 0.12 | 0.13 | 0.20 | 0.20 | 0.13 | 0.13 | 0.20 |
| 2/0 | 0.043 | 0.054 | 0.10 | 0.10 | 0.16 | 0.16 | 0.11 | 0.11 | 0.16 |
| 3/0 | 0.042 | 0.052 | 0.077 | 0.082 | 0.13 | 0.13 | 0.088 | 0.092 | 0.13 |
| 4/0 | 0.041 | 0.051 | 0.062 | 0.067 | 0.11 | 0.11 | 0.074 | 0.078 | 0.11 |
| 5/0 | 0.041 | 0.052 | 0.052 | 0.057 | 0.085 | 0.090 | 0.066 | 0.070 | 0.084 |
| 300 | 0.041 | 0.051 | 0.044 | 0.049 | 0.071 | 0.076 | 0.059 | 0.063 | 0.082 |
| 350 | 0.040 | 0.050 | 0.038 | 0.043 | 0.061 | 0.063 | 0.053 | 0.058 | 0.073 |
| 400 | 0.040 | 0.049 | 0.033 | 0.038 | 0.054 | 0.059 | 0.055 | 0.059 | 0.086 |
| 500 | 0.039 | 0.048 | 0.027 | 0.032 | 0.043 | 0.045 | 0.048 | 0.043 | 0.087 |
| 600 | 0.039 | 0.048 | 0.023 | 0.028 | 0.036 | 0.041 | 0.038 | 0.044 | 0.091 |
| 750 | 0.038 | 0.048 | 0.019 | 0.024 | 0.021 | 0.029 | 0.034 | 0.043 | 0.095 |
| 1000 | 0.037 | 0.046 | 0.015 | 0.019 | 0.018 | 0.023 | 0.027 | 0.036 | 0.092 |

Notes: See NEC Table 9, page 70-568 for assumptions and explanations.
See Ugly's page 127 - 135 for metric conversion.

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ALLOWABLE AMPACITIES OF CONDUCTORS

Allowable Ampacities of Insulated Conductors Rated 0 - 2000 Volts, 60°C Through 90°C (140°F Through 194°F), Not More Than Three Current-Carrying Conductors in Raceway, Cable, or Earth (Directly Buried), Based on Ambient Air Temperature of 30°C (86°F)

| SIZE | 60°C (140°F) | 75°C (167°F) | 90°C (194°F) | 60°C (140°F) | 75°C (167°F) | 90°C (194°F) | SIZE |
|--------------------|---------------------|--|---------------------|---|--|--------------------|------|
| AWG or kcmil | TYPES TWH, UF | TYPES TBS, SA, SIS, FEP, FEPB, MI, RHH, RHW-2, THHN, THW, THWN, XHHW, THW-2, THWN-2, USE-2, XHH, XHHW, XHHW-2, ZW-2 | TYPES TWH, UF | TYPES TWH, THHN, THW, THWN, XHHW, USE | TYPES TBS, SA, SIS, FEP, FEPB, MI, RHH, RHW-2, THHN, THW, THWN-2, THW-2, RHH, RHW-2, USE-2, XHH, XHHW, XHHW-2, ZW-2 | AWG or kcmil | |
| 14* | 20 | 20 | 25 | --- | --- | --- | 14* |
| 12* | 25 | 25 | 30 | 20 | 20 | 25 | 12* |
| 10* | 30 | 35 | 40 | 25 | 30 | 35 | 10* |
| 8 | 40 | 50 | 55 | 30 | 40 | 45 | 8 |
| 6 | 55 | 65 | 75 | 40 | 50 | 60 | 6 |
| 4 | 70 | 85 | 95 | 55 | 65 | 75 | 4 |
| 3 | 85 | 100 | 110 | 65 | 75 | 85 | 3 |
| 2 | 95 | 115 | 130 | 75 | 90 | 100 | 2 |
| 1 | 110 | 130 | 150 | 85 | 100 | 115 | 1 |
| 1/0 | 125 | 150 | 170 | 100 | 120 | 135 | 1/0 |
| 2/0 | 145 | 175 | 195 | 115 | 135 | 150 | 2/0 |
| 3/0 | 165 | 200 | 225 | 130 | 155 | 175 | 3/0 |
| 4/0 | 195 | 230 | 260 | 150 | 180 | 205 | 4/0 |
| 250 | 215 | 255 | 290 | 170 | 205 | 230 | 250 |
| 300 | 240 | 285 | 320 | 190 | 230 | 255 | 300 |
| 350 | 260 | 310 | 350 | 210 | 250 | 280 | 350 |
| 400 | 280 | 335 | 380 | 225 | 270 | 305 | 400 |
| 500 | 320 | 380 | 430 | 260 | 310 | 350 | 500 |
| 600 | 355 | 420 | 475 | 285 | 340 | 385 | 600 |
| 700 | 385 | 460 | 520 | 310 | 375 | 420 | 700 |
| 750 | 400 | 475 | 535 | 320 | 385 | 435 | 750 |
| 800 | 410 | 490 | 555 | 330 | 395 | 450 | 800 |
| 900 | 435 | 520 | 585 | 355 | 425 | 480 | 900 |
| 1000 | 455 | 545 | 615 | 375 | 445 | 500 | 1000 |
| 1250 | 495 | 590 | 665 | 405 | 485 | 545 | 1250 |
| 1500 | 520 | 625 | 705 | 435 | 520 | 585 | 1500 |
| 1750 | 545 | 650 | 735 | 455 | 545 | 615 | 1750 |
| 2000 | 560 | 665 | 750 | 470 | 560 | 630 | 2000 |

TEMPERATURE CORRECTION FACTORS

For ambient temperatures other than 30°C, multiply the allowable ampacities shown above by the appropriate factor shown below.

| Ambient Temp °C | 1.08 | 1.05 | 1.04 | 1.08 | 1.05 | 1.04 | 70 - 77 |
|-----------------|------|------|------|------|------|------|-----------|
| 21 - 25 | 1.08 | 1.05 | 1.04 | 1.08 | 1.05 | 1.04 | 78 - 86 |
| 26 - 30 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| 31 - 35 | 0.91 | 0.94 | 0.96 | 0.91 | 0.94 | 0.96 | 87 - 95 |
| 36 - 40 | 0.82 | 0.88 | 0.91 | 0.82 | 0.88 | 0.91 | 96 - 104 |
| 41 - 45 | 0.71 | 0.82 | 0.87 | 0.71 | 0.82 | 0.87 | 105 - 113 |
| 46 - 50 | 0.58 | 0.75 | 0.82 | 0.58 | 0.75 | 0.82 | 114 - 122 |
| 51 - 55 | 0.41 | 0.67 | 0.76 | 0.41 | 0.67 | 0.76 | 123 - 131 |
| 56 - 60 | — | 0.58 | 0.71 | — | 0.58 | 0.71 | 132 - 140 |
| 61 - 70 | — | 0.33 | 0.58 | — | 0.33 | 0.58 | 141 - 158 |
| 71 - 80 | — | 0.41 | — | — | 0.41 | — | 159 - 176 |

See UGLY'S page 78 for Footnotes to this page, Overcurrent Protection (Fuses and Circuit Breakers), Adjustment Factors based on Number of Conductors, Adjustment Examples and copyright statement. See NEC 240.4(D).

ALLOWABLE AMPACIES OF CONDUCTORS

Allowable Ampacities of Single Insulated Conductors Rated 0 - 2000 Volts in Free Air, Based on Ambient Air Temperature of 30°C (86°F)

| SIZE | 60°C (140°F) | 75°C (167°F) | 90°C (194°F) | 60°C (140°F) | 75°C (167°F) | 90°C (194°F) | SIZE | |
|--------------------|---------------------|--|---------------------|--|---------------------|--|---------------------|--|
| AWG or kcmil | TYPES TWH, UF | TYPES TBS, SA, SIS, FEP, FEPB, MI, RHH, RHW-2, THHN, THW, THWN, XHHW, THW-2, THWN-2, USE-2, XHH, XHHW, XHHW-2, ZW-2 | TYPES TWH, UF | TYPES TBS, SA, SIS, FEP, FEPB, MI, RHH, RHW-2, THHN, THW, THWN, XHHW, THW-2, THWN-2, USE-2, XHH, XHHW, XHHW-2, ZW-2 | TYPES TWH, UF | TYPES TBS, SA, SIS, FEP, FEPB, MI, RHH, RHW-2, THHN, THW, THWN, XHHW, THW-2, THWN-2, USE-2, XHH, XHHW, XHHW-2, ZW-2 | TYPES TWH, UF | TYPES TBS, SA, SIS, FEP, FEPB, MI, RHH, RHW-2, THHN, THW, THWN, XHHW, THW-2, THWN-2, USE-2, XHH, XHHW, XHHW-2, ZW-2 |
| 14* | 25 | 30 | 35 | — | — | — | 14* | |
| 12* | 30 | 35 | 40 | 25 | 30 | 35 | 12* | |
| 10* | 40 | 50 | 55 | 35 | 40 | 40 | 10* | |
| 8 | 60 | 70 | 80 | 45 | 55 | 60 | 8 | |
| 6 | 80 | 95 | 105 | 60 | 75 | 80 | 6 | |
| 4 | 105 | 125 | 140 | 80 | 100 | 110 | 4 | |
| 3 | 120 | 145 | 165 | 95 | 115 | 130 | 3 | |
| 2 | 140 | 170 | 190 | 110 | 135 | 150 | 2 | |
| 1 | 165 | 195 | 220 | 130 | 155 | 175 | 1 | |
| 1/0 | 195 | 230 | 260 | 150 | 180 | 205 | 1/0 | |
| 2/0 | 225 | 265 | 300 | 175 | 210 | 235 | 2/0 | |
| 3/0 | 260 | 310 | 350 | 200 | 240 | 275 | 3/0 | |
| 4/0 | 300 | 360 | 405 | 235 | 280 | 315 | 4/0 | |
| 250 | 340 | 405 | 455 | 265 | 315 | 355 | 250 | |
| 300 | 375 | 445 | 505 | 290 | 350 | 395 | 300 | |
| 350 | 420 | 505 | 570 | 330 | 395 | 445 | 350 | |
| 400 | 455 | 545 | 615 | 355 | 425 | 480 | 400 | |
| 500 | 515 | 620 | 700 | 405 | 485 | 545 | 500 | |
| 600 | 575 | 690 | 780 | 455 | 540 | 615 | 600 | |
| 700 | 630 | 755 | 855 | 500 | 595 | 675 | 700 | |
| 750 | 655 | 785 | 885 | 515 | 620 | 700 | 750 | |
| 800 | 680 | 815 | 920 | 535 | 645 | 725 | 800 | |
| 900 | 730 | 870 | 985 | 580 | 700 | 785 | 900 | |
| 1000 | 780 | 935 | 1055 | 625 | 750 | 845 | 1000 | |
| 1250 | 890 | 1065 | 1200 | 710 | 855 | 960 | 1250 | |
| 1500 | 980 | 1175 | 1325 | 795 | 950 | 1075 | 1500 | |
| 1750 | 1070 | 1280 | 1445 | 875 | 1050 | 1185 | 1750 | |
| 2000 | 1155 | 1385 | 1560 | 960 | 1150 | 1335 | 2000 | |

TEMPERATURE CORRECTION FACTORS

For ambient temperatures other than 30°C, multiply the allowable ampacities shown above by the appropriate factor shown below.

| | | | | | | | |
|---------|------|------|------|------|------|------|-----------|
| 21 - 25 | 1.08 | 1.05 | 1.04 | 1.08 | 1.05 | 1.04 | 70 - 77 |
| 26 - 30 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 78 - 86 |
| 31 - 35 | 0.91 | 0.94 | 0.96 | 0.91 | 0.94 | 0.96 | 87 - 95 |
| 36 - 40 | 0.82 | 0.88 | 0.91 | 0.82 | 0.88 | 0.91 | 96 - 104 |
| 41 - 45 | 0.71 | 0.82 | 0.87 | 0.71 | 0.82 | 0.87 | 105 - 113 |
| 46 - 50 | 0.58 | 0.75 | 0.82 | 0.58 | 0.75 | 0.82 | 114 - 122 |
| 51 - 55 | 0.41 | 0.67 | 0.76 | 0.41 | 0.67 | 0.76 | 123 - 131 |
| 56 - 60 | — | 0.58 | 0.71 | — | 0.58 | 0.71 | 132 - 140 |
| 61 - 70 | — | 0.33 | 0.58 | — | 0.33 | 0.58 | 141 - 158 |
| 71 - 80 | — | 0.41 | — | — | 0.41 | — | 159 - 176 |

See UGLY'S page 78 for Footnotes to this page, Overcurrent Protection (Fuses and Circuit Breakers), Adjustment Factors based on Number of Conductors, Adjustment Examples and copyright statement. See NEC 240.4(D).

ALLOWABLE AMPACITIES OF CONDUCTORS

Allowable Ampacities of Insulated Conductors Rated 0 - 2000 Volts, 150°C Through 250°C (302°F Through 482°F), Not More Than Three Current-Carrying Conductors in Raceway or Cable, Based on Ambient Air Temperature of 40°C (104°F)

| SIZE | 150°C (302°F) | 200°C (392°F) | 250°C (482°F) | 150°C (302°F) | SIZE |
|--------------------|--|--------------------------------------|--------------------------------------|--|--------------------|
| AWG or kcmil | TYPE Z | TYPES FEP, FEPB, PFA, SA | TYPES PFH, TFE | TYPE Z | AWG or kcmil |
| | | COPPER | NICKEL or NICKEL-COATED COPPER | ALUMINUM or COPPER-CLAD ALUMINUM | |
| 14 | 34 | 36 | 39 | --- | 14 |
| 12 | 43 | 45 | 54 | 30 | 12 |
| 10 | 55 | 60 | 73 | 44 | 10 |
| 8 | 76 | 83 | 93 | 57 | 8 |
| 6 | 96 | 110 | 117 | 75 | 6 |
| 4 | 120 | 125 | 148 | 94 | 4 |
| 3 | 143 | 152 | 166 | 109 | 3 |
| 2 | 160 | 171 | 191 | 124 | 2 |
| 1 | 186 | 197 | 215 | 145 | 1 |
| 1/0 | 215 | 229 | 244 | 169 | 1/0 |
| 2/0 | 251 | 260 | 273 | 198 | 2/0 |
| 3/0 | 288 | 297 | 308 | 227 | 3/0 |
| 4/0 | 332 | 346 | 361 | 260 | 4/0 |
| Ambient Temp °C | TEMPERATURE CORRECTION FACTORS | | | | Ambient Temp F° |
| | For ambient temperatures other than 40°C, multiply the allowable ampacities shown above by the appropriate factor shown below. | | | | |
| 41 - 50 | 0.95 | 0.97 | 0.98 | 0.95 | 105 - 122 |
| 51 - 60 | 0.90 | 0.94 | 0.95 | 0.90 | 123 - 140 |
| 61 - 70 | 0.85 | 0.90 | 0.93 | 0.85 | 141 - 158 |
| 71 - 80 | 0.80 | 0.87 | 0.90 | 0.80 | 159 - 176 |
| 81 - 90 | 0.74 | 0.83 | 0.87 | 0.74 | 177 - 194 |
| 91 - 100 | 0.67 | 0.79 | 0.85 | 0.67 | 195 - 212 |
| 101 - 120 | 0.52 | 0.71 | 0.79 | 0.52 | 213 - 248 |
| 121 - 140 | 0.30 | 0.61 | 0.72 | 0.30 | 249 - 284 |
| 141 - 160 | --- | 0.50 | 0.65 | --- | 285 - 320 |
| 161 - 180 | --- | 0.35 | 0.58 | --- | 321 - 356 |
| 181 - 200 | --- | --- | 0.49 | --- | 357 - 392 |
| 201 - 225 | --- | --- | 0.35 | --- | 393 - 437 |

ALLOWABLE AMPACITIES OF CONDUCTORS

Allowable Ampacities of Single Insulated Conductors, Rated 0 - 2000 Volts, 150°C Through 250°C (302°F Through 482°F), in Free Air, Based on Ambient Air Temperature of 40°C (104°F)

| SIZE | 150°C (302°F) | 200°C (392°F) | 250°C (482°F) | 150°C (302°F) | SIZE |
|--------------------|--|--------------------------------------|--------------------------------------|--|--------------------|
| AWG or kcmil | TYPE Z | TYPES FEP, FEPB, PFA, SA | TYPES PFH, TFE | TYPE Z | AWG or kcmil |
| | | COPPER | NICKEL or NICKEL-COATED COPPER | ALUMINUM or COPPER-CLAD ALUMINUM | |
| 14 | 46 | 54 | 59 | --- | 14 |
| 12 | 60 | 68 | 78 | 47 | 12 |
| 10 | 80 | 90 | 107 | 63 | 10 |
| 8 | 106 | 124 | 142 | 83 | 8 |
| 6 | 155 | 165 | 205 | 112 | 6 |
| 4 | 190 | 220 | 278 | 148 | 4 |
| 3 | 214 | 252 | 327 | 170 | 3 |
| 2 | 255 | 293 | 381 | 198 | 2 |
| 1 | 293 | 344 | 440 | 228 | 1 |
| 1/0 | 339 | 399 | 532 | 263 | 1/0 |
| 2/0 | 390 | 467 | 591 | 305 | 2/0 |
| 3/0 | 451 | 546 | 708 | 351 | 3/0 |
| 4/0 | 529 | 629 | 830 | 411 | 4/0 |
| Ambient Temp °C | TEMPERATURE CORRECTION FACTORS | | | | Ambient Temp F° |
| | For ambient temperatures other than 40°C, multiply the allowable ampacities shown above by the appropriate factor shown below. | | | | |
| 41 - 50 | 0.95 | 0.97 | 0.98 | 0.95 | 105 - 122 |
| 51 - 60 | 0.90 | 0.94 | 0.95 | 0.90 | 123 - 140 |
| 61 - 70 | 0.85 | 0.90 | 0.93 | 0.85 | 141 - 158 |
| 71 - 80 | 0.80 | 0.87 | 0.90 | 0.80 | 159 - 176 |
| 81 - 90 | 0.74 | 0.83 | 0.87 | 0.74 | 177 - 194 |
| 91 - 100 | 0.67 | 0.79 | 0.85 | 0.67 | 195 - 212 |
| 101 - 120 | 0.52 | 0.71 | 0.79 | 0.52 | 213 - 248 |
| 121 - 140 | 0.30 | 0.61 | 0.72 | 0.30 | 249 - 284 |
| 141 - 160 | --- | 0.50 | 0.65 | --- | 285 - 320 |
| 161 - 180 | --- | 0.35 | 0.58 | --- | 321 - 356 |
| 181 - 200 | --- | --- | 0.49 | --- | 357 - 392 |
| 201 - 225 | --- | --- | 0.35 | --- | 393 - 437 |

See UGLY'S page 78 for Footnotes to this page, Overcurrent Protection (Fuses and Circuit Breakers), Adjustment Factors based on Number of Conductors, Adjustment Examples and copyright statement. See NEC 240.4(D).

See UGLY'S page 78 for Footnotes to this page, Overcurrent Protection (Fuses and Circuit Breakers), Adjustment Factors based on Number of Conductors, Adjustment Examples and copyright statement. See NEC 240.4(D).

* FOOTNOTES TO PAGES 74 - 78

Unless specifically permitted in 240.4(E) or 240.4(G), the overcurrent protection shall not exceed 15 amperes for 14 AWG, 20 amperes for 12 AWG, and 30 amperes for 10 AWG copper; or 15 amperes for 12 AWG and 25 amperes for 10 AWG aluminum and copper-clad aluminum after any correction factors for ambient temperature and number of conductors have been applied.

AMPACTY CORRECTION AND ADJUSTMENT FACTORS

EXAMPLES

UGLY'S page 74 shows ampacity values for not more than three current-carrying conductors in a raceway or cable and an ambient (surrounding) temperature of 30°C (86°F).

(Example 1) A raceway contains three #3 THWN conductors for a three phase circuit at an ambient temperature of 30°C.

UGLY'S page 74, 75° column indicates **100 amperes**.

(Example 2) A raceway contains three #3 THWN conductors for a three phase circuit at an ambient temperature of 40°C. UGLY'S page 74, 75° column indicates **100 amperes**. This value must be corrected for ambient temperature (see Temperature Correction Factors at bottom of UGLY'S page 74). 40°C factor is .88

$$100 \text{ amperes} \times .88 = \mathbf{88 \text{ amperes}} = \text{corrected ampacity}$$

(Example 3) A raceway contains six #3 THWN conductors for two three phase circuits at an ambient temperature of 30°C.

UGLY'S page 74, 75° column indicates **100 amperes**. This value must be adjusted for more than three current-carrying conductors. The Table on UGLY'S page 79 requires an adjustment of **80%** for four through six current-carrying conductors. $100 \text{ amperes} \times 80\% = \mathbf{80 \text{ amperes}}$

The adjusted ampacity is **80 amperes**

(Example 4) A raceway contains six #3 THWN conductors for two three phase circuits in an ambient temperature of 40°C. These conductors must be derated for both temperature and number of conductors.

UGLY'S page 74, 75° column indicates **100 amperes**

UGLY'S page 74, 40°C temperature factor is **.88**

UGLY'S page 79, 4 - 6 conductor factor is **.80**

$$100 \text{ amperes} \times .88 \times .80 = \mathbf{70.4 \text{ amperes}}$$

The new derated ampacity is **70.4 amperes**.

ADJUSTMENT FACTORS

for More than Three Current-Carrying Conductors in a Raceway or Cable

| Number of Current-Carrying Conductors | Percent of Values in Tables 310-16 through 310-19 as Adjusted for Ambient Temperature if Necessary |
|---------------------------------------|--|
| 4 - 6 | 80 |
| 7 - 9 | 70 |
| 10 - 20 | 50 |
| 21 - 30 | 45 |
| 31 - 40 | 40 |
| 41 and above | 35 |

INSULATION CHART

| TRADE NAME | LETTER | MAX. TEMP. | APPLICATION PROVISIONS |
|--|-------------------|---------------------------------|--|
| FLUORINATED ETHYLENE PROPYLENE | FEP OR FEPB | 90°C 194°F 200°C 392°F | DRY AND DAMP LOCATIONS DRY LOCATIONS - SPECIAL APPLICATIONS ² |
| MINERAL INSULATION (METAL SHEATHED) | MI | 90°C 194°F 250°C 482°F | DRY AND WET LOCATIONS SPECIAL APPLICATIONS ² |
| MOISTURE, HEAT-, AND OIL-RESISTANT THERMOPLASTIC | MTW | 60°C 140°F 90°C 194°F | MACHINE TOOL WIRING IN WET LOCATIONS MACHINE TOOL WIRING IN DRY LOCATIONS, FPN: See NFPA 79 |
| PAPER | | 85°C 185°F | FOR UNDERGROUND SERVICE CONDUCTORS, OR BY SPECIAL PERMISSION |
| PERFLUOROALKOXY | PFA | 90°C 194°F 200°C 392°F | DRY AND DAMP LOCATIONS DRY LOCATIONS - SPECIAL APPLICATIONS ² |

SEE UGLY'S PAGE 74 FOR SPECIAL PROVISIONS AND/OR APPLICATIONS.

INSULATION CHART

| TRADE NAME | LETTER | MAX. TEMP. | APPLICATION PROVISIONS |
|---|------------------|---------------------------------|---|
| PERFLUOROALKOXY | PFAH | 250°C 482°F | DRY LOCATIONS ONLY. ONLY FOR LEADS WITHIN APPARATUS OR WITHIN RACEWAYS CONNECTED TO APPARATUS, (NICKEL OR NICKEL-COATED COPPER ONLY). |
| THERMOSET | RHH | 90°C 194°F | DRY AND DAMP LOCATIONS |
| MOISTURE-RESISTANT THERMOSET | RHW ⁴ | 75°C 167°F | DRY & WET LOCATIONS |
| MOISTURE-RESISTANT THERMOSET | RHW-2 | 90°C 194°F | DRY AND WET LOCATIONS |
| SILICONE | SA | 90°C 194°F 200°C 392°F | DRY AND DAMP LOCATIONS FOR SPECIAL APPLICATIONS ² |
| THERMOSET | SIS | 90°C 194°F | SWITCHBOARD WIRING ONLY |
| THERMOPLASTIC AND FIBROUS OUTER BRAID | TBS | 90°C 194°F | SWITCHBOARD WIRING ONLY |
| EXTENDED POLYTETRAFLUORO-ETHYLENE | TFE | 250°C 482°F | DRY LOCATIONS ONLY. ONLY FOR LEADS WITHIN APPARATUS OR WITHIN RACEWAYS CONNECTED TO APPARATUS, OR AS OPEN WIRING (NICKEL OR NICKEL-COATED COPPER ONLY). |
| HEAT-RESISTANT THERMOPLASTIC | THHN | 90°C 194°F | DRY AND DAMP LOCATIONS |
| MOISTURE-AND HEAT-RESISTANT THERMOPLASTIC | THHW | 75°C 167°F 90°C 194°F | WET LOCATION DRY LOCATION |

SEE UGLY'S PAGE 74 FOR SPECIAL PROVISIONS AND/OR APPLICATIONS.

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INSULATION CHART

| TRADE NAME | LETTER | MAX. TEMP. | APPLICATION PROVISIONS |
|--|-------------------|---|--|
| MOISTURE - AND HEAT-RESISTANT THERMOPLASTIC | THW ⁴ | 75°C 167°F 90°C 194°F | DRY & WET LOCATIONS SPECIAL APPL. WITHIN ELECTRIC DISCHARGE LIGHTING EQUIPMENT, LIMITED TO 1000 OPEN-CIRCUIT VOLTS OR LESS, (SIZE 14-8 ONLY AS PERMITTED IN SECTION 410-33) |
| MOISTURE - AND HEAT-RESISTANT THERMOPLASTIC | THWN ⁴ | 75°C 167°F | DRY AND WET LOCATIONS |
| MOISTURE-RESISTANT THERMOPLASTIC | TW | 60°C 140°F | DRY AND WET LOCATIONS |
| UNDERGROUND FEEDER AND BRANCH-CIRCUIT CABLE-SINGLE CONDUCTOR, (FOR TYPE "UF" CABLE EMPLOYING MORE THAN 1 CONDUCTOR. (SEE NEC ART. 340) | UF | 60°C 140°F 75°C 167°F ⁷ | SEE ARTICLE 340 N.E.C. |
| UNDERGROUND SERVICE-ENTRANCE CABLE-SINGLE CONDUCTOR, (FOR TYPE "USE" CABLE EMPLOYING MORE THAN 1 CONDUCTOR. SEE N.E.C. ART. 338) | USE ⁴ | 75°C 167°F | SEE ARTICLE 338 N.E.C. |
| THERMOSET | XHH | 90°C 194°F | DRY AND DAMP LOCATIONS |

SEE UGLY'S PAGE 74 FOR SPECIAL PROVISIONS AND/OR APPLICATIONS.

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INSULATION CHART

| TRADE NAME | LETTER | MAX. TEMP. | APPLICATION PROVISIONS |
|--|-------------------|--|--|
| MOISTURE-RESISTANT THERMOSET | XHHW ⁴ | 90°C 194°F 75°C 167°F | DRY AND DAMP LOCATIONS WET LOCATIONS |
| MOISTURE-RESISTANT THERMOSET | XHHW-2 | 90°C 194°F | DRY AND WET LOCATIONS |
| MODIFIED ETHYLENE TETRAFLUORO-ETHYLENE | Z | 90°C 194°F 150°C 302°F | DRY AND DAMP LOCATIONS DRY LOCATIONS - SPECIAL APPLICATIONS ² |
| MODIFIED ETHYLENE TETRAFLUORO-ETHYLENE | ZW ⁴ | 75°C 167°F 90°C 194°F 150°C 302°F | WET LOCATIONS DRY AND DAMP LOCATIONS DRY LOCATIONS - SPECIAL APPLICATIONS ² |

FOOTNOTES:

- 1 Some insulations do not require an outer covering.
- 2 Where design conditions require maximum conductor operating temperatures above 90°C (194°F).
- 3 For signaling circuits permitting 300-volt insulation.
- 4 Listed wire types designated with the suffix "-2," such as RHW-2, shall be permitted to be used at a continuous 90°C (194°F) operating temperature, wet or dry.
- 5 Some rubber insulations do not require an outer covering.
- 6 Includes integral jacket.
- 7 For ampacity limitation, see Section 340.80 NEC.
- 8 Insulation thickness shall be permitted to be 2.03 mm (80 mils) for listed Type USE conductors that have been subjected to special investigations. The non-metallic covering over individual rubber-covered conductors of aluminum-sheathed cable and of lead-sheathed or multiconductor cable shall not be required to be flame retardant. For Type MC cable, see 330.104. For nonmetallic-sheathed cable, see Article 334, Part III. For Type UF cable, see Article 340, Part III.

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MAXIMUM NUMBER OF CONDUCTORS IN TRADE SIZES OF CONDUIT OR TUBING

The 2002 National Electrical Code® shows 85 tables for conduit fill. There is a separate table for each type of conduit. In order to keep *Ugly's Electrical References*® in a compact and easy to use format, the following tables are included:

Electrical Metallic Tubing (EMT), Electrical Nonmetallic Tubing (ENT), PVC 40, PVC 80, Rigid Metal Conduit, Flexible Metal Conduit and Liquidtight Flexible Metal Conduit.

When other types of conduit are used, refer to Appendix C2002 *NEC* or use method shown below to figure conduit size.

Example #1 - All same wire size and type insulation.

10 - #12 RHH in Intermediate Metal Conduit.

Go to the RHH Conductor Square Inch Area Table. (*Ugly's page 98*)

#12 RHH = .0353 sq. in. 10 x .0353 sq. in. = .353 sq. in.

Go to Intermediate Metal Conduit Square Inch Area Table. (*Ugly's page 101*)

Use "Over 2 Wires 40%" column.

$\frac{3}{4}$ inch conduit = .235 sq. in. (less than .353, so it's too small).

1 inch conduit = .384 sq. in. (greater than .353, so it's correct size).

Example #2 - Different wire sizes or types insulation.

10 - #12 RHH and 10 - #10 THHN in Liquidtight Nonmetallic Conduit (LFNC-B).

Go to the RHH Conductor Square Inch Area Table. (*Ugly's page 98*)

#12 RHH = .0353 sq. in. 10 x .0353 sq. in. = .353 sq. in.

Go to the THHN Conductor Square Inch Area Table. (*Ugly's page 98*)

#10 THHN = .0211 sq. in. 10 x .0211 sq. in. = .211 sq. in.

.353 sq. in. + .211 sq. in. = .564 sq. in.

Go to Liquidtight Nonmetallic Conduit (LFNC-B) Square Inch Table. (*Ugly's page 102*)

Use "Over 2 Wires 40%" column.

1 inch conduit = .349 sq. in. (less than .564, so it's too small).

$1\frac{1}{4}$ inch conduit = .611 sq. in. (greater than .564, so it's correct size).

NOTE 1*: All conductors must be counted including grounding conductors for fill percentage.

NOTE 2: When all conductors are same type and size, decimals .8 and larger must be rounded up.

NOTE 3**: These are minimum size calculations, under certain conditions jamming can occur and the next size conduit must be used.

NOTE 4***: CAUTION - When over three current carrying conductors are used in same circuit, conductor ampacity must be lower (derated).

* See Appendix C and Chapter Nine 2002 *NEC* for complete tables and examples.

** See Chapter nine Table one and Notes 1 - 10, 2002 *NEC*.

*** See notes to Ampacity Tables, Note 8, 2002 *NEC*.

MAXIMUM NUMBER OF CONDUCTORS IN ELECTRICAL METALLIC TUBING

| Type Letters | Cond. Size AWG/kcmil | Trade Sizes in Inches | | | | | | | | | |
|--------------|----------------------|-----------------------|-----|----|-------|-------|-----|-------|-----|-------|-----|
| | | 1/8 | 1/4 | 1 | 1 1/4 | 1 1/2 | 2 | 2 1/2 | 3 | 3 1/2 | 4 |
| RHH, RHW, | 14 | 4 | 7 | 11 | 20 | 27 | 46 | 80 | 120 | 157 | 201 |
| RHW-2 | 12 | 3 | 6 | 9 | 17 | 23 | 38 | 66 | 100 | 131 | 167 |
| | 10 | 2 | 5 | 8 | 13 | 18 | 30 | 53 | 81 | 105 | 135 |
| | 8 | 1 | 2 | 4 | 7 | 9 | 16 | 28 | 42 | 55 | 70 |
| | 6 | 1 | 1 | 3 | 5 | 8 | 13 | 22 | 34 | 44 | 56 |
| | 4 | 1 | 1 | 2 | 4 | 6 | 10 | 17 | 26 | 34 | 44 |
| | 3 | 1 | 1 | 1 | 4 | 5 | 9 | 15 | 23 | 30 | 38 |
| | 2 | 1 | 1 | 1 | 3 | 4 | 7 | 13 | 20 | 26 | 33 |
| | 1 | 0 | 1 | 1 | 1 | 3 | 5 | 9 | 13 | 17 | 22 |
| | 1/0 | 0 | 1 | 1 | 1 | 2 | 4 | 7 | 11 | 15 | 19 |
| | 2/0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 10 | 13 | 17 |
| | 3/0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 8 | 11 | 14 |
| | 4/0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 9 | 12 |
| | 250 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 9 |
| | 300 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 6 | 8 |
| | 350 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 6 | 7 |
| | 400 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 6 | 8 |
| | 500 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 5 |
| | 600 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 5 |
| | 700 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 4 |
| | 750 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 3 | 4 |
| TW, | 14 | 8 | 15 | 25 | 43 | 58 | 96 | 168 | 254 | 332 | 424 |
| THHW, | 12 | 6 | 11 | 19 | 33 | 45 | 74 | 129 | 195 | 255 | 326 |
| THW, | 10 | 5 | 8 | 14 | 24 | 33 | 55 | 96 | 145 | 190 | 243 |
| THW-2 | 8 | 2 | 5 | 8 | 13 | 18 | 30 | 53 | 81 | 105 | 135 |
| RHH*, RHW*, | 14 | 6 | 10 | 16 | 28 | 39 | 64 | 112 | 169 | 221 | 282 |
| RHW-2* | 12 | 4 | 8 | 13 | 23 | 31 | 51 | 90 | 136 | 177 | 227 |
| | 10 | 3 | 6 | 10 | 18 | 24 | 40 | 70 | 106 | 138 | 177 |
| | 8 | 1 | 4 | 6 | 10 | 14 | 24 | 42 | 63 | 83 | 106 |
| RHH*, RHW*, | 6 | 1 | 3 | 4 | 8 | 11 | 18 | 32 | 48 | 63 | 81 |
| RHW-2*, TW, | 4 | 1 | 1 | 3 | 6 | 8 | 13 | 24 | 36 | 47 | 60 |
| THW, THHW, | 3 | 1 | 1 | 3 | 5 | 7 | 12 | 20 | 31 | 40 | 52 |
| THW-2 | 2 | 1 | 1 | 2 | 4 | 6 | 10 | 17 | 26 | 34 | 44 |
| | 1 | 1 | 1 | 1 | 3 | 4 | 7 | 12 | 18 | 24 | 31 |
| | 1/0 | 0 | 1 | 1 | 2 | 3 | 5 | 9 | 13 | 17 | 26 |
| | 2/0 | 0 | 1 | 1 | 1 | 3 | 5 | 9 | 13 | 17 | 26 |
| | 3/0 | 0 | 1 | 1 | 1 | 2 | 4 | 7 | 11 | 15 | 19 |
| | 4/0 | 0 | 0 | 1 | 1 | 1 | 3 | 6 | 9 | 12 | 16 |
| | 250 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 10 | 13 |
| | 300 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 8 | 11 |
| | 350 | 0 | 0 | 0 | 1 | 1 | 1 | 4 | 6 | 7 | 10 |
| | 400 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 9 |
| | 500 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 7 |
| | 600 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 4 | 6 |
| | 700 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 5 |
| | 750 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 5 |
| THHN, | 14 | 12 | 22 | 35 | 61 | 84 | 138 | 241 | 364 | 476 | 608 |
| THWN, | 12 | 9 | 16 | 26 | 45 | 61 | 101 | 176 | 266 | 347 | 443 |
| THWN-2 | 10 | 5 | 10 | 16 | 28 | 38 | 63 | 111 | 167 | 219 | 279 |
| | 8 | 3 | 6 | 9 | 16 | 22 | 36 | 64 | 96 | 126 | 161 |
| | 6 | 2 | 4 | 7 | 12 | 16 | 26 | 46 | 69 | 91 | 116 |
| | 4 | 1 | 2 | 4 | 7 | 10 | 16 | 28 | 43 | 56 | 71 |
| | 3 | 1 | 1 | 3 | 6 | 8 | 13 | 24 | 36 | 47 | 60 |
| | 2 | 1 | 1 | 3 | 5 | 7 | 11 | 20 | 30 | 40 | 51 |
| | 1 | 1 | 1 | 1 | 4 | 5 | 8 | 15 | 22 | 29 | 37 |
| | 1/0 | 1 | 1 | 1 | 3 | 4 | 7 | 12 | 19 | 25 | 32 |
| | 2/0 | 0 | 1 | 1 | 2 | 3 | 6 | 10 | 16 | 20 | 26 |
| | 3/0 | 0 | 1 | 1 | 1 | 3 | 5 | 8 | 13 | 17 | 22 |

MAXIMUM NUMBER OF CONDUCTORS IN ELECTRICAL METALLIC TUBING

| Type Letters | Cond. Size AWG/kcmil | Trade Sizes in Inches | | | | | | | | | |
|-------------------|----------------------|-----------------------|-----|----|-------|-------|-----|-------|-----|-------|-----|
| | | 1/8 | 1/4 | 1 | 1 1/4 | 1 1/2 | 2 | 2 1/2 | 3 | 3 1/2 | 4 |
| THHN, | 4/0 | 0 | 1 | 1 | 1 | 2 | 4 | 7 | 11 | 14 | 18 |
| | 250 | 0 | 0 | 1 | 1 | 1 | 3 | 6 | 9 | 11 | 15 |
| THWN- | 300 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 10 | 13 |
| | 350 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 9 | 11 |
| | 400 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 10 |
| | 500 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 6 |
| | 600 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 5 |
| | 700 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 4 |
| | 750 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 5 |
| FEP, FEPB, | 14 | 12 | 21 | 34 | 60 | 81 | 134 | 234 | 354 | 462 | 590 |
| PFA, PFAH, | 12 | 9 | 15 | 25 | 43 | 59 | 98 | 171 | 258 | 337 | 430 |
| TFE | 10 | 6 | 11 | 18 | 31 | 42 | 70 | 122 | 185 | 241 | 309 |
| | 8 | 3 | 6 | 10 | 18 | 24 | 40 | 70 | 106 | 138 | 177 |
| | 6 | 2 | 4 | 7 | 12 | 17 | 28 | 50 | 75 | 98 | 126 |
| | 4 | 1 | 3 | 5 | 9 | 12 | 20 | 35 | 53 | 69 | 88 |
| | 3 | 1 | 2 | 4 | 7 | 10 | 16 | 29 | 44 | 57 | 73 |
| | 2 | 1 | 1 | 3 | 6 | 8 | 13 | 24 | 36 | 47 | 60 |
| PFA, PFAH, TFE | 1 | 1 | 1 | 2 | 4 | 6 | 9 | 16 | 25 | 33 | 42 |
| PFA, PFAH, TFE, Z | 1/0 | 1 | 1 | 1 | 3 | 5 | 8 | 14 | 21 | 27 | 35 |
| | 2/0 | 0 | 1 | 1 | 3 | 4 | 6 | 11 | 17 | 22 | 29 |
| | 3/0 | 0 | 1 | 1 | 2 | 3 | 5 | 9 | 14 | 18 | 24 |
| | 4/0 | 0 | 1 | 1 | 1 | 2 | 4 | 8 | 11 | 15 | 19 |
| Z | 14 | 14 | 25 | 41 | 72 | 98 | 161 | 282 | 426 | 556 | 711 |
| | 12 | 10 | 18 | 29 | 51 | 69 | 114 | 200 | 302 | 394 | 504 |
| | 10 | 6 | 11 | 18 | 31 | 42 | 70 | 122 | 185 | 241 | 309 |
| | 8 | 4 | 7 | 11 | 20 | 27 | 44 | 77 | 117 | 153 | 195 |
| | 6 | 3 | 5 | 8 | 14 | 19 | 31 | 54 | 82 | 107 | 137 |
| | 4 | 1 | 3 | 5 | 9 | 13 | 21 | 37 | 56 | 74 | 94 |
| | 3 | 1 | 2 | 4 | 7 | 9 | 15 | 27 | 41 | 54 | 69 |
| | 2 | 1 | 1 | 3 | 6 | 8 | 13 | 22 | 34 | 45 | 57 |
| | 1 | 1 | 1 | 2 | 4 | 6 | 10 | 18 | 28 | 36 | 46 |
| XHH, XHHW, | 14 | 8 | 15 | 25 | 43 | 58 | 96 | 168 | 254 | 332 | 424 |
| XHHW-2 | 12 | 6 | 11 | 19 | 33 | 45 | 74 | 129 | 195 | 255 | 326 |
| | 10 | 5 | 8 | 14 | 24 | 33 | 55 | 96 | 145 | 190 | 243 |
| | 8 | 2 | 5 | 8 | 13 | 18 | 30 | 53 | 81 | 105 | 135 |
| | 6 | 1 | 3 | 6 | 10 | 14 | 22 | 39 | 60 | 78 | 100 |
| | 4 | 1 | 2 | 4 | 7 | 10 | 16 | 28 | 43 | 56 | 72 |
| | 3 | 1 | 1 | 3 | 6 | 8 | 14 | 24 | 36 | 48 | 61 |
| | 2 | 1 | 1 | 3 | 5 | 7 | 11 | 20 | 31 | 40 | 51 |
| XHH, XHHW, XHHW-2 | 1 | 1 | 1 | 1 | 4 | 5 | 8 | 15 | 23 | 30 | 38 |
| | 1/0 | 1 | 1 | 1 | 3 | 4 | 7 | 13 | 19 | 25 | 32 |
| | 2/0 | 0 | 1 | 1 | 2 | 3 | 6 | 10 | 16 | 21 | 27 |
| | 3/0 | 0 | 1 | 1 | 1 | 3 | 5 | 9 | 13 | 17 | 22 |
| | 4/0 | 0 | 1 | 1 | 1 | 2 | 4 | 7 | 11 | 14 | 18 |
| | 250 | 0 | 0 | 1 | 1 | 1 | 3 | 6 | 9 | 12 | 15 |
| | 300 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 7 | 9 | 11 |
| | 350 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 7 | 9 | 11 |
| | 400 | 0 | 0 | 0 | 1 | 1 | 1 | 4 | 6 | 8 | 10 |
| | 500 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 6 | 8 |
| | 600 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 5 | 6 |
| | 700 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 3 | 4 | 6 |
| | 750 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 5 |

* Types RHH, RHW, AND RHW-2 without outer covering.

See Ugly's page 131 for Trade Size / Metric Designator conversion.

MAXIMUM NUMBER OF CONDUCTORS IN NONMETALLIC TUBING

| Type Letters | Cond. Size AWG/kcmil | 1/2 | 3/4 | Trade Sizes In Inches | 1 | 1 1/4 | 1 1/2 | 2 |
|---|----------------------|-----|-----|-----------------------|----|-------|-------|---|
| RHH, RHW, RHW-2 | 14 | 3 | 6 | 10 | 19 | 26 | 43 | |
| | 12 | 2 | 5 | 9 | 16 | 22 | 36 | |
| | 10 | 1 | 4 | 7 | 13 | 17 | 29 | |
| | 8 | 1 | 1 | 3 | 6 | 9 | 15 | |
| | 6 | 1 | 1 | 3 | 5 | 7 | 12 | |
| | 4 | 1 | 1 | 2 | 4 | 6 | 9 | |
| | 3 | 1 | 1 | 1 | 3 | 5 | 8 | |
| | 2 | 0 | 1 | 1 | 3 | 4 | 7 | |
| | 1 | 0 | 1 | 1 | 1 | 3 | 5 | |
| | 1/0 | 0 | 0 | 1 | 1 | 2 | 4 | |
| | 2/0 | 0 | 0 | 1 | 1 | 1 | 3 | |
| | 3/0 | 0 | 0 | 1 | 1 | 1 | 3 | |
| | 4/0 | 0 | 0 | 1 | 1 | 1 | 2 | |
| | 250 | 0 | 0 | 0 | 1 | 1 | 1 | |
| | 300 | 0 | 0 | 0 | 1 | 1 | 1 | |
| | 350 | 0 | 0 | 0 | 1 | 1 | 1 | |
| | 400 | 0 | 0 | 0 | 1 | 1 | 1 | |
| | 500 | 0 | 0 | 0 | 0 | 1 | 1 | |
| | 600 | 0 | 0 | 0 | 0 | 1 | 1 | |
| | 700 | 0 | 0 | 0 | 0 | 0 | 1 | |
| | 750 | 0 | 0 | 0 | 0 | 0 | 1 | |
| TW | 14 | 7 | 13 | 22 | 40 | 55 | 92 | |
| THHW, | 12 | 5 | 10 | 17 | 31 | 42 | 71 | |
| THW, | 10 | 4 | 7 | 13 | 23 | 32 | 52 | |
| THW-2 | 8 | 1 | 4 | 7 | 13 | 17 | 29 | |
| RHH*, RHW*, RHW-2* | 14 | 4 | 8 | 15 | 27 | 37 | 61 | |
| | 12 | 3 | 7 | 12 | 21 | 29 | 49 | |
| | 10 | 3 | 5 | 9 | 17 | 23 | 38 | |
| | 8 | 1 | 3 | 5 | 10 | 14 | 23 | |
| RHH*, RHW*, RHW-2*, TW, THW, THHW, THW-2 | 6 | 1 | 2 | 4 | 7 | 10 | 17 | |
| | 4 | 1 | 1 | 3 | 5 | 8 | 13 | |
| | 3 | 1 | 1 | 2 | 5 | 7 | 11 | |
| | 2 | 1 | 1 | 2 | 4 | 6 | 9 | |
| | 1 | 0 | 1 | 1 | 3 | 4 | 6 | |
| | 1/0 | 0 | 1 | 1 | 2 | 3 | 5 | |
| | 2/0 | 0 | 1 | 1 | 1 | 3 | 5 | |
| | 3/0 | 0 | 0 | 1 | 1 | 2 | 4 | |
| | 4/0 | 0 | 0 | 1 | 1 | 1 | 3 | |
| | 250 | 0 | 0 | 1 | 1 | 1 | 2 | |
| | 300 | 0 | 0 | 0 | 1 | 1 | 2 | |
| | 350 | 0 | 0 | 0 | 1 | 1 | 1 | |
| | 400 | 0 | 0 | 0 | 1 | 1 | 1 | |
| | 500 | 0 | 0 | 0 | 1 | 1 | 1 | |
| | 600 | 0 | 0 | 0 | 0 | 1 | 1 | |
| | 700 | 0 | 0 | 0 | 0 | 1 | 1 | |
| | 750 | 0 | 0 | 0 | 0 | 1 | 1 | |
| THHN, | 14 | 10 | 18 | 32 | 58 | 80 | 132 | |
| THWN, | 12 | 7 | 13 | 23 | 42 | 58 | 96 | |
| THWN-2 | 10 | 4 | 8 | 15 | 26 | 36 | 60 | |
| | 8 | 2 | 5 | 8 | 15 | 21 | 35 | |
| | 6 | 1 | 3 | 6 | 11 | 15 | 25 | |
| | 4 | 1 | 1 | 4 | 7 | 9 | 15 | |
| | 3 | 1 | 1 | 3 | 5 | 8 | 13 | |
| | 2 | 1 | 1 | 2 | 5 | 6 | 11 | |
| | 1 | 1 | 1 | 1 | 3 | 5 | 8 | |
| | 1/0 | 0 | 1 | 1 | 3 | 4 | 7 | |
| | 2/0 | 0 | 1 | 1 | 2 | 3 | 5 | |
| | 3/0 | 0 | 1 | 1 | 1 | 3 | 4 | |

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MAXIMUM NUMBER OF CONDUCTORS IN NONMETALLIC TUBING

| Type Letters | Cond. Size AWG/kcmil | 1/2 | 3/4 | Trade Sizes In Inches | 1 | 1 1/4 | 1 1/2 | 2 |
|---------------------------------|----------------------|-----|-----|-----------------------|----|-------|-------|---|
| THHN, | 4/0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 |
| THWN, | 250 | 0 | 0 | 1 | 1 | 1 | 1 | 3 |
| THWN-2 | 300 | 0 | 0 | 1 | 1 | 1 | 1 | 2 |
| | 350 | 0 | 0 | 0 | 1 | 1 | 1 | 2 |
| | 400 | 0 | 0 | 0 | 1 | 1 | 1 | 1 |
| | 500 | 0 | 0 | 0 | 1 | 1 | 1 | 1 |
| | 600 | 0 | 0 | 0 | 1 | 1 | 1 | 1 |
| | 700 | 0 | 0 | 0 | 0 | 1 | 1 | 1 |
| | 750 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| FEP, FEPB, PFA, PFAH, TFE | 14 | 10 | 18 | 31 | 56 | 77 | 128 | |
| | 12 | 7 | 13 | 23 | 41 | 56 | 93 | |
| | 10 | 5 | 9 | 16 | 29 | 40 | 67 | |
| | 8 | 3 | 5 | 9 | 17 | 23 | 38 | |
| | 6 | 1 | 4 | 6 | 12 | 16 | 27 | |
| | 4 | 1 | 2 | 4 | 8 | 11 | 19 | |
| | 3 | 1 | 1 | 4 | 7 | 9 | 16 | |
| | 2 | 1 | 1 | 3 | 5 | 8 | 13 | |
| PFA, PFAH, TFE | 1 | 1 | 1 | 1 | 4 | 5 | 9 | |
| PFA, PFAH, TFE, Z | 1/0 | 0 | 1 | 1 | 3 | 4 | 7 | |
| | 2/0 | 0 | 1 | 1 | 2 | 4 | 6 | |
| | 3/0 | 0 | 1 | 1 | 1 | 3 | 5 | |
| | 4/0 | 0 | 1 | 1 | 1 | 2 | 4 | |
| Z | 14 | 12 | 22 | 38 | 68 | 93 | 154 | |
| | 12 | 8 | 15 | 27 | 48 | 66 | 109 | |
| | 10 | 5 | 9 | 16 | 29 | 40 | 67 | |
| | 8 | 3 | 6 | 10 | 18 | 25 | 42 | |
| | 6 | 1 | 4 | 7 | 13 | 18 | 30 | |
| | 4 | 1 | 3 | 5 | 9 | 12 | 20 | |
| | 3 | 1 | 1 | 3 | 6 | 9 | 15 | |
| | 2 | 1 | 1 | 3 | 5 | 7 | 12 | |
| | 1 | 1 | 1 | 2 | 4 | 6 | 10 | |
| XHH, | 14 | 7 | 13 | 22 | 40 | 55 | 92 | |
| XHHW, | 12 | 5 | 10 | 17 | 31 | 42 | 71 | |
| XHHW-2, | 10 | 4 | 7 | 13 | 23 | 32 | 52 | |
| ZW | 8 | 1 | 4 | 7 | 13 | 17 | 29 | |
| | 6 | 1 | 3 | 5 | 9 | 13 | 21 | |
| | 4 | 1 | 1 | 4 | 7 | 9 | 15 | |
| | 3 | 1 | 1 | 3 | 6 | 8 | 13 | |
| | 2 | 1 | 1 | 2 | 5 | 6 | 11 | |
| XHH, XHHW, XHHW-2 | 1 | 1 | 1 | 1 | 3 | 5 | 8 | |
| | 1/0 | 0 | 1 | 1 | 3 | 4 | 7 | |
| | 2/0 | 0 | 1 | 1 | 2 | 3 | 6 | |
| | 3/0 | 0 | 1 | 1 | 1 | 3 | 5 | |
| | 4/0 | 0 | 0 | 1 | 1 | 2 | 4 | |
| | 250 | 0 | 0 | 1 | 1 | 1 | 3 | |
| | 300 | 0 | 0 | 1 | 1 | 1 | 2 | |
| | 350 | 0 | 0 | 1 | 1 | 1 | 2 | |
| | 400 | 0 | 0 | 0 | 1 | 1 | 1 | |
| | 500 | 0 | 0 | 0 | 1 | 1 | 1 | |
| | 600 | 0 | 0 | 0 | 1 | 1 | 1 | |
| | 700 | 0 | 0 | 0 | 0 | 1 | 1 | |
| | 750 | 0 | 0 | 0 | 0 | 0 | 1 | |

* Types RHH, RHW, AND RHW-2 without outer covering.

See Ugly's page 131 for Trade Size / Metric Designator conversion.

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MAXIMUM NUMBER OF CONDUCTORS IN RIGID PVC CONDUIT, SCHEDULE 40

| Type Letters | Cond. Size AWG/kcmil | Trade Sizes In Inches | | | | | | | | | | | |
|--------------------------|----------------------|-----------------------|-----|----|-------|-------|-----|-------|-----|-------|-----|-----|------|
| | | 1/2 | 3/4 | 1 | 1 1/4 | 1 1/2 | 2 | 2 1/2 | 3 | 3 1/2 | 4 | 5 | 6 |
| RHH, RHW, RHW-2 | 14 | 4 | 7 | 11 | 20 | 27 | 45 | 64 | 99 | 133 | 171 | 269 | 390 |
| | 12 | 3 | 5 | 9 | 16 | 22 | 37 | 53 | 82 | 110 | 142 | 224 | 323 |
| | 10 | 2 | 4 | 7 | 13 | 18 | 30 | 43 | 66 | 89 | 115 | 181 | 261 |
| | 8 | 1 | 2 | 4 | 7 | 9 | 15 | 22 | 35 | 46 | 60 | 94 | 137 |
| | 6 | 1 | 1 | 3 | 5 | 7 | 12 | 18 | 28 | 37 | 48 | 76 | 109 |
| | 4 | 1 | 1 | 2 | 4 | 6 | 10 | 14 | 22 | 29 | 37 | 59 | 85 |
| | 3 | 1 | 1 | 1 | 4 | 5 | 8 | 12 | 19 | 25 | 33 | 52 | 75 |
| | 2 | 1 | 1 | 1 | 3 | 4 | 7 | 10 | 16 | 22 | 28 | 45 | 65 |
| | 1 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 11 | 14 | 19 | 29 | 43 |
| | 1/0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 9 | 13 | 16 | 26 | 37 |
| | 2/0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 8 | 11 | 14 | 22 | 32 |
| | 3/0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 7 | 9 | 12 | 19 | 28 |
| | 4/0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 8 | 10 | 16 | 24 |
| | 250 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 8 | 12 | 18 |
| | 300 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 5 | 7 | 11 | 16 |
| | 350 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 6 | 10 | 14 |
| | 400 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 9 | 13 | 20 |
| | 500 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 9 | 13 | 19 |
| | 600 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 9 | 13 | 19 |
| | 700 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 9 | 13 |
| | 750 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 8 | 12 |
| TW | 14 | 8 | 14 | 24 | 42 | 57 | 94 | 135 | 209 | 280 | 361 | 568 | 822 |
| THHW, | 12 | 6 | 11 | 18 | 32 | 44 | 72 | 103 | 160 | 215 | 277 | 436 | 631 |
| THW, | 10 | 4 | 8 | 13 | 24 | 32 | 54 | 77 | 119 | 160 | 206 | 325 | 470 |
| THW-2 | 8 | 2 | 4 | 7 | 13 | 18 | 30 | 43 | 66 | 89 | 115 | 181 | 261 |
| RHH*, RHW*, RHW-2* | 14 | 5 | 9 | 16 | 28 | 38 | 63 | 90 | 139 | 186 | 240 | 378 | 546 |
| | 12 | 4 | 8 | 12 | 22 | 30 | 50 | 72 | 112 | 150 | 193 | 304 | 439 |
| | 10 | 3 | 6 | 10 | 17 | 24 | 39 | 56 | 87 | 117 | 150 | 237 | 343 |
| | 8 | 1 | 3 | 6 | 10 | 14 | 23 | 33 | 52 | 70 | 90 | 142 | 205 |
| TW, THW, THHHW, THW-2 | 6 | 1 | 2 | 4 | 8 | 11 | 18 | 26 | 40 | 53 | 69 | 109 | 157 |
| | 4 | 1 | 1 | 3 | 6 | 8 | 13 | 19 | 30 | 40 | 51 | 81 | 117 |
| | 3 | 1 | 1 | 3 | 5 | 7 | 11 | 16 | 25 | 34 | 44 | 69 | 100 |
| | 2 | 1 | 1 | 2 | 4 | 6 | 10 | 14 | 22 | 29 | 37 | 59 | 85 |
| | 1 | 0 | 1 | 1 | 3 | 4 | 7 | 10 | 15 | 20 | 26 | 41 | 60 |
| | 1/0 | 0 | 1 | 1 | 2 | 3 | 6 | 8 | 13 | 17 | 22 | 35 | 51 |
| | 2/0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 11 | 15 | 19 | 30 | 43 |
| | 3/0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 9 | 12 | 16 | 25 | 36 |
| | 4/0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 8 | 10 | 13 | 21 | 30 |
| | 250 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 8 | 11 | 17 | 25 |
| | 300 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 7 | 9 | 15 | 21 |
| | 350 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 8 | 13 | 19 |
| | 400 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 7 | 12 | 17 |
| | 500 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 6 | 10 | 14 |
| | 600 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 5 | 8 | 11 |
| | 700 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 4 | 7 | 10 |
| | 750 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 4 | 6 | 10 |
| THHN, THWN, THWN-2 | 14 | 11 | 21 | 34 | 60 | 82 | 135 | 193 | 299 | 401 | 517 | 815 | 1178 |
| | 12 | 8 | 15 | 25 | 43 | 59 | 99 | 141 | 218 | 293 | 377 | 594 | 859 |
| | 10 | 5 | 9 | 15 | 27 | 37 | 62 | 89 | 137 | 184 | 238 | 374 | 541 |
| | 8 | 3 | 5 | 9 | 16 | 21 | 36 | 51 | 79 | 106 | 137 | 216 | 312 |
| | 6 | 1 | 4 | 6 | 11 | 15 | 26 | 37 | 57 | 77 | 99 | 156 | 225 |
| | 4 | 1 | 2 | 4 | 7 | 9 | 16 | 22 | 35 | 47 | 61 | 96 | 138 |
| | 3 | 1 | 1 | 3 | 6 | 8 | 13 | 19 | 30 | 40 | 51 | 81 | 117 |
| | 2 | 1 | 1 | 3 | 5 | 7 | 11 | 16 | 25 | 33 | 43 | 68 | 98 |
| | 1 | 1 | 1 | 1 | 3 | 5 | 8 | 12 | 18 | 25 | 32 | 50 | 73 |
| | 1/0 | 1 | 1 | 1 | 3 | 4 | 7 | 10 | 15 | 21 | 27 | 42 | 61 |
| | 2/0 | 0 | 1 | 1 | 2 | 3 | 6 | 8 | 13 | 17 | 22 | 35 | 51 |
| | 3/0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 11 | 14 | 18 | 29 | 42 |

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MAXIMUM NUMBER OF CONDUCTORS IN RIGID PVC CONDUIT, SCHEDULE 40

| Type Letters | Cond. Size AWG/kcmil | Trade Sizes In Inches | | | | | | | | | | | |
|----------------|----------------------|-----------------------|-----|----|-------|-------|-----|-------|-----|-------|-----|-----|------|
| | | 1/2 | 3/4 | 1 | 1 1/4 | 1 1/2 | 2 | 2 1/2 | 3 | 3 1/2 | 4 | 5 | 6 |
| THHN, | 4/0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 9 | 12 | 15 | 24 | 35 |
| THWN, | 250 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 10 | 12 | 20 | 28 |
| THWN-2 | 300 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 8 | 11 | 17 | 24 |
| | 350 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 7 | 9 | 15 | 21 |
| | 400 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 5 | 6 | 8 | 13 |
| | 500 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 5 | 7 | 11 | 16 |
| | 600 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 5 | 7 | 9 | 13 |
| | 700 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 4 | 5 | 8 | 11 |
| | 750 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 4 | 7 | 11 |
| FEP, FEPB, | 14 | 11 | 20 | 33 | 58 | 79 | 131 | 188 | 290 | 389 | 502 | 790 | 1142 |
| PFA, PFAH, | 12 | 8 | 15 | 24 | 42 | 58 | 96 | 137 | 212 | 284 | 366 | 577 | 834 |
| TFE | 10 | 6 | 10 | 17 | 30 | 41 | 69 | 98 | 152 | 204 | 263 | 414 | 598 |
| | 8 | 3 | 6 | 10 | 17 | 24 | 39 | 56 | 87 | 117 | 150 | 237 | 343 |
| | 6 | 2 | 4 | 7 | 12 | 17 | 28 | 40 | 62 | 83 | 107 | 169 | 244 |
| | 4 | 1 | 3 | 5 | 8 | 12 | 19 | 28 | 43 | 58 | 75 | 118 | 170 |
| | 3 | 1 | 2 | 4 | 7 | 10 | 16 | 23 | 36 | 48 | 62 | 98 | 142 |
| | 2 | 1 | 1 | 3 | 6 | 8 | 13 | 19 | 30 | 40 | 51 | 81 | 117 |
| PFA, PFAH, TFE | 1 | 1 | 1 | 2 | 4 | 5 | 9 | 13 | 20 | 28 | 36 | 56 | 81 |
| PFA, PFAH, | 1/0 | 1 | 1 | 1 | 3 | 4 | 8 | 11 | 17 | 23 | 30 | 47 | 68 |
| TFE, Z | 2/0 | 0 | 1 | 1 | 3 | 4 | 6 | 9 | 14 | 19 | 24 | 39 | 56 |
| | 3/0 | 0 | 1 | 1 | 2 | 3 | 5 | 7 | 12 | 16 | 20 | 32 | 46 |
| | 4/0 | 0 | 1 | 1 | 2 | 4 | 6 | 9 | 13 | 16 | 26 | 38 | 58 |
| Z | 14 | 13 | 24 | 40 | 70 | 95 | 158 | 226 | 350 | 469 | 605 | 952 | 1376 |
| | 12 | 9 | 17 | 28 | 49 | 68 | 112 | 160 | 248 | 333 | 429 | 675 | 976 |
| | 10 | 6 | 10 | 17 | 30 | 41 | 69 | 95 | 152 | 204 | 263 | 414 | 598 |
| | 8 | 3 | 6 | 11 | 19 | 26 | 43 | 62 | 96 | 129 | 166 | 261 | 378 |
| | 6 | 2 | 4 | 7 | 13 | 18 | 30 | 43 | 67 | 90 | 116 | 184 | 265 |
| | 4 | 1 | 3 | 5 | 9 | 12 | 21 | 30 | 46 | 62 | 80 | 126 | 183 |
| | 3 | 1 | 2 | 4 | 6 | 9 | 15 | 22 | 34 | 45 | 58 | 92 | 133 |
| | 2 | 1 | 1 | 3 | 5 | 7 | 12 | 18 | 28 | 38 | 49 | 77 | 111 |
| | 1 | 1 | 1 | 2 | 4 | 6 | 10 | 14 | 23 | 30 | 39 | 62 | 90 |
| XHH, XHHW, | 1 | 1 | 1 | 3 | 5 | 8 | 12 | 19 | 25 | 32 | 51 | 74 | |
| XHHW-2 | 1/0 | 1 | 1 | 1 | 3 | 4 | 7 | 10 | 16 | 21 | 27 | 43 | 62 |
| | 2/0 | 0 | 1 | 1 | 2 | 3 | 6 | 8 | 13 | 17 | 23 | 36 | 52 |
| | 3/0 | 0 | 1 | 1 | 3 | 5 | 7 | 11 | 14 | 19 | 30 | 43 | |
| | 4/0 | 0 | 1 | 1 | 2 | 4 | 6 | 9 | 12 | 15 | 24 | 35 | |
| | 250 | 0 | 0 | 1 | 1 | 3 | 5 | 7 | 10 | 13 | 20 | 29 | |
| | 300 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 8 | 11 | 25 | |
| | 350 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 7 | 9 | 15 | |
| | 400 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 6 | 8 | 13 | |
| | 500 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 5 | 7 | 11 | |
| | 600 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 3 | 4 | 5 | 9 | |
| | 700 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 5 | 8 | |
| | 750 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 4 | 7 | |

* Types RHH, RHW, AND RHW-2 without outer covering.

See Ugly's page 131 for Trade Size / Metric Designator conversion.

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MAXIMUM NUMBER OF CONDUCTORS IN RIGID PVC CONDUIT, SCHEDULE 80

| Type Letters | Cond. Size AWG/kcmil | Trade Sizes In Inches | | | | | | | | | | | |
|--------------|----------------------|-----------------------|-----|----|-------|-------|-----|-------|-----|-------|-----|-----|------|
| | | 1/2 | 3/4 | 1 | 1 1/4 | 1 1/2 | 2 | 2 1/2 | 3 | 3 1/2 | 4 | 5 | 6 |
| RHH, RHW, | 14 | 3 | 5 | 9 | 17 | 23 | 39 | 56 | 88 | 118 | 153 | 243 | 349 |
| RHW-2 | 12 | 2 | 4 | 7 | 14 | 19 | 32 | 46 | 73 | 98 | 127 | 202 | 290 |
| | 10 | 1 | 3 | 6 | 11 | 15 | 26 | 37 | 59 | 79 | 103 | 163 | 234 |
| | 8 | 1 | 1 | 3 | 6 | 8 | 13 | 19 | 31 | 41 | 54 | 85 | 122 |
| | 6 | 1 | 1 | 2 | 4 | 6 | 11 | 16 | 24 | 33 | 43 | 68 | 98 |
| | 4 | 1 | 1 | 1 | 3 | 5 | 8 | 12 | 19 | 26 | 33 | 53 | 77 |
| | 3 | 0 | 1 | 1 | 3 | 4 | 7 | 11 | 17 | 23 | 29 | 47 | 67 |
| | 2 | 0 | 1 | 1 | 3 | 4 | 6 | 9 | 14 | 20 | 25 | 41 | 58 |
| | 1 | 0 | 1 | 1 | 2 | 4 | 6 | 9 | 13 | 17 | 27 | 38 | |
| | 1,0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 8 | 11 | 15 | 23 | 33 |
| | 2,0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 7 | 10 | 13 | 20 | 29 |
| | 3,0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 8 | 11 | 17 | 25 |
| | 4,0 | 0 | 0 | 0 | 1 | 1 | 2 | 3 | 5 | 7 | 9 | 15 | 21 |
| | 250 | 0 | 0 | 0 | 1 | 1 | 2 | 4 | 4 | 5 | 7 | 11 | 16 |
| | 300 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 6 | 10 | 14 |
| | 350 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 5 | 9 | 13 | |
| | 400 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 4 | 4 | 5 | 8 | 12 |
| | 500 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 4 | 4 | 5 | 6 | 10 |
| | 600 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 3 | 4 | 7 |
| | 700 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 2 | 4 |
| | 750 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 7 |
| TW | 14 | 6 | 11 | 20 | 35 | 49 | 82 | 118 | 185 | 250 | 324 | 514 | 736 |
| THHW, | 12 | 5 | 9 | 15 | 27 | 38 | 63 | 91 | 142 | 192 | 248 | 394 | 565 |
| THW, | 10 | 3 | 6 | 11 | 20 | 28 | 47 | 67 | 106 | 143 | 185 | 294 | 421 |
| THW-2 | 8 | 1 | 3 | 6 | 11 | 15 | 26 | 37 | 59 | 79 | 103 | 163 | 234 |
| RHH*, RHW*, | 14 | 4 | 8 | 13 | 23 | 32 | 55 | 79 | 123 | 166 | 215 | 341 | 490 |
| RHW-2* | 12 | 3 | 6 | 10 | 19 | 26 | 44 | 63 | 99 | 133 | 173 | 274 | 394 |
| | 10 | 2 | 5 | 8 | 15 | 20 | 34 | 49 | 77 | 104 | 135 | 214 | 307 |
| | 8 | 1 | 3 | 5 | 9 | 12 | 20 | 29 | 46 | 62 | 81 | 128 | 184 |
| RHH*, RHW*, | 6 | 1 | 1 | 3 | 7 | 9 | 16 | 22 | 35 | 48 | 62 | 98 | 141 |
| RHW-2*, TW, | 4 | 1 | 1 | 3 | 5 | 7 | 12 | 17 | 26 | 35 | 46 | 73 | 105 |
| THW, THHW, | 3 | 1 | 1 | 2 | 4 | 6 | 10 | 14 | 22 | 30 | 39 | 63 | 90 |
| THW-2 | 2 | 1 | 1 | 1 | 3 | 5 | 8 | 12 | 19 | 26 | 33 | 53 | 77 |
| | 1 | 0 | 1 | 1 | 2 | 3 | 6 | 8 | 13 | 18 | 23 | 37 | 54 |
| | 1,0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 11 | 15 | 20 | 32 | 46 |
| | 2,0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 10 | 13 | 17 | 27 | 39 |
| | 3,0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 8 | 11 | 14 | 23 | 33 |
| | 4,0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 7 | 9 | 12 | 19 | 27 |
| | 250 | 0 | 0 | 0 | 1 | 1 | 2 | 3 | 5 | 7 | 9 | 15 | 22 |
| | 300 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 6 | 8 | 13 | 19 |
| | 350 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 7 | 12 | 17 |
| | 400 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 5 | 7 | 10 | 15 |
| | 500 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 5 | 9 | 13 |
| | 600 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 4 | 7 | 10 |
| | 700 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 4 | 6 | 9 |
| | 750 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 8 |
| THHN, | 14 | 9 | 17 | 28 | 51 | 70 | 118 | 170 | 265 | 358 | 464 | 736 | 1055 |
| THWN, | 12 | 6 | 12 | 20 | 37 | 51 | 86 | 124 | 193 | 261 | 338 | 537 | 770 |
| THWN-2 | 10 | 4 | 7 | 13 | 23 | 32 | 54 | 78 | 122 | 164 | 213 | 338 | 485 |
| | 8 | 2 | 4 | 7 | 13 | 18 | 31 | 45 | 70 | 95 | 123 | 195 | 279 |
| | 6 | 1 | 3 | 5 | 9 | 13 | 22 | 32 | 51 | 68 | 89 | 141 | 202 |
| | 4 | 1 | 1 | 3 | 6 | 8 | 14 | 20 | 31 | 42 | 54 | 86 | 124 |
| | 3 | 1 | 1 | 3 | 5 | 7 | 12 | 17 | 26 | 35 | 46 | 73 | 105 |
| | 2 | 1 | 1 | 2 | 4 | 6 | 10 | 14 | 22 | 30 | 39 | 61 | 88 |
| | 1 | 0 | 1 | 1 | 3 | 4 | 7 | 10 | 16 | 22 | 29 | 45 | 65 |
| | 1,0 | 0 | 1 | 1 | 2 | 3 | 6 | 9 | 14 | 18 | 24 | 38 | 55 |
| | 2,0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 11 | 15 | 20 | 32 | 46 |
| | 3,0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 9 | 13 | 17 | 27 | 38 |

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MAXIMUM NUMBER OF CONDUCTORS IN RIGID PVC CONDUIT, SCHEDULE 80

| Type Letters | Cond. Size AWG/kcmil | Trade Sizes In Inches | | | | | | | | | | | | |
|----------------|----------------------|-----------------------|-----|----|-------|-------|-----|-------|-----|-------|-----|-----|------|-----|
| | | 1/2 | 3/4 | 1 | 1 1/4 | 1 1/2 | 2 | 2 1/2 | 3 | 3 1/2 | 4 | 5 | 6 | |
| THHN, | 4/0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 8 | 10 | 14 | 22 | 31 | |
| | 250 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 8 | 11 | 18 | 25 | |
| THWN, | 300 | 0 | 0 | 0 | 1 | 1 | 2 | 3 | 5 | 7 | 9 | 15 | 22 | |
| THWN-2 | 350 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 7 | 12 | 17 | |
| | 400 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 7 | 12 | 17 | |
| | 500 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 3 | 5 | 6 | 10 | 14 | |
| | 600 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 5 | 8 | 12 | |
| | 700 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 4 | 7 | 10 | |
| | 750 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 4 | 7 | 9 | |
| FEP, FEPB, | 14 | 8 | 16 | 27 | 49 | 68 | 115 | 164 | 257 | 347 | 450 | 714 | 1024 | |
| | 12 | 6 | 12 | 20 | 36 | 50 | 84 | 120 | 188 | 253 | 328 | 521 | 747 | |
| PFA, PFAH, | 10 | 4 | 8 | 14 | 26 | 36 | 60 | 86 | 135 | 182 | 235 | 374 | 536 | |
| TFE | 8 | 2 | 5 | 8 | 15 | 20 | 34 | 49 | 77 | 104 | 135 | 214 | 307 | |
| | 6 | 1 | 3 | 6 | 10 | 14 | 24 | 35 | 55 | 74 | 96 | 152 | 218 | |
| | 4 | 1 | 2 | 4 | 7 | 10 | 17 | 24 | 38 | 52 | 67 | 106 | 153 | |
| | 3 | 1 | 1 | 3 | 6 | 8 | 14 | 20 | 32 | 43 | 56 | 89 | 127 | |
| | 2 | 1 | 1 | 3 | 5 | 7 | 12 | 17 | 26 | 35 | 46 | 73 | 105 | |
| PFA, PFAH, TFE | 1 | 1 | 1 | 1 | 3 | 5 | 8 | 11 | 18 | 25 | 32 | 51 | 73 | |
| PFA, PFAH, | 1/0 | 0 | 1 | 1 | 3 | 4 | 7 | 10 | 15 | 20 | 27 | 42 | 61 | |
| TFE, Z | 2/0 | 0 | 1 | 1 | 2 | 3 | 5 | 8 | 12 | 17 | 22 | 35 | 50 | |
| | 3/0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 10 | 14 | 18 | 29 | 41 | |
| | 4/0 | 0 | 0 | 1 | 1 | 1 | 4 | 5 | 8 | 11 | 15 | 24 | 34 | |
| Z | 14 | 10 | 19 | 33 | 59 | 82 | 138 | 198 | 310 | 418 | 542 | 860 | 1233 | |
| | 12 | 7 | 14 | 23 | 42 | 58 | 98 | 141 | 220 | 297 | 385 | 610 | 875 | |
| | 10 | 4 | 8 | 14 | 26 | 36 | 60 | 86 | 135 | 182 | 235 | 374 | 536 | |
| | 8 | 3 | 5 | 9 | 16 | 22 | 38 | 54 | 85 | 115 | 149 | 236 | 339 | |
| | 6 | 2 | 4 | 6 | 11 | 16 | 26 | 38 | 60 | 81 | 104 | 166 | 238 | |
| | 4 | 1 | 2 | 4 | 8 | 11 | 18 | 26 | 41 | 55 | 72 | 114 | 164 | |
| | 3 | 1 | 2 | 3 | 5 | 8 | 13 | 19 | 30 | 40 | 52 | 83 | 119 | |
| | 2 | 1 | 1 | 2 | 5 | 6 | 11 | 16 | 25 | 33 | 43 | 69 | 99 | |
| | 1 | 0 | 1 | 2 | 4 | 5 | 9 | 13 | 20 | 27 | 35 | 56 | 80 | |
| XHH, XHHW, | 14 | 6 | 11 | 20 | 35 | 49 | 82 | 118 | 185 | 250 | 324 | 514 | 736 | |
| | 12 | 5 | 9 | 15 | 27 | 38 | 63 | 91 | 142 | 192 | 248 | 394 | 565 | |
| XHHW-2, | 10 | 3 | 6 | 11 | 20 | 28 | 47 | 67 | 106 | 143 | 185 | 294 | 421 | |
| ZW | 8 | 1 | 3 | 6 | 11 | 15 | 26 | 37 | 59 | 79 | 103 | 163 | 234 | |
| | 6 | 1 | 2 | 4 | 8 | 11 | 19 | 28 | 43 | 59 | 76 | 121 | 173 | |
| | 4 | 1 | 1 | 3 | 6 | 8 | 14 | 20 | 31 | 42 | 55 | 87 | 125 | |
| | 3 | 1 | 1 | 1 | 3 | 5 | 7 | 12 | 17 | 26 | 36 | 47 | 74 | 106 |
| | 2 | 1 | 1 | 2 | 4 | 6 | 10 | 14 | 22 | 30 | 39 | 62 | 89 | |
| XHH, XHHW, | 1 | 0 | 1 | 1 | 3 | 4 | 7 | 10 | 16 | 22 | 29 | 46 | 66 | |
| | 1/0 | 0 | 1 | 1 | 2 | 3 | 6 | 9 | 14 | 19 | 24 | 39 | 56 | |
| | 2/0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 11 | 16 | 20 | 32 | 46 | |
| | 3/0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 9 | 13 | 17 | 27 | 38 | |
| | 4/0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 8 | 11 | 14 | 22 | 32 | |
| | 250 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 9 | 11 | 18 | 26 | |
| | 300 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 7 | 10 | 15 | 22 | |
| | 350 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 6 | 8 | 14 | 20 | |
| | 400 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 7 | 12 | 17 | |
| | 500 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 6 | 10 | 14 | |
| | 600 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 5 | 8 | 11 | |
| | 700 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 4 | 7 | 10 | |
| | 750 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 4 | 6 | 9 | |

* Types RHH, RHW, AND RHW-2 without outer covering.
See Ugly's page 131 for Trade Size / Metric Designator conversion.

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MAXIMUM NUMBER OF CONDUCTORS IN RIGID METAL CONDUIT

| Trade Sizes In Inches | | | | | | | | | | | | | |
|-----------------------|----------------------|-----|-----|----|-------|-------|-----|-------|-----|-------|-----|-----|------|
| Type Letters | Cond. Size AWG/kcmil | 1/2 | 3/4 | 1 | 1 1/4 | 1 1/2 | 2 | 2 1/2 | 3 | 3 1/2 | 4 | 5 | 6 |
| RHH, RHW, | 14 | 4 | 7 | 12 | 21 | 28 | 46 | 66 | 102 | 136 | 176 | 276 | 398 |
| RHW-2 | 12 | 3 | 6 | 10 | 17 | 23 | 38 | 55 | 85 | 113 | 146 | 229 | 330 |
| | 10 | 3 | 5 | 8 | 14 | 19 | 31 | 44 | 68 | 91 | 118 | 185 | 267 |
| | 8 | 1 | 2 | 4 | 7 | 10 | 16 | 23 | 36 | 48 | 61 | 97 | 139 |
| | 6 | 1 | 1 | 3 | 6 | 8 | 13 | 18 | 29 | 38 | 49 | 77 | 112 |
| | 4 | 1 | 1 | 2 | 4 | 6 | 10 | 14 | 22 | 30 | 38 | 60 | 87 |
| | 3 | 1 | 1 | 2 | 4 | 5 | 9 | 12 | 19 | 26 | 34 | 53 | 76 |
| | 2 | 1 | 1 | 1 | 3 | 4 | 7 | 11 | 17 | 23 | 29 | 46 | 66 |
| | 1 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 11 | 15 | 19 | 30 | 44 |
| 1/0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 10 | 13 | 17 | 26 | 38 | |
| 2/0 | 0 | 1 | 1 | 1 | 2 | 4 | 5 | 8 | 11 | 14 | 23 | 33 | |
| 3/0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 7 | 10 | 12 | 20 | 28 | |
| 4/0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 8 | 11 | 17 | 24 | |
| 250 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 8 | 13 | 18 | |
| 300 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 5 | 7 | 11 | 16 | |
| 350 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 5 | 6 | 10 | 15 | |
| 400 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 4 | 6 | 9 | 13 | |
| 500 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 3 | 4 | 5 | 8 | 11 | |
| 600 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 4 | 6 | 8 | |
| 700 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 3 | 4 | 6 | 8 | |
| 750 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 3 | 3 | 5 | 8 | |
| TW | 14 | 9 | 15 | 25 | 44 | 59 | 98 | 140 | 216 | 288 | 370 | 581 | 839 |
| THHW, | 12 | 7 | 12 | 19 | 33 | 45 | 75 | 107 | 165 | 221 | 284 | 446 | 644 |
| THW, | 10 | 5 | 9 | 14 | 25 | 34 | 56 | 80 | 123 | 164 | 212 | 332 | 480 |
| THW-2 | 8 | 3 | 5 | 8 | 14 | 19 | 31 | 44 | 68 | 91 | 118 | 185 | 267 |
| RHH*, RHW*, | 14 | 6 | 10 | 17 | 29 | 39 | 65 | 93 | 143 | 191 | 246 | 387 | 558 |
| RHW-2* | 12 | 5 | 8 | 13 | 23 | 32 | 52 | 75 | 115 | 154 | 198 | 311 | 448 |
| | 10 | 3 | 6 | 10 | 18 | 25 | 41 | 58 | 90 | 120 | 154 | 242 | 350 |
| | 8 | 1 | 4 | 6 | 11 | 15 | 24 | 35 | 54 | 72 | 92 | 145 | 209 |
| RHH*, RHW*, | 6 | 1 | 3 | 5 | 8 | 11 | 18 | 27 | 41 | 55 | 71 | 111 | 160 |
| RHW-2*, TW* | 4 | 1 | 1 | 3 | 6 | 8 | 14 | 20 | 31 | 41 | 53 | 83 | 120 |
| THW, THHW, | 3 | 1 | 1 | 3 | 5 | 7 | 12 | 17 | 26 | 35 | 45 | 71 | 103 |
| THW-2 | 2 | 1 | 1 | 2 | 4 | 6 | 10 | 14 | 22 | 30 | 38 | 60 | 87 |
| | 1 | 1 | 1 | 1 | 3 | 4 | 7 | 10 | 15 | 21 | 27 | 42 | 61 |
| 1/0 | 0 | 1 | 1 | 2 | 3 | 6 | 8 | 13 | 18 | 23 | 36 | 52 | |
| 2/0 | 0 | 1 | 1 | 2 | 3 | 5 | 7 | 11 | 15 | 19 | 31 | 44 | |
| 3/0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 9 | 13 | 16 | 26 | 37 | |
| 4/0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 8 | 10 | 14 | 21 | 31 | |
| 250 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 8 | 11 | 17 | 25 | |
| 300 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 7 | 9 | 15 | 22 | |
| 350 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 6 | 8 | 13 | 19 | |
| 400 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 7 | 12 | 17 | |
| 500 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 6 | 10 | 14 | |
| 600 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 3 | 4 | 5 | 8 | 12 | |
| 700 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 4 | 7 | 10 | |
| 750 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 4 | 7 | 10 | |
| THHN, | 14 | 13 | 22 | 36 | 63 | 85 | 140 | 200 | 309 | 412 | 531 | 833 | 1202 |
| THWN, | 12 | 9 | 16 | 26 | 46 | 62 | 102 | 146 | 225 | 301 | 387 | 608 | 877 |
| THWN-2 | 10 | 6 | 10 | 17 | 29 | 39 | 64 | 92 | 142 | 189 | 244 | 383 | 552 |
| | 8 | 3 | 6 | 9 | 16 | 22 | 37 | 53 | 82 | 109 | 140 | 221 | 318 |
| | 6 | 2 | 4 | 7 | 12 | 16 | 27 | 38 | 59 | 79 | 101 | 159 | 230 |
| | 4 | 1 | 2 | 4 | 7 | 10 | 16 | 23 | 36 | 48 | 62 | 98 | 141 |
| | 3 | 1 | 1 | 3 | 6 | 8 | 14 | 20 | 31 | 41 | 53 | 83 | 120 |
| | 2 | 1 | 1 | 3 | 5 | 7 | 11 | 17 | 26 | 34 | 44 | 70 | 100 |
| | 1 | 1 | 1 | 1 | 4 | 5 | 8 | 12 | 19 | 25 | 33 | 51 | 74 |
| 1/0 | 1 | 1 | 1 | 3 | 4 | 7 | 10 | 16 | 21 | 27 | 43 | 63 | |
| 2/0 | 0 | 1 | 1 | 2 | 3 | 6 | 8 | 13 | 18 | 23 | 36 | 52 | |
| 3/0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 11 | 15 | 19 | 30 | 43 | |

MAXIMUM NUMBER OF CONDUCTORS IN RIGID METAL CONDUIT

| Trade Sizes In Inches | | | | | | | | | | | | | |
|-----------------------|----------------------|-----|-----|----|-------|-------|-----|-------|-----|-------|-----|-----|------|
| Type Letters | Cond. Size AWG/kcmil | 1/2 | 3/4 | 1 | 1 1/4 | 1 1/2 | 2 | 2 1/2 | 3 | 3 1/2 | 4 | 5 | 6 |
| THHN, | 4/0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 9 | 12 | 16 | 25 | 36 |
| THWN, | 250 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 10 | 13 | 20 | 29 |
| THWN-2 | 300 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 8 | 11 | 17 | 25 |
| | 350 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 7 | 10 | 15 | 22 |
| | 400 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 7 | 8 | 13 | 20 |
| | 500 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 5 | 7 | 11 | 16 |
| | 600 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 3 | 4 | 6 | 9 | 13 |
| | 700 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 3 | 4 | 5 | 8 |
| | 750 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 5 | 7 |
| FEP, FEPB, | 14 | 12 | 22 | 35 | 61 | 83 | 136 | 194 | 300 | 400 | 515 | 808 | 1166 |
| | 12 | 9 | 16 | 26 | 44 | 60 | 99 | 142 | 219 | 292 | 376 | 590 | 851 |
| TFE | 10 | 6 | 11 | 18 | 32 | 43 | 71 | 102 | 157 | 209 | 269 | 423 | 610 |
| | 8 | 3 | 6 | 10 | 18 | 25 | 41 | 58 | 90 | 120 | 154 | 242 | 350 |
| | 6 | 2 | 4 | 7 | 13 | 17 | 29 | 41 | 64 | 85 | 110 | 172 | 249 |
| | 4 | 1 | 3 | 5 | 9 | 12 | 20 | 29 | 44 | 59 | 77 | 120 | 174 |
| | 3 | 1 | 2 | 4 | 7 | 10 | 17 | 24 | 37 | 50 | 64 | 100 | 145 |
| | 2 | 1 | 1 | 3 | 6 | 8 | 14 | 20 | 31 | 41 | 53 | 83 | 120 |
| PFA, PFAH, TFE | 1 | 1 | 1 | 2 | 4 | 6 | 9 | 14 | 21 | 28 | 37 | 57 | 83 |
| PFA, PFAH, | 1/0 | 1 | 1 | 1 | 3 | 5 | 8 | 11 | 18 | 24 | 30 | 48 | 69 |
| TFE, Z | 2/0 | 1 | 1 | 1 | 3 | 4 | 6 | 9 | 14 | 19 | 25 | 40 | 57 |
| | 3/0 | 0 | 1 | 1 | 2 | 3 | 5 | 8 | 12 | 16 | 21 | 33 | 47 |
| | 4/0 | 0 | 1 | 1 | 2 | 4 | 6 | 9 | 16 | 20 | 33 | 43 | 63 |
| Z | 14 | 15 | 26 | 42 | 73 | 100 | 164 | 234 | 361 | 482 | 621 | 974 | 1405 |
| | 12 | 10 | 18 | 30 | 52 | 71 | 116 | 166 | 256 | 324 | 440 | 691 | 997 |
| | 10 | 6 | 11 | 18 | 32 | 43 | 71 | 102 | 157 | 209 | 269 | 423 | 610 |
| | 8 | 4 | 7 | 11 | 20 | 27 | 45 | 64 | 99 | 132 | 170 | 267 | 386 |
| | 6 | 3 | 5 | 8 | 14 | 19 | 31 | 45 | 69 | 93 | 120 | 188 | 271 |
| | 4 | 1 | 3 | 5 | 9 | 13 | 22 | 31 | 48 | 62 | 82 | 129 | 186 |
| | 3 | 1 | 2 | 4 | 7 | 9 | 16 | 22 | 35 | 47 | 60 | 94 | 136 |
| | 2 | 1 | 1 | 3 | 6 | 8 | 13 | 19 | 29 | 39 | 50 | 78 | 113 |
| | 1 | 1 | 1 | 2 | 5 | 6 | 10 | 15 | 23 | 31 | 40 | 63 | 92 |
| XHH, XHHW, | 14 | 9 | 15 | 25 | 44 | 59 | 98 | 140 | 216 | 288 | 370 | 581 | 839 |
| | 12 | 7 | 12 | 19 | 33 | 45 | 75 | 107 | 165 | 221 | 284 | 446 | 644 |
| XHHW-2, | 10 | 5 | 9 | 14 | 25 | 34 | 56 | 80 | 123 | 164 | 212 | 332 | 480 |
| | 8 | 3 | 5 | 8 | 14 | 19 | 31 | 44 | 68 | 91 | 118 | 185 | 267 |
| | 6 | 1 | 3 | 6 | 10 | 14 | 23 | 33 | 51 | 68 | 87 | 137 | 197 |
| | 4 | 1 | 2 | 4 | 7 | 10 | 16 | 24 | 37 | 49 | 63 | 99 | 143 |
| | 3 | 1 | 1 | 3 | 6 | 8 | 14 | 20 | 31 | 41 | 53 | 84 | 121 |
| | 2 | 1 | 1 | 3 | 5 | 7 | 12 | 17 | 26 | 35 | 45 | 70 | 101 |
| XHH, XHHW, | 1 | 1 | 1 | 1 | 4 | 5 | 9 | 12 | 19 | 26 | 33 | 52 | 76 |
| | 1/0 | 1 | 1 | 1 | 3 | 4 | 7 | 10 | 16 | 22 | 28 | 44 | 64 |
| 2/0 | 0 | 1 | 1 | 2 | 3 | 6 | 9 | 13 | 18 | 23 | 37 | 53 | |
| 3/0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 11 | 15 | 19 | 30 | 44 | |
| 4/0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 9 | 12 | 16 | 25 | 36 | |
| 250 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 10 | 13 | 20 | 30 | |
| 300 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 9 | 11 | 18 | 25 | |
| 350 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 6 | 7 | 10 | 15 | 22 | |
| 400 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 6 | 7 | 9 | 14 | 20 | |
| 500 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 5 | 7 | 11 | 16 | |
| 600 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 3 | 4 | 6 | 9 | 13 | |
| 700 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 3 | 4 | 5 | 8 | 11 | |
| 750 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 5 | 7 | 11 | |

* Types RHH, RHW, AND RHW-2 without outer covering.
 See Ugly's page 131 for Trade Size / Metric Designator conversion.

MAXIMUM NUMBER OF CONDUCTORS IN FLEXIBLE METAL CONDUIT

| Type Letters | Cond. Size AWG/kcmil | Trade Sizes In Inches | | | | | | | | | |
|--------------|----------------------|-----------------------|-----|----|-------|-------|-----|-------|-----|-------|-----|
| | | 1/2 | 3/4 | 1 | 1 1/4 | 1 1/2 | 2 | 2 1/2 | 3 | 3 1/2 | 4 |
| RHH, RHW, | 14 | 4 | 7 | 11 | 17 | 25 | 44 | 67 | 96 | 131 | 171 |
| RHW-2 | 12 | 3 | 6 | 9 | 14 | 21 | 37 | 55 | 80 | 109 | 142 |
| | 10 | 3 | 5 | 7 | 11 | 17 | 30 | 45 | 64 | 88 | 115 |
| | 8 | 1 | 2 | 4 | 6 | 9 | 15 | 23 | 34 | 46 | 60 |
| | 6 | 1 | 1 | 3 | 5 | 7 | 12 | 19 | 27 | 37 | 48 |
| | 4 | 1 | 1 | 2 | 4 | 5 | 10 | 14 | 21 | 29 | 37 |
| | 3 | 1 | 1 | 3 | 5 | 8 | 13 | 18 | 25 | 33 | 33 |
| | 2 | 1 | 1 | 1 | 3 | 4 | 7 | 11 | 16 | 22 | 28 |
| | 1 | 0 | 1 | 1 | 2 | 5 | 7 | 10 | 14 | 19 | 19 |
| 1/0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 9 | 12 | 16 | 16 |
| 2/0 | 0 | 1 | 1 | 1 | 1 | 3 | 5 | 8 | 11 | 14 | 14 |
| 3/0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 9 | 12 | 12 |
| 4/0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 8 | 10 | 10 |
| 250 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 8 | 8 |
| 300 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 5 | 7 | 7 |
| 350 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 6 | 6 |
| 400 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 6 |
| 500 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 5 |
| 600 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 |
| 700 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 3 |
| 750 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 |
| TW | 14 | 9 | 15 | 23 | 36 | 53 | 94 | 141 | 203 | 277 | 361 |
| THHW, | 12 | 7 | 11 | 18 | 28 | 41 | 72 | 108 | 156 | 212 | 277 |
| THW, | 10 | 5 | 8 | 13 | 21 | 30 | 54 | 81 | 116 | 158 | 207 |
| THW-2 | 8 | 3 | 5 | 7 | 11 | 17 | 30 | 45 | 64 | 88 | 115 |
| RHH*, RHW*, | 14 | 6 | 10 | 15 | 24 | 35 | 62 | 94 | 135 | 184 | 240 |
| RHW-2* | 12 | 5 | 8 | 12 | 19 | 28 | 50 | 75 | 108 | 148 | 193 |
| | 10 | 4 | 6 | 10 | 15 | 22 | 39 | 59 | 85 | 115 | 151 |
| | 8 | 1 | 4 | 6 | 9 | 13 | 23 | 35 | 51 | 69 | 90 |
| RHH*, RHW*, | 6 | 1 | 3 | 4 | 7 | 10 | 18 | 27 | 39 | 53 | 69 |
| RHW-2*, TW, | 4 | 1 | 1 | 3 | 5 | 7 | 13 | 20 | 29 | 39 | 51 |
| THW, THHW, | 3 | 1 | 1 | 3 | 4 | 6 | 11 | 17 | 25 | 34 | 44 |
| THW-2 | 2 | 1 | 1 | 2 | 4 | 5 | 10 | 14 | 21 | 29 | 37 |
| | 1 | 1 | 1 | 1 | 2 | 4 | 7 | 10 | 15 | 20 | 26 |
| 1/0 | 0 | 1 | 1 | 1 | 3 | 6 | 9 | 12 | 17 | 22 | 22 |
| 2/0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 10 | 14 | 19 | 19 |
| 3/0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 9 | 12 | 16 | 16 |
| 4/0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 10 | 13 | 13 |
| 250 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 8 | 11 |
| 300 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 7 | 9 |
| 350 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 8 |
| 400 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 7 |
| 500 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 6 |
| 600 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 5 |
| 700 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 4 |
| 750 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 4 |
| THHN, | 14 | 13 | 22 | 33 | 52 | 76 | 134 | 202 | 291 | 396 | 518 |
| THWN, | 12 | 9 | 16 | 24 | 38 | 56 | 98 | 147 | 212 | 289 | 378 |
| THWN-2 | 10 | 6 | 10 | 15 | 24 | 35 | 62 | 93 | 134 | 182 | 238 |
| | 8 | 3 | 6 | 9 | 14 | 20 | 35 | 53 | 77 | 105 | 137 |
| | 6 | 2 | 4 | 6 | 10 | 14 | 25 | 38 | 55 | 76 | 99 |
| | 4 | 1 | 2 | 4 | 6 | 9 | 16 | 24 | 34 | 46 | 61 |
| | 3 | 1 | 1 | 3 | 5 | 7 | 13 | 20 | 29 | 39 | 51 |
| | 2 | 1 | 1 | 3 | 4 | 6 | 11 | 17 | 24 | 33 | 43 |
| | 1 | 1 | 1 | 1 | 3 | 4 | 8 | 12 | 18 | 24 | 32 |
| 1/0 | 0 | 1 | 1 | 1 | 2 | 4 | 7 | 10 | 15 | 20 | 27 |
| 2/0 | 0 | 1 | 1 | 1 | 3 | 6 | 9 | 12 | 17 | 22 | 22 |
| 3/0 | 0 | 1 | 1 | 1 | 2 | 5 | 7 | 10 | 14 | 19 | 18 |

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MAXIMUM NUMBER OF CONDUCTORS IN FLEXIBLE METAL CONDUIT

| Type Letters | Cond. Size AWG/kcmil | Trade Sizes In Inches | | | | | | | | | |
|-------------------|----------------------|-----------------------|-----|----|-------|-------|-----|-------|-----|-------|-----|
| | | 1/2 | 3/4 | 1 | 1 1/4 | 1 1/2 | 2 | 2 1/2 | 3 | 3 1/2 | 4 |
| THHN, | 4/0 | 0 | 1 | 1 | 1 | 1 | 4 | 6 | 8 | 12 | 15 |
| THWN, | 250 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 9 | 12 |
| THWN-2 | 300 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 8 | 11 |
| | 350 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 7 | 9 |
| | 400 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 6 | 8 |
| | 500 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 5 | 7 |
| | 600 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 5 |
| | 700 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 |
| | 750 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 |
| FEP, FEPB, | 14 | 12 | 21 | 32 | 51 | 74 | 130 | 196 | 282 | 385 | 502 |
| PFA, PFAH, | 12 | 9 | 15 | 24 | 37 | 54 | 95 | 143 | 206 | 281 | 367 |
| TFE | 10 | 6 | 11 | 17 | 26 | 39 | 68 | 103 | 148 | 201 | 263 |
| | 8 | 4 | 6 | 10 | 15 | 22 | 39 | 59 | 85 | 115 | 151 |
| | 6 | 2 | 4 | 7 | 11 | 16 | 28 | 42 | 60 | 82 | 107 |
| | 4 | 1 | 3 | 5 | 7 | 11 | 19 | 29 | 42 | 57 | 75 |
| | 3 | 1 | 2 | 4 | 6 | 9 | 16 | 24 | 35 | 48 | 62 |
| | 2 | 1 | 1 | 3 | 5 | 7 | 13 | 20 | 29 | 39 | 51 |
| PFA, PFAH, TFE | 1 | 1 | 1 | 2 | 3 | 5 | 9 | 14 | 20 | 27 | 36 |
| PFA, PFAH, TFE, Z | 1/0 | 1 | 1 | 1 | 3 | 4 | 8 | 11 | 17 | 23 | 30 |
| | 2/0 | 1 | 1 | 1 | 2 | 3 | 6 | 9 | 14 | 19 | 24 |
| | 3/0 | 0 | 1 | 1 | 1 | 3 | 5 | 8 | 11 | 15 | 20 |
| | 4/0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 9 | 13 | 16 |
| Z | 14 | 15 | 25 | 39 | 61 | 89 | 157 | 236 | 340 | 463 | 605 |
| | 12 | 11 | 18 | 28 | 43 | 63 | 111 | 168 | 241 | 329 | 429 |
| | 10 | 6 | 11 | 17 | 26 | 39 | 68 | 103 | 148 | 201 | 263 |
| | 8 | 4 | 7 | 11 | 17 | 24 | 43 | 65 | 93 | 127 | 166 |
| | 6 | 3 | 5 | 7 | 12 | 17 | 30 | 45 | 65 | 89 | 117 |
| | 4 | 1 | 3 | 5 | 8 | 12 | 21 | 31 | 45 | 61 | 80 |
| | 3 | 1 | 2 | 4 | 6 | 8 | 15 | 23 | 33 | 45 | 58 |
| | 2 | 1 | 1 | 3 | 5 | 7 | 12 | 19 | 27 | 37 | 49 |
| | 1 | 1 | 1 | 2 | 4 | 6 | 10 | 15 | 22 | 30 | 39 |
| XHH, XHHW, | 14 | 9 | 15 | 23 | 36 | 53 | 94 | 141 | 203 | 277 | 361 |
| XHHW-2 | 12 | 7 | 11 | 18 | 28 | 41 | 72 | 108 | 156 | 212 | 277 |
| ZW | 10 | 5 | 8 | 13 | 21 | 30 | 54 | 81 | 116 | 158 | 207 |
| | 8 | 3 | 5 | 7 | 11 | 17 | 30 | 45 | 64 | 88 | 115 |
| | 6 | 1 | 3 | 5 | 8 | 12 | 22 | 33 | 48 | 65 | 85 |
| | 4 | 1 | 2 | 4 | 6 | 9 | 16 | 24 | 34 | 47 | 61 |
| | 3 | 1 | 1 | 3 | 5 | 7 | 13 | 20 | 29 | 40 | 52 |
| | 2 | 1 | 1 | 3 | 4 | 6 | 11 | 17 | 24 | 33 | 44 |
| XHH, XHHW, XHHW-2 | 1 | 1 | 1 | 1 | 3 | 5 | 8 | 13 | 18 | 25 | 32 |
| | 1/0 | 1 | 1 | 1 | 2 | 4 | 7 | 10 | 15 | 21 | 27 |
| | 2/0 | 0 | 1 | 1 | 2 | 3 | 6 | 9 | 13 | 17 | 23 |
| | 3/0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 10 | 14 | 19 |
| | 4/0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 9 | 12 | 15 |
| | 250 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 10 | 13 |
| | 300 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 8 | 11 |
| | 350 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 5 | 7 | 9 |
| | 400 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 6 | 8 |
| | 500 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 5 | 7 |
| | 600 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 5 |
| | 700 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 5 |
| | 750 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 4 |

* Types RHH, RHW, AND RHW-2 without outer covering.

See Ugly's page 131 for Trade Size / Metric Designator conversion.

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MAXIMUM NUMBER OF CONDUCTORS IN LIQUIDTIGHT FLEXIBLE METAL CONDUIT

| Type Letters | Cond. Size AWG/kcmil | Trade Sizes In Inches | | | | | | | | | |
|--------------|----------------------|-----------------------|-----|----|-------|-------|-----|-------|-----|-------|-----|
| | | 1/8 | 3/4 | 1 | 1 1/4 | 1 1/2 | 2 | 2 1/2 | 3 | 3 1/2 | 4 |
| RHH, RHW, | 14 | 4 | 7 | 12 | 21 | 27 | 44 | 66 | 102 | 133 | 173 |
| RHW-2 | 12 | 3 | 6 | 10 | 17 | 22 | 36 | 55 | 84 | 110 | 144 |
| | 10 | 3 | 5 | 8 | 14 | 18 | 29 | 44 | 68 | 89 | 116 |
| | 8 | 1 | 2 | 4 | 7 | 9 | 15 | 23 | 36 | 46 | 61 |
| | 6 | 1 | 1 | 3 | 6 | 7 | 12 | 18 | 28 | 37 | 48 |
| | 4 | 1 | 1 | 2 | 4 | 6 | 9 | 14 | 22 | 29 | 38 |
| | 3 | 1 | 1 | 1 | 4 | 5 | 8 | 13 | 19 | 25 | 33 |
| | 2 | 1 | 1 | 1 | 3 | 4 | 7 | 11 | 17 | 22 | 29 |
| | 1 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 11 | 14 | 19 |
| 1/0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 10 | 13 | 16 | |
| 2/0 | 0 | 1 | 1 | 1 | 1 | 3 | 5 | 8 | 11 | 14 | |
| 3/0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 7 | 9 | 12 | |
| 4/0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 8 | 10 | |
| 250 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 8 | |
| 300 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 5 | 7 | |
| 350 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 6 | |
| 400 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 3 | 4 | 6 | |
| 500 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 2 | 4 | |
| 600 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 1 | 3 | |
| 700 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 3 | |
| 750 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | |
| TW | 14 | 9 | 15 | 25 | 44 | 57 | 93 | 140 | 215 | 280 | 365 |
| THHW, | 12 | 7 | 12 | 19 | 33 | 43 | 71 | 108 | 165 | 215 | 280 |
| THW, | 10 | 5 | 9 | 14 | 25 | 32 | 53 | 80 | 123 | 160 | 209 |
| THW-2 | 8 | 3 | 5 | 8 | 14 | 18 | 29 | 44 | 68 | 89 | 116 |
| RHH*, RHW*, | 14 | 6 | 10 | 16 | 29 | 38 | 62 | 93 | 143 | 186 | 243 |
| RHW-2* | 12 | 5 | 8 | 13 | 23 | 30 | 50 | 75 | 115 | 149 | 195 |
| | 10 | 3 | 6 | 10 | 18 | 23 | 39 | 58 | 89 | 117 | 152 |
| | 8 | 1 | 4 | 6 | 11 | 14 | 23 | 35 | 53 | 70 | 91 |
| RHH*, RHW*, | 6 | 1 | 3 | 5 | 8 | 11 | 18 | 27 | 41 | 53 | 70 |
| RHW-2*, TW, | 4 | 1 | 1 | 3 | 6 | 8 | 13 | 20 | 30 | 40 | 52 |
| THW, THHW, | 3 | 1 | 1 | 3 | 5 | 7 | 11 | 17 | 26 | 34 | 44 |
| THW-2 | 2 | 1 | 1 | 2 | 4 | 6 | 9 | 14 | 22 | 29 | 38 |
| | 1 | 1 | 1 | 1 | 3 | 4 | 7 | 10 | 15 | 20 | 26 |
| 1/0 | 0 | 1 | 1 | 2 | 3 | 6 | 8 | 13 | 17 | 23 | |
| 2/0 | 0 | 1 | 1 | 2 | 3 | 5 | 7 | 11 | 15 | 19 | |
| 3/0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 9 | 12 | 16 | |
| 4/0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 8 | 10 | 13 | |
| 250 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 8 | 11 |
| 300 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 7 | 9 |
| 350 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 6 | 8 | |
| 400 | 0 | 0 | 0 | 0 | 1 | 1 | 3 | 4 | 6 | 7 | |
| 500 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 3 | 5 | 6 | |
| 600 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 5 | |
| 700 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | |
| 750 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 3 | 4 | |
| THHN, | 14 | 13 | 22 | 36 | 63 | 81 | 133 | 201 | 308 | 401 | 523 |
| THWN, | 12 | 9 | 16 | 26 | 46 | 59 | 97 | 146 | 225 | 292 | 381 |
| THWN-2 | 10 | 6 | 10 | 16 | 29 | 37 | 61 | 92 | 141 | 184 | 240 |
| | 8 | 3 | 6 | 9 | 16 | 21 | 35 | 53 | 81 | 106 | 138 |
| | 6 | 2 | 4 | 7 | 12 | 15 | 25 | 38 | 59 | 76 | 100 |
| | 4 | 1 | 2 | 4 | 7 | 9 | 15 | 23 | 36 | 47 | 61 |
| | 3 | 1 | 1 | 3 | 6 | 8 | 13 | 20 | 30 | 40 | 52 |
| | 2 | 1 | 1 | 3 | 5 | 7 | 11 | 17 | 26 | 33 | 44 |
| | 1 | 1 | 1 | 1 | 4 | 5 | 8 | 12 | 19 | 25 | 32 |
| 1/0 | 0 | 1 | 1 | 1 | 3 | 4 | 7 | 10 | 16 | 21 | 27 |
| 2/0 | 0 | 1 | 1 | 2 | 3 | 6 | 8 | 13 | 17 | 23 | |
| 3/0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 11 | 14 | 19 | |

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MAXIMUM NUMBER OF CONDUCTORS IN LIQUIDTIGHT FLEXIBLE METAL CONDUIT

| Type Letters | Cond. Size AWG/kcmil | Trade Sizes In Inches | | | | | | | | | |
|-------------------|----------------------|-----------------------|-----|----|-------|-------|-----|-------|-----|-------|-----|
| | | 1/8 | 3/4 | 1 | 1 1/4 | 1 1/2 | 2 | 2 1/2 | 3 | 3 1/2 | 4 |
| THHN, | 4/0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 9 | 12 | 15 |
| THWN, | 250 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 10 | 12 |
| THWN-2 | 300 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 8 | 11 |
| | 350 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 7 | 9 |
| | 400 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 6 |
| | 500 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 |
| | 600 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 3 | 4 |
| | 700 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 |
| | 750 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 3 | 5 |
| FEP, FEPB, | 14 | 12 | 21 | 35 | 61 | 79 | 129 | 195 | 299 | 389 | 507 |
| PFA, PFAH, | 12 | 9 | 15 | 25 | 44 | 57 | 94 | 142 | 218 | 284 | 370 |
| TFE | 10 | 6 | 11 | 18 | 32 | 41 | 68 | 102 | 156 | 203 | 266 |
| | 8 | 3 | 6 | 10 | 18 | 23 | 39 | 58 | 89 | 117 | 152 |
| | 6 | 2 | 4 | 7 | 13 | 17 | 27 | 41 | 64 | 83 | 108 |
| | 4 | 1 | 3 | 5 | 9 | 12 | 19 | 29 | 44 | 58 | 75 |
| | 3 | 1 | 2 | 4 | 7 | 10 | 16 | 24 | 37 | 48 | 63 |
| | 2 | 1 | 1 | 3 | 6 | 8 | 13 | 20 | 30 | 40 | 52 |
| PFA, PFAH, TFE | 1 | 1 | 1 | 2 | 4 | 5 | 9 | 14 | 21 | 28 | 36 |
| PFA, PFAH, TFE, Z | 1/0 | 1 | 1 | 1 | 3 | 4 | 7 | 11 | 18 | 23 | 30 |
| | 2/0 | 1 | 1 | 1 | 2 | 3 | 4 | 6 | 9 | 14 | 25 |
| | 3/0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 8 | 12 | 20 |
| | 4/0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 10 | 13 | 17 |
| Z | 14 | 20 | 26 | 42 | 73 | 95 | 156 | 235 | 360 | 469 | 611 |
| | 12 | 14 | 18 | 30 | 52 | 67 | 111 | 167 | 255 | 332 | 434 |
| | 10 | 8 | 11 | 18 | 32 | 41 | 68 | 102 | 156 | 203 | 266 |
| | 8 | 5 | 7 | 11 | 20 | 26 | 43 | 64 | 99 | 129 | 168 |
| | 6 | 4 | 5 | 8 | 14 | 18 | 30 | 45 | 69 | 90 | 118 |
| | 4 | 2 | 3 | 5 | 9 | 12 | 20 | 31 | 48 | 62 | 81 |
| | 3 | 2 | 2 | 4 | 7 | 9 | 15 | 23 | 35 | 45 | 59 |
| | 2 | 1 | 1 | 3 | 6 | 7 | 12 | 19 | 29 | 38 | 49 |
| | 1 | 1 | 1 | 2 | 5 | 6 | 10 | 15 | 23 | 30 | 40 |
| XHH, XHHW, | 14 | 9 | 15 | 25 | 44 | 57 | 93 | 140 | 215 | 280 | 365 |
| XHHW-2, | 12 | 7 | 12 | 19 | 33 | 43 | 71 | 108 | 165 | 215 | 280 |
| ZW | 10 | 5 | 9 | 14 | 25 | 32 | 53 | 80 | 123 | 160 | 209 |
| | 8 | 3 | 5 | 8 | 14 | 18 | 29 | 44 | 68 | 89 | 116 |
| | 6 | 1 | 3 | 6 | 10 | 13 | 22 | 33 | 50 | 66 | 86 |
| | 4 | 1 | 2 | 4 | 7 | 9 | 16 | 24 | 36 | 48 | 62 |
| | 3 | 1 | 1 | 3 | 6 | 8 | 13 | 20 | 31 | 40 | 52 |
| | 2 | 1 | 1 | 3 | 5 | 7 | 11 | 17 | 26 | 34 | 44 |
| XHH, XHHW, XHHW-2 | 1 | 1 | 1 | 1 | 4 | 5 | 8 | 12 | 19 | 25 | 33 |
| | 1/0 | 1 | 1 | 1 | 3 | 4 | 7 | 10 | 16 | 21 | 28 |
| | 2/0 | 0 | 1 | 1 | 2 | 3 | 6 | 9 | 13 | 17 | 23 |
| | 3/0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 11 | 14 | 19 |
| | 4/0 | 0 | 1 | 1 | 1 | 2 | 4 | 6 | 9 | 12 | 16 |
| | 250 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 7 | 10 | 13 |
| | 300 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 | 8 | 11 |
| | 350 | 0 | 0 | 1 | 1 | 1 | 2 | 3 | 5 | 7 | 10 |
| | 400 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 5 | 6 | 8 |
| | 500 | 0 | 0 | 0 | 1 | 1 | 1 | 2 | 4 | 5 | 7 |
| | 600 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 4 | 6 |
| | 700 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 3 | 4 |
| | 750 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 3 | 3 |

* Types RHH, RHW, AND RHW-2 without outer covering.

See Ugly's page 131 for Trade Size / Metric Designator conversion.

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DIMENSIONS OF INSULATED CONDUCTORS & FIXTURE WIRES

| TYPE | SIZE | APPROX. AREA SQ. IN. | TYPE | SIZE | APPROX. AREA SQ. IN. |
|--------------------|--------|----------------------|------------------------|------|----------------------|
| RFH-2 | 18 | 0.0145 | THHW, THW, AF, XF, XFF | 10 | 0.0333 |
| FFH-2 | 16 | 0.0172 | RHH*, RHW*, RHW-2* | 8 | 0.0556 |
| RHW-2, RHH | 14 | 0.0293 | TW, THW | 6 | 0.0726 |
| RHW | 12 | 0.0353 | THHW | 4 | 0.0973 |
| | 10 | 0.0437 | THW-2 | 3 | 0.1134 |
| | 8 | 0.0835 | RHH* | 2 | 0.1333 |
| | 6 | 0.1041 | RHW* | 1 | 0.1901 |
| | 4 | 0.1333 | RHW-2* | 1/0 | 0.2223 |
| | 3 | 0.1521 | | 2/0 | 0.2624 |
| | 2 | 0.1750 | | 3/0 | 0.3117 |
| | 1 | 0.2660 | | 4/0 | 0.3718 |
| 1/0 | 0.3039 | | | 250 | 0.4596 |
| 2/0 | 0.3505 | | | 300 | 0.5281 |
| 3/0 | 0.4072 | | | 350 | 0.5958 |
| 4/0 | 0.4754 | | | 400 | 0.6619 |
| 250 | 0.6291 | | | 500 | 0.7901 |
| 300 | 0.7088 | | | 600 | 0.9729 |
| 350 | 0.7870 | | | 700 | 1.1010 |
| 400 | 0.8626 | | | 750 | 1.1652 |
| 500 | 1.0082 | | | 800 | 1.2272 |
| 600 | 1.2135 | | | 900 | 1.3561 |
| 700 | 1.3561 | | | 1000 | 1.4784 |
| 750 | 1.4272 | | | 1250 | 1.8602 |
| 800 | 1.4957 | | | 1500 | 2.1695 |
| 900 | 1.6377 | | | 1750 | 2.4773 |
| 1000 | 1.7719 | | | 2000 | 2.7818 |
| 1250 | 2.3479 | | TFN | 18 | 0.0055 |
| 1500 | 2.6938 | | TFFN | 16 | 0.0072 |
| 1750 | 3.0357 | | THHN | 14 | 0.0097 |
| 2000 | 3.3719 | | THWN | 12 | 0.0133 |
| SF-2, SFF-2 | 18 | 0.0115 | THWN-2 | 10 | 0.0211 |
| | 16 | 0.0139 | | 8 | 0.0366 |
| | 14 | 0.0172 | | 6 | 0.0507 |
| SF-1, SFF-1 | 18 | 0.0065 | | 4 | 0.0824 |
| RFH-1, XF, XFF | 18 | 0.0080 | | 3 | 0.0973 |
| TF, TFF, XF, XFF | 16 | 0.0109 | | 2 | 0.1158 |
| TW, XF, XFF, | 14 | 0.0139 | | 1 | 0.1562 |
| THHW, THW, THW-2 | | | | 1/0 | 0.1855 |
| TW, THHW, | 12 | 0.0181 | | 2/0 | 0.2223 |
| THW, THW-2 | 10 | 0.0243 | | 3/0 | 0.2679 |
| | 8 | 0.0437 | | 4/0 | 0.3237 |
| RHH*, RHW*, RHW-2* | 14 | 0.0209 | | 250 | 0.3970 |
| | 12 | 0.0260 | | 300 | 0.4608 |

*Types RHH, RHW, and RHW-2 without outer covering

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DIMENSIONS OF INSULATED CONDUCTORS & FIXTURE WIRES

| TYPE | SIZE | APPROX. AREA SQ. IN. | TYPE | SIZE | APPROX. AREA SQ. IN. |
|----------------------|------|----------------------|--------|------|----------------------|
| THHN | 750 | 1.0496 | XHHW | 300 | 0.4536 |
| THWN | 800 | 1.1085 | XHHW-2 | 350 | 0.5166 |
| THWN-2 | 900 | 1.2311 | XHH | 400 | 0.5782 |
| | 1000 | 1.3478 | | 500 | 0.6984 |
| PF, PGFF, PGF, PFF, | 18 | 0.0058 | | 600 | 0.8709 |
| PTF, PAF, PTFF, PAFF | 16 | 0.0075 | | 750 | 1.0532 |
| PF, PGFF, PGF, PFF, | 14 | 0.0100 | | 800 | 1.1122 |
| PTF, PAF, PTFF, PAFF | | | | 900 | 1.2351 |
| TFE, FEP, PFA | | | | 1000 | 1.3519 |
| FEPB, PFAH | | | | 1250 | 1.7180 |
| TFE, FEP, | 12 | 0.0137 | | 1500 | 2.0157 |
| PFA, FEPB, | 10 | 0.0191 | | 1750 | 2.3127 |
| PFAH | 8 | 0.0333 | | 2000 | 2.6073 |
| | 6 | 0.0468 | KF-2 | 18 | 0.0031 |
| | 4 | 0.0670 | KFF-2 | 16 | 0.0044 |
| | 3 | 0.0804 | | 14 | 0.0064 |
| | 2 | 0.0973 | | 12 | 0.0093 |
| TFE, PFAH | 1 | 0.1399 | | 10 | 0.0139 |
| TFE, | 1/0 | 0.1676 | KF-1 | 18 | 0.0026 |
| PFA, | 2/0 | 0.2027 | KFF-1 | 16 | 0.0037 |
| PAFH, Z | 3/0 | 0.2463 | | 14 | 0.0055 |
| | 4/0 | 0.3000 | | 12 | 0.0083 |
| ZF, ZFF | 18 | 0.0045 | | 10 | 0.0127 |
| | 16 | 0.0061 | | | |
| Z, ZF, ZFF | 14 | 0.0083 | | | |
| Z | 12 | 0.0117 | | | |
| | 10 | 0.0191 | | | |
| | 8 | 0.0302 | | | |
| | 6 | 0.0430 | | | |
| | 4 | 0.0625 | | | |
| | 3 | 0.0855 | | | |
| | 2 | 0.1029 | | | |
| | 1 | 0.1269 | | | |
| XHHW, ZW | 14 | 0.0139 | | | |
| XHHW-2 | 12 | 0.0181 | | | |
| XHH | 10 | 0.0243 | | | |
| | 8 | 0.0437 | | | |
| | 6 | 0.0590 | | | |
| | 4 | 0.0814 | | | |
| | 3 | 0.0962 | | | |
| | 2 | 0.1146 | | | |
| XHHW | 1 | 0.1534 | | | |
| XHHW-2 | 1/0 | 0.1825 | | | |
| XHH | 2/0 | 0.2190 | | | |
| | 3/0 | 0.2642 | | | |
| | 4/0 | 0.3197 | | | |
| | 250 | 0.3904 | | | |

*Types RHH, RHW, and RHW-2 without outer covering
See Ugly's page 129 - 135 for conversion of Square inches to mm².

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| COMPACT ALUMINUM BUILDING WIRE NOMINAL DIMENSIONS* AND AREAS | | | | | | | | | |
|--|-------------------------|-----------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|-------------------------|
| Size AWG or kcmil | Number of Strands | Bare Conductor | | Types THW and THHW | | Type THHN | | Type XHHW | |
| | | Diam. inches | Approx. Diam. inches | Approx. Area Sq. In. | Approx. Diam. inches | Approx. Area Sq. In. | Approx. Diam. inches | Approx. Area Sq. In. | Size Avg or kcmil |
| 8 | 7 | 0.134 | 0.255 | 0.0510 | 0.0510 | — | 0.224 | 0.0394 | 8 |
| 6 | 7 | 0.169 | 0.290 | 0.0660 | 0.240 | 0.0452 | 0.260 | 0.0530 | 6 |
| 4 | 7 | 0.213 | 0.335 | 0.0881 | 0.305 | 0.0730 | 0.305 | 0.0730 | 4 |
| 2 | 7 | 0.268 | 0.390 | 0.1194 | 0.360 | 0.1017 | 0.360 | 0.1017 | 2 |
| 1 | 19 | 0.299 | 0.465 | 0.1698 | 0.415 | 0.1352 | 0.415 | 0.1352 | 1 |
| 1/0 | 19 | 0.336 | 0.500 | 0.1963 | 0.450 | 0.1590 | 0.450 | 0.1590 | 10 |
| 2/0 | 19 | 0.376 | 0.545 | 0.2332 | 0.495 | 0.1924 | 0.490 | 0.1885 | 20 |
| 3/0 | 19 | 0.423 | 0.590 | 0.2733 | 0.540 | 0.2290 | 0.540 | 0.2290 | 30 |
| 4/0 | 19 | 0.475 | 0.645 | 0.3267 | 0.595 | 0.2780 | 0.590 | 0.2733 | 40 |
| 250 | 37 | 0.520 | 0.725 | 0.4128 | 0.570 | 0.3325 | 0.660 | 0.3421 | 250 |
| 300 | 37 | 0.570 | 0.775 | 0.4717 | 0.720 | 0.4071 | 0.715 | 0.4015 | 300 |
| 350 | 37 | 0.616 | 0.820 | 0.5281 | 0.770 | 0.4656 | 0.760 | 0.4536 | 350 |
| 400 | 37 | 0.659 | 0.865 | 0.5876 | 0.815 | 0.5216 | 0.800 | 0.5026 | 400 |
| 500 | 37 | 0.736 | 0.940 | 0.6939 | 0.885 | 0.6151 | 0.880 | 0.6082 | 500 |
| 600 | 61 | 0.813 | 1.050 | 0.8659 | 0.985 | 0.7620 | 0.980 | 0.7542 | 600 |
| 700 | 61 | 0.877 | 1.110 | 0.9676 | 1.050 | 0.8859 | 1.050 | 0.8659 | 700 |
| 750 | 61 | 0.908 | 1.150 | 1.0386 | 1.075 | 0.9076 | 1.090 | 0.9331 | 750 |
| 1000 | 61 | 1.060 | 1.285 | 1.2968 | 1.255 | 1.2370 | 1.230 | 1.1882 | 1000 |

* Dimensions are from industry sources.

See Ugly's page 127 - 135 for metric conversions.

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DIMENSIONS AND PERCENT AREA OF CONDUIT AND TUBING

(for the combinations of wires permitted in Table 1, Chapter 9, NEC®)

(See Ugly's page 127 - 135 for metric conversion)

| Trade Size Inches | Internal Diameter Inches | ELECTRICAL METALLIC TUBING (EMT) | | | |
|----------------------|--------------------------------|----------------------------------|----------------|----------------|----------------|
| | | 100% Sq. in. | 31% Sq. in. | 40% Sq. in. | 53% Sq. in. |
| 1/2 | 0.622 | 0.304 | 0.094 | 0.122 | 0.161 |
| 3/4 | 0.824 | 0.533 | 0.165 | 0.213 | 0.283 |
| 1 | 1.049 | 0.864 | 0.268 | 0.346 | 0.458 |
| 1 1/4 | 1.380 | 1.496 | 0.464 | 0.598 | 0.793 |
| 1 1/2 | 1.610 | 2.036 | 0.631 | 0.814 | 1.079 |
| 2 | 2.067 | 3.356 | 1.040 | 1.342 | 1.778 |
| 2 1/2 | 2.731 | 5.858 | 1.816 | 2.343 | 3.105 |
| 3 | 3.356 | 8.846 | 2.742 | 3.538 | 4.688 |
| 3 1/2 | 3.834 | 11.545 | 3.579 | 4.618 | 6.119 |
| 4 | 4.334 | 14.753 | 4.573 | 5.901 | 7.819 |

ELECTRICAL NONMETALLIC TUBING (ENT)

| | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|
| 1/2 | 0.560 | 0.246 | 0.076 | 0.099 | 0.131 | 0.148 |
| 3/4 | 0.760 | 0.454 | 0.141 | 0.181 | 0.240 | 0.272 |
| 1 | 1.000 | 0.785 | 0.243 | 0.314 | 0.416 | 0.471 |
| 1 1/4 | 1.340 | 1.410 | 0.437 | 0.564 | 0.747 | 0.846 |
| 1 1/2 | 1.570 | 1.936 | 0.600 | 0.774 | 1.026 | 1.162 |
| 2 | 2.020 | 3.205 | 0.993 | 1.282 | 1.699 | 1.923 |
| 2 1/2 | — | — | — | — | — | — |
| 3 | — | — | — | — | — | — |
| 3 1/2 | — | — | — | — | — | — |
| 4 | — | — | — | — | — | — |

FLEXIBLE METAL CONDUIT (FMC)

| | | | | | | |
|-------|-------|--------|-------|-------|-------|-------|
| 3/8 | 0.384 | 0.116 | 0.036 | 0.046 | 0.061 | 0.069 |
| 1/2 | 0.635 | 0.317 | 0.098 | 0.127 | 0.168 | 0.190 |
| 3/4 | 0.824 | 0.533 | 0.165 | 0.213 | 0.283 | 0.320 |
| 1 | 1.020 | 0.817 | 0.253 | 0.327 | 0.433 | 0.490 |
| 1 1/4 | 1.275 | 1.277 | 0.396 | 0.511 | 0.677 | 0.766 |
| 1 1/2 | 1.538 | 1.858 | 0.576 | 0.743 | 0.985 | 1.115 |
| 2 | 2.040 | 3.269 | 1.013 | 1.307 | 1.732 | 1.961 |
| 2 1/2 | 2.500 | 4.909 | 1.522 | 1.963 | 2.602 | 2.945 |
| 3 | 3.000 | 7.069 | 2.191 | 2.827 | 3.746 | 4.241 |
| 3 1/2 | 3.500 | 9.621 | 2.983 | 3.848 | 5.099 | 5.773 |
| 4 | 4.000 | 12.566 | 3.896 | 5.027 | 6.660 | 7.540 |

INTERMEDIATE METAL CONDUIT (IMC)

| | | | | | | |
|-------|-------|--------|-------|-------|-------|-------|
| 3/8 | 0.660 | 0.342 | 0.106 | 0.137 | 0.181 | 0.205 |
| 1/2 | 0.864 | 0.586 | 0.182 | 0.235 | 0.311 | 0.352 |
| 1 | 1.105 | 0.959 | 0.297 | 0.384 | 0.508 | 0.575 |
| 1 1/4 | 1.448 | 1.647 | 0.510 | 0.659 | 0.873 | 0.988 |
| 1 1/2 | 1.683 | 2.225 | 0.690 | 0.890 | 1.179 | 1.335 |
| 2 | 2.150 | 3.630 | 1.125 | 1.452 | 1.924 | 2.178 |
| 2 1/2 | 2.557 | 5.135 | 1.592 | 2.054 | 2.722 | 3.081 |
| 3 | 3.176 | 7.922 | 2.456 | 3.169 | 4.199 | 4.753 |
| 3 1/2 | 3.671 | 10.584 | 3.281 | 4.234 | 5.610 | 6.351 |
| 4 | 4.166 | 13.631 | 4.226 | 5.452 | 7.224 | 8.179 |

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DIMENSIONS AND PERCENT AREA OF CONDUIT AND TUBING

(for the combinations of wires permitted in Table 1, Chapter 9, NEC®)

(See Ugly's page 127 - 135 for metric conversion)

| Trade Size | Internal Diameter | Total Area | 2 Wires | Over 2 Wires | 1 Wire | 100% | 31% | 40% | 53% | 60% |
|--|-------------------|------------|---------|--------------|---------|-------|-----|-----|-----|-----|
| Inches | Inches | Sq. in. | Sq. in. | Sq. in. | Sq. in. | | | | | |
| LIQUIDTIGHT FLEXIBLE NONMETALLIC CONDUIT (TYPE LFNC-B*) | | | | | | | | | | |
| 3/8 | 0.494 | 0.192 | 0.059 | 0.077 | 0.102 | 0.115 | | | | |
| 1/2 | 0.632 | 0.314 | 0.097 | 0.125 | 0.166 | 0.188 | | | | |
| 5/8 | 0.830 | 0.541 | 0.168 | 0.216 | 0.287 | 0.325 | | | | |
| 1 | 1.054 | 0.873 | 0.270 | 0.349 | 0.462 | 0.524 | | | | |
| 1 1/4 | 1.395 | 1.528 | 0.474 | 0.611 | 0.810 | 0.917 | | | | |
| 1 1/2 | 1.588 | 1.981 | 0.614 | 0.792 | 1.050 | 1.188 | | | | |
| 2 | 2.033 | 3.246 | 1.006 | 1.298 | 1.720 | 1.948 | | | | |

* Corresponds to Section 356.2(2).

LIQUIDTIGHT FLEXIBLE NONMETALLIC CONDUIT (TYPE LFNC-A*)

| | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|
| 3/8 | 0.495 | 0.192 | 0.060 | 0.077 | 0.102 | 0.115 |
| 1/2 | 0.630 | 0.312 | 0.097 | 0.125 | 0.165 | 0.187 |
| 5/8 | 0.825 | 0.535 | 0.166 | 0.214 | 0.283 | 0.321 |
| 1 | 1.043 | 0.854 | 0.265 | 0.342 | 0.453 | 0.513 |
| 1 1/4 | 1.383 | 1.502 | 0.466 | 0.601 | 0.796 | 0.901 |
| 1 1/2 | 1.603 | 2.018 | 0.626 | 0.807 | 1.070 | 1.211 |
| 2 | 2.063 | 3.343 | 1.036 | 1.337 | 1.772 | 2.006 |

* Corresponds to Section 356.2(1).

LIQUIDTIGHT FLEXIBLE METAL CONDUIT (LFMC)

| | | | | | | |
|-------|-------|--------|-------|-------|-------|-------|
| 3/8 | 0.494 | 0.192 | 0.059 | 0.077 | 0.102 | 0.115 |
| 1/2 | 0.632 | 0.314 | 0.097 | 0.125 | 0.166 | 0.188 |
| 5/8 | 0.830 | 0.541 | 0.168 | 0.216 | 0.287 | 0.325 |
| 1 | 1.054 | 0.873 | 0.270 | 0.349 | 0.462 | 0.524 |
| 1 1/4 | 1.395 | 1.528 | 0.474 | 0.611 | 0.810 | 0.917 |
| 1 1/2 | 1.588 | 1.981 | 0.614 | 0.792 | 1.050 | 1.188 |
| 2 | 2.033 | 3.246 | 1.006 | 1.298 | 1.720 | 1.948 |
| 2 1/2 | 2.493 | 4.881 | 1.513 | 1.953 | 2.587 | 2.929 |
| 3 | 3.085 | 7.475 | 2.317 | 2.990 | 3.962 | 4.485 |
| 3 1/2 | 3.520 | 9.731 | 3.017 | 3.893 | 5.158 | 5.839 |
| 4 | 4.020 | 12.692 | 3.935 | 5.077 | 6.727 | 7.615 |

RIGID METAL CONDUIT (RMC)

| | | | | | | |
|-------|-------|--------|-------|--------|--------|--------|
| 3/8 | - | - | - | - | - | - |
| 1/2 | 0.632 | 0.314 | 0.097 | 0.125 | 0.166 | 0.188 |
| 5/8 | 0.836 | 0.549 | 0.170 | 0.220 | 0.291 | 0.329 |
| 1 | 1.063 | 0.887 | 0.275 | 0.355 | 0.470 | 0.532 |
| 1 1/4 | 1.394 | 1.526 | 0.473 | 0.610 | 0.809 | 0.916 |
| 1 1/2 | 1.624 | 2.071 | 0.642 | 0.829 | 1.098 | 1.243 |
| 2 | 2.083 | 3.408 | 1.056 | 1.363 | 1.806 | 2.045 |
| 2 1/2 | 2.489 | 4.866 | 1.508 | 1.946 | 2.579 | 2.919 |
| 3 | 3.090 | 7.499 | 2.325 | 3.000 | 3.974 | 4.499 |
| 3 1/2 | 3.570 | 10.010 | 3.103 | 4.004 | 5.305 | 6.006 |
| 4 | 4.050 | 12.882 | 3.994 | 5.153 | 6.828 | 7.729 |
| 5 | 5.073 | 20.212 | 6.266 | 8.085 | 10.713 | 12.127 |
| 6 | 6.093 | 29.158 | 9.039 | 11.663 | 15.454 | 17.495 |

DIMENSIONS AND PERCENT AREA OF CONDUIT AND TUBING

(for the combinations of wires permitted in Table 1, Chapter 9, NEC®)

(See Ugly's page 127 - 135 for metric conversion)

| Trade Size | Diameter | Total Area | 2 Wires | Over 2 Wires | 1 Wire | 100% | 31% | 40% | 53% | 60% |
|---|----------|------------|---------|--------------|---------|--------|-----|-----|-----|-----|
| Inches | Inches | Sq. in. | Sq. in. | Sq. in. | Sq. in. | | | | | |
| RIGID PVC CONDUIT (RNC), SCHEDULE 80 | | | | | | | | | | |
| 1/2 | 0.526 | 0.217 | 0.067 | 0.087 | 0.115 | 0.130 | | | | |
| 3/4 | 0.722 | 0.409 | 0.127 | 0.164 | 0.217 | 0.246 | | | | |
| 1 | 0.936 | 0.688 | 0.213 | 0.275 | 0.365 | 0.413 | | | | |
| 1 1/4 | 1.255 | 1.237 | 0.383 | 0.495 | 0.656 | 0.742 | | | | |
| 1 1/2 | 1.476 | 1.711 | 0.530 | 0.684 | 0.907 | 1.027 | | | | |
| 2 | 1.913 | 2.874 | 0.891 | 1.150 | 1.523 | 1.725 | | | | |
| 2 1/2 | 2.290 | 4.119 | 1.277 | 1.647 | 2.183 | 2.471 | | | | |
| 3 | 2.864 | 6.442 | 1.997 | 2.577 | 3.414 | 3.865 | | | | |
| 3 1/2 | 3.326 | 8.688 | 2.693 | 3.475 | 4.605 | 5.213 | | | | |
| 4 | 3.786 | 11.258 | 3.490 | 4.503 | 5.967 | 6.755 | | | | |
| 5 | 4.768 | 17.855 | 5.535 | 7.142 | 9.463 | 10.713 | | | | |
| 6 | 5.709 | 25.598 | 7.935 | 10.239 | 13.567 | 15.359 | | | | |

RIGID PVC CONDUIT (RNC), SCHEDULE 40 & HDPE CONDUIT

| | | | | | | |
|-------|-------|--------|-------|--------|--------|--------|
| 1/2 | 0.602 | 0.285 | 0.088 | 0.114 | 0.151 | 0.171 |
| 3/4 | 0.804 | 0.508 | 0.157 | 0.203 | 0.269 | 0.305 |
| 1 | 1.029 | 0.832 | 0.258 | 0.333 | 0.441 | 0.499 |
| 1 1/4 | 1.360 | 1.453 | 0.450 | 0.581 | 0.770 | 0.872 |
| 1 1/2 | 1.590 | 1.986 | 0.616 | 0.794 | 1.052 | 1.191 |
| 2 | 2.047 | 3.291 | 1.020 | 1.316 | 1.744 | 1.975 |
| 2 1/2 | 2.445 | 4.695 | 1.455 | 1.878 | 2.488 | 2.817 |
| 3 | 3.042 | 7.268 | 2.253 | 2.907 | 3.852 | 4.361 |
| 3 1/2 | 3.521 | 9.737 | 3.018 | 3.895 | 5.161 | 5.842 |
| 4 | 3.998 | 12.554 | 3.892 | 5.022 | 6.654 | 7.532 |
| 5 | 5.016 | 19.761 | 6.126 | 7.904 | 10.473 | 11.856 |
| 6 | 6.031 | 28.567 | 8.856 | 11.427 | 15.141 | 17.140 |

TYPE A, RIGID PVC CONDUIT (RNC)

| | | | | | | |
|-------|-------|--------|-------|-------|-------|-------|
| 1/2 | 0.700 | 0.385 | 0.119 | 0.154 | 0.204 | 0.231 |
| 3/4 | 0.910 | 0.650 | 0.202 | 0.260 | 0.345 | 0.390 |
| 1 | 1.175 | 1.084 | 0.336 | 0.434 | 0.575 | 0.651 |
| 1 1/4 | 1.500 | 1.767 | 0.548 | 0.707 | 0.937 | 1.060 |
| 1 1/2 | 1.720 | 2.324 | 0.720 | 0.929 | 1.231 | 1.394 |
| 2 | 2.155 | 3.647 | 1.131 | 1.459 | 1.933 | 2.188 |
| 2 1/2 | 2.635 | 5.453 | 1.690 | 2.181 | 2.890 | 3.272 |
| 3 | 3.230 | 8.194 | 2.540 | 3.278 | 4.343 | 4.916 |
| 3 1/2 | 3.690 | 10.694 | 3.315 | 4.278 | 5.668 | 6.416 |
| 4 | 4.180 | 13.723 | 4.254 | 5.489 | 7.273 | 8.234 |

TYPE EB, PVC CONDUIT (RNC)

| | | | | | | |
|-------|-------|--------|-------|--------|--------|--------|
| 2 | 2.221 | 3.874 | 1.201 | 1.550 | 2.053 | 2.325 |
| 2 1/2 | - | - | - | - | - | - |
| 3 | 3.330 | 8.709 | 2.700 | 3.484 | 4.616 | 5.226 |
| 3 1/2 | 3.804 | 11.365 | 3.523 | 4.546 | 6.023 | 6.819 |
| 4 | 4.289 | 14.448 | 4.479 | 5.779 | 7.657 | 8.669 |
| 5 | 5.316 | 22.195 | 6.881 | 8.878 | 11.763 | 13.317 |
| 6 | 6.336 | 31.530 | 9.774 | 12.612 | 16.711 | 18.918 |

MULTIPLE OVERLAPPING
FD-MINIMUM INTERNAL DEPTH 2-3/8

FS-MINIMUM INTERNAL DEPTH 1-3/4
FD-MINIMUM INTERNAL DEPTH 2-3/8

SINGLE COVERAGE
FS-MINIMUM INTERNAL DEPTH 1-3/4

3-3/4" X 3-1/2" WASHDOWN BOX/GANG
FS-MINIMUM INTERNAL DEPTH 2-3/8

4 X 2-1/8" X 2-1/8" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

3 X 2 X 2-1/2" DEVIATION
FS-MINIMUM INTERNAL DEPTH 1-3/4

NOTE: For all type push button station, use size 1-7/32" knock-out punch.
For connectors, (male connectors and adapters), use size 1-7/32".

METAL BOXES

MAXIMUM NUMBER OF CONNECTORS

CU. IN.

CAPACITY

NO. 12

NO. 14

NO. 16

NO. 18

NO. 20

NO. 22

NO. 24

NO. 26

NO. 28

NO. 30

NO. 32

NO. 34

NO. 36

NO. 38

NO. 40

NO. 42

NO. 44

NO. 46

NO. 48

NO. 50

NO. 52

NO. 54

NO. 56

NO. 58

NO. 60

HOLE SAW CHART *

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* NOTE: For all type push button station, use size 1-7/32" knock-out punch.
For connectors, (male connectors and adapters), use size 1-7/32".

MINIMUM COVER REQUIREMENTS 0 - 600 VOLTS, NOMINAL

Cover is defined as the distance between the top surface of direct burial cable, conduit, or other raceways and the finished surface.

| WIRING METHOD | MINIMUM BURIAL (INCHES) |
|--|-------------------------|
| DIRECT BURIAL CABLES | 24 |
| RIGID METAL CONDUIT | 6* |
| INTERMEDIATE METAL CONDUIT | 6* |
| RIGID NONMETALLIC CONDUIT (APPROVED FOR DIRECT BURIAL WITHOUT CONCRETE ENCASEMENT) | 18* |

*For most locations, for complete details, refer to National Electrical Code® Table 300-5 for exceptions such as highways, dwellings, airports, driveways, parking lots, etc. See Ugly's page 127 - 135 for metric conversions.

VOLUME REQUIRED PER CONDUCTOR

| SIZE OF CONDUCTOR | FREE SPACE WITHIN BOX FOR EACH CONDUCTOR |
|-------------------|--|
| No. 18 | 1.5 CUBIC INCHES |
| No. 16 | 1.75 CUBIC INCHES |
| No. 14 | 2 CUBIC INCHES |
| No. 12 | 2.25 CUBIC INCHES |
| No. 10 | 2.5 CUBIC INCHES |
| No. 8 | 3 CUBIC INCHES |
| No. 6 | 5 CUBIC INCHES |

For complete details see NEC 314.16B. See Ugly's page 127 - 135 for metric conversions.

VERTICAL CONDUCTOR SUPPORTS

| AWG or Circular-Mil Size of Wire | Support of Conductors in Vertical Raceways | CONDUCTORS | | |
|----------------------------------|--|----------------------------------|----------|--|
| | | Aluminum or Copper-Clad Aluminum | Copper | |
| 18 AWG through 8 AWG | Not greater than | 100 feet | 100 feet | |
| 6 AWG through 1/0 AWG | Not greater than | 200 feet | 100 feet | |
| 2/0 AWG through 4/0 AWG | Not greater than | 180 feet | 80 feet | |
| Over 4/0 AWG through 350 kcmil | Not greater than | 135 feet | 60 feet | |
| Over 350 kcmil through 500 kcmil | Not greater than | 120 feet | 50 feet | |
| Over 500 kcmil through 750 kcmil | Not greater than | 95 feet | 40 feet | |
| Over 750 kcmil | Not greater than | 85 feet | 35 feet | |

For SI units: one foot = 0.3048 meter. See Ugly's page 127 - 135 for metric conversions.

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MINIMUM DEPTH OF CLEAR WORKING SPACE IN FRONT OF ELECTRICAL EQUIPMENT

| NOMINAL VOLTAGE TO GROUND | CONDITIONS | | |
|--------------------------------------|------------|-------|----|
| | 1 | 2 | 3 |
| Minimum clear distance (feet) | | | |
| 0 - 150 | 3 | 3 | 3 |
| 151 - 600 | 3 | 3 1/2 | 4 |
| 601 - 2500 | 3 | 4 | 5 |
| 2501 - 9000 | 4 | 5 | 6 |
| 9001 - 25,000 | 5 | 6 | 9 |
| 25,001 - 75 KV | 6 | 8 | 10 |
| Above 75 KV | 8 | 10 | 12 |

NOTES:

1. For SI units, 1 ft. = 0.3048 m.
2. Where the conditions are as follows:
 - Condition 1** – Exposed live parts on one side of the working space and no live or grounded parts on the other side of the working space, or exposed live parts on both sides of the working space that are effectively guarded by insulating materials.
 - Condition 2** – Exposed live parts on one side of the working space and grounded parts on the other side of the working space. Concrete, brick, or tile walls shall be considered as grounded.
 - Condition 3** – Exposed live parts on both sides of the work space.

See Ugly's page 127 - 135 for metric conversion.

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MINIMUM CLEARANCE OF LIVE PARTS

| NOMINAL VOLTAGE RATING KV | IMPULSE WITHSTAND B.I.L. KV | | *MINIMUM CLEARANCE OF LIVE PARTS, INCHES | | | |
|---------------------------|-----------------------------|----------|--|----------|-----------------|----------|
| | | | PHASE-TO-PHASE | | PHASE-TO-GROUND | |
| | INDOORS | OUTDOORS | INDOORS | OUTDOORS | INDOORS | OUTDOORS |
| 2.4 - 4.16 | 60 | 95 | 4.5 | 7 | 3.0 | 6 |
| 7.2 | 75 | 95 | 5.5 | 7 | 4.0 | 6 |
| 13.8 | 95 | 110 | 7.5 | 12 | 5.0 | 7 |
| 14.4 | 110 | 110 | 9.0 | 12 | 6.5 | 7 |
| 23 | 125 | 150 | 10.5 | 15 | 7.5 | 10 |
| 34.5 | 150 | 150 | 12.5 | 15 | 9.5 | 10 |
| | 200 | 200 | 18.0 | 18 | 13.0 | 13 |
| 46 | | 200 | | 18 | | 13 |
| | | 250 | | 21 | | 17 |
| 69 | | 250 | | 21 | | 17 |
| | | 350 | | 31 | | 25 |
| 115 | | 550 | | 53 | | 42 |
| 138 | | 550 | | 53 | | 42 |
| | | 650 | | 63 | | 50 |
| 161 | | 650 | | 63 | | 50 |
| | | 750 | | 72 | | 58 |
| 230 | | 750 | | 72 | | 58 |
| | | 900 | | 89 | | 71 |
| | | 1050 | | 105 | | 83 |

For SI units: one inch = 25.4 millimeters

* The values given are the minimum clearance for rigid parts and bare conductors under favorable service conditions. They shall be increased for conductor movement or under unfavorable service conditions, or wherever space limitations permit. The selection of the associated impulse withstand voltage for a particular system voltage is determined by the characteristics of the surge protective equipment.

See Ugly's page 127 - 135 for metric conversion.

MINIMUM SIZE EQUIPMENT GROUNDING CONDUCTORS FOR GROUNDING RACEWAY AND EQUIPMENT

| RATING OR SETTING OF AUTOMATIC OVERCURRENT DEVICE IN CIRCUIT AHEAD OF EQUIPMENT, CONDUIT, ETC., NOT EXCEEDING (AMPERES) | SIZE | |
|---|-----------|-----------------------------------|
| | COPPER | ALUMINUM OR COPPER-CLAD ALUMINUM* |
| 15 | 14 | 12 |
| 20 | 12 | 10 |
| 30 | 10 | 8 |
| 40 | 10 | 8 |
| 60 | 10 | 8 |
| 100 | 8 | 6 |
| 200 | 6 | 4 |
| 300 | 4 | 2 |
| 400 | 3 | 1 |
| 500 | 2 | 1/0 |
| 600 | 1 | 2/0 |
| 800 | 1/0 | 3/0 |
| 1000 | 2/0 | 4/0 |
| 1200 | 3/0 | 250 kcmil |
| 1600 | 4/0 | 350 kcmil |
| 2000 | 250 kcmil | 400 kcmil |
| 2500 | 350 kcmil | 600 kcmil |
| 3000 | 400 kcmil | 600 kcmil |
| 4000 | 500 kcmil | 800 kcmil |
| 5000 | 700 kcmil | 1200 kcmil |
| 6000 | 800 kcmil | 1200 kcmil |

NOTE: Where necessary to comply with Section 250.4(A)(5) or 250.4(B)(4), the equipment grounding conductor shall be sized larger than given in this table.

* See installation restrictions in NEC 250.120.

GROUNDING ELECTRODE CONDUCTOR FOR ALTERNATING-CURRENT SYSTEMS

| SIZE OF LARGEST UNGROUNDED SERVICE-ENTRANCE CONDUCTOR OR EQUIVALENT AREA FOR PARALLEL CONDUCTORS* | | SIZE OF GROUNDING ELECTRODE CONDUCTOR | |
|---|----------------------------------|---------------------------------------|------------------------------------|
| COPPER | ALUMINUM OR COPPER-CLAD ALUMINUM | COPPER | ALUMINUM OR COPPER-CLAD ALUMINUM** |
| 2 OR SMALLER | 1/0 OR SMALLER | 8 | 6 |
| 1 OR 1/0 | 2/0 OR 3/0 | 6 | 4 |
| 2/0 OR 3/0 | 4/0 OR 250 kcmil | 4 | 2 |
| OVER 3/0 THRU 350kcmil | OVER 250 THRU 500 kcmil | 2 | 1/0 |
| OVER 350 kcmil | OVER 500 kcmil | | |
| THRU 600 kcmil | THRU 900 kcmil | 1/0 | 3/0 |
| OVER 600 kcmil | OVER 900 kcmil | | |
| THRU 1100 kcmil | THRU 1750 kcmil | 2/0 | 4/0 |
| OVER 1100 kcmil | OVER 1750 kcmil | 3/0 | 250 kcmil |

NOTES:

- Where multiple sets of service-entrance conductors are used as permitted in Section 230.40, Exception No. 2, the equivalent size of the largest service-entrance conductor shall be determined by the largest sum of the areas of the corresponding conductors of each set.
- Where there are no service-entrance conductors, the grounding electrode conductor size shall be determined by the equivalent size of the largest service-entrance conductor required for the load to be served.

*This table also applies to the derived conductors of separately derived ac systems.

**See installation restrictions in Section 250.64(a).

FPN: See Section 250-24(c) for size of ac system conductor brought to service equipment.

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GENERAL LIGHTING LOADS BY OCCUPANCY

| TYPE OF OCCUPANCY | VOLT-AMPERES PER SQUARE FOOT | TYPE OF OCCUPANCY | VOLT-AMPERES PER SQUARE FOOT |
|---|------------------------------|---|------------------------------|
| Armories & auditoriums | 1 | Lodge rooms | 1½ |
| Banks | 3 1/2 ^b | Office buildings | 3 1/2 ^b |
| Barber shops & beauty parlors | 3 | Restaurants | 2 |
| Churches | 1 | Schools | 3 |
| Clubs | 2 | Stores | 3 |
| Court rooms | 2 | Warehouses (storage) | 1/4 |
| Dwelling units ^a | 3 | In any of the preceding occupancies except one-family dwellings & individual dwelling units of two-family & multi-family dwellings: | |
| Garages - commercial (storage) | 1/2 | Assembly halls & auditoriums | 1 |
| Hospitals | 2 | Halls, corridors, closets, stairways | 1/2 |
| Hotels & motels, including apartment houses without provision for cooking by tenants ^a | 2 | Storage spaces | 1/4 |
| Industrial commercial (loft) buildings | 2 | | |

^a See 220.3(B)(10)

^b In addition, a unit load of 11 volt-amperes/m² or 1 volt-ampere/ft² shall be included for general-purpose receptacle outlets where the actual number of general-purpose receptacle outlets is unknown.

LIGHTING LOAD DEMAND FACTORS

| Type of Occupancy | Portion of Lighting Load to Which Demand Factor Applies (Volt-Amperes) | Demand Factor (Percent) |
|---|---|-------------------------|
| Dwelling units | First 3000 or less at From 3001 to 120,000 at Remainder over 120,000 at | 100 35 25 |
| Hospitals* | First 50,000 or less at Remainder over 50,000 at | 40 20 |
| Hotels and motels, including apartment houses without provision for cooking by tenants* | First 20,000 or less at From 20,001 to 100,000 at Remainder over 100,000 at | 50 40 30 |
| Warehouses (Storage) | First 12,500 or less at Remainder over 12,500 at | 100 50 |
| All others | Total volt-amperes | 100 |

* The demand factors of this table shall not apply to the computed load of feeders or services supplying areas in hospitals, hotels, and motels where the entire lighting is likely to be used at one time, as in operating rooms, ballrooms, or dining rooms.

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DEMAND FACTORS FOR NONDWELLING RECEPTACLE LOADS

| Portion of Receptacle Load to Which Demand Factor Applies (Volt-Amperes) | Demand Factor (Percent) |
|--|-------------------------|
| First 10 kVA or less at | 100 |
| Remainder over 10 kVA at | 50 |

DEMAND FACTORS FOR HOUSEHOLD ELECTRIC CLOTHES DRYERS

| Number of Dryers | Demand Factor (Percent) |
|------------------|--|
| 1 - 4 | 100% |
| 5 | 85% |
| 6 | 75% |
| 7 | 65% |
| 8 | 60% |
| 9 | 55% |
| 10 | 50% |
| 11 | 47% |
| 12 - 22 | % = 47 - (number of dryers - 11) |
| 23 | 35% |
| 24 - 42 | % = 35 - [0.5 x (number of dryers - 23)] |
| 43 and over | 25% |

DEMAND FACTORS FOR KITCHEN EQUIPMENT - OTHER THAN DWELLING UNIT(S)

| Number of Units of Equipment | Demand Factor (Percent) |
|------------------------------|-------------------------|
| 1 | 100 |
| 2 | 100 |
| 3 | 90 |
| 4 | 80 |
| 5 | 70 |
| 6 and over | 65 |

DEMAND LOADS FOR HOUSEHOLD ELECTRIC RANGES, WALL-MOUNTED OVENS, COUNTER-MOUNTED COOKING UNITS, and OTHER HOUSEHOLD COOKING APPLIANCES over 1 3/4 kW RATING

(Column C to be used in all cases except as otherwise permitted in note 3)

| Number of Appliances | Demand Factor (Percent) (See Notes) | | Column C Maximum Demand (kW) (See Notes) (not over 12 kW Rating) |
|----------------------|---|---|--|
| | Column A (less than 3 1/2 kW Rating) | Column B (3 1/2 kW to 8 3/4 kW Rating) | |
| 1 | 80 | 80 | 8 |
| 2 | 75 | 65 | 11 |
| 3 | 70 | 55 | 14 |
| 4 | 66 | 50 | 17 |
| 5 | 62 | 45 | 20 |
| 6 | 59 | 43 | 21 |
| 7 | 56 | 40 | 23 |
| 8 | 53 | 36 | 23 |
| 9 | 51 | 35 | 24 |
| 10 | 49 | 34 | 25 |
| 11 | 47 | 32 | 26 |
| 12 | 45 | 32 | 27 |
| 13 | 43 | 32 | 28 |
| 14 | 41 | 32 | 29 |
| 15 | 40 | 32 | 30 |
| 16 | 39 | 28 | 31 |
| 17 | 38 | 28 | 32 |
| 18 | 37 | 28 | 33 |
| 19 | 36 | 28 | 34 |
| 20 | 35 | 28 | 35 |
| 21 | 34 | 26 | 36 |
| 22 | 33 | 26 | 37 |
| 23 | 32 | 26 | 38 |
| 24 | 31 | 26 | 39 |
| 25 | 30 | 26 | 40 |
| 26 - 30 | 30 | 24 | 15 kW + 1 kW |
| 31 - 40 | 30 | 22 | for each range |
| 41 - 50 | 30 | 20 | 25 kW + 3/4 kW |
| 51 - 60 | 30 | 18 | for each range |
| 61 and over | 30 | 16 | |

See Next page for Notes to this table

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DEMAND LOADS FOR HOUSEHOLD ELECTRIC RANGES, WALL-MOUNTED OVENS, COUNTER-MOUNTED COOKING UNITS, and OTHER HOUSEHOLD COOKING APPLIANCES over 1 3/4 kW RATING

NOTES

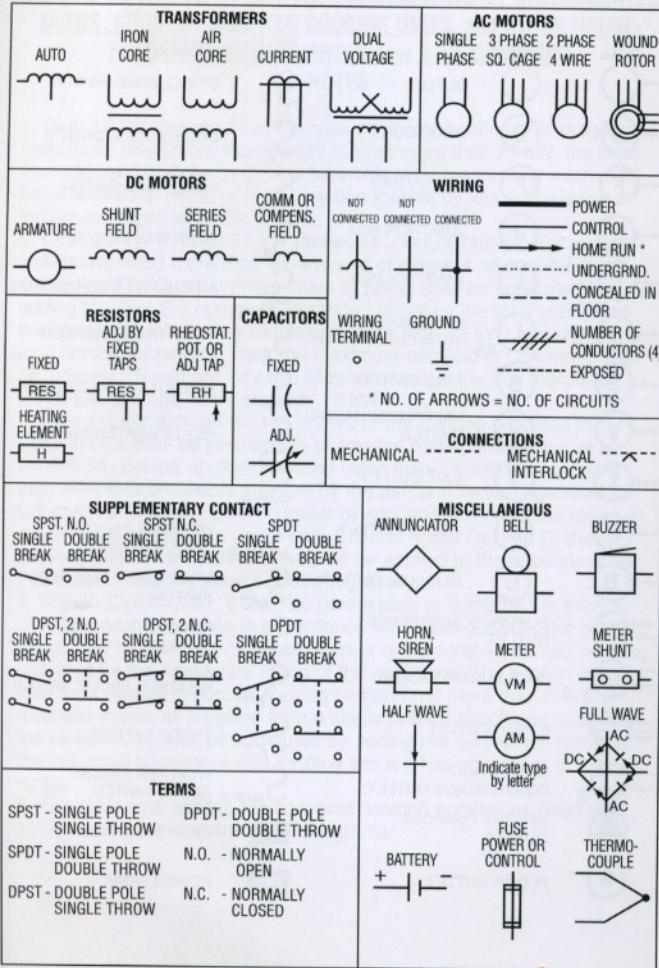
- Over 12 kW through 27 kW ranges all of same rating. For ranges individually rated more than 12 kW but not more than 27 kW, the maximum demand in Column C shall be increased 5 percent for each additional kilowatt of rating or major fraction thereof by which the rating of individual ranges exceeds 12 kW.
- Over 8 3/4 kW through 27 kW ranges of unequal ratings. For ranges individually rated more than 8 3/4 kW and of different ratings, but none exceeding 27 kW, an average value of rating shall be computed by adding together the ratings of all ranges to obtain the total connected load (using 12 kW for any range rated less than 12 kW) and dividing the total number of ranges. Then the maximum demand in Column C shall be increased 5 percent for each kilowatt or major fraction thereof by which this average value exceeds 12 kW.
- Over 1 3/4 kW through 8 3/4 kW. In lieu of the method provided in Column C, it shall be permissible to add the nameplate ratings of all household cooking appliances rated more than 1 3/4 kW but not more than 8 3/4 kW and multiply the sum by the demand factors specified in Column A or B for the given number of appliances. Where the rating of cooking appliances falls under both Column A and Column B, the demand factors for each column shall be applied to the appliances for that column, and the results added together.
- Branch-Circuit Load. It shall be permissible to compute the branch-circuit load for one range in accordance with Table 220.19. The branch-circuit load for one wall-mounted oven or one counter-mounted cooking unit shall be the nameplate rating of the appliance. The branch-circuit load for a counter-mounted cooking unit and not more than two wall-mounted ovens, all supplied from a single branch circuit and located in the same room, shall be computed by adding the nameplate rating of the individual appliances and treating this total as equivalent to one range.
- This table also applies to household cooking appliances rated over 1 3/4 kW and used in instructional programs.

ELECTRICAL SYMBOLS

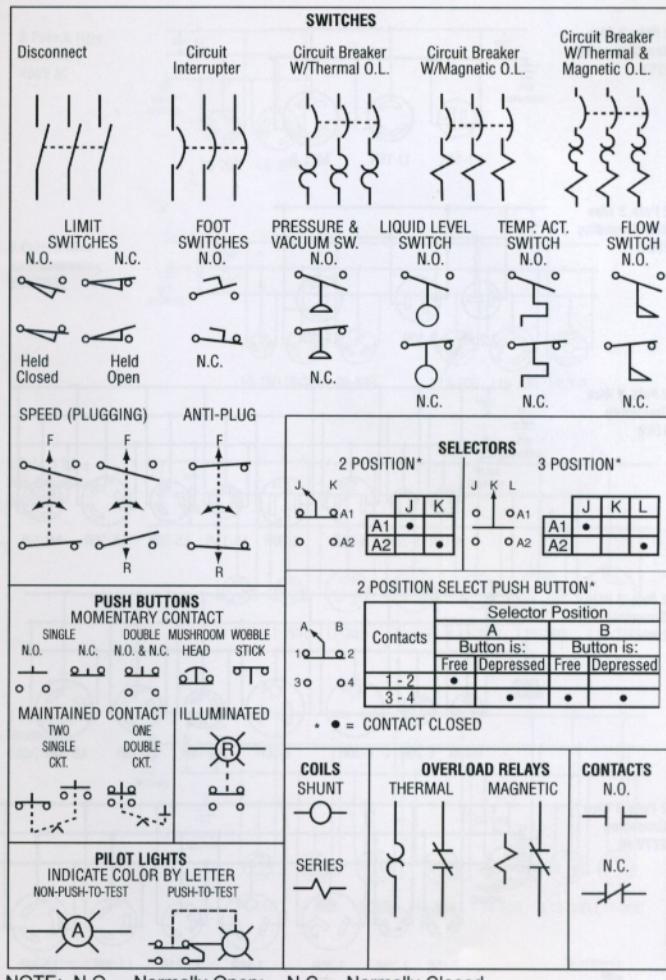
| <u>WALL</u> | <u>CEILING</u> | <u>SWITCH OUTLETS</u> | |
|--------------------|--------------------|-------------------------------|--|
| —○— | ○— | OUTLET | S SINGLE POLE SWITCH |
| —D— | ○D○ | DROP CORD | S ₂ DOUBLE POLE SWITCH |
| —F— | ○F○ | FAN OUTLET | S ₃ THREE WAY SWITCH |
| —J— | ○J○ | JUNCTION BOX | S ₄ FOUR WAY SWITCH |
| —L— | ○L○ | LAMP HOLDER | S _D AUTOMATIC DOOR SWITCH |
| —L _{PS} — | ○L _{PS} ○ | LAMP HOLDER WITH PULL SWITCH | S _E ELECTROLIER SWITCH |
| —S— | ○S○ | PULL SWITCH | S _P SWITCH AND PILOT LAMP |
| —V— | ○V○ | VAPOR DISCHARGE SWITCH | S _K KEY OPERATED SWITCH |
| —X— | ○X○ | EXIT OUTLET | S _{CB} CIRCUIT BREAKER |
| —C— | ○C○ | CLOCK OUTLET | S _{WCB} WEATHER PROOF CIRCUIT BREAKER |
| —B— | ○B○ | BLANKED OUTLET | S _{MC} MOMENTARY CONTACT SWITCH |
| —○— | —○— | DUPLEX CONVENIENCE OUTLET | S _{RC} REMOTE CONTROL SWITCH |
| —○— _{1.3} | —○— | SINGLE, TRIPLEX, ETC. | S _{WP} WEATHER PROOF SWITCH |
| —○— | —○— | RANGE OUTLET | S _F FUSED SWITCH |
| —○— _s | —○— | SWITCH AND CONVENIENCE OUTLET | S _{WPF} WEATHER PROOF FUSED SWITCH |
| —○— | △—○— | SPECIAL PURPOSE OUTLET | —■— LIGHTING PANEL |
| —○— | ●—○— | FLOOR OUTLET | —▨— POWER PANEL |

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ELECTRICAL SYMBOLS

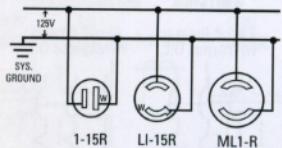


ELECTRICAL SYMBOLS

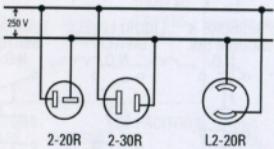


WIRING DIAGRAMS FOR NEMA CONFIGURATIONS

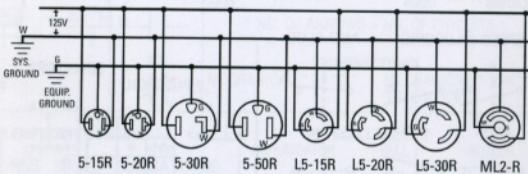
2 Pole, 2 Wire
Non-Grounding
125V



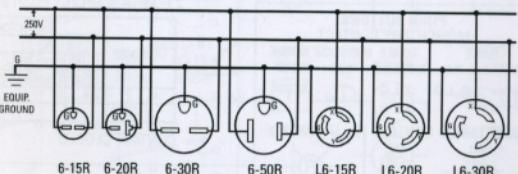
2 Pole, 2 Wire
Non-Grounding
250V



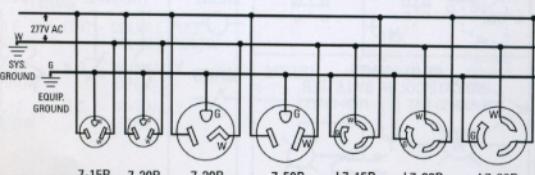
2 Pole, 3 Wire
Grounding
125V



2 Pole, 3 Wire
Grounding
250V



2 Pole, 3 Wire
Grounding
277V AC

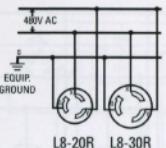


Courtesy of

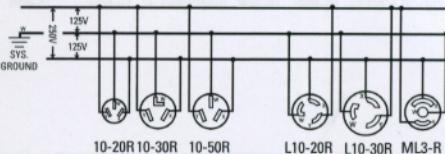
COOPER Wiring Devices
The New Power in Wiring Devices

WIRING DIAGRAMS FOR NEMA CONFIGURATIONS

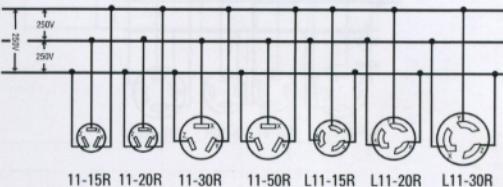
2 Pole, 3 Wire
Grounding
480V AC



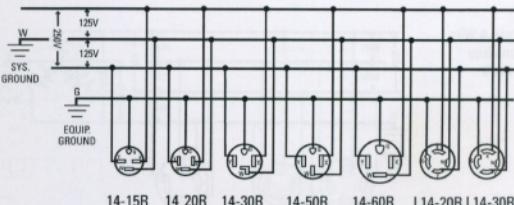
3 Pole, 3 Wire
Non-Grounding
125/250V



3 Pole, 3 Wire
Non-Grounding
3 ϕ 250V

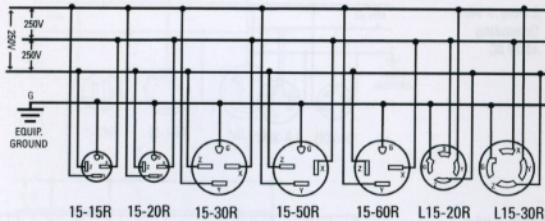


3 Pole, 4 Wire
Grounding
125/250V

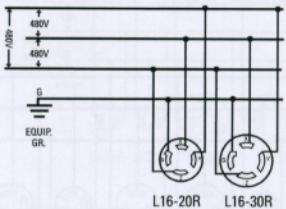


WIRING DIAGRAMS FOR NEMA CONFIGURATIONS

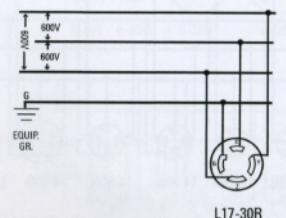
3 Pole, 4 Wire
Grounding
3 ϕ 250V



3 Pole, 4 Wire
Grounding
3 ϕ 480V



3 Pole, 4 Wire
Grounding
3 ϕ 600V

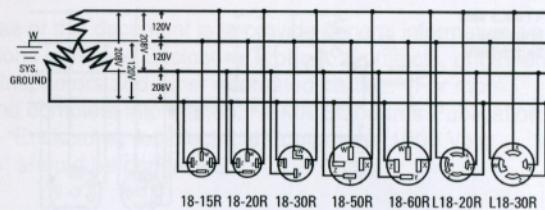


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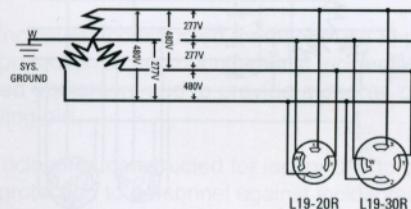
COOPER Wiring Devices
The New Power in Wiring Devices

WIRING DIAGRAMS FOR NEMA CONFIGURATIONS

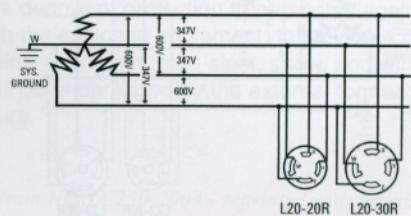
4 Pole, 4 Wire
Non-Grounding
3 ϕ 120/208V



4 Pole, 4 Wire
Non-Grounding
3 ϕ 277/480V



4 Pole, 4 Wire
Non-Grounding
3 ϕ 347/600V

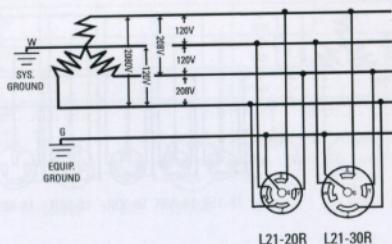


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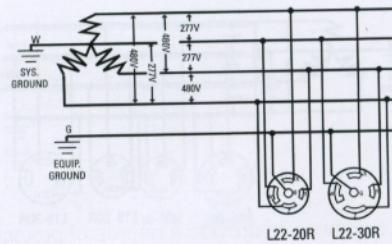
COOPER Wiring Devices
The New Power in Wiring Devices

WIRING DIAGRAMS FOR NEMA CONFIGURATIONS

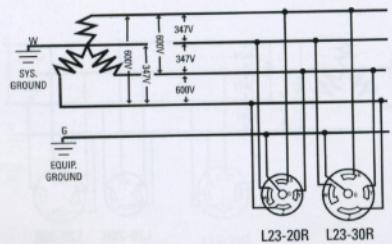
4 Pole, 5 Wire
Grounding
3 ϕ 120/208V



4 Pole, 5 Wire
Grounding
3 ϕ 277/480V



4 Pole, 5 Wire
Grounding
3 ϕ 347/600V



NEMA ENCLOSURE TYPES NON-HAZARDOUS LOCATIONS

The purpose of this document is to provide general information on the definitions of NEMA Enclosure Types to architects, engineers, installers, inspectors and other interested parties. [For more detailed and complete information, NEMA Standards Publication 250-2003, "Enclosures for Electrical Equipment (1000 Volts Maximum)" should be consulted.

In **Non-Hazardous Locations**, the specific enclosure Types, their applications, and the environmental conditions they are designed to protect against, when completely and properly installed, are as follows:

Type 1 - Enclosures constructed for indoor use to provide a degree of protection to personnel against incidental contact with the enclosed equipment and to provide a degree of protection against falling dirt.

Type 2 - Enclosures constructed for indoor use to provide a degree of protection to personnel against incidental contact with the enclosed equipment, to provide a degree of protection against falling dirt, and to provide a degree of protection against dripping and light splashing of liquids.

Type 3 - Enclosures constructed for either indoor or outdoor use to provide a degree of protection to personnel against incidental contact with the enclosed equipment; to provide a degree of protection against falling dirt, rain, sleet, snow, and windblown dust; and that will be undamaged by the external formation of ice on the enclosure.

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NEMA ENCLOSURE TYPES (cont'd)

NON-HAZARDOUS LOCATIONS

Type 3R - Enclosures constructed for either indoor or outdoor use to provide a degree of protection to personnel against incidental contact with the enclosed equipment; to provide a degree of protection against falling dirt, rain, sleet, and snow; and that will be undamaged by the external formation of ice on the enclosure.

Type 3S - Enclosures constructed for either indoor or outdoor use to provide a degree of protection to personnel against incidental contact with the enclosed equipment; to provide a degree of protection against falling dirt, rain, sleet, snow, and windblown dust; and in which the external mechanism(s) remain operable when ice laden.

Type 4 - Enclosures constructed for either indoor or outdoor use to provide a degree of protection to personnel against incidental contact with the enclosed equipment; to provide a degree of protection against falling dirt, rain, sleet, snow, windblown dust, splashing water, and hose-directed water; and that will be undamaged by the external formation of ice on the enclosure.

Type 4X - Enclosures constructed for either indoor or outdoor use to provide a degree of protection to personnel against incidental contact with the enclosed equipment; to provide a degree of protection against falling dirt, rain, sleet, snow, windblown dust, splashing water, hose-directed water, and corrosion; and that will be undamaged by the external formation of ice on the enclosure.

Type 5 - Enclosures constructed for indoor use to provide a degree of protection to personnel against incidental contact with the enclosed equipment; to provide a degree of protection against falling dirt; against settling airborne dust, lint, fibers, and flyings; and to provide a degree of protection against dripping and light splashing of liquids.

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NEMA ENCLOSURE TYPES (cont'd)

NON-HAZARDOUS LOCATIONS

Type 6 - Enclosures constructed for either indoor or outdoor use to provide a degree of protection to personnel against incidental contact with the enclosed equipment; to provide a degree of protection against falling dirt; against hose-directed water and the entry of water during occasional temporary submersion at a limited depth; and that will be undamaged by the external formation of ice on the enclosure.

Type 6P - Enclosures constructed for either indoor or outdoor use to provide a degree of protection to personnel against incidental contact with the enclosed equipment; to provide a degree of protection against falling dirt; against hose-directed water and the entry of water during prolonged submersion at a limited depth; and that will be undamaged by the external formation of ice on the enclosure.

Type 12 - Enclosures constructed (without knockouts) for indoor use to provide a degree of protection to personnel against incidental contact with the enclosed equipment; to provide a degree of protection against falling dirt; against circulating dust, lint, fibers, and flyings; and against dripping and light splashing of liquids.

Type 12K - Enclosures constructed (with knockouts) for indoor use to provide a degree of protection to personnel against incidental contact with the enclosed equipment; to provide a degree of protection against falling dirt; against circulating dust, lint, fibers, and flyings; and against dripping and light splashing of liquids.

Type 13 - Enclosures constructed for indoor use to provide a degree of protection to personnel against incidental contact with the enclosed equipment; to provide a degree of protection against falling dirt; against circulating dust, lint, fibers, and flyings; and against the spraying, splashing, and seepage of water, oil, and noncorrosive coolants.

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NEMA ENCLOSURE TYPES (cont'd)
HAZARDOUS LOCATIONS

In Hazardous Locations, when completely and properly installed and maintained, Type 7 and Type 10 enclosures are designed to contain an internal explosion without causing an external hazard. Type 8 enclosures are designed to prevent combustion through the use of oil-immersed equipment. Type 9 enclosures are designed to prevent the ignition of combustible dust.

Type 7 - Enclosures constructed for indoor use in hazardous locations classified as Class I, Division 1, Groups A, B, C or D as defined in NFPA 70.

Type 8 - Enclosures constructed for either indoor or outdoor use in hazardous locations classified as Class I, Division 1, Groups A, B, C or D as defined in NFPA 70.

Type 9 - Enclosures constructed for indoor use in hazardous conditions classified as Class II, Division 1, Groups E, F or G as defined in NFPA 70.

Type 10 - Enclosures constructed to meet the requirements of the Mine Safety and Health Administration, 30 CFR, Part 18.

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U.S. WEIGHTS AND MEASURES

LINEAR MEASURE

| | | | | | | | |
|-----|----------|---|---|---------|---|-------|-------------|
| 12 | INCHES | = | 1 | INCH | = | 2.540 | CENTIMETERS |
| 3 | FEET | = | 1 | YARD | = | 3.048 | DECIMETERS |
| 5.5 | YARDS | = | 1 | ROD | = | 9.144 | DECIMETERS |
| 40 | RODS | = | 1 | FURLONG | = | 5.029 | METERS |
| 8 | FURLONGS | = | 1 | MILE | = | 2.018 | HECTOMETERS |
| | | | | | | 1.609 | KILOMETERS |

MILE MEASUREMENTS

| | | | | |
|---|---------------|---|--------|------|
| 1 | STATUTE MILE | = | 5,280 | FEET |
| 1 | SCOTS MILE | = | 5,952 | FEET |
| 1 | IRISH MILE | = | 6,720 | FEET |
| 1 | RUSSIAN VERST | = | 3,504 | FEET |
| 1 | ITALIAN MILE | = | 4,401 | FEET |
| 1 | SPANISH MILE | = | 15,084 | FEET |

OTHER LINEAR MEASUREMENTS

| | | | | | | | | | | |
|---|-------|---|----|--------|---|---|---------|---|------|--------|
| 1 | HAND | = | 4 | INCHES | = | 1 | LINK | = | 7.92 | INCHES |
| 1 | SPAN | = | 9 | INCHES | = | 1 | FATHOM | = | 6 | FEET |
| 1 | CHAIN | = | 22 | YARDS | = | 1 | FURLONG | = | 10 | CHAINS |
| | | | | | | | CABLE | = | 608 | FEET |

SQUARE MEASURE

| | | | | |
|------------------|---------------|---|---|-------------|
| 144 | SQUARE INCHES | = | 1 | SQUARE FOOT |
| 9 | SQUARE FEET | = | 1 | SQUARE YARD |
| 30 $\frac{1}{4}$ | SQUARE YARDS | = | 1 | SQUARE ROD |
| 40 | RODS | = | 1 | ROOD |
| 4 | ROODS | = | 1 | ACRE |
| 640 | ACRES | = | 1 | SQUARE MILE |
| 1 | SQUARE MILE | = | 1 | SECTION |
| 36 | SECTIONS | = | 1 | TOWNSHIP |

CUBIC OR SOLID MEASURE

| | | | | |
|---|-------------------|---|-------------------|---------------------|
| 1 | CU. FOOT | = | 1728 | CU. INCHES |
| 1 | CU. YARD | = | 27 | CU. FEET |
| 1 | CU. FOOT | = | 7.48 | GALLONS |
| 1 | GALLON (WATER) | = | 8.34 | LBS. |
| 1 | GALLON (U.S.) | = | 231 | CU. INCHES OF WATER |
| 1 | GALLON (IMPERIAL) | = | 277 $\frac{1}{4}$ | CU. INCHES OF WATER |

U.S. WEIGHTS AND MEASURES

LIQUID MEASUREMENTS

| | | |
|----------|---|-------------------------------------|
| 1 PINT | = | 4 GILLS |
| 1 QUART | = | 2 PINTS |
| 1 GALLON | = | 4 QUARTS |
| 1 FIRKIN | = | 9 GALLONS (ALE OR BEER) |
| 1 BARREL | = | 42 GALLONS (PETROLEUM OR CRUDE OIL) |

DRY MEASURE

| | | |
|----------|---|----------|
| 1 QUART | = | 2 PINTS |
| 1 PECK | = | 8 QUARTS |
| 1 BUSHEL | = | 4 PECKS |

WEIGHT MEASUREMENT (MASS)

A. AVOIRDUPOIS WEIGHT:

| | | |
|-----------------|---|--------------|
| 1 OUNCE | = | 16 DRAMS |
| 1 POUND | = | 16 OUNCES |
| 1 HUNDREDWEIGHT | = | 100 POUNDS |
| 1 TON | = | 2,000 POUNDS |

B. TROY WEIGHT:

| | | |
|---------------------------|---|------------------------|
| 1 CARAT | = | 3.17 GRAINS |
| 1 PENNYWEIGHT | = | 20 GRAINS |
| 1 OUNCE | = | 20 PENNYWEIGHTS |
| 1 POUND | = | 12 OUNCES |
| 1 LONG HUNDRED- WEIGHT | = | 112 POUNDS |
| 1 LONG TON | = | 20 LONG HUNDREDWEIGHTS |
| | = | 2240 POUNDS |

C. APOTHECARIES WEIGHT:

| | | | | |
|-----------|---|------------|---|----------------|
| 1 SCRUPLE | = | 20 GRAINS | = | 1.296 GRAMS |
| 1 DRAM | = | 3 SCRUPLES | = | 3.888 GRAMS |
| 1 OUNCE | = | 8 DRAMS | = | 31.1035 GRAMS |
| 1 POUND | = | 12 OUNCES | = | 373.2420 GRAMS |

D. KITCHEN WEIGHTS AND MEASURES:

| | | |
|----------------|---|------------------------------|
| 1 U.S. PINT | = | 16 FL. OUNCES |
| 1 STANDARD CUP | = | 8 FL. OUNCES |
| 1 TABLESPOON | = | 0.5 FL. OUNCES (15 CU. CMS.) |
| 1 TEASPOON | = | 0.16 FL. OUNCES (5 CU. CMS.) |

METRIC SYSTEM

PREFIXES:

| | | | | | |
|----------|---|-----------|----------|---|----------|
| A. MEGA | = | 1,000,000 | E. DECI | = | 0.1 |
| B. KILO | = | 1,000 | F. CENTI | = | 0.01 |
| C. HECTO | = | 100 | G. MILLI | = | 0.001 |
| D. DEKA | = | 10 | H. MICRO | = | 0.000001 |

LINEAR MEASURE:

(THE UNIT IS THE METER = 39.37 INCHES)

| | | | | |
|--------------|---|----------------|---|----------------|
| 1 CENTIMETER | = | 10 MILLIMETERS | = | 0.3937011 IN. |
| 1 DECIMETER | = | 10 CENTIMETERS | = | 3.9370113 INS. |
| 1 METER | = | 10 DECIMETERS | = | 1.0936143 YDS. |
| | | | = | 3.2808429 FT. |
| 1 DEKAMETER | = | 10 METERS | = | 10.936143 YDS. |
| 1 HECTOMETER | = | 10 DEKAMETERS | = | 109.36143 YDS. |
| 1 KILOMETER | = | 10 HECTOMETERS | = | 0.62137 MILE |
| 1 MYRIAMETER | = | 10,000 METERS | | |

SQUARE MEASURE:

(THE UNIT IS THE SQUARE METER = 1549.9969 SQ. INCHES)

| | | | | |
|------------------|---|---------------------|---|-----------------|
| 1 SQ. CENTIMETER | = | 100 SQ. MILLIMETERS | = | 0.1550 SQ. IN. |
| 1 SQ. DECIMETER | = | 100 SQ. CENTIMETERS | = | 15.550 SQ. INS. |
| 1 SQ. METER | = | 100 SQ. DECIMETERS | = | 10.7639 SQ. FT. |
| 1 SQ. DEKAMETER | = | 100 SQ. METERS | = | 119.60 SQ. YDS. |
| 1 SQ. HECTOMETER | = | 100 SQ. DEKAMETERS | | |
| 1 SQ. KILOMETER | = | 100 SQ. HECTOMETERS | | |

(THE UNIT IS THE "ARE" = 100 SQ. METERS)

| | | | | |
|-----------------|---|--------------|---|-------------------|
| 1 CENTIARE | = | 10 MILLIARES | = | 10.7643 SQ. FT. |
| 1 DECIARE | = | 10 CENTIARES | = | 11.96033 SQ. YDS. |
| 1 ARE | = | 10 DECIARES | = | 119.6033 SQ. YDS. |
| 1 DEKARE | = | 10 ARE | = | 0.247110 ACRES |
| 1 HEKTARE | = | 10 DEKARES | = | 2.471098 ACRES |
| 1 SQ. KILOMETER | = | 100 HEKTARES | = | 0.38611 SQ. MILE |

CUBIC MEASURE:

(THE UNIT IS THE "STERE" = 61,025.38659 CU. INS.)

| | | | | |
|-------------|---|----------------|---|-------------------|
| 1 DECISTERE | = | 10 CENTISTERES | = | 3.531562 CU. FT. |
| 1 STERE | = | 10 DECISTERES | = | 1.307986 CU. YDS. |
| 1 DEKASTERE | = | 10 STERES | = | 13.07986 CU. YDS. |

METRIC SYSTEM

CUBIC MEASURE:

(THE UNIT IS THE METER = 39.37 INCHES)

| | | |
|------------------------------|------------------------|--------------------|
| 1 CU. CENTIMETER | = 1000 CU. MILLIMETERS | = 0.06102 CU. IN. |
| 1 CU. DECIMETER | = 1000 CU. CENTIMETERS | = 61.02374 CU. IN. |
| 1 CU. METER | = 1000 CU. DECIMETERS | = 35.31467 CU. FT. |
| | = 1 STERE | = 1.30795 CU. YDS. |
| 1 CU. CENTIMETER (WATER) | | = 1 GRAM |
| 1000 CU. CENTIMETERS (WATER) | = 1 LITER | = 1 KILOGRAM |
| 1 CU. METER (1000 LITERS) | | = 1 METRIC TON |

MEASURES OF WEIGHT:

(THE UNIT IS THE GRAM = 0.035274 OUNCES)

| | | |
|--------------|---------------------|---------------------|
| 1 MILLIGRAM | = | = 0.015432 GRAINS |
| 1 CENTIGRAM | = 10 MILLIGRAMS | = 0.15432 GRAINS |
| 1 DECIGRAM | = 10 CENTIGRAMS | = 1.5432 GRAINS |
| 1 GRAM | = 10 DECIGRAMS | = 15.4323 GRAINS |
| 1 DEKAGRAM | = 10 GRAMS | = 5.6438 DRAMS |
| 1 HECTOGRAM | = 10 DEKAGRAMS | = 3.5274 OUNCES |
| 1 KILOGRAM | = 10 HECTOGRAMS | = 2.2046223 POUNDS |
| 1 MYRIAGRAM | = 10 KILOGRAMS | = 22.046223 POUNDS |
| 1 QUINTAL | = 10 MYRIAGRAMS | = 1.986412 CWT. |
| 1 METRIC TON | = 10 QUINTAL | = 2,2045.622 POUNDS |
| 1 GRAM | = 0.56438 DRAMS | |
| 1 DRAM | = 1.77186 GRAMS | |
| | = 27.3438 GRAINS | |
| 1 METRIC TON | = 2,204.6223 POUNDS | |

MEASURES OF CAPACITY:

(THE UNIT IS THE LITER = 1.0567 LIQUID QUARTS)

| | | |
|--------------|------------------|----------------------|
| 1 CENTILITER | = 10 MILLILITERS | = 0.338 FLUID OUNCES |
| 1 DECILITER | = 10 CENTILITERS | = 3.38 FLUID OUNCES |
| 1 LITER | = 10 DECILITERS | = 33.8 FLUID OUNCES |
| 1 DEKALITER | = 10 LITERS | = 0.284 BUSHEL |
| 1 HECTOLITER | = 10 DEKALITERS | = 2.84 BUSHELS |
| 1 KILOLITER | = 10 HECTOLITERS | = 264.2 GALLONS |

NOTE: $\frac{\text{KILOMETERS}}{8} \times 5 = \text{MILES}$ or $\frac{\text{MILES}}{5} \times 8 = \text{KILOMETERS}$

METRIC DESIGNATOR AND TRADE SIZES

| METRIC DESIGNATOR | | | | | | | | | | | | |
|-------------------|---------------|---------------|----|----------------|----------------|----|----------------|----|----------------|-----|-----|-----|
| 12 | 16 | 21 | 27 | 35 | 41 | 53 | 63 | 78 | 91 | 103 | 129 | 155 |
| $\frac{3}{8}$ | $\frac{1}{2}$ | $\frac{3}{4}$ | 1 | $1\frac{1}{4}$ | $1\frac{1}{2}$ | 2 | $2\frac{1}{2}$ | 3 | $3\frac{1}{2}$ | 4 | 5 | 6 |
| TRADE SIZE | | | | | | | | | | | | |

U.S. WEIGHTS & MEASURES / METRIC EQUIVALENT CHART

| | In. | Ft. | Yd. | Mile | Mm | Cm | M | Km |
|----------|--------|----------|-------------------------|-------------------------|-----------|-----------|-----------|------------------------|
| 1 Inch = | 1 | .0833 | .0278 | 1.578×10^{-5} | 25.4 | 2.54 | .0254 | 2.54×10^{-5} |
| 1 Foot = | 12 | 1 | .333 | 1.894×10^{-4} | 304.8 | 30.48 | .3048 | 3.048×10^{-4} |
| 1 Yard = | 36 | 3 | 1 | 5.6818×10^{-4} | 914.4 | 91.44 | .9144 | 9.144×10^{-4} |
| 1 Mile = | 63,360 | 5,280 | 1,760 | 1 | 1,609,344 | 160,934.4 | 1,609,344 | 1.609344 |
| 1 mm = | .03937 | .0032808 | 1.0936×10^{-3} | 6.2137×10^{-7} | 1 | 0.1 | .0001 | 0.000001 |
| 1 cm = | .3937 | .0328084 | .0109361 | 6.2137×10^{-6} | 10 | 1 | .001 | 0.00001 |
| 1 m = | 39.37 | 3.28084 | 1.09361 | 6.2137×10^{-4} | 1000 | 100 | 1 | .001 |
| 1 km = | 39,370 | 3,280.84 | 1,093.61 | 0.62137 | 1,000,000 | 100,000 | 1,000 | 1 |

In. = Inches Ft. = Foot Yd. = Yard Mi. = Mile Mm = Millimeter Cm = Centimeter M = Meter Km = Kilometer

EXPLANATION OF SCIENTIFIC NOTATION:

Scientific Notation is simply a way of expressing very large or very small numbers in a more compact format. Any number can be expressed as a number between 1 & 10, multiplied by a power of 10 (which indicates the correct position of the decimal point in the original number). Numbers greater than 10 have positive powers of 10, and numbers less than 1 have negative powers of 10.

Example: $186,000 = 1.86 \times 10^5$ $0.000524 = 5.24 \times 10^{-4}$

USEFUL CONVERSIONS / EQUIVALENTS

| | | |
|----------------|-------|----------------------------|
| 1 BTU | | Raises 1 LB. of water 1°F |
| 1 GRAM CALORIE | | Raises 1 Gram of water 1°C |
| 1 CIRCULAR MIL | | Equals 0.7854 sq. mil |
| 1 SQ. MIL | | Equals 1.27 cir. mils |
| 1 MIL | | Equals 0.001 in. |

To determine circular mil of a conductor:

ROUND CONDUCTOR CM = (Diameter in mils)²

BUS BAR CM = Width (mils) x Thickness (mils)
0.7854

NOTES: 1 Millimeter = 39.37 Mils 1 Cir. Millimeter = 1550 Cir. Mils
1 Sq. Millimeter = 1974 Cir. Mils

DECIMAL EQUIVALENTS

| FRACTION | | | | DECIMAL |
|----------|-------|------|-----|---------|
| 1/64 | | | | .0156 |
| 2/64 | 1/32 | | | .0313 |
| 3/64 | | | | .0469 |
| 4/64 | 2/32 | 1/16 | | .0625 |
| 5/64 | | | | .0781 |
| 6/64 | 3/32 | | | .0938 |
| 7/64 | | | | .1094 |
| 8/64 | 4/32 | 2/16 | 1/8 | .125 |
| 9/64 | | | | .1406 |
| 10/64 | 5/32 | | | .1563 |
| 11/64 | | | | .1719 |
| 12/64 | 6/32 | 3/16 | | .1875 |
| 13/64 | | | | .2031 |
| 14/64 | 7/32 | | | .2188 |
| 15/64 | | | | .2344 |
| 16/64 | 8/32 | 4/16 | 2/8 | 1/4 |
| 17/64 | | | | .25 |
| 18/64 | 9/32 | | | .2656 |
| 19/64 | | | | .2813 |
| 20/64 | 10/32 | 5/16 | | .2969 |
| 21/64 | | | | .3125 |
| 22/64 | 11/32 | | | .3281 |
| 23/64 | | | | .3438 |
| 24/64 | 12/32 | 6/16 | 3/8 | .3594 |
| 25/64 | | | | .375 |
| 26/64 | 13/32 | | | .3906 |
| 27/64 | | | | .4063 |
| 28/64 | 14/32 | 7/16 | | .4219 |
| 29/64 | | | | .4375 |
| 30/64 | 15/32 | | | .4531 |
| 31/64 | | | | .4688 |
| 32/64 | 16/32 | 8/16 | 4/8 | 2/4 |
| | | | | .5 |

Decimals are rounded to the nearest 10,000th.

TWO-WAY CONVERSION TABLE

To convert from the unit of measure in Column B to the unit of measure in Column C, multiply the number of units in Column B by the multiplier in Column A. To convert from Column C to B, use the multiplier in Column D.

EXAMPLE: To convert 1000 BTU's to CALORIES, find the "BTU - CALORIE" combination in Columns B and C. "BTU" is in Column B and "CALORIE" is in Column C; so we are converting from B to C. Therefore, we use Column A multiplier. $1000 \text{ BTU's} \times 251.996 = 251,996 \text{ Calories}$. To convert 251,996 Calories to BTU's, use the same "BTU - CALORIE" combination. But this time you are converting from C to B. Therefore, use Column D multiplier. $251,996 \text{ Calories} \times .0039683 = 1,000 \text{ BTU's}$.

$$A \times B = C$$

&

$$D \times C = B$$

To convert from B to C,
Multiply B x A:

To convert from C to B,
Multiply C x D:

| A | B | C | D |
|--------------------------|--------------------|--------------------------|--------------------------|
| 43,560 | Acre | Sq. Foot | 2.2956×10^{-5} |
| 1.5625×10^{-3} | Acre | Sq. Mile | 640 |
| 6.4516 | Ampere per sq. cm. | Ampere per sq. in. | .155003 |
| 1.256637 | Ampere (turn) | Gilberts | 0.79578 |
| 33.89854 | Atmosphere | Foot of H ₂ O | 0.029499 |
| 29.92125 | Atmosphere | Inch of Hg | 0.033421 |
| 14.69595 | Atmosphere | Pound force/sq. in. | 0.06804 |
| 251.996 | BTU | Calorie | 3.96832×10^{-3} |
| 778.169 | BTU | Foot-pound force | 1.28507×10^{-3} |
| 3.93015×10^{-4} | BTU | Horsepower-hour | 2544.43 |
| 1055.056 | BTU | Joule | 9.47817×10^{-4} |
| 2.9307×10^{-4} | BTU | Kilowatt-hour | 3412.14 |
| 3.93015×10^{-4} | BTU/hour | Horsepower | 2544.43 |
| 2.93071×10^{-4} | BTU/hour | Kilowatt | 3412.1412 |
| 0.293071 | BTU/hour | Watt | 3.41214 |
| 4.19993 | BTU/minute | Calorie/second | 0.23809 |
| 0.0235809 | BTU/minute | Horsepower | 42.4072 |
| 17.5843 | BTU/minute | Watt | 0.0568 |

TWO-WAY CONVERSION TABLE (continued)

To convert from B to C,
Multiply B x A:

To convert from C to B,
Multiply C x D:

| A | B | C | D |
|--------------------------|--------------------------|------------------|------------------------|
| 4.1868 | Calorie | Joule | .238846 |
| 0.0328084 | Centimeter | Foot | 30.48 |
| 0.3937 | Centimeter | Inch | 2.54 |
| 0.00001 | Centimeter | Kilometer | 100,000 |
| 0.01 | Centimeter | Meter | 100 |
| 6.2137×10^{-6} | Centimeter | Mile | 160,934.4 |
| 10 | Centimeter | Millimeter | 0.1 |
| 0.010936 | Centimeter | Yard | 91.44 |
| 7.85398×10^{-7} | Circular mil | Sq. Inch | 1.273239×10^6 |
| 0.000507 | Circular mil | Sq. Millimeter | 1973.525 |
| 0.06102374 | Cubic Centimeter | Cubic Inch | 16.387065 |
| 0.028317 | Cubic Foot | Cubic Meter | 35.31467 |
| 1.0197×10^{-3} | Dyne | Gram Force | 980.665 |
| 1×10^{-5} | Dyne | Newton | 100,000 |
| 1 | Dyne centimeter | Erg | 1 |
| 7.376×10^{-8} | Erg | Foot pound force | 1.355818×10^7 |
| 2.777×10^{-14} | Erg | Kilowatt-hour | 3.6×10^{13} |
| 1.0×10^{-7} | Erg/second | Watt | 1.0×10^7 |
| 12 | Foot | Inch | 0.0833 |
| 3.048×10^{-4} | Foot | Kilometer | 3,280.84 |
| 0.3048 | Foot | Meter | 3,280.84 |
| 1.894×10^{-4} | Foot | Mile | 5,280 |
| 304.8 | Foot | Millimeter | 0.00328 |
| 0.333 | Foot | Yard | 3 |
| 10.7639 | Foot candle | Lux | 0.0929 |
| 0.882671 | Foot of H ₂ O | Inch of Hg | 1.13292 |
| 5.0505×10^{-7} | Foot pound force | Horsepower-hour | 1.98×10^6 |
| 1.35582 | Foot pound force | Joule | 0.737562 |
| 3.76616×10^{-7} | Foot pound force | Kilowatt-hour | 2.655223×10^6 |
| 3.76616×10^{-4} | Foot pound force | Watt-hour | 2655.22 |
| 3.76616×10^{-7} | Foot pnd force/hour | Kilowatt | 2.6552×10^6 |
| 3.0303×10^{-5} | Foot pnd force/minute | Horsepower | 33,000 |

TWO-WAY CONVERSION TABLE (continued)

To convert from B to C,
Multiply B x A:

To convert from C to B,
Multiply C x D:

| A | B | C | D |
|---------------------------|--------------------------|---------------|-------------------------|
| 2.2597×10^{-5} | Foot pnd force/minute | Kilowatt | 44,253.7 |
| 0.022597 | Foot pnd force/minute | Watt | 44.2537 |
| 1.81818×10^{-3} | Foot pnd force/second | Horsepower | 550 |
| 1.355818×10^{-3} | Foot pnd force/second | Kilowatt | 737.562 |
| 0.7457 | Horsepower | Kilowatt | 1.34102 |
| 745.7 | Horsepower | Watt | 0.00134 |
| .0022046 | Gram | Pound mass | 453.592 |
| 2.54×10^{-5} | Inch | Kilometer | 39,370 |
| 0.0254 | Inch | Meter | 39.37 |
| 1.578×10^{-5} | Inch | Mile | 63,360 |
| 25.4 | Inch | Millimeter | 0.03937 |
| 0.0278 | Inch | Yard | 36 |
| 0.07355 | Inch of H ₂ O | Inch of Hg | 13.5951 |
| 2.7777×10^{-7} | Joule | Kilowatt-hour | 3.6×10^6 |
| 2.7777×10^{-4} | Joule | Watt hour | 3600 |
| 1 | Joule | Watt second | 1 |
| 1,000 | Kilometer | Meter | 0.001 |
| 0.62137 | Kilometer | Mile | 1.609344 |
| 1,000,000 | Kilometer | Millimeter | 0.000001 |
| 1,093.61 | Kilometer | Yard | 9.144×10^{-4} |
| 0.000621 | Meter | Mile | 1,609.344 |
| 1,000 | Meter | Millimeter | 0.001 |
| 1,0936 | Meter | Yard | 0.9144 |
| 1,609,344 | Mile | Millimeter | 6.2137×10^{-7} |
| 1,760 | Mile | Yard | 5.681×10^{-4} |
| 1.0936×10^{-3} | Millimeter | Yard | 914.4 |
| 0.224809 | Newton | Pound force | 4.44822 |
| 0.03108 | Pound | Slug | 32.174 |
| 0.0005 | Pound | Ton (short) | 2,000 |
| 0.155 | Sq. Centimeter | Sq. Inch | 6.4516 |
| 0.092903 | Sq. Foot | Sq. Meter | 10.76391 |
| 0.386102 | Sq. Kilometer | Sq. Mile | 2.589988 |

METALS

| METAL | SYMB | SPEC. GRAV. | MELT POINT | | ELEC. COND. % COPPER | LBS. CU. " |
|------------------|------|-------------|------------|-------|-------------------------|---------------|
| | | | C° | F° | | |
| ALUMINUM | AL | 2.71 | 660 | 1220 | 64.9 | .0978 |
| ANTIMONY | SB | 6.62 | 630 | 1167 | 4.42 | .2390 |
| ARSENIC | AS | 5.73 | - | - | 4.9 | .2070 |
| BERYLLIUM | BE | 1.83 | 1280 | 2336 | 9.32 | .0660 |
| BISMUTH | BI | 9.80 | 271 | 520 | 1.50 | .3540 |
| BRASS (70-30) | | 8.51 | 900 | 1652 | 28.0 | .3070 |
| BRONZE (5% SN) | | 8.87 | 1000 | 1382 | 18.0 | .3200 |
| CADMIUM | CD | 8.65 | 321 | 610 | 22.7 | .3120 |
| CALCIUM | CA | 1.55 | 850 | 1562 | 50.1 | .0560 |
| COBALT | CO | 8.90 | 1495 | 2723 | 17.8 | .3210 |
| COPPER | CU | 8.89 | 1083 | 1981 | 100.0 | .3210 |
| ROLLED TUBING | | 8.95 | - | - | 100.0 | .3230 |
| GOLD | AU | 19.30 | 1063 | 1945 | 71.2 | .6970 |
| GRAPHITE | | 2.25 | 3500 | 6332 | 10^{-3} | .0812 |
| INDIUM | IN | 7.30 | 156 | 311 | 20.6 | .2640 |
| IRIDIUM | IR | 22.40 | 2450 | 4442 | 32.5 | .8090 |
| IRON | FE | 7.20 | TO | TO | 17.6 | .2600 |
| | | | 1400 | 2552 | | |
| | | | 1500 | 2732 | | |
| MALLEABLE | | 7.20 | TO | TO | 10 | .2600 |
| | | | 1600 | 2912 | | |
| | | | 1500 | 2732 | | |
| WROUGHT | | 7.70 | TO | TO | 10 | .2780 |
| | | | 1600 | 2912 | | |
| LEAD | PB | 11.40 | 327 | 621 | 8.35 | .4120 |
| MAGNESIUM | MG | 1.74 | 651 | 1204 | 38.7 | .0628 |
| MANGANESE | MN | 7.20 | 1245 | 2273 | 0.9 | .2600 |
| MERCURY | HG | 13.65 | -38.9 | -37.7 | 1.80 | .4930 |
| MOLYBDENUM | MO | 10.20 | 2620 | 4748 | 36.1 | .3680 |
| MONEL (63 - 37) | | 8.87 | 1300 | 2372 | 3.0 | .3200 |
| NICKEL | NI | 8.90 | 1452 | 2646 | 25.0 | .3210 |
| PHOSPHOROUS | P | 1.82 | 44.1 | 111.4 | 10^{17} | .0657 |
| PLATINUM | PT | 21.46 | 1773 | 3221 | 17.5 | .7750 |
| POTASSIUM | K | 0.860 | 62.3 | 144.1 | 28 | .0310 |
| SELENIUM | SE | 4.81 | 220 | 428 | 14.4 | .1740 |
| SILICON | SI | 2.40 | 1420 | 2588 | 10^{-5} | .0866 |
| SILVER | AG | 10.50 | 960 | 1760 | 106 | .3790 |
| STEEL (CARBON) | | 7.84 | TO | TO | 10 | .2830 |
| | | | 1380 | 2516 | | |
| STAINLESS (18-8) | | 7.92 | 1500 | 2732 | 2.5 | .2860 |
| (13-CR) | | 7.78 | 1520 | 2768 | 3.5 | .2810 |

METALS

| METAL | SYMB | SPEC. GRAV. | MELT POINT | | ELEC. COND. % COPPER | LBS. CU. " |
|-----------|------|-------------|------------|------|-------------------------|---------------|
| | | | C | F | | |
| TANTALUM | TA | 16.60 | 2900 | 5414 | 13.9 | .599 |
| TELLURIUM | TE | 6.20 | 450 | 846 | 10^{-5} | .224 |
| THORIUM | TH | 11.70 | 1845 | 3353 | 9.10 | .422 |
| TIN | SN | 7.30 | 232 | 449 | 15.00 | .264 |
| TITANIUM | TI | 4.50 | 1800 | 3272 | 2.10 | .162 |
| TUNGSTEN | W | 19.30 | 3410 | | 31.50 | .697 |
| URANIUM | U | 18.70 | 1130 | 2066 | 2.80 | .675 |
| VANADIUM | V | 5.96 | 1710 | 3110 | 6.63 | .215 |
| ZINC | ZN | 7.14 | 419 | 786 | 29.10 | .258 |
| ZIRCONIUM | ZR | 6.40 | 1700 | 3092 | 4.20 | .231 |

SPECIFIC RESISTANCE (K)

THE SPECIFIC RESISTANCE (K) OF A MATERIAL IS THE RESISTANCE OFFERED BY A WIRE OF THIS MATERIAL WHICH IS ONE FOOT LONG WITH A DIAMETER OF 1 MIL.

| MATERIAL | "K" | MATERIAL | "K" |
|-------------------|------|----------|------|
| BRASS | 43.0 | ALUMINUM | 17.0 |
| CONSTANTAN | 295 | MONEL | 253 |
| COPPER | 10.8 | NICHROME | 600 |
| GERMAN SILVER 18% | 200 | NICKEL | 947 |
| GOLD | 14.7 | TANTALUM | 93.3 |
| IRON (PURE) | 60.0 | TIN | 69.0 |
| MAGNESIUM | 276 | TUNGSTEN | 34.0 |
| MANGANIN | 265 | SILVER | 9.7 |

NOTE: 1. The resistance of a wire is directly proportional to the specific resistance of the material.
 2. "K" = Specific Resistance
 3. Resistance varies with temperature. See NEC, Chapter 9, Table 8, NOTES

USEFUL MATH FORMULAS

CENTIGRADE AND FAHRENHEIT THERMOMETER SCALES

| DEG-C | DEG-F | DEG-C | DEG-F | DEG-C | DEG-F | DEG-C | DEG-F |
|-------|-------|-------|-------|-------|-------|-------|-------|
| 0 | 32 | 26 | 78.8 | 51 | 123.8 | 76 | 168.8 |
| 1 | 33.8 | 27 | 80.6 | 52 | 125.6 | 77 | 170.6 |
| 2 | 35.6 | 28 | 82.4 | 53 | 127.4 | 78 | 172.4 |
| 3 | 37.4 | 29 | 84.2 | 54 | 129.2 | 79 | 174.2 |
| 4 | 39.2 | 30 | 86 | 55 | 131 | 80 | 176 |
| 5 | 41 | 31 | 87.8 | 56 | 132.8 | 81 | 177.8 |
| 6 | 42.8 | 32 | 89.6 | 57 | 134.6 | 82 | 179.6 |
| 7 | 44.6 | 33 | 91.4 | 58 | 136.4 | 83 | 181.4 |
| 8 | 46.4 | 34 | 93.2 | 59 | 138.2 | 84 | 183.2 |
| 9 | 48.2 | 35 | 95 | 60 | 140 | 85 | 185 |
| 10 | 50 | 36 | 96.8 | 61 | 141.8 | 86 | 186.8 |
| 11 | 51.8 | 37 | 98.6 | 62 | 143.6 | 87 | 188.6 |
| 12 | 53.6 | 38 | 100.4 | 63 | 145.4 | 88 | 190.4 |
| 13 | 55.4 | 39 | 102.2 | 64 | 147.2 | 89 | 192.2 |
| 14 | 57.2 | 40 | 104 | 65 | 149 | 90 | 194 |
| 15 | 59 | 41 | 105.8 | 66 | 150.8 | 91 | 195.8 |
| 16 | 60.8 | 42 | 107.6 | 67 | 152.6 | 92 | 197.6 |
| 17 | 62.6 | 43 | 109.4 | 68 | 154.4 | 93 | 199.4 |
| 18 | 64.4 | 44 | 111.2 | 69 | 156.2 | 94 | 201.2 |
| 19 | 66.2 | 45 | 113 | 70 | 158 | 95 | 203 |
| 20 | 68 | 46 | 114.8 | 71 | 159.8 | 96 | 204.8 |
| 21 | 69.8 | 47 | 116.6 | 72 | 161.6 | 97 | 206.6 |
| 22 | 71.6 | 48 | 118.4 | 73 | 163.4 | 98 | 208.4 |
| 23 | 73.4 | 49 | 120.2 | 74 | 165.2 | 99 | 210.2 |
| 24 | 75.2 | 50 | 122 | 75 | 167 | 100 | 212 |
| 25 | 77 | | | | | | |

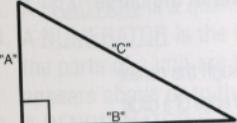
1. TEMP. C° = $\frac{5}{9} \times (\text{TEMP. F}^{\circ} - 32)$

2. TEMP F° = $(\frac{9}{5} \times \text{TEMP. C}^{\circ}) + 32$

3. Ambient temperature is the temperature of the surrounding cooling medium.

4. Rated temperature rise is the permissible rise in temperature above ambient when operating under load.

RIGHT TRIANGLE



$$A = \sqrt{C^2 - B^2}$$

$$B = \sqrt{C^2 - A^2}$$

$$C = \sqrt{A^2 + B^2}$$

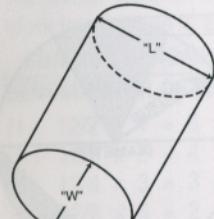
$$\text{AREA} = .5 \times A \times B$$



SPHERE

$$\text{AREA} = D^2 \times 3.1416$$

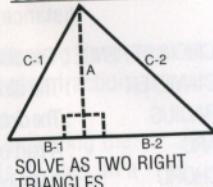
$$\text{VOLUME} = D^3 \times 0.5236$$



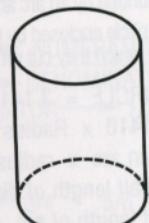
ELLIPTICAL

SOLVE THE SAME AS CYLINDRICAL

OBIQUE TRIANGLE

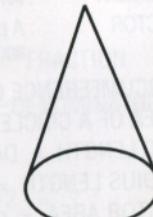


SOLVE AS TWO RIGHT TRIANGLES



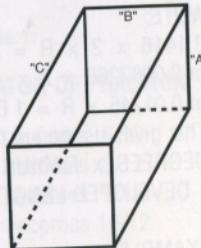
CYLINDRICAL

$$\text{VOLUME} = \text{AREA OF END} \times \text{HEIGHT}$$



CONE

$$\text{VOLUME} = \text{AREA OF END} \times \text{HEIGHT} \div 3$$



$$\text{VOLUME} = A \times B \times C$$

$$\text{AREA} = 2(AB + AC + BC)$$

See next page for CIRCLE

THE CIRCLE

DEFINITION: A closed plane curve having every point an equal distance from a fixed point within the curve.

- CIRCUMFERENCE : The distance around a circle
 DIAMETER : The distance across a circle through the center
 RADIUS : The distance from the center to the edge of a circle
 ARC : A part of the circumference
 CHORD : A straight line connecting the ends of an arc.
 SEGMENT : An area bounded by an arc and a chord
 SECTOR : A part of a circle enclosed by two radii and the arc which they cut off

CIRCUMFERENCE OF A CIRCLE = $3.1416 \times 2 \times \text{Radius}$
 AREA OF A CIRCLE = $3.1416 \times \text{Radius}^2$

ARC LENGTH = Degrees in arc \times radius \times 0.01745

RADIUS LENGTH = one half length of diameter

SECTOR AREA = one half length of arc \times radius

CHORD LENGTH = $2\sqrt{A \times B}$

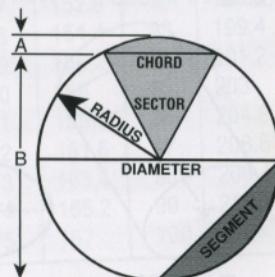
SEGMENT AREA = Sector area minus triangle area

NOTE:

$3.1416 \times 2 \times R = 360$ Degrees,
 or $0.0087266 \times 2 \times R = 1$ Degree,
 or $0.01745 \times R = 1$ Degree

This gives us the arc formula.

DEGREES \times RADIUS \times 0.01745 =
 DEVELOPED LENGTH



EXAMPLE:

For a ninety degree conduit bend,
 having a radius of 17.25":

$$90 \times 17.25" \times 0.01745 = \text{Developed Length}$$

$$27.09" = \text{Developed Length}$$

FRACTIONS

DEFINITIONS:

- A. A **FRACTION** is a quantity less than a unit.
 B. A **NUMERATOR** is the term of a fraction indicating how many of the parts of a unit are to be taken. In a common fraction, it appears above or to the left of the line.
 C. A **DENOMINATOR** is the term of a fraction indicating the number of equal parts into which the unit is divided. In a common fraction, it appears below or to the right of the line.
 D. EXAMPLES:

- (1.) $\frac{1}{2}$ → **NUMERATOR**
 → **DENOMINATOR** = FRACTION
 (2.) **NUMERATOR** → $1/2$ ← **DENOMINATOR**

TO ADD OR SUBTRACT:

TO SOLVE: $\frac{1}{2} - \frac{2}{3} + \frac{3}{4} - \frac{5}{6} + \frac{7}{12} = ?$

A. Determine the lowest common denominator that each of the denominators 2, 3, 4, 6, and 12 will divide into an even number of times.

The lowest common denominator is 12.

B. Work one fraction at a time using the formula:

COMMON DENOMINATOR \times **NUMERATOR OF FRACTION**
DENOMINATOR OF FRACTION \times **NUMERATOR OF FRACTION**

- | | |
|--|---------------------|
| (1.) $12/2 \times 1 = 6 \times 1 = 6$ | 1/2 becomes $6/12$ |
| (2.) $12/3 \times 2 = 4 \times 2 = 8$ | 2/3 becomes $8/12$ |
| (3.) $12/4 \times 3 = 3 \times 3 = 9$ | 3/4 becomes $9/12$ |
| (4.) $12/6 \times 5 = 2 \times 5 = 10$ | 5/6 becomes $10/12$ |
| (5.) $7/12$ remains $7/12$ | |

(continued next page)

FRACTIONS

TO ADD OR SUBTRACT (CONTINUED):

- C. We can now convert the problem from its original form to its new form using 12 as the common denominator.

$$\frac{1}{2} - \frac{2}{3} + \frac{3}{4} - \frac{5}{6} + \frac{7}{12} = \text{Original form}$$

$$\begin{array}{r} 6 - 8 + 9 - 10 + 7 \\ \hline 12 \end{array} = \text{Present form}$$

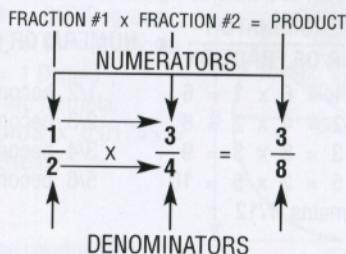
$$\frac{4}{12} = \frac{1}{3} \text{ Reduced to lowest form}$$

- D. To convert fractions to decimal form, simply divide the numerator of the fraction by the denominator of the fraction.

EXAMPLE: $\frac{1}{3} = 1 \text{ DIVIDED BY } 3 = 0.333$

TO MULTIPLY:

- A. The numerator of fraction #1 times the numerator of fraction #2 is equal to the numerator of the product.
- B. The denominator of fraction #1 times the denominator of fraction #2 is equal to the denominator of the product.
- C. EXAMPLE:



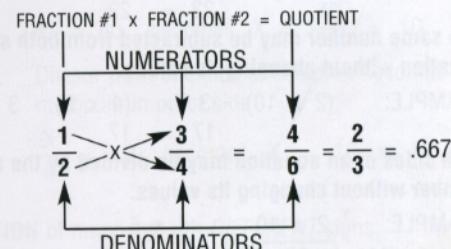
NOTE: To change 3/8 to decimal form, divide 3 by 8 = .375

FRACTIONS

TO DIVIDE:

- A. The numerator of fraction #1 times the denominator of fraction #2 is equal to the numerator of the quotient.
- B. The denominator of fraction #1 times the numerator of fraction #2 is equal to the denominator of the quotient.

- C. EXAMPLE: $\frac{1}{2} \div \frac{3}{4}$



- D. Alternate method for dividing by a fraction is to multiply by the reciprocal of the divisor. (the second fraction in a division problem).

- E. EXAMPLE: $\frac{1}{2} \div \frac{3}{4}$

The reciprocal of $\frac{3}{4}$ is $\frac{4}{3}$

$$\text{so, } \frac{1}{2} \div \frac{3}{4} = \frac{1}{2} \times \frac{4}{3} = \frac{4}{6} = \frac{2}{3} = 0.667$$

EQUATIONS

The word "EQUATION" means equal or the same as.

A. EXAMPLE:
$$\begin{array}{rcl} 2 \times 10 & = & 4 \times 5 \\ & & 20 = 20 \end{array}$$

RULES:

A. The same number may be added to both sides of an equation without changing its values.

EXAMPLE:
$$\begin{array}{rcl} (2 \times 10) + 3 & = & (4 \times 5) + 3 \\ & & 23 = 23 \end{array}$$

B. The same number may be subtracted from both sides of an equation without changing its values.

EXAMPLE:
$$\begin{array}{rcl} (2 \times 10) - 3 & = & (4 \times 5) - 3 \\ & & 17 = 17 \end{array}$$

C. Both sides of an equation may be divided by the same number without changing its values.

EXAMPLE:
$$\begin{array}{rcl} \frac{2 \times 10}{20} & = & \frac{4 \times 5}{20} \\ & & 1 = 1 \end{array}$$

D. Both sides of an equation may be multiplied by the same number without changing its values.

EXAMPLE:
$$\begin{array}{rcl} 3 \times (2 \times 10) & = & 3 \times (4 \times 5) \\ & & 60 = 60 \end{array}$$

E. TRANSPOSITION:

The process of moving a quantity from one side of an equation to the other side of an equation by changing its sign of operation.

1. A term may be transposed if its sign is changed from plus (+) to minus (-), or from minus (-) to plus (+).

EXAMPLE:
$$\begin{array}{rcl} X + 5 & = & 25 \\ X + 5 - 5 & = & 25 - 5 \\ X & = & 20 \end{array}$$

EQUATIONS

E. TRANSPOSITION (continued):

2. A multiplier may be removed from one side of an equation by making it a divisor in the other side; or a divisor may be removed from one side of an equation by making it a multiplier in the other side.

EXAMPLE: Multiplier from one side of equation (4) becomes divisor in other side.

$$4X = 40 \text{ becomes } X = \frac{40}{4} = 10$$

EXAMPLE: Divisor from one side of equation becomes multiplier in other side.

$$\frac{X}{4} = 10 \text{ becomes } X = 10 \times 4$$

SIGNS:

A. ADDITION of numbers with *DIFFERENT* signs:

1. RULE: Use the sign of the larger and subtract.

EXAMPLE:
$$\begin{array}{r} +3 \\ + -2 \\ \hline +1 \end{array} \quad \begin{array}{r} -2 \\ + +3 \\ \hline +1 \end{array}$$

B. ADDITION of numbers with the *SAME* signs:

2. RULE: Use the common sign and add.

EXAMPLE:
$$\begin{array}{r} +3 \\ + +2 \\ \hline +5 \end{array} \quad \begin{array}{r} -3 \\ + -2 \\ \hline -5 \end{array}$$

C. SUBTRACTION of numbers with *DIFFERENT* signs:

3. RULE: Change the sign of the subtrahend (the second number in a subtraction problem) and proceed as in addition.

EXAMPLE:
$$\begin{array}{r} +3 \\ - -2 \\ \hline +5 \end{array} = \begin{array}{r} +3 \\ + +2 \\ \hline +5 \end{array} \quad \begin{array}{r} -2 \\ - +3 \\ \hline -5 \end{array} = \begin{array}{r} -2 \\ + -3 \\ \hline -5 \end{array}$$

EQUATIONS

SIGNS (continued):

D. SUBTRACTION of numbers with the *SAME* signs:

4. RULE: Change the sign of the subtrahend (the second number in a subtraction problem) and proceed as in addition.

$$\begin{array}{cccc} \text{EXAMPLE: } & +3 & +3 & -3 \\ & -+2 & + -2 & - -2 \\ \hline & = +1 & = +2 & = -1 \end{array}$$

E. MULTIPLICATION:

5. RULE: The product of any two numbers having **LIKE** signs is **POSITIVE**. The product of any two numbers having **UNLIKE** signs is **NEGATIVE**.

$$\begin{array}{l} \text{EXAMPLE: } (+3) \times (-2) = -6 \\ \quad (-3) \times (+2) = -6 \\ \quad (+3) \times (+2) = +6 \\ \quad (-3) \times (-2) = +6 \end{array}$$

F. DIVISION:

6. RULE: If the divisor and the dividend have **LIKE** signs, the sign of the quotient is **POSITIVE**. If the divisor and dividend have **UNLIKE** signs, the sign of the quotient is **NEGATIVE**.

EXAMPLE:

$$\begin{array}{rcl} \frac{+6}{-2} & = -3 & \frac{+6}{+2} = +3 \\ \\ \frac{-6}{+2} & = -3 & \frac{-6}{-2} = +3 \end{array}$$

NATURAL TRIGONOMETRIC FUNCTIONS

| ANGLE | SINE | COSINE | TANGENT | COTANGENT | SECANT | COSECANT | |
|-------|--------|--------|----------|-----------|----------|----------|-------|
| 0 | .0000 | 1.0000 | .0000 | 57.2900 | 1.0002 | 57.2987 | 90 |
| 1 | .0175 | .9998 | .0175 | 28.6363 | 1.0006 | 28.6537 | 88 |
| 2 | .0349 | .9994 | .0349 | 19.0811 | 1.0014 | 19.1073 | 87 |
| 3 | .0523 | .9986 | .0524 | 14.3007 | 1.0024 | 14.3356 | 86 |
| 4 | .0698 | .9976 | .0699 | 11.4301 | 1.0038 | 11.4737 | 85 |
| 5 | .0872 | .9962 | .0875 | 8.9568 | 1.0055 | 9.5668 | 84 |
| 6 | .1045 | .9945 | .1051 | 6.3925 | 1.0075 | 8.2055 | 83 |
| 7 | .1219 | .9925 | .1228 | 4.1336 | 1.0125 | 7.1853 | 82 |
| 8 | .1392 | .9903 | .1405 | 2.9238 | 1.0154 | 6.3925 | 81 |
| 9 | .1564 | .9877 | .1584 | 2.7475 | 1.0187 | 5.7588 | 80 |
| 10 | .1736 | .9848 | .1763 | 2.4586 | 1.0223 | 5.2408 | 79 |
| 11 | .1908 | .9816 | .1944 | 2.0642 | 1.0263 | 4.4454 | 77 |
| 12 | .2079 | .9781 | .2126 | 1.7018 | 1.0306 | 4.1336 | 76 |
| 13 | .2250 | .9744 | .2309 | 1.3559 | 1.0353 | 3.8637 | 75 |
| 14 | .2419 | .9703 | .2493 | 1.0642 | 1.0403 | 3.6280 | 74 |
| 15 | .2588 | .9659 | .2679 | 0.9098 | 1.0457 | 3.4203 | 73 |
| 16 | .2756 | .9613 | .2867 | 0.7114 | 1.0515 | 3.2361 | 72 |
| 17 | .2924 | .9563 | .3057 | 0.5593 | 1.0576 | 3.0716 | 71 |
| 18 | .3090 | .9511 | .3249 | 0.4454 | 1.0642 | 2.9238 | 70 |
| 19 | .3256 | .9455 | .3443 | 0.3559 | 1.0711 | 2.7904 | 69 |
| 20 | .3420 | .9397 | .3640 | 0.2745 | 1.0785 | 2.6695 | 68 |
| 21 | .3584 | .9336 | .3839 | 0.2064 | 1.0864 | 2.5593 | 67 |
| 22 | .3746 | .9272 | .4040 | 0.1523 | 1.0946 | 2.4586 | 66 |
| 23 | .3907 | .9205 | .4245 | 0.1126 | 1.1034 | 2.3662 | 65 |
| 24 | .4067 | .9135 | .4452 | 0.0827 | 1.1126 | 2.2812 | 64 |
| 25 | .4226 | .9063 | .4663 | 0.0595 | 1.1223 | 2.2027 | 63 |
| 26 | .4384 | .8988 | .4877 | 0.0360 | 1.1326 | 2.1301 | 62 |
| 27 | .4540 | .8910 | .5095 | 0.0162 | 1.1434 | 2.0627 | 61 |
| 28 | .4695 | .8829 | .5317 | 0.0059 | 1.1547 | 2.0000 | 60 |
| 29 | .4848 | .8746 | .5543 | 0.0000 | 1.1666 | 1.9416 | 59 |
| 30 | .5000 | .8660 | .5774 | 0.0000 | 1.1792 | 1.8871 | 58 |
| 31 | .5150 | .8572 | .6009 | 0.0000 | 1.1924 | 1.8361 | 57 |
| 32 | .5299 | .8480 | .6249 | 0.0000 | 1.2208 | 1.7883 | 56 |
| 33 | .5446 | .8387 | .6494 | 0.0000 | 1.2482 | 1.7434 | 55 |
| 34 | .5592 | .8290 | .6745 | 0.0000 | 1.2765 | 1.7013 | 54 |
| 35 | .5736 | .8192 | .7002 | 0.0000 | 1.3027 | 1.6616 | 53 |
| 36 | .5878 | .8090 | .7265 | 0.0000 | 1.3270 | 1.6243 | 52 |
| 37 | .6018 | .7986 | .7536 | 0.0000 | 1.3547 | 1.5890 | 51 |
| 38 | .6157 | .7880 | .7813 | 0.0000 | 1.3866 | 1.4945 | 48 |
| 39 | .6293 | .7771 | .8098 | 0.0000 | 1.4185 | 1.4463 | 47 |
| 40 | .6428 | .7660 | .8391 | 0.0000 | 1.4504 | 1.3902 | 46 |
| 41 | .6561 | .7547 | .8693 | 0.0000 | 1.4822 | 1.3456 | 45 |
| 42 | .6691 | .7431 | .9004 | 0.0000 | 1.5142 | 1.2957 | 44 |
| 43 | .6820 | .7314 | .9325 | 0.0000 | 1.5462 | 1.2473 | 43 |
| 44 | .6947 | .7193 | .9657 | 0.0000 | 1.5780 | 1.1996 | 42 |
| 45 | .7071 | .7071 | 1.0000 | 0.0000 | 1.6108 | 1.1517 | 41 |
| | COSINE | SINE | COTANGT. | TANGENT | COSECANT | SECANT | ANGLE |

Note: For Angles 0 - 45, use Top Row & Left Column.

For Angles 45 - 90, use Bottom Row & Right Column

TRIGONOMETRY

TRIGONOMETRY is the mathematics dealing with the relations of sides and angles of triangles.

A **TRIANGLE** is a figure enclosed by three straight sides. The sum of the three angles is 180 degrees. All triangles have six parts: three angles and three sides opposite the angles.

RIGHT TRIANGLES are triangles that have one angle of 90 degrees and two angles of less than 90 degrees.

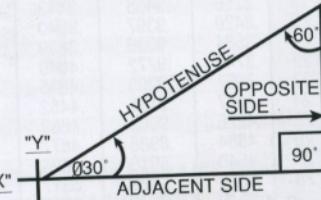
To help you remember the six trigonometric functions, memorize:

"OH HELL ANOTHER HOUR OF ANDY"

$$\text{SINE } \theta = \frac{\text{(OH) OPPOSITE SIDE}}{\text{HYPOTENUSE (HELL)}}$$

$$\text{COSINE } \theta = \frac{\text{(ANOTHER) ADJACENT SIDE}}{\text{HYPOTENUSE (HOUR)}}$$

$$\text{TANGENT } \theta = \frac{\text{(OF) OPPOSITE SIDE}}{\text{ADJACENT SIDE (ANDY)}}$$



Now, use backwards: "ANDY OF HOUR ANOTHER HELL OH"

$$\text{COTANGENT } \theta = \frac{\text{(ANDY) ADJACENT SIDE}}{\text{OPPOSITE SIDE (OF)}}$$

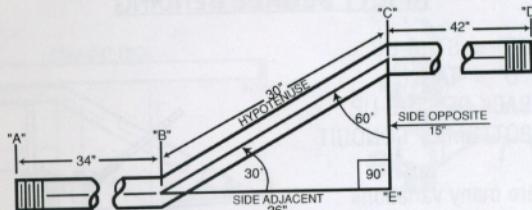
Always place the angle to be solved at the vertex (where "X" and "Y" cross)

$$\text{SECANT } \theta = \frac{\text{(HOUR) HYPOTENUSE}}{\text{ADJACENT SIDE (ANOTHER)}}$$

$$\text{COSECANT } \theta = \frac{\text{(HELL) HYPOTENUSE}}{\text{OPPOSITE SIDE (OH)}}$$

Note:
 θ = Theta = Any Angle

BENDING OFF-SETS WITH TRIGONOMETRY



THE COSECANT OF THE ANGLE TIMES THE OFF-SET DESIRED IS EQUAL TO THE DISTANCE BETWEEN THE CENTERS OF THE BENDS.

EXAMPLE:

To make a fifteen inch (15") off-set, using thirty (30) degree bends:

1. Use Trig. Table (page 147) to find the Cosecant of a thirty (30) degree angle. We find it to be two (2).
2. Multiply two (2) times the off-set desired, which is fifteen (15) inches to determine the distance between bend "B" and bend "C". The answer is thirty (30) inches.

To mark the conduit for bending:

1. Measure from end of Conduit "A" thirty-four (34) inches to center of first bend "B", and mark.
 2. Measure from mark "B" thirty (30) inches to center of second bend "C" and mark.
 3. Measure from mark "C" forty-two (42) inches to "D", and mark.
- Cut, ream, and thread conduit before bending.

ROLLING OFF-SETS:

To determine how much off-set is needed to make a rolling off-set:

1. Measure vertical required. Use work table (any square will do) and measure from corner this amount and mark.
2. Measure horizontal required. Measure ninety degrees from the vertical line measurement (starting in same corner) and mark.
3. The diagonal distance between these marks will be the amount of off-set required.

Note: Shrink is hypotenuse minus the side adjacent.

CHICAGO-TYPE BENDERS NINETY DEGREE BENDING

"A" to "C" = STUB-UP

"C" to "D" = TAIL

"C" = BACK OF STUB-UP

"C" = BOTTOM OF CONDUIT

Note:

There are many variations of this type bender, but most manufacturers offer two sizes.

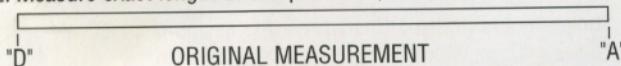
The *small* size shoe takes 1 $\frac{1}{2}$, 3/4" and 1" conduit.

The *large* size shoe takes 1 $\frac{1}{4}$ and 1 $\frac{1}{2}$ " conduit.

TO DETERMINE THE "TAKE-UP" AND "SHRINK" OF EACH SIZE CONDUIT FOR A PARTICULAR BENDER TO MAKE NINETY DEGREE BENDS:

1. Use a straight piece of scrap conduit.

2. Measure exact length of scrap conduit, "A" to "D".



3. Place conduit in bender. Mark at edge of shoe, "B".

4. Level conduit. Bend ninety, and count number of pumps. Be sure to keep notes on each size conduit used.

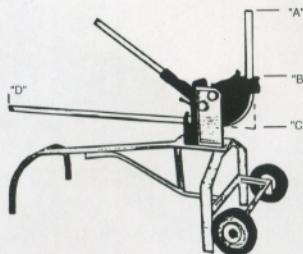
5. After bending ninety:

A. Distance between "B" and "C" is the TAKE-UP.

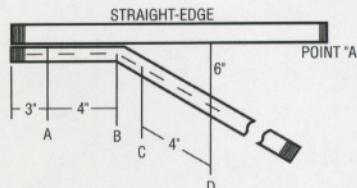
B. Original measurement of the scrap piece of conduit subtracted from (distance "A" to "C" plus distance "C" to "D") is the SHRINK.

Note: Both time and energy will be saved if conduit can be cut, reamed and threaded before bending.

The same method can be used on hydraulic benders.



CHICAGO-TYPE BENDERS OFF-SETS



CHICAGO TYPE BENDER

EXAMPLE: To bend a 6" off-set:

1. Make a mark 3" from conduit end. Place conduit in bender with mark at outside edge of jaw.
2. Make three full pumps, making sure handle goes all the way down to the stop.
3. Remove conduit from bender and place alongside straight-edge.
4. Measure 6" from straight-edge to center of conduit. Mark point "D". Use square for accuracy.
5. Mark center of conduit from both directions through bend as shown by broken line. Where lines intersect is point "B".
6. Measure from "A" to "B" to determine distance from "D" to "C". Mark "C" and place conduit in bender with mark at outside edge of jaw, and with the kick pointing down. Use a level to prevent dogging conduit.
7. Make three full pumps, making sure handle goes all the way down to the stop.

Note: 1. There are several methods of bending rigid conduit with a Chicago Type Bender, and any method that gets the job done in a minimal amount of time with craftsmanship is acceptable.

2. Whatever method is used, quality will improve with experience.

MULTI-SHOT NINETY DEGREE CONDUIT BENDING

PROBLEM:

- A. To measure, thread, cut and ream conduit before bending.
- B. To accurately bend conduit to the desired height of the stub-up (H), and to the desired length of the tail (L).

GIVEN:

- A. Size of conduit = 2"
- B. Space between conduit (center to center) = 6"
- C. Height of stub-up = 36"
- D. Length of tail = 48"

SOLUTION:

A. TO DETERMINE RADIUS (R):

Conduit #1 (inside conduit) will use the minimum radius unless otherwise specified. The minimum radius is eight times the size of the conduit. (see page 154)

$$\text{RADIUS OF CONDUIT } \#1 = 8 \times 2" + 1.25" = 17.25"$$

$$\text{RADIUS OF CONDUIT } \#2 = \text{RADIUS } \#1 + 6" = 23.25"$$

$$\text{RADIUS OF CONDUIT } \#3 = \text{RADIUS } \#2 + 6" = 29.25"$$

B. TO DETERMINE DEVELOPED LENGTH (DL): $\text{RADIUS} \times 1.57 = \text{DL}$

$$\text{DL OF CONDUIT } \#1 = R \times 1.57 = 17.25" \times 1.57 = 27"$$

$$\text{DL OF CONDUIT } \#2 = R \times 1.57 = 23.25" \times 1.57 = 36.5"$$

$$\text{DL OF CONDUIT } \#3 = R \times 1.57 = 29.25" \times 1.57 = 46"$$

C. TO DETERMINE LENGTH OF NIPPLE:

$$\begin{aligned}\text{LENGTH OF NIPPLE, CONDUIT } \#1 &= L + H + \text{DL} - 2R \\ &= 48" + 36" + 27" - 34.5" \\ &= 76.5"\end{aligned}$$

$$\begin{aligned}\text{LENGTH OF NIPPLE, CONDUIT } \#2 &= L + H + \text{DL} - 2R \\ &= 54" + 42" + 36.5" - 46.5" \\ &= 86"\end{aligned}$$

$$\begin{aligned}\text{LENGTH OF NIPPLE, CONDUIT } \#3 &= L + H + \text{DL} - 2R \\ &= 60" + 48" + 46" - 58.5" \\ &= 95.5"\end{aligned}$$

- Note: 1. For 90 degree bends, SHRINK = $2R - \text{DL}$
2. For off-set bends, SHRINK = HYPOTENUSE - SIDE ADJACENT

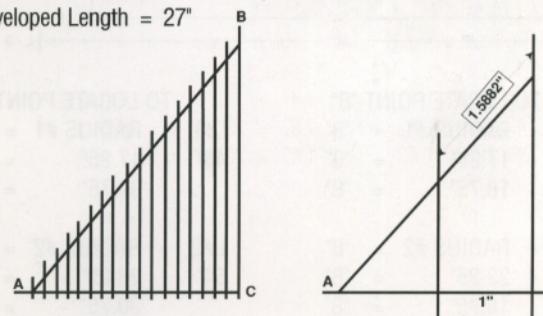
MULTI-SHOT NINETY DEGREE CONDUIT BENDING

LAYOUT AND BENDING:

- A. To locate point "B", measure from point "A", the length of the stub-up minus the radius. On all three conduit, point "B" will be 18.75" from point "A". (see page 154).
- B. To locate point "C", measure from point "D", the length minus the radius, (see page 154). On all three conduit, point "C" will be 30.75" from point "D". (see page 154).
- C. Divide the developed length (point "B" to point "C") into equal spaces. Spaces should not be more than 1.75" to prevent wrinkling of the conduit. On Conduit #1, seventeen spaces of 1.5882" each would give us eighteen shots of 5 degrees each. Remember there is always one less space than shot. When determining the number of shots, choose a number that will divide into ninety an even number of times.
- D. If an elastic numbered tape is not available, try the method illustrated.

A to B = Conduit #1

Developed Length = 27"



A to C = 17 1" spaces

A to B = 17 1.5882" spaces

C = table or plywood corner

Measure from Point "C" (table corner) 17 inches along table edge to Point "A" and mark. Place end of rule at Point "A". Point "B" will be located where 27" mark meets table edge B-C. Mark on board, then transfer to conduit.

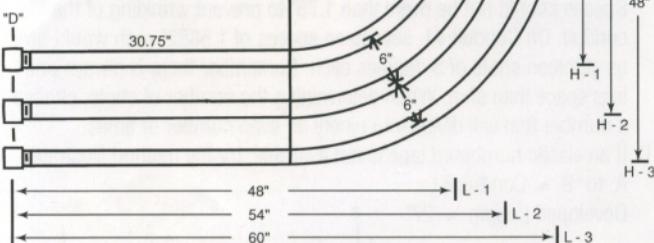
MULTI-SHOT NINETY DEGREE CONDUIT BENDING

$$L + H + DL - 2R = \text{NIPPLE}$$

$$1.57 \times R = DL$$

$$H - R = "B"$$

$$L - R = "C"$$



TO LOCATE POINT "B"

| | |
|-----------------------|-----------------------|
| H#1 - RADIUS #1 = "B" | L#1 - RADIUS #1 = "C" |
| 36" - 17.25" = "B" | 48" - 17.25" = "C" |
| 18.75" = "B" | 30.75" = "C" |

H#2 - RADIUS #2 = "B"

| | |
|-----------------------|-----------------------|
| H#2 - RADIUS #2 = "B" | L#2 - RADIUS #2 = "C" |
| 42" - 23.25" = "B" | 54" - 23.25" = "C" |

H#3 - RADIUS #3 = "B"

| | |
|-----------------------|-----------------------|
| H#3 - RADIUS #3 = "B" | L#3 - RADIUS #3 = "C" |
| 48" - 29.25" = "B" | 60" - 29.25" = "C" |

Points "B" and "C" are the same distance from the end on all three conduits.

OFFSET BENDS - EMT - USING HAND BENDER

An offset bend is used to change the level, or plane, of the conduit. This is usually necessitated by the presence of an obstruction in the original conduit path.

Step One:

Determine the offset depth. (X)



Step Two:

Multiply the offset depth "x" the multiplier for the degree of bend used to determine the distance between bends.

| ANGLE | MULTIPLIER |
|-------------|------------|
| 10° x 10° | = 6 |
| 22½° x 22½° | = 2.6 |
| 30° x 30° | = 2 |
| 45° x 45° | = 1.4 |
| 60° x 60° | = 1.2 |

Example: If the offset depth required (X) is 6", and you intend to use 30° bends, the distance between bends is 6" x 2 = 12".

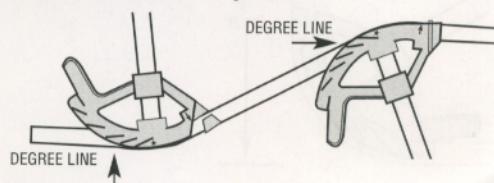
| ← DISTANCE BETWEEN BENDS → |

Step Three:

Mark at the appropriate points, align the arrow on the bender with the first mark, and bend to desired degree by aligning EMT with chosen degree line on bender.

Step Four:

Slide down the EMT, align the arrow with the second mark, and bend to the same degree line. Be sure to note the orientation of the bender head. Check alignment.



90° BENDS - EMT - USING HAND BENDER

The stub is the most common bend.

Step One:

Determine the height of the stub-up required, and mark on EMT.

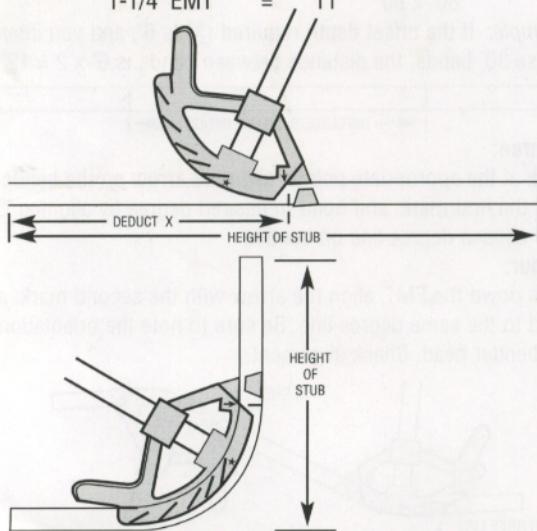
Step Two:

Find the "Deduct" or "Take-up" amount from the Take-Up Chart. Subtract the take-up amount from the stub height, and mark the EMT that distance from the end.

Step Three:

Align the arrow on bender with the last mark made on the EMT, and bend to the 90° mark on the bender.

| DESCRIPTION | TAKE-UP |
|-------------|---------|
| 1/2" EMT | = 5" |
| 3/4" EMT | = 6" |
| 1" EMT | = 8" |
| 1-1/4" EMT | = 11" |



BACK-TO-BACK BENDS - EMT- USING HAND BENDER

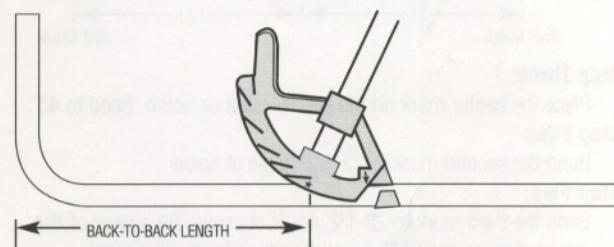
A back-to-back bend results in a "U" shape in a length of conduit. It's used for a conduit which runs along the floor or ceiling which turns up or down a wall.

Step One:

After the first 90° bend is made, determine the back-to-back length and mark on EMT.

Step Two:

Align this back-to-back mark with the star mark on the bender, and bend to 90°.



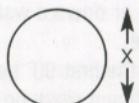
3-POINT SADDLE BENDS - EMT- USING HAND BENDER

The 3-point saddle bend is used when encountering an obstacle (usually another pipe)

Step One:

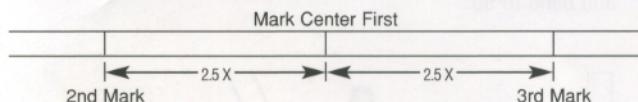
Measure the height of the obstruction.

Mark the center point on EMT.



Step Two:

Multiply the height of the obstruction by 2.5 and mark this distance on each side of the center mark.



Step Three:

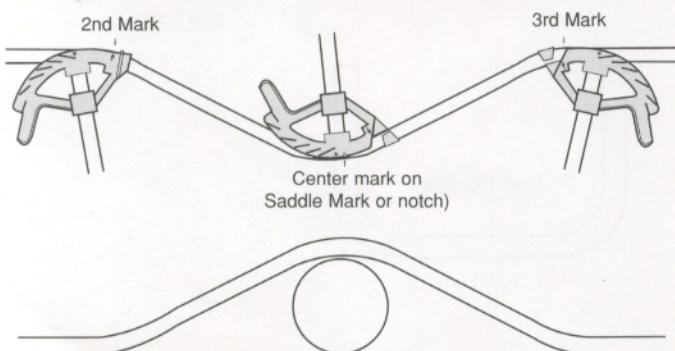
Place the center mark on the saddle mark or notch. Bend to 45°.

Step Four:

Bend the second mark to 22-1/2° angle at arrow.

Step Five:

Bend the third mark to 22-1/2° angle at arrow. Be aware of the orientation of the EMT on all bends. Check alignment.



PULLEY CALCULATIONS

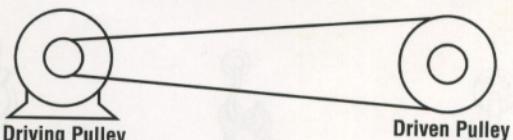
The most common configuration consists of a motor with a pulley attached to its shaft, connected by a belt to a second pulley. The motor pulley is referred to as the **Driving Pulley**. The second pulley is called the **Driven Pulley**. The speed at which the Driven Pulley turns is determined by the speed at which the Driving Pulley turns as well as the diameters of both pulleys. The following formulas may be used to determine the relationships between the motor, pulley diameters and pulley speeds.

D = Diameter of Driving Pulley

d' = Diameter of Driven Pulley

S = Speed of Driving Pulley (revolutions per minute)

s' = Speed of Driven Pulley (revolutions per minute)



- To determine the speed of the Driven Pulley (Driven RPM):

$$s' = \frac{D \times S}{d'} \quad \text{or} \quad \text{Driven RPM} = \frac{\text{Driving Pulley Dia.} \times \text{Driving RPM}}{\text{Driven Pulley Dia.}}$$

- To determine the speed of the Driving Pulley (Driving RPM):

$$S = \frac{d' \times s'}{D} \quad \text{or} \quad \text{Driving RPM} = \frac{\text{Driven Pulley Dia.} \times \text{Driven RPM}}{\text{Driving Pulley Dia.}}$$

- To determine the diameter of the Driven Pulley (Driven Dia.):

$$d' = \frac{D \times S}{s'} \quad \text{or} \quad \text{Driven Dia.} = \frac{\text{Driving Pulley Dia.} \times \text{Driving RPM}}{\text{Driven RPM}}$$

- To determine the diameter of the Driving Pulley (Driving Dia.):

$$D = \frac{d' \times s'}{S} \quad \text{or} \quad \text{Driving Dia.} = \frac{\text{Driven Pulley Dia.} \times \text{Driven RPM}}{\text{Driving RPM}}$$

USEFUL KNOTS



BOWLINE



RUNNING BOWLINE



BOWLINE ON THE
BIGHT



CLOVE HITCH



SHEEPSHANK



ROLLING HITCH



SINGLE
BLACKWALL
HITCH



CATPAW



DOUBLE
BLACKWALL
HITCH



SQUARE KNOT



TIMBER HITCH
WITH HALF HITCH



SINGLE
SHEET
BEND



STOP



DOG
EVERYTHING



EMERGENCY
STOP



TRAVEL



TRAVEL
BOTH TRACKS
(CRAWLER CRANES ONLY)



TRAVEL
ONE TRACK
(CRAWLERS)



RETRACT
BOOM



EXTEND
BOOM



SWING
BOOM

HAND SIGNALS



RAISE LOAD



LOWER LOAD



MAIN HOIST



MOVE SLOWLY



RAISE BOOM AND LOWER LOAD (FLEX FINGERS)



LOWER BOOM AND RAISE LOAD (FLEX FINGERS)



USE WHIP LINE



BOOM UP



BOOM DOWN



FIRST AID

The American Red Cross recommends certification in a CPR training course annually and certification in a first aid course every three years. (Also refer to author's and publisher's disclaimer on inside front cover)

GENERAL DIRECTIONS FOR FIRST AID:

While help is being summoned, do the following:

- 1) **CHECK** - Check the scene and the injured person.
- 2) **CALL** - Call 9-1-1 or the local emergency number.
- 3) **CARE** - Care for the injured person.

URGENT CARE:

BLEEDING

First Aid:

- 1) Direct Pressure and Elevation:
 - * Place dressing and apply pressure directly over the wound, then elevate above the level of the heart, unless there is evidence of a fracture.
- 2) Apply pressure bandage.
 - * Wrap bandage snugly over the dressing.
- 3) Pressure Points
 - * If bleeding doesn't stop after direct pressure, elevation and the pressure bandage, compress the pressure point.
 - * Arm: Use the brachial artery - pushing the artery against the upper arm bone.
 - * Leg: Apply pressure on femoral artery, pushing it against the pelvic bone.
- 4) Nosebleed:

To control a nosebleed, have the victim lean forward and pinch the nostrils together until bleeding stops.

POISONING

Signals: Vomiting, heavy labored breathing, sudden onset of pain or illness, burns or odor around the lips or mouth, unusual behavior.

(Poisoning, continued)

First Aid:

* If you think someone has been poisoned, call your poison control center at **1-800-222-1222** or local emergency number and follow their directions.

* Try to identify the poison - be prepared to inform poison center of the type of poison, when incident occurred, victim's age, symptoms, and how much poison may have been ingested, inhaled, absorbed, or injected.

If unconscious or nauseous:

- 1) Position victim on side and monitor vital signs (i.e. pulse and breathing).
- 2) Call Poison Control and identify the poison.
- 3) DO NOT give anything by mouth.

SHOCK

Signals: Cool, moist, pale, bluish skin, weak rapid pulse (over 100), nausea, increased rate of breathing, apathetic.

First Aid:

Caring for shock involves the following simple steps:

- 1) Have the victim lie down in the most comfortable position to minimize any pain. Pain can intensify the body's stress and accelerate the progression of shock. Help the victim to rest comfortably.
- 2) Control any external bleeding
- 3) Help the victim maintain normal body temperature. If the victim is cool, try to cover to avoid chill.
- 4) Try to reassure the victim.
- 5) Elevate the legs about 12" unless you suspect head, neck back injuries or possible broken bones involving the hips or legs. If victim is having difficulty breathing, elevate the shoulders. If unsure of the victim's condition, leave the victim lying flat.
- 6) Do not give the victim anything to eat or drink.
- 7) Call 911 or your local emergency number immediately.

Shock **cannot** be managed effectively by first aid alone. A victim of shock requires advanced medical care as soon as possible.

BURNS

Signals: Small or large thin (surface) burns:

redness, pain and swelling.

Deep burns: blisters, deep tissue destruction, charred appearance.

First Aid:

- 1) Stop the burning - put out flames or remove the victim from the source of the burn.
- 2) Cool all burns (except electrical) - run or pour cool water on burn. Immerse if possible. Cool until pain is reduced.
- 3) Cover the burn - Use dry, sterile dressing and bandage.
- 4) Keep victim comfortable as possible, **not** chilled or over heated.

Chemical burn - must be flushed with large amounts of water until EMS arrives.

Electrical burn - make sure power is turned off before touching the victim. Cover with sterile dressing and care for life threatening injury.

ELECTRICAL SHOCK

Signals: Unconsciousness, absence of breathing & pulse.

First Aid:

- 1) TURN OFF THE POWER SOURCE - Call EMS.
(DO NOT approach the victim until power has been turned off.)
- 2) DO NOT move a victim of electrical injury unless there is immediate danger.
- 3) Administer rescue breathing or CPR if necessary.
- 4) Treat for shock.
- 5) Check for other injuries and monitor victim until Medical help arrives.

FROSTBITE

Signals: Flushed, white or gray skin. Pain. The nose, cheeks, ears, fingers, and toes are most likely to be affected. Pain may be felt early and then subside. Blisters may appear later.

(Frostbite, continued)

First Aid:

- 1) Cover the frozen part. Loosen restrictive clothing or boots.
- 2) Bring victim indoors ASAP.
- 3) Give the victim a warm drink. (DO NOT give alcoholic beverages, tea, or coffee)
- 4) Immerse frozen part in warm water (100° - 105°), or wrap in a sheet and warm blankets. DO NOT rewarm if there is a possibility of refreezing.
- 5) Remove from water and discontinue warming once part becomes flushed.
- 6) Elevate the injured area and protect from further injury.
- 7) DO NOT rub the frozen part. DO NOT break the blisters. DO NOT use extreme or dry heat to rewarm the part.
- 8) If fingers or toes are involved, place dry, sterile gauze between them and bandage loosely.

HYPOTHERMIA

Signals: Lowered body core temperature. Persistent shivering, lips may be blue, slow slurred speech, memory lapses. Most cases occur when air temperature ranges from 30° - 50° or water temperature is below 70°F. Presence of wind and high humidity are also factors.

First Aid:

- 1) Move victim to shelter and remove wet clothing if necessary.
- 2) Rewarm victim with blankets or body-to-body contact in sleeping bag.
- 3) If victim is conscious and able to swallow, give warm liquids.
- 4) Keep victim warm and quiet.
- 5) DO NOT give alcoholic beverages, or beverages containing caffeine.
- 6) Constantly monitor victim and give Rescue Breathing and CPR if necessary.

HEAT EXHAUSTION / HEAT STROKE

Signals: Heat Exhaustion: Pale, clammy skin, profuse perspiration, weakness, nausea, headache.

Heat Stroke: Hot dry red skin, no perspiration, rapid & weak pulse. High body temperature (105°+).

This is an immediate life threatening emergency; Call 911.

First Aid:

- 1) Get the victim out of the heat.
- 2) Loosen tight clothing or restrictive clothing.
- 3) Remove perspiration soaked clothing.
- 4) Apply cool, wet cloths to the skin.
- 5) Fan the victim.
- 6) If victim is conscious, give cool water to drink.
- 7) Call for an ambulance if victim refuses water, vomits, or starts to lose consciousness.

RESCUE BREATHING

RESCUE BREATHING

1. CHECK THE VICTIM

Tap and shout "Are you okay?", to see if the person responds.

If no response...

2. CALL EMS.

3. CARE FOR THE VICTIM.

Step 1: Look, listen and feel for breathing for about 5 seconds.

If the person is not breathing or you can't tell...

Step 2: Position victim on back, while supporting head and neck.

Step 3: Tilt head back and lift chin.

Step 4: Look, listen, and feel for breathing for about 5 seconds.



(Rescue Breathing, continued)

If not breathing...

- Step 5: Give two slow gentle breaths.
- Step 6: Check signs of circulation (pulse) for up to 10 seconds.
- Step 7: Check for severe bleeding.

4. GIVE RESCUE BREATHING

If pulse is present but person is still not breathing...

- Step 1: Give one slow breath about every five seconds. Do this for about one minute (12 breaths).
- Step 2: Recheck signs of circulation (pulse) and breathing about every minute.

Continue rescue breathing as long as pulse is present but person is not breathing.

5. BEGIN CARDIOPULMONARY RESUSCITATION (CPR) If there is no sign of circulation (pulse) and no breathing.

FIRST AID FOR CHOKING

1. Check the victim.

When an adult is choking:

- Step 1: Ask, "Are you choking?" If victim cannot cough, speak, or breathe, is coughing weakly or is making high-pitched noises...
- Step 2: Shout "HELP!".
- Step 3: Phone EMS for help - Send someone to call for an ambulance.
- Step 4: Do Abdominal Thrusts.
 - A. Wrap your arms around victim's waist. Make a fist. Place thumbside of fist against middle of abdomen just above the navel. Grasp fist with other hand.
 - B. Give quick, upward thrusts.

Repeat until object is coughed up or person becomes unconscious.



Have You Saved A Life Today?



Together, we can save a life

New Emergency Cardiovascular Care (ECC) 2000 Guidelines mandated key changes to lifesaving CPR techniques. Your American Red Cross did far more than just update our courses. We acted on suggestions from customers like you to create a comprehensive workplace safety training program that brings you unprecedented flexibility – plus the latest in emergency preparedness training.

Here's what you can expect...

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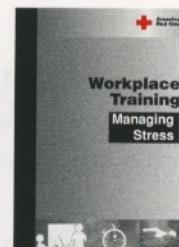
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Together, we can save a life

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The American Red Cross recommends CPR certification annually and first aid certification every three years.

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2005 CALENDAR

JANUARY

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2006 CALENDAR

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2007 CALENDAR

JANUARY

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FEBRUARY

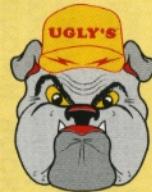
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MARCH

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